SUBDIVISION COMMITTEE
METROPOLITAN AREA PLANNING COMMISSION

AGENDA ITEM NO. 8

May 23, 1996

STAFF REPORT
(Final Plat)

CASE NUMBER: S/D 96-28 NORTHRIDGE LAKES 2ND ADDITION

OWNER/APPLICANT: Northridge Lakes, Inc., 7926 W. 21st St. North, Wichita, KS 67205

SURVEYOR/ENGINEER: P.E.C., P.A., c/o Rob Hartman, 303 S. Topeka, Wichita, KS 67202

LOCATION: East of Tyler and south of 29th Street North

SITE SIZE: 3.2 Acres

NUMBER OF LOTS

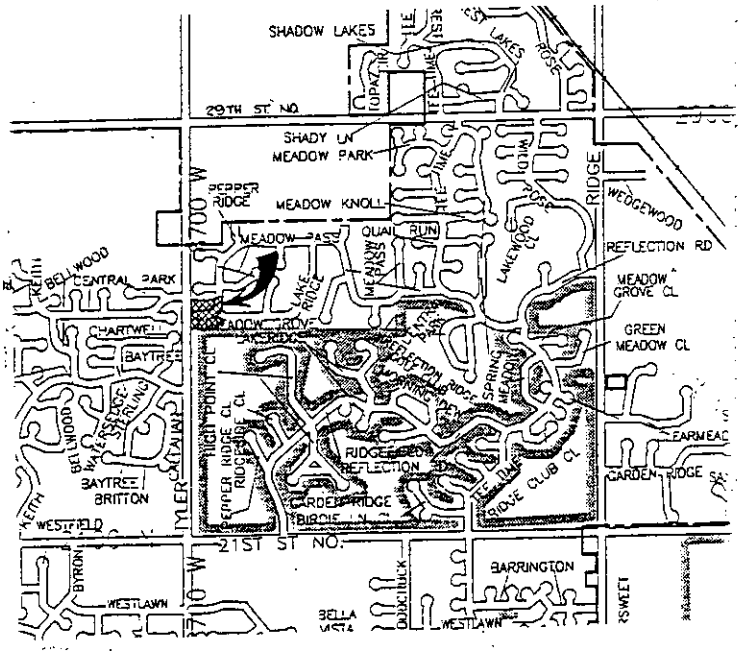
Residential:	5
Office:	
Commercial:	
Industrial:	
Total:	5

MINIMUM LOT AREA: 9,000 square feet

CURRENT ZONING: "SF-6" Single Family

PROPOSED ZONING:

VICINITY MAP:



NOTE: This plat is replatting six (6) lots, Reserves, and street right-of-way at the entrance area of the original Northridge Lakes (1st) Addition. The primary purpose for the replat is to create a more attractive entrance to the Addition(s) from Tyler Road. Reserves and landscaped areas are now being shown either side of Meadow Grove.

STAFF COMMENTS:

A. **Traffic Engineering** needs to comment on the acceptability of this plat's change in regard to the shifting of Meadow Grove's entrance northward. This alignment would now appear to be in possible conflict with Bradford South's street entrance at Tyler and Central Park. That is, the offset of these two addition's entrances is being reduced to the point where only several vehicles turning left into each addition could block each other.

   If the offset is not sufficient to handle left-turning vehicles, **Traffic Engineering** needs to indicate if improvements are being planned or still need to be guaranteed to rectify any such traffic conflicts.

B. **City Engineering** needs to indicate if new guarantees are required for this replat of if agreements can be submitted to respread existing assessments. Also, **Engineering** needs to indicate if any existing projects are being abandoned due to this replat and if any costs are involved.

C. The applicant shall resubmit covenants involving the ownership, maintenance, drainage use, etc. of the Reserves now being platted. Such covenant shall also note that this Addition is part of the original Northridge Lake development in regard to the use of, responsibility to maintain and ownership of the Reserves to both Additions.

D. The applicant shall submit a covenant which provides for four (4) off-street parking spaces per dwelling unit on each lot which abuts a 58-foot street. The covenant shall inventory the affected lots by lot and block number and shall state that the covenant runs with the land and is binding on future owners and assigns.

E. The applicant shall install or guarantee the installation of all utilities and facilities which are applicable and described in Article 8 of the MAPC Subdivision Regulations. (Water service and fire hydrants required by Article 8 for fire protection shall be as per the direction and approval of the Chief of the Fire Department.)

F. The applicant's engineer is advised that the Register of Deeds is requiring the name(s) of the notary public, who acknowledges the signatures on this plat, to be printed beneath the notary's signature.

G. To receive mail delivery without delay; and to avoid unnecessary expense, the applicant is advised of the necessity to meet with the U.S. Postal Service Growth Management Coordinator (phone 316-729-0102) prior to development of the plat so that the type of delivery, and the tentative mailbox locations can be determined.

H. Perimeter closure computations shall be submitted with the final plat tracing. Section 5-101(c).

I. Recording of the plat within 30 days after approval by the City Council.

J. To receive mail delivery without delay, and to avoid unnecessary expense, the applicant is advised of the necessity to meet with the U.S. Postal Service Growth Management Coordinator (phone 316-729-0102) prior to development of the plat so that the type of delivery, and the tentative mailbox locations can be determined.

K. The applicant is advised that the legal in the plat references a Lot 3 of Block 3 in the original addition, but the area shown on the face of the plat does not appear to include portion of this lot within the Addition's perimeter.

L. The representatives from **City Engineering** should be prepared to comment on the status of the applicant's drainage plan.

Note: This plat has been submitted in final form only.

PROFESSIONAL ENGINEERING CONSULTANTS, PA
303 South Topeka
WICHITA, KANSAS 67202

(316) 262-2691

LETTER OF TRANSMITTAL

DATE	JOB NO.
5-6-96	
ATTENTION: V. R. Huang, P.E.	
RE: NorthRidge Lakes 2nd Add	

TO City Engineer's Office
455 N. Main
Wichita, KS 67202

WE ARE SENDING YOU ☒ Attached ☐ Under separate cover via _____ the following items:

☐ Shop drawings ☐ Prints ☐ Plans ☐ Samples ☐ Specifications
☐ Copy of letter ☐ Change order ☒ Drainage Computations

COPIES	DATE	NO.	DESCRIPTION

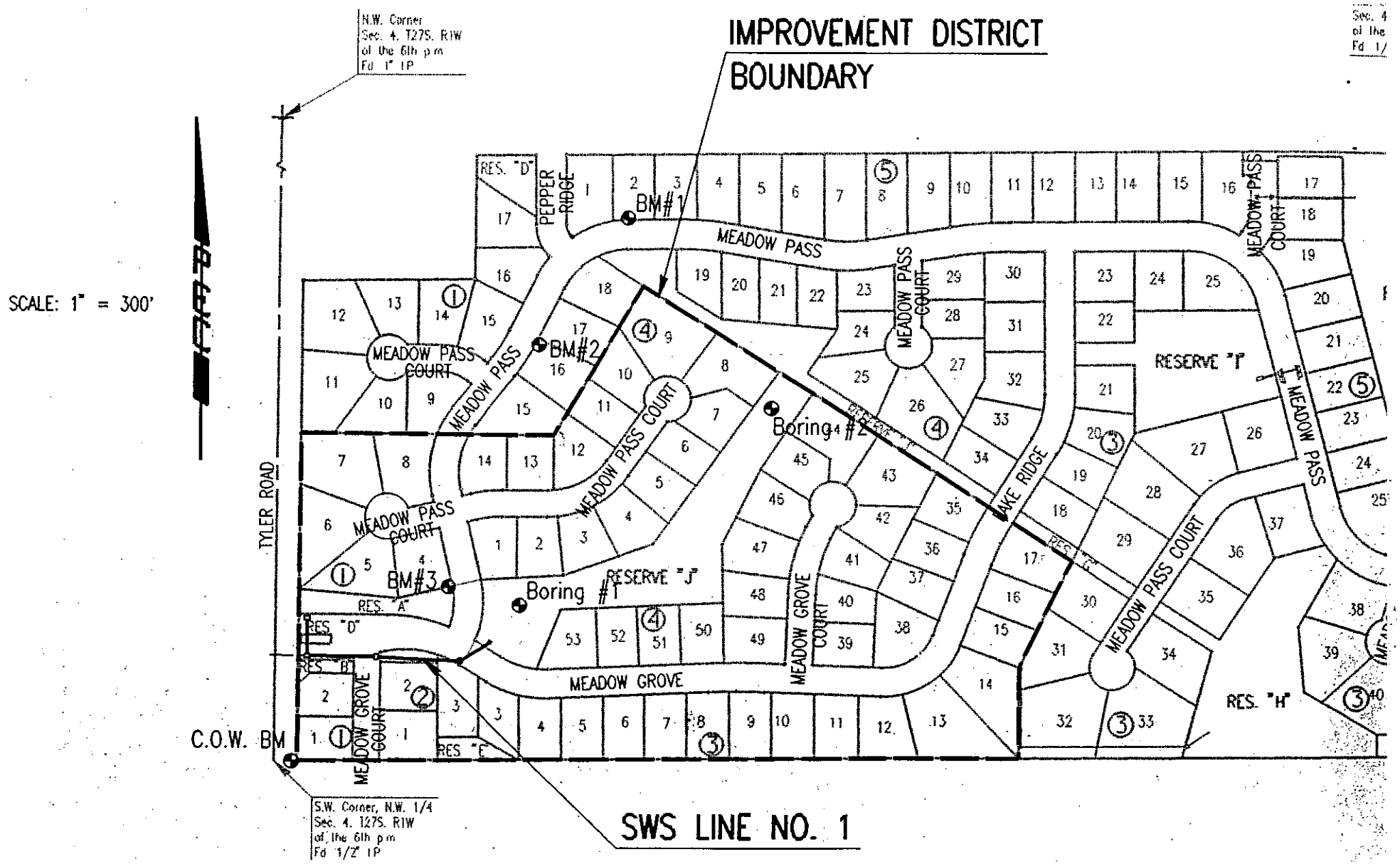
THESE ARE TRANSMITTED as checked below:

☐ For approval ☐ Approved as submitted ☐ Resubmit _____ copies for approval
☐ For your use ☐ Approved as noted ☐ Submit _____ copies for distribution
☐ As requested ☐ Returned for corrections ☐ Return _____ corrected prints
☒ For review and comment ☐ _____
☐ FOR BIDS DUE _____ 19____ ☐ PRINTS RETURNED AFTER LOAN TO US

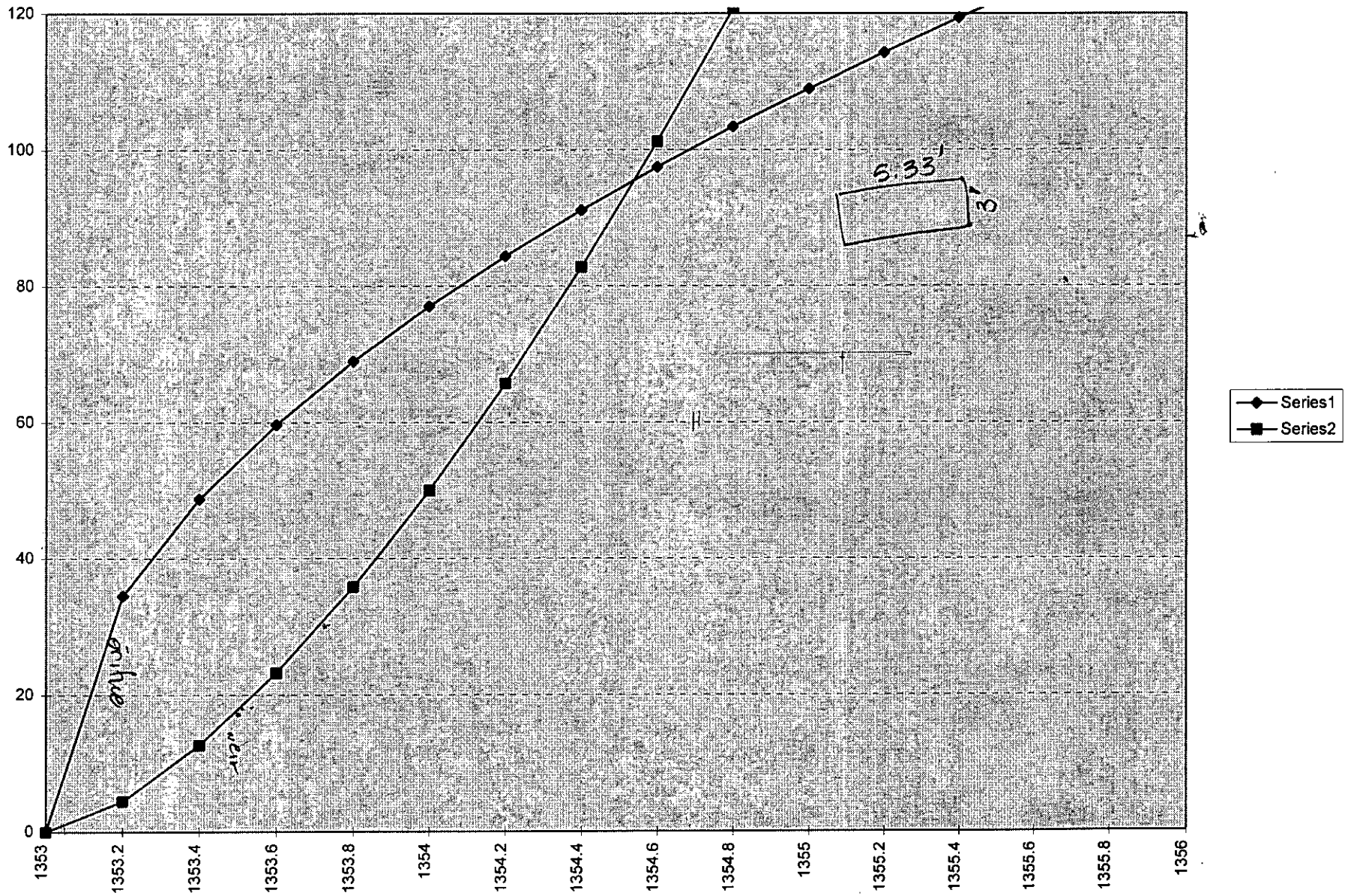
REMARKS These computations reflect the revised SWS # 463.
All other system components are essentially the same as those initially proposed for NorthRidge Lakes, and a new drainage plan has not been prepared.

COPY TO _____

SIGNED: Michael W Beall


IMPROVEMENT DISTRICT
BOUNDARY
N.W. Corner
Sec. 4, T27S, R1W
of the 6th p.m.
Fd 1" I.P.
SCALE: 1" = 300'
BLANCA
TYLER ROAD
PEPPER RIDGE
MEADOW PASS
MEADOW PASS COURT
MEADOW GROVE
MEADOW GROVE COURT
LAKE RIDGE
RESERVE "I"
RESERVE "J"
RES. "A"
RES. "B"
RES. "C"
RES. "D"
RES. "E"
RES. "F"
RES. "H"
BM#1
BM#2
BM#3
Boring #1
Boring #2
C.O.W. BM
S.W. Corner, N.W. 1/4
Sec. 4, T27S, R1W
of the 6th p.m.
Fd 1/2" I.P.
SWS LINE NO. 1

Sheet1 Chart 3



FILM 1704 PAGE 0044

STATE OF KANSAS } SS
SEDGWICK COUNTY }
FILED FOR RECORD AT
9:00 A M

1614469 5-15

LARRY CONSOLVER
REGISTER OF DEEDS
Deputy

AFFIDAVIT

STATE OF KANSAS, COUNTY OF SEDGWICK: ss.

Michael E. Lindebak, P.E., City Engineer for the City of Wichita, Kansas, being first duly sworn, on oath states:

I have examined the recorded plats of Northridge Lakes and Northridge Lakes 2nd Addition to Wichita, Sedgwick County Kansas, and have found that three street names should be changed as follows:

MEADOW GROVE ST, from N Tyler Rd to Lake Ridge St; adjacent to lot 2 Block 1, and lots 2 & 3 Block 2, in the Northridge Lakes 2nd Addition; lots 3-13 Block 3, lots 38 & 39 Block 4, and lots 49-53 Block 4 in the Northridge Lakes Addition should be changed to **W NORTHRIDGE ST**.

MEADOW GROVE CT; adjacent to lots 1 & 2 Block 1; and lots 1 & 2 Block 2 in the Northridge Lakes 2nd Addition should be changed to **W NORTHRIDGE CT**.

MEADOW GROVE CT; adjacent to lots 39-49 Block 4 in the Northridge Lakes Addition should be changed to **W NORTHRIDGE CT**.

FURTHER AFFIANT SAITH NOT.

Michael E. Lindebak, P.E.

Dated this 16th day of June, 1997

(Seal)

ATTEST:

Taylor Levins, Office of Central Inspection
Permits Examiner

Lori Wilkerson, City of Wichita
Address Subcommittee Chairperson

P.00

PEC
GARY WILEY
303 S. TOPEKA
67207

STATE OF KANSAS, COUNTY OF SEDGWICK: ss.

Be it remembered that on this 16th, day of June, 1997, before me a notary public in and for said County and State, came Michael E. Lindebak, to me known to be the same person who executed the foregoing instrument duly acknowledged by me. In testimony whereof, I have hereunto set my hand and affixed my Notarial Seal the day and year above written.

JACK L. LOVE
Notary Public - State of Kansas
My Appt. Expires 1-5-95

My Appointment Expires 1/5/95

CURRENT DATE: 03-20-1996
CURRENT TIME: 10:45:38

FILE DATE: 03-20-1996
FILE NAME: NRLKS

FHWA CULVERT ANALYSIS
HY-8, VERSION 3.2

C U L V	SITE DATA: INLET ELEV. (FT)	SITE DATA: OUTLET ELEV. (FT)	SITE DATA: CULVERT LENGTH (FT)	CULVERT SHAPE, MATERIAL, INLET: BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	1348.00	1346.10	500.00	1 RCP	3.50	3.50	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (CFS) FILE: NRLKS DATE: 03-20-1996

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
1354.00	30	30	0	0	0	0	0	0	1
1354.27	36	36	0	0	0	0	0	0	1
1354.58	42	42	0	0	0	0	0	0	1
1354.94	48	48	0	0	0	0	0	0	1
1355.35	54	54	0	0	0	0	0	0	1
1355.81	60	60	0	0	0	0	0	0	1
1356.32	66	66	0	0	0	0	0	0	1
1356.77	72	71	0	0	0	0	0	0	30
1356.83	78	72	0	0	0	0	0	6	7
1356.87	84	72	0	0	0	0	0	11	5
1356.91	90	72	0	0	0	0	0	17	5
1356.76	71	71	0	0	0	0	0	OVERTOPPING	

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: NRLKS DATE: 03-20-1996

HEAD ELEV(FT)	HEAD ERROR(FT)	TOTAL FLOW(CFS)	FLOW ERROR(CFS)	% FLOW ERROR
1354.00	0.00	30	0	0.00
1354.27	0.00	36	0	0.00
1354.58	0.00	42	0	0.00
1354.94	0.00	48	0	0.00
1355.35	0.00	54	0	0.00
1355.81	0.00	60	0	0.00
1356.32	0.00	66	0	0.00
1356.77	-0.00	72	1	1.40
1356.83	-0.00	78	1	0.85
1356.87	-0.00	84	1	0.87
1356.91	-0.00	90	0	0.56

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

CURRENT DATE: 03-20-1996 FILE DATE: 03-20-1996
CURRENT TIME: 10:45:38 FILE NAME: NRLKS

CULVERT # 1

PERFORMANCE CURVE FOR 1 BARREL(S)

Q (cfs)	HWE (ft)	TWE (ft)	ICH (ft)	OCH (ft)	FLOW TYPE	CCE (ft)	FCE (ft)	TCE (ft)	VO (fps)
30	1354.00	1353.40	2.48	6.00	4-FF	0.00	0.00	0.00	3.12
36	1354.27	1353.40	2.77	6.27	4-FF	0.00	0.00	0.00	3.74
42	1354.58	1353.40	3.05	6.58	4-FF	0.00	0.00	0.00	4.37
48	1354.94	1353.40	3.32	6.94	4-FF	0.00	0.00	0.00	4.99
54	1355.35	1353.40	3.61	7.35	4-FF	0.00	0.00	0.00	5.61
60	1355.81	1353.40	3.91	7.81	4-FF	0.00	0.00	0.00	6.24
66	1356.32	1353.40	4.23	8.32	4-FF	0.00	0.00	0.00	6.86
71	1356.76	1353.40	4.50	8.76	4-FF	0.00	0.00	0.00	7.36
72	1356.83	1353.40	4.56	8.83	4-FF	0.00	0.00	0.00	7.44
72	1356.87	1353.40	4.57	8.87	4-FF	0.00	0.00	0.00	7.48
72	1356.91	1353.40	4.59	8.91	4-FF	0.00	0.00	0.00	7.52

El. inlet face invert 1348.00 ft El. outlet invert 1346.10 ft
El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

***** SITE DATA ***** CULVERT INVERT **********

INLET STATION (FT)	0.00
INLET ELEVATION (FT)	1348.00
OUTLET STATION (FT)	500.00
OUTLET ELEVATION (FT)	1346.10
NUMBER OF BARRELS	1.00
SLOPE (V-FT/H-FT)	0.0038
CULVERT LENGTH ALONG SLOPE (FT)	500.00

***** CULVERT DATA SUMMARY **********

BARREL SHAPE	CIRCULAR
BARREL DIAMETER	3.50 FT
BARREL MATERIAL	CONCRETE
BARREL MANNING'S N	0.012
INLET TYPE	CONVENTIONAL
INLET EDGE AND WALL	SQUARE EDGE WITH HEADWALL
INLET DEPRESSION	NONE

CURRENT DATE: 03-20-1996
CURRENT TIME: 10:45:38

FILE DATE: 03-20-1996
FILE NAME: NRLKS

TAILWATER

CONSTANT WATER SURFACE ELEVATION
1353.40

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH (FT)	30.00
CREST LENGTH (FT)	100.00
OVERTOPPING CREST ELEVATION (FT)	1356.76

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1*****************************************
*                                       *
*   FLOOD HYDROGRAPH PACKAGE  (HEC-1)   *
*             MAY  1991                 *
*          VERSION 4.0.1E               *
*     Lahey F77L-EM/32 version 5.01     *
*       Dodson & Associates, Inc.       *
*  RUN DATE  03/20/96  TIME  10:47:29   *
*****************************************
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*****************************************
*                                       *
*   U.S. ARMY CORPS OF ENGINEERS        *
*   HYDROLOGIC ENGINEERING CENTER       *
*         609 SECOND STREET             *
*       DAVIS, CALIFORNIA 95616         *
*           (916) 551-1748              *
*                                       *
*****************************************
```

```
X     X  XXXXXXX   XXXXX          X
X     X  X        X     X       XX
X     X  X        X             X
XXXXXXX  XXXX     X       XXXXX X
X     X  X        X             X
X     X  X        X     X       X
X     X  XXXXXXX   XXXXX        XXX
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

```
         LINE          ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

           1           ID    STERLING FARMS 2ND ADDITION DRAINAGE PLAN
           2           ID    PEC PROJECT NO 36-92600-2051
           3           ID    STAGE STORAGE ANALYSIS ---  100 YR
           4           ID    PROFESSIONAL ENGINEERING CONSULTANTS, P.A.
           5           ID    COMPUTED BY M.W.BERRY, P.E.  02/11/93
           6           ID    FILENAME='A:\MISCHEC1\STERFAR2.HEC'  DISKNAME="MWB01"
           7           ID    REVISED BY DRC  3-21-96
           8           ID    FILENAME:'T:\DAR\HEC1\STERFAR2.IH1'
*** FREE ***
*** LIST ***
                       *DIAGRAM
           9           IT      5 11FEB93     600       0 11FEB93    1800
          10           IO      0     0
          11           IN     30 11FEB93     600

          12           KK    EASTPART OF KASTEN'S PROP. - 1/4 AC. RESIDENTIAL LOTS. DRAINS TO LAKE.
          13           BA  .05809
          14           PB    7.8
          15           PC   0.08   0.09   0.10   0.11   0.12   0.133  0.147  0.163  0.181  0.204
          16           PC  0.235  0.283  0.663  0.735  0.772  0.799  0.820  0.835  0.850  0.865
          17           PC  0.880  0.890  0.900  0.910  0.916  0.925  0.934  0.943  0.952  0.958
          18           PC  0.964  0.970  0.976  0.982  0.988  0.994  1.000
          19           LS     0     83      0
          20           UD  0.25

          21           KK   PONDA
          22           RS     1    ELEV  1353.0
          23           SA   2.35   3.00
          24           SE   1353  1356.5
          25           SQ      0     30     36     42     48     54     60     66     72
          26           SE 1353.4   1354. 1354.27 1354.58 1354.94 1355.35 1355.81 1356.32 1356.83

          27           KK  RENESTOFF SITE DRAINAGE - WEST PORTION OF REFLECTION RIDGE
          28           BA  0.0828
          29           PB    7.8
          30           PC   0.08   0.09   0.10   0.11   0.12   0.133  0.147  0.163  0.181  0.204
          31           PC  0.235  0.283  0.663  0.735  0.772  0.799  0.820  0.835  0.850  0.865
          32           PC  0.880  0.890  0.900  0.910  0.916  0.925  0.934  0.943  0.952  0.958
          33           PC  0.964  0.970  0.976  0.982  0.988  0.994  1.000
          34           LS     0     69      0
          35           UD  0.40
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 36          KK   PONDB
 37          RS      1    ELEV  1350.0
 38          SA   1.00    1.35
 39          SE  1350.0  1352.5
 40          SS  1350.0    24.0     3.0     1.5

 41          KK    WESTPART OF KASTEN'S PROP. - 1/4 AC. RES. LOTS. DRAINS TO TYLER
 42          BA  .01452
 43          PB    7.8
 44          PC   0.08    0.09    0.10    0.11    0.12    0.133   0.147   0.163   0.181   0.204
 45          PC  0.235   0.283   0.663   0.735   0.772   0.799   0.820   0.835   0.850   0.865
 46          PC  0.880   0.890   0.900   0.910   0.916   0.925   0.934   0.943   0.952   0.958
 47          PC  0.964   0.970   0.976   0.982   0.988   0.994   1.000
1                                          HEC-1 INPUT                                        PAGE  2

LINE         ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

 48          LS      0      83       0
 49          UD    .25

 50          KK  BASIN1
 51          BA  0.0047
 52          PB    7.8
 53          PC   0.08    0.09    0.10    0.11    0.12    0.133   0.147   0.163   0.181   0.204
 54          PC  0.235   0.283   0.663   0.735   0.772   0.799   0.820   0.835   0.850   0.865
 55          PC  0.880   0.890   0.900   0.910   0.916   0.925   0.934   0.943   0.952   0.958
 56          PC  0.964   0.970   0.976   0.982   0.988   0.994   1.000
 57          LS      0      79       0
 58          UD   0.25

 59          KK  BASIN2
 60          BA  0.0578
 61          PB    7.8
 62          PC   0.08    0.09    0.10    0.11    0.12    0.133   0.147   0.163   0.181   0.204
 63          PC  0.235   0.283   0.663   0.735   0.772   0.799   0.820   0.835   0.850   0.865
 64          PC  0.880   0.890   0.900   0.910   0.916   0.925   0.934   0.943   0.952   0.958
 65          PC  0.964   0.970   0.976   0.982   0.988   0.994   1.000
 66          LS      0      81       0
 67          UD   0.25

 68          KK   INTO2
 69          HC      5

 70          KK  PON1$2
             *  pond #1 static pool lowered to 1346.5
             *  pond #1 & #2 combined to function together
 71          RS      1    ELEV  1346.5
 72          SA    2.8     3.9
 73          SE  1346.5  1351.5
             * note: cofq=1.8 for submergence correction
 74          SS  1346.5    30.0     1.8     1.5

 75          KK  BASIN3
 76          BA   0.150
 77          PB    7.8
 78          PC   0.08    0.09    0.10    0.11    0.12    0.133   0.147   0.163   0.181   0.204
 79          PC  0.235   0.283   0.663   0.735   0.772   0.799   0.820   0.835   0.850   0.865
 80          PC  0.880   0.890   0.900   0.910   0.916   0.925   0.934   0.943   0.952   0.958
 81          PC  0.964   0.970   0.976   0.982   0.988   0.994   1.000
 82          LS      0      82       0
 83          UD   0.25

 84          KK   INTO3
 85          HC      2

 86          KK   POND3
 87          RS      1    ELEV    1345
 88          SV      0       8      16      23      31      35
 89          SQ      0      40     220     325     400     440
 90          SE  1344.7  1346.0  1347.0  1348.0  1349.0  1349.5
1                                          HEC-1 INPUT                                        PAGE  3

LINE         ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

 91          KK  BASIN4
 92          BA  0.0188
 93          PB    7.8
 94          PC   0.08    0.09    0.10    0.11    0.12    0.133   0.147   0.163   0.181   0.204
 95          PC  0.235   0.283   0.663   0.735   0.772   0.799   0.820   0.835   0.850   0.865
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          96          PC   0.880   0.890   0.900   0.910   0.916   0.925   0.934   0.943   0.952   0.958
          97          PC   0.964   0.970   0.976   0.982   0.988   0.994   1.000
          98          LS       0      76       0
          99          UD    0.25

         100          KK   INTO4
         101          HC       2

         102          KK   POND4
         103          RS       1    ELEV  1344.7
         104          SV     0.0     0.6     1.1     1.7     2.3     2.8
         105          SQ       0      40     210     350     450     530
         106          SE  1344.7  1345.7  1346.7  1347.7  1348.7  1349.7
         107          ZZ
1
                SCHEMATIC DIAGRAM OF STREAM NETWORK

 INPUT
  LINE      (V) ROUTING          (--->) DIVERSION OR PUMP FLOW

   NO.      (.) CONNECTOR        (<---) RETURN OF DIVERTED OR PUMPED FLOW

    12        EAST
              V
              V
    21        PONDA
              .
              .
    27        .       RRWEST
              .         V
              .         V
    36        .       PONDB
              .         .
              .         .
    41        .         .       WEST
              .         .         .
              .         .         .
    50        .         .         .       BASIN1
              .         .         .         .
              .         .         .         .
    59        .         .         .         .       BASIN2
              .         .         .         .         .
              .         .         .         .         .
    68        INTO2.....................................
              V
              V
    70        PON1$2
              .
              .
    75        .       BASIN3
              .         .
              .         .
    84        INTO3.............
              V
              V
    86        POND3
              .
              .
    91        .       BASIN4
              .         .
              .         .
   100        INTO4.............
              V
              V
   102        POND4

  (***) RUNOFF ALSO COMPUTED AT THIS LOCATION
1*****************************************
*                                       *
*   FLOOD HYDROGRAPH PACKAGE  (HEC-1)   *
*             MAY  1991                 *
*          VERSION 4.0.1E               *
*     Lahey F77L-EM/32 version 5.01     *
*       Dodson & Associates, Inc.       *
*  RUN DATE  03/20/96  TIME  10:47:29   *
*****************************************

*****************************************
*                                       *
*    U.S. ARMY CORPS OF ENGINEERS       *
*    HYDROLOGIC ENGINEERING CENTER      *
*          609 SECOND STREET            *
*        DAVIS, CALIFORNIA 95616        *
*          (916) 551-1748               *
*                                       *
*****************************************
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                    STERLING FARMS 2ND ADDITION DRAINAGE PLAN
                    PEC PROJECT NO 36-92600-2051
                    STAGE STORAGE ANALYSIS --- 100 YR
                    PROFESSIONAL ENGINEERING CONSULTANTS, P.A.
                    COMPUTED BY M.W.BERRY, P.E.  02/11/93
                    FILENAME="A:\MISCHEC1\STERFAR2.HEC"  DISKNAME="MWB01"
                    REVISED BY DRC  3-21-96
                    FILENAME:"T:\DAR\HEC1\STERFAR2.IH1"

 10 IO        OUTPUT CONTROL VARIABLES
                   IPRNT          0  PRINT CONTROL
                   IPLOT          0  PLOT CONTROL
                   QSCAL          0.  HYDROGRAPH PLOT SCALE

    IT        HYDROGRAPH TIME DATA
                    NMIN          5  MINUTES IN COMPUTATION INTERVAL
                   IDATE     11FEB93  STARTING DATE
                   ITIME       0600  STARTING TIME
                      NQ        145  NUMBER OF HYDROGRAPH ORDINATES
                  NDDATE     11FEB93  ENDING DATE
                  NDTIME       1800  ENDING TIME
                   ICENT         19  CENTURY MARK

                COMPUTATION INTERVAL    0.08 HOURS
                   TOTAL TIME BASE   12.00 HOURS

          ENGLISH UNITS
              DRAINAGE AREA         SQUARE MILES
              PRECIPITATION DEPTH   INCHES
              LENGTH, ELEVATION     FEET
              FLOW                  CUBIC FEET PER SECOND
              STORAGE VOLUME        ACRE-FEET
              SURFACE AREA          ACRES
              TEMPERATURE           DEGREES FAHRENHEIT


*** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** ***


            **************
            *            *
 12 KK      *     EAST   *     PART OF KASTEN'S PROP. - 1/4 AC. RESIDENTIAL LOTS. DRAINS TO LAKE.
            *            *
            **************

 11 IN        TIME DATA FOR INPUT TIME SERIES
                 JXMIN         30  TIME INTERVAL IN MINUTES
                JXDATE     11FEB93  STARTING DATE
                JXTIME        600  STARTING TIME

            SUBBASIN RUNOFF DATA

 13 BA        SUBBASIN CHARACTERISTICS
                 TAREA       0.06  SUBBASIN AREA

              PRECIPITATION DATA

 14 PB            STORM       7.80  BASIN TOTAL PRECIPITATION

 15 PI          INCREMENTAL PRECIPITATION PATTERN
                  0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                  0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                  0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                  0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                  0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                  0.00     0.00     0.00     0.00     0.01     0.01     0.01     0.01     0.01     0.01
                  0.01     0.01     0.01     0.01     0.01     0.01     0.06     0.06     0.06     0.06
                  0.06     0.06     0.01     0.01     0.01     0.01     0.01     0.01     0.01     0.01
                  0.01     0.01     0.01     0.01     0.00     0.00     0.00     0.00     0.00     0.00
                  0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                  0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                  0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                  0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                  0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                  0.00     0.00     0.00     0.00

 19 LS        SCS LOSS RATE
                 STRTL       0.41  INITIAL ABSTRACTION
                CRVNBR      83.00  CURVE NUMBER
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RTIMP 0.00 PERCENT IMPERVIOUS AREA

20 UD SCS DIMENSIONLESS UNITGRAPH
TLAG 0.25 LAG

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WARNING *** TIME INTERVAL IS GREATER THAN .29*LAG

UNIT HYDROGRAPH
17 END-OF-PERIOD ORDINATES

17. 58. 93. 93. 72. 43. 27. 17. 11. 7.
4. 3. 2. 1. 1. 0. 0.

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HYDROGRAPH AT STATION EAST

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DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
11 FEB 0600	1	0.00	0.00	0.00	0.	11 FEB 1205	74	0.11	0.01	0.10	199.
11 FEB 0605	2	0.02	0.02	0.00	0.	11 FEB 1210	75	0.11	0.01	0.10	186.
11 FEB 0610	3	0.02	0.02	0.00	0.	11 FEB 1215	76	0.11	0.01	0.10	154.
11 FEB 0615	4	0.02	0.02	0.00	0.	11 FEB 1220	77	0.11	0.01	0.10	119.
11 FEB 0620	5	0.02	0.02	0.00	0.	11 FEB 1225	78	0.11	0.01	0.10	91.
11 FEB 0625	6	0.02	0.02	0.00	0.	11 FEB 1230	79	0.11	0.01	0.10	75.
11 FEB 0630	7	0.02	0.02	0.00	0.	11 FEB 1235	80	0.06	0.00	0.05	64.
11 FEB 0635	8	0.02	0.02	0.00	0.	11 FEB 1240	81	0.06	0.00	0.05	54.
11 FEB 0640	9	0.02	0.02	0.00	0.	11 FEB 1245	82	0.06	0.00	0.05	45.
11 FEB 0645	10	0.02	0.02	0.00	0.	11 FEB 1250	83	0.06	0.00	0.05	38.
11 FEB 0650	11	0.02	0.02	0.00	0.	11 FEB 1255	84	0.06	0.00	0.05	33.
11 FEB 0655	12	0.02	0.02	0.00	0.	11 FEB 1300	85	0.06	0.00	0.05	29.
11 FEB 0700	13	0.02	0.02	0.00	0.	11 FEB 1305	86	0.04	0.00	0.04	27.
11 FEB 0705	14	0.02	0.02	0.00	0.	11 FEB 1310	87	0.04	0.00	0.04	25.
11 FEB 0710	15	0.02	0.02	0.00	0.	11 FEB 1315	88	0.04	0.00	0.04	23.
11 FEB 0715	16	0.02	0.02	0.00	0.	11 FEB 1320	89	0.04	0.00	0.04	21.
11 FEB 0720	17	0.02	0.02	0.00	0.	11 FEB 1325	90	0.04	0.00	0.04	20.
11 FEB 0725	18	0.02	0.02	0.00	0.	11 FEB 1330	91	0.04	0.00	0.04	19.
11 FEB 0730	19	0.02	0.02	0.00	0.	11 FEB 1335	92	0.03	0.00	0.03	18.
11 FEB 0735	20	0.02	0.02	0.00	0.	11 FEB 1340	93	0.03	0.00	0.03	18.
11 FEB 0740	21	0.02	0.02	0.00	0.	11 FEB 1345	94	0.03	0.00	0.03	17.
11 FEB 0745	22	0.02	0.02	0.00	0.	11 FEB 1350	95	0.03	0.00	0.03	16.
11 FEB 0750	23	0.02	0.02	0.00	0.	11 FEB 1355	96	0.03	0.00	0.03	15.
11 FEB 0755	24	0.02	0.02	0.00	0.	11 FEB 1400	97	0.03	0.00	0.03	15.
11 FEB 0800	25	0.02	0.02	0.00	0.	11 FEB 1405	98	0.02	0.00	0.02	14.
11 FEB 0805	26	0.02	0.02	0.00	0.	11 FEB 1410	99	0.02	0.00	0.02	13.
11 FEB 0810	27	0.02	0.02	0.00	0.	11 FEB 1415	100	0.02	0.00	0.02	13.
11 FEB 0815	28	0.02	0.02	0.00	0.	11 FEB 1420	101	0.02	0.00	0.02	12.
11 FEB 0820	29	0.02	0.02	0.00	0.	11 FEB 1425	102	0.02	0.00	0.02	11.
11 FEB 0825	30	0.02	0.02	0.00	0.	11 FEB 1430	103	0.02	0.00	0.02	11.
11 FEB 0830	31	0.02	0.02	0.00	0.	11 FEB 1435	104	0.02	0.00	0.02	10.
11 FEB 0835	32	0.02	0.02	0.00	0.	11 FEB 1440	105	0.02	0.00	0.02	10.
11 FEB 0840	33	0.02	0.02	0.00	0.	11 FEB 1445	106	0.02	0.00	0.02	10.
11 FEB 0845	34	0.02	0.02	0.00	1.	11 FEB 1450	107	0.02	0.00	0.02	10.
11 FEB 0850	35	0.02	0.02	0.00	1.	11 FEB 1455	108	0.02	0.00	0.02	10.
11 FEB 0855	36	0.02	0.02	0.00	1.	11 FEB 1500	109	0.02	0.00	0.02	10.
11 FEB 0900	37	0.02	0.02	0.00	1.	11 FEB 1505	110	0.02	0.00	0.02	10.
11 FEB 0905	38	0.02	0.02	0.00	1.	11 FEB 1510	111	0.02	0.00	0.02	10.
11 FEB 0910	39	0.02	0.02	0.01	1.	11 FEB 1515	112	0.02	0.00	0.02	10.
11 FEB 0915	40	0.02	0.02	0.01	2.	11 FEB 1520	113	0.02	0.00	0.02	10.
11 FEB 0920	41	0.02	0.02	0.01	2.	11 FEB 1525	114	0.02	0.00	0.02	10.
11 FEB 0925	42	0.02	0.02	0.01	2.	11 FEB 1530	115	0.02	0.00	0.02	10.
11 FEB 0930	43	0.02	0.02	0.01	2.	11 FEB 1535	116	0.02	0.00	0.02	10.
11 FEB 0935	44	0.03	0.02	0.01	3.	11 FEB 1540	117	0.02	0.00	0.02	10.
11 FEB 0940	45	0.03	0.02	0.01	3.	11 FEB 1545	118	0.02	0.00	0.02	10.
11 FEB 0945	46	0.03	0.02	0.01	3.	11 FEB 1550	119	0.02	0.00	0.02	10.
11 FEB 0950	47	0.03	0.02	0.01	3.	11 FEB 1555	120	0.02	0.00	0.02	10.
11 FEB 0955	48	0.03	0.02	0.01	4.	11 FEB 1600	121	0.02	0.00	0.02	10.
11 FEB 1000	49	0.03	0.02	0.01	4.	11 FEB 1605	122	0.02	0.00	0.01	10.
11 FEB 1005	50	0.04	0.02	0.01	4.	11 FEB 1610	123	0.02	0.00	0.01	9.
11 FEB 1010	51	0.04	0.02	0.01	4.	11 FEB 1615	124	0.02	0.00	0.01	9.
11 FEB 1015	52	0.04	0.02	0.01	5.	11 FEB 1620	125	0.02	0.00	0.01	8.
11 FEB 1020	53	0.04	0.02	0.02	5.	11 FEB 1625	126	0.02	0.00	0.01	8.
11 FEB 1025	54	0.04	0.02	0.02	6.	11 FEB 1630	127	0.02	0.00	0.01	7.
11 FEB 1030	55	0.04	0.02	0.02	6.	11 FEB 1635	128	0.02	0.00	0.01	7.
11 FEB 1035	56	0.05	0.03	0.02	7.	11 FEB 1640	129	0.02	0.00	0.01	7.
11 FEB 1040	57	0.05	0.02	0.02	7.	11 FEB 1645	130	0.02	0.00	0.01	7.
11 FEB 1045	58	0.05	0.02	0.02	8.	11 FEB 1650	131	0.02	0.00	0.01	7.

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11 FEB 1050  59  0.05  0.02  0.03     9.   *  11 FEB 1655 132  0.02  0.00  0.01     7.
11 FEB 1055  60  0.05  0.02  0.03    10.   *  11 FEB 1700 133  0.02  0.00  0.01     7.
11 FEB 1100  61  0.05  0.02  0.03    10.   *  11 FEB 1705 134  0.02  0.00  0.01     7.
11 FEB 1105  62  0.07  0.03  0.04    11.   *  11 FEB 1710 135  0.02  0.00  0.01     7.
11 FEB 1110  63  0.07  0.03  0.04    12.   *  11 FEB 1715 136  0.02  0.00  0.01     7.
11 FEB 1115  64  0.07  0.03  0.05    14.   *  11 FEB 1720 137  0.02  0.00  0.01     7.
11 FEB 1120  65  0.07  0.03  0.05    16.   *  11 FEB 1725 138  0.02  0.00  0.01     7.
11 FEB 1125  66  0.07  0.03  0.05    18.   *  11 FEB 1730 139  0.02  0.00  0.01     7.
11 FEB 1130  67  0.07  0.03  0.05    19.   *  11 FEB 1735 140  0.01  0.00  0.01     7.
11 FEB 1135  68  0.59  0.17  0.42    26.   *  11 FEB 1740 141  0.01  0.00  0.01     6.
11 FEB 1140  69  0.59  0.13  0.46    49.   *  11 FEB 1745 142  0.01  0.00  0.01     6.
11 FEB 1145  70  0.59  0.10  0.49    87.   *  11 FEB 1750 143  0.01  0.00  0.01     5.
11 FEB 1150  71  0.59  0.08  0.51   128.   *  11 FEB 1755 144  0.01  0.00  0.01     5.
11 FEB 1155  72  0.59  0.06  0.53   163.   *  11 FEB 1800 145  0.01  0.00  0.01     4.
11 FEB 1200  73  0.59  0.05  0.54   188.   *
                                           *
*******************************************************************************************

 TOTAL RAINFALL =   7.80, TOTAL LOSS =   2.01, TOTAL EXCESS =   5.79

PEAK FLOW    TIME                  MAXIMUM AVERAGE FLOW
                           6-HR      24-HR     72-HR    12.00-HR
+  (CFS)     (HR)
                   (CFS)
+   199.     6.08            33.       18.       18.       18.
                 (INCHES)  5.355     5.749     5.749     5.749
                  (AC-FT)    17.       18.       18.       18.

                 CUMULATIVE AREA =    0.06 SQ MI


*** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** ***

        **************
        *            *
 21 KX  *    PONDA   *
        *            *
        **************

          HYDROGRAPH ROUTING DATA

 22 RS      STORAGE ROUTING
               NSTPS         1  NUMBER OF SUBREACHES
                ITYP      ELEV  TYPE OF INITIAL CONDITION
              RSVRIC   1353.00  INITIAL CONDITION
                   X      0.00  WORKING R AND D COEFFICIENT

 23 SA          AREA       2.3       3.0

 24 SE      ELEVATION  1353.00   1356.50

 25 SQ      DISCHARGE       0.       30.      36.      42.      48.      54.      60.      66.      72.

 26 SE      ELEVATION  1353.40   1354.00  1354.27  1354.58  1354.94  1355.35  1355.81  1356.32  1356.83
                                                 ***

                                    COMPUTED STORAGE-ELEVATION DATA

      STORAGE      0.00      9.34
    ELEVATION   1353.00   1356.50

                                 COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

      STORAGE      0.00      0.95      2.44      3.13      3.93      4.89      6.02      7.32      8.80      9.34
      OUTFLOW      0.00      0.00     30.00     36.00     42.00     48.00     54.00     60.00     66.00     68.12
    ELEVATION   1353.00   1353.40   1354.00   1354.27   1354.58   1354.94   1355.35   1355.81   1356.32   1356.50

      STORAGE     10.34
      OUTFLOW     72.00
    ELEVATION   1356.83

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                                   HYDROGRAPH AT STATION    PONDA

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DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE
11	FEB	0600	1	0.	0.0	1353.0	11	FEB	1005	50	0.	0.3	1353.1	11	FEB	1410	99	43.	4.2	1354.7
11	FEB	0605	2	0.	0.0	1353.0	11	FEB	1010	51	0.	0.3	1353.1	11	FEB	1415	100	42.	4.0	1354.6
11	FEB	0610	3	0.	0.0	1353.0	11	FEB	1015	52	0.	0.3	1353.1	11	FEB	1420	101	41.	3.8	1354.5
11	FEB	0615	4	0.	0.0	1353.0	11	FEB	1020	53	0.	0.4	1353.1	11	FEB	1425	102	39.	3.6	1354.4
11	FEB	0620	5	0.	0.0	1353.0	11	FEB	1025	54	0.	0.4	1353.2	11	FEB	1430	103	38.	3.4	1354.4
11	FEB	0625	6	0.	0.0	1353.0	11	FEB	1030	55	0.	0.4	1353.2	11	FEB	1435	104	36.	3.2	1354.3
11	FEB	0630	7	0.	0.0	1353.0	11	FEB	1035	56	0.	0.5	1353.2	11	FEB	1440	105	35.	3.0	1354.2
11	FEB	0635	8	0.	0.0	1353.0	11	FEB	1040	57	0.	0.5	1353.2	11	FEB	1445	106	34.	2.8	1354.2
11	FEB	0640	9	0.	0.0	1353.0	11	FEB	1045	58	0.	0.6	1353.2	11	FEB	1450	107	32.	2.7	1354.1
11	FEB	0645	10	0.	0.0	1353.0	11	FEB	1050	59	0.	0.6	1353.3	11	FEB	1455	108	31.	2.5	1354.0
11	FEB	0650	11	0.	0.0	1353.0	11	FEB	1055	60	0.	0.7	1353.3	11	FEB	1500	109	29.	2.4	1354.0
11	FEB	0655	12	0.	0.0	1353.0	11	FEB	1100	61	0.	0.8	1353.3	11	FEB	1505	110	27.	2.3	1353.9
11	FEB	0700	13	0.	0.0	1353.0	11	FEB	1105	62	0.	0.8	1353.4	11	FEB	1510	111	25.	2.2	1353.9
11	FEB	0705	14	0.	0.0	1353.0	11	FEB	1110	63	0.	0.9	1353.4	11	FEB	1515	112	23.	2.1	1353.9
11	FEB	0710	15	0.	0.0	1353.0	11	FEB	1115	64	1.	1.0	1353.4	11	FEB	1520	113	21.	2.0	1353.8
11	FEB	0715	16	0.	0.0	1353.0	11	FEB	1120	65	3.	1.1	1353.5	11	FEB	1525	114	20.	1.9	1353.8
11	FEB	0720	17	0.	0.0	1353.0	11	FEB	1125	66	5.	1.2	1353.5	11	FEB	1530	115	18.	1.9	1353.8
11	FEB	0725	18	0.	0.0	1353.0	11	FEB	1130	67	7.	1.3	1353.5	11	FEB	1535	116	17.	1.8	1353.7
11	FEB	0730	19	0.	0.0	1353.0	11	FEB	1135	68	9.	1.4	1353.6	11	FEB	1540	117	16.	1.8	1353.7
11	FEB	0735	20	0.	0.0	1353.0	11	FEB	1140	69	13.	1.6	1353.7	11	FEB	1545	118	15.	1.7	1353.7
11	FEB	0740	21	0.	0.0	1353.0	11	FEB	1145	70	20.	1.9	1353.8	11	FEB	1550	119	15.	1.7	1353.7
11	FEB	0745	22	0.	0.0	1353.0	11	FEB	1150	71	31.	2.5	1354.0	11	FEB	1555	120	14.	1.7	1353.7
11	FEB	0750	23	0.	0.0	1353.0	11	FEB	1155	72	37.	3.3	1354.3	11	FEB	1600	121	14.	1.6	1353.7
11	FEB	0755	24	0.	0.0	1353.0	11	FEB	1200	73	44.	4.2	1354.7	11	FEB	1605	122	13.	1.6	1353.7
11	FEB	0800	25	0.	0.0	1353.0	11	FEB	1205	74	50.	5.2	1355.1	11	FEB	1610	123	13.	1.6	1353.7
11	FEB	0805	26	0.	0.0	1353.0	11	FEB	1210	75	55.	6.2	1355.4	11	FEB	1615	124	12.	1.6	1353.6
11	FEB	0810	27	0.	0.0	1353.0	11	FEB	1215	76	58.	7.0	1355.7	11	FEB	1620	125	12.	1.5	1353.6
11	FEB	0815	28	0.	0.0	1353.0	11	FEB	1220	77	61.	7.5	1355.9	11	FEB	1625	126	11.	1.5	1353.6
11	FEB	0820	29	0.	0.0	1353.0	11	FEB	1225	78	62.	7.8	1356.0	11	FEB	1630	127	11.	1.5	1353.6
11	FEB	0825	30	0.	0.0	1353.0	11	FEB	1230	79	63.	7.9	1356.0	11	FEB	1635	128	10.	1.5	1353.6
11	FEB	0830	31	0.	0.0	1353.0	11	FEB	1235	80	63.	8.0	1356.0	11	FEB	1640	129	10.	1.4	1353.6
11	FEB	0835	32	0.	0.0	1353.0	11	FEB	1240	81	63.	8.0	1356.0	11	FEB	1645	130	9.	1.4	1353.6
11	FEB	0840	33	0.	0.0	1353.0	11	FEB	1245	82	62.	7.9	1356.0	11	FEB	1650	131	9.	1.4	1353.6
11	FEB	0845	34	0.	0.0	1353.0	11	FEB	1250	83	62.	7.7	1356.0	11	FEB	1655	132	9.	1.4	1353.6
11	FEB	0850	35	0.	0.0	1353.0	11	FEB	1255	84	61.	7.6	1355.9	11	FEB	1700	133	8.	1.4	1353.6
11	FEB	0855	36	0.	0.0	1353.0	11	FEB	1300	85	60.	7.4	1355.8	11	FEB	1705	134	8.	1.4	1353.6
11	FEB	0900	37	0.	0.0	1353.0	11	FEB	1305	86	59.	7.1	1355.7	11	FEB	1710	135	8.	1.4	1353.6
11	FEB	0905	38	0.	0.0	1353.0	11	FEB	1310	87	58.	6.9	1355.7	11	FEB	1715	136	8.	1.3	1353.6
11	FEB	0910	39	0.	0.0	1353.0	11	FEB	1315	88	57.	6.7	1355.6	11	FEB	1720	137	8.	1.3	1353.6
11	FEB	0915	40	0.	0.1	1353.0	11	FEB	1320	89	56.	6.4	1355.5	11	FEB	1725	138	8.	1.3	1353.6
11	FEB	0920	41	0.	0.1	1353.0	11	FEB	1325	90	55.	6.2	1355.4	11	FEB	1730	139	7.	1.3	1353.5
11	FEB	0925	42	0.	0.1	1353.0	11	FEB	1330	91	54.	6.0	1355.3	11	FEB	1735	140	7.	1.3	1353.5
11	FEB	0930	43	0.	0.1	1353.0	11	FEB	1335	92	52.	5.7	1355.2	11	FEB	1740	141	7.	1.3	1353.5
11	FEB	0935	44	0.	0.1	1353.0	11	FEB	1340	93	51.	5.5	1355.2	11	FEB	1745	142	7.	1.3	1353.5
11	FEB	0940	45	0.	0.1	1353.1	11	FEB	1345	94	50.	5.3	1355.1	11	FEB	1750	143	7.	1.3	1353.5
11	FEB	0945	46	0.	0.2	1353.1	11	FEB	1350	95	49.	5.0	1355.0	11	FEB	1755	144	7.	1.3	1353.5
11	FEB	0950	47	0.	0.2	1353.1	11	FEB	1355	96	47.	4.8	1354.9	11	FEB	1800	145	6.	1.3	1353.5
11	FEB	0955	48	0.	0.2	1353.1	11	FEB	1400	97	46.	4.6	1354.8							
11	FEB	1000	49	0.	0.2	1353.1	11	FEB	1405	98	45.	4.4	1354.7							

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PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	12.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 63.	6.58		33.	17.	17.	17.
		(INCHES)	5.219	5.340	5.340	5.340
		(AC-FT)	16.	17.	17.	17.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	12.00-HR
+ (AC-FT)	(HR)				
8.	6.58	4.	2.	2.	2.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	12.00-HR
+ (FEET)	(HR)				
1356.04	6.58	1354.43	1353.78	1353.78	1353.78

CUMULATIVE AREA = 0.06 SQ MI

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              *            *
27 KK         *   RRWEST   *     OFF SITE DRAINAGE - WEST PORTION OF REFLECTION RIDGE
              *            *
              **************

11 IN             TIME DATA FOR INPUT TIME SERIES
                      JXMIN          30  TIME INTERVAL IN MINUTES
                     JXDATE     11FEB93  STARTING DATE
                     JXTIME         600  STARTING TIME

                SUBBASIN RUNOFF DATA

28 BA             SUBBASIN CHARACTERISTICS
                      TAREA        0.08  SUBBASIN AREA

                  PRECIPITATION DATA

29 PB                 STORM        7.80  BASIN TOTAL PRECIPITATION

30 PI              INCREMENTAL PRECIPITATION PATTERN
                    0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                    0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                    0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                    0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                    0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                    0.00     0.00     0.00     0.00     0.01     0.01     0.01     0.01     0.01     0.01
                    0.01     0.01     0.01     0.01     0.01     0.01     0.06     0.06     0.06     0.06
                    0.06     0.06     0.01     0.01     0.01     0.01     0.01     0.01     0.01     0.01
                    0.01     0.01     0.01     0.01     0.00     0.00     0.00     0.00     0.00     0.00
                    0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                    0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                    0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                    0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                    0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                    0.00     0.00     0.00     0.00

34 LS              SCS LOSS RATE
                     STRTL         0.90  INITIAL ABSTRACTION
                    CRVNBR        69.00  CURVE NUMBER
                     RTIMP         0.00  PERCENT IMPERVIOUS AREA

35 UD              SCS DIMENSIONLESS UNITGRAPH
                      TLAG         0.40  LAG

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                                        UNIT HYDROGRAPH
                                    26 END-OF-PERIOD ORDINATES
                  8.       26.       54.       80.       90.       88.       76.       61.       42.       31.
                 23.       17.       12.        9.        7.        5.        4.        3.        2.        1.
                  1.        1.        1.        0.        0.        0.

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                                HYDROGRAPH AT STATION   RRWEST

*******************************************************************************************************
                                                   *
  DA MON HRMN  ORD    RAIN    LOSS  EXCESS    COMP Q   *   DA MON HRMN  ORD    RAIN    LOSS  EXCESS    COMP Q
                                                   *
  11 FEB 0600    1    0.00    0.00    0.00        0.   *   11 FEB 1205   74    0.11    0.03    0.08      144.
  11 FEB 0605    2    0.02    0.02    0.00        0.   *   11 FEB 1210   75    0.11    0.03    0.09      164.
  11 FEB 0610    3    0.02    0.02    0.00        0.   *   11 FEB 1215   76    0.11    0.03    0.09      169.
  11 FEB 0615    4    0.02    0.02    0.00        0.   *   11 FEB 1220   77    0.11    0.03    0.09      161.
  11 FEB 0620    5    0.02    0.02    0.00        0.   *   11 FEB 1225   78    0.11    0.02    0.09      145.
  11 FEB 0625    6    0.02    0.02    0.00        0.   *   11 FEB 1230   79    0.11    0.02    0.09      126.
  11 FEB 0630    7    0.02    0.02    0.00        0.   *   11 FEB 1235   80    0.06    0.01    0.05      108.
  11 FEB 0635    8    0.02    0.02    0.00        0.   *   11 FEB 1240   81    0.06    0.01    0.05       92.
  11 FEB 0640    9    0.02    0.02    0.00        0.   *   11 FEB 1245   82    0.06    0.01    0.05       80.
  11 FEB 0645   10    0.02    0.02    0.00        0.   *   11 FEB 1250   83    0.06    0.01    0.05       69.
  11 FEB 0650   11    0.02    0.02    0.00        0.   *   11 FEB 1255   84    0.06    0.01    0.05       60.
  11 FEB 0655   12    0.02    0.02    0.00        0.   *   11 FEB 1300   85    0.06    0.01    0.05       53.
  11 FEB 0700   13    0.02    0.02    0.00        0.   *   11 FEB 1305   86    0.04    0.01    0.03       46.
  11 FEB 0705   14    0.02    0.02    0.00        0.   *   11 FEB 1310   87    0.04    0.01    0.03       41.
  11 FEB 0710   15    0.02    0.02    0.00        0.   *   11 FEB 1315   88    0.04    0.01    0.03       37.
  11 FEB 0715   16    0.02    0.02    0.00        0.   *   11 FEB 1320   89    0.04    0.01    0.03       34.
  11 FEB 0720   17    0.02    0.02    0.00        0.   *   11 FEB 1325   90    0.04    0.01    0.03       31.
  11 FEB 0725   18    0.02    0.02    0.00        0.   *   11 FEB 1330   91    0.04    0.01    0.03       29.
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11 FEB 0730	19	0.02	0.02	0.00	0.
11 FEB 0735	20	0.02	0.02	0.00	0.
11 FEB 0740	21	0.02	0.02	0.00	0.
11 FEB 0745	22	0.02	0.02	0.00	0.
11 FEB 0750	23	0.02	0.02	0.00	0.
11 FEB 0755	24	0.02	0.02	0.00	0.
11 FEB 0800	25	0.02	0.02	0.00	0.
11 FEB 0805	26	0.02	0.02	0.00	0.
11 FEB 0810	27	0.02	0.02	0.00	0.
11 FEB 0815	28	0.02	0.02	0.00	0.
11 FEB 0820	29	0.02	0.02	0.00	0.
11 FEB 0825	30	0.02	0.02	0.00	0.
11 FEB 0830	31	0.02	0.02	0.00	0.
11 FEB 0835	32	0.02	0.02	0.00	0.
11 FEB 0840	33	0.02	0.02	0.00	0.
11 FEB 0845	34	0.02	0.02	0.00	0.
11 FEB 0850	35	0.02	0.02	0.00	0.
11 FEB 0855	36	0.02	0.02	0.00	0.
11 FEB 0900	37	0.02	0.02	0.00	0.
11 FEB 0905	38	0.02	0.02	0.00	0.
11 FEB 0910	39	0.02	0.02	0.00	0.
11 FEB 0915	40	0.02	0.02	0.00	0.
11 FEB 0920	41	0.02	0.02	0.00	0.
11 FEB 0925	42	0.02	0.02	0.00	0.
11 FEB 0930	43	0.02	0.02	0.00	0.
11 FEB 0935	44	0.03	0.03	0.00	0.
11 FEB 0940	45	0.03	0.03	0.00	0.
11 FEB 0945	46	0.03	0.03	0.00	0.
11 FEB 0950	47	0.03	0.03	0.00	0.
11 FEB 0955	48	0.03	0.03	0.00	0.
11 FEB 1000	49	0.03	0.03	0.00	0.
11 FEB 1005	50	0.04	0.03	0.00	0.
11 FEB 1010	51	0.04	0.03	0.00	0.
11 FEB 1015	52	0.04	0.03	0.00	0.
11 FEB 1020	53	0.04	0.03	0.00	0.
11 FEB 1025	54	0.04	0.03	0.00	0.
11 FEB 1030	55	0.04	0.03	0.00	1.
11 FEB 1035	56	0.05	0.04	0.01	1.
11 FEB 1040	57	0.05	0.04	0.01	1.
11 FEB 1045	58	0.05	0.04	0.01	2.
11 FEB 1050	59	0.05	0.04	0.01	2.
11 FEB 1055	60	0.05	0.04	0.01	3.
11 FEB 1100	61	0.05	0.04	0.01	3.
11 FEB 1105	62	0.07	0.06	0.02	4.
11 FEB 1110	63	0.07	0.06	0.02	4.
11 FEB 1115	64	0.07	0.06	0.02	5.
11 FEB 1120	65	0.07	0.05	0.02	6.
11 FEB 1125	66	0.07	0.05	0.02	7.
11 FEB 1130	67	0.07	0.05	0.02	9.
11 FEB 1135	68	0.59	0.36	0.23	12.
11 FEB 1140	69	0.59	0.29	0.30	19.
11 FEB 1145	70	0.59	0.25	0.34	33.
11 FEB 1150	71	0.59	0.21	0.38	55.
11 FEB 1155	72	0.59	0.18	0.41	84.
11 FEB 1200	73	0.59	0.16	0.43	115.
11 FEB 1335	92	0.03	0.01	0.03	27.
11 FEB 1340	93	0.03	0.01	0.03	25.
11 FEB 1345	94	0.03	0.01	0.03	24.
11 FEB 1350	95	0.03	0.01	0.03	22.
11 FEB 1355	96	0.03	0.01	0.03	21.
11 FEB 1400	97	0.03	0.01	0.03	20.
11 FEB 1405	98	0.02	0.00	0.02	19.
11 FEB 1410	99	0.02	0.00	0.02	18.
11 FEB 1415	100	0.02	0.00	0.02	18.
11 FEB 1420	101	0.02	0.00	0.02	17.
11 FEB 1425	102	0.02	0.00	0.02	16.
11 FEB 1430	103	0.02	0.00	0.02	15.
11 FEB 1435	104	0.02	0.00	0.02	14.
11 FEB 1440	105	0.02	0.00	0.02	14.
11 FEB 1445	106	0.02	0.00	0.02	13.
11 FEB 1450	107	0.02	0.00	0.02	13.
11 FEB 1455	108	0.02	0.00	0.02	13.
11 FEB 1500	109	0.02	0.00	0.02	13.
11 FEB 1505	110	0.02	0.00	0.02	13.
11 FEB 1510	111	0.02	0.00	0.02	13.
11 FEB 1515	112	0.02	0.00	0.02	12.
11 FEB 1520	113	0.02	0.00	0.02	12.
11 FEB 1525	114	0.02	0.00	0.02	12.
11 FEB 1530	115	0.02	0.00	0.02	12.
11 FEB 1535	116	0.02	0.00	0.02	12.
11 FEB 1540	117	0.02	0.00	0.02	12.
11 FEB 1545	118	0.02	0.00	0.02	12.
11 FEB 1550	119	0.02	0.00	0.02	12.
11 FEB 1555	120	0.02	0.00	0.02	12.
11 FEB 1600	121	0.02	0.00	0.02	12.
11 FEB 1605	122	0.02	0.00	0.01	12.
11 FEB 1610	123	0.02	0.00	0.01	12.
11 FEB 1615	124	0.02	0.00	0.01	12.
11 FEB 1620	125	0.02	0.00	0.01	11.
11 FEB 1625	126	0.02	0.00	0.01	11.
11 FEB 1630	127	0.02	0.00	0.01	10.
11 FEB 1635	128	0.02	0.00	0.01	10.
11 FEB 1640	129	0.02	0.00	0.01	9.
11 FEB 1645	130	0.02	0.00	0.01	9.
11 FEB 1650	131	0.02	0.00	0.01	9.
11 FEB 1655	132	0.02	0.00	0.01	9.
11 FEB 1700	133	0.02	0.00	0.01	9.
11 FEB 1705	134	0.02	0.00	0.01	9.
11 FEB 1710	135	0.02	0.00	0.01	9.
11 FEB 1715	136	0.02	0.00	0.01	8.
11 FEB 1720	137	0.02	0.00	0.01	8.
11 FEB 1725	138	0.02	0.00	0.01	8.
11 FEB 1730	139	0.02	0.00	0.01	8.
11 FEB 1735	140	0.01	0.00	0.01	8.
11 FEB 1740	141	0.01	0.00	0.01	8.
11 FEB 1745	142	0.01	0.00	0.01	8.
11 FEB 1750	143	0.01	0.00	0.01	8.
11 FEB 1755	144	0.01	0.00	0.01	7.
11 FEB 1800	145	0.01	0.00	0.01	7.

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TOTAL RAINFALL = 7.80, TOTAL LOSS = 3.62, TOTAL EXCESS = 4.18

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	12.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 169.	6.25		35.	18.	18.	18.
		(INCHES)	3.981	4.122	4.122	4.122
		(AC-FT)	18.	18.	18.	18.

CUMULATIVE AREA = 0.08 SQ MI

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          *            *
36 KK     *    PONDB   *
          *            *
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HYDROGRAPH ROUTING DATA

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37 RS          STORAGE ROUTING
                    NSTPS          1  NUMBER OF SUBREACHES
                     ITYP       ELEV  TYPE OF INITIAL CONDITION
                    RSVRIC    1350.00  INITIAL CONDITION
                        X       0.00 WORKING R AND D COEFFICIENT

38 SA              AREA        1.0       1.4

39 SE          ELEVATION     1350.00   1352.50

40 SS          SPILLWAY
                     CREL     1350.00  SPILLWAY CREST ELEVATION
                    SPWID       24.00  SPILLWAY WIDTH
                     COQW        3.00  WEIR COEFFICIENT
                     EXPW        1.50  EXPONENT OF HEAD
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COMPUTED STORAGE-ELEVATION DATA

STORAGE	0.00	2.93
ELEVATION	1350.00	1352.50

COMPUTED OUTFLOW-ELEVATION DATA

OUTFLOW	0.00	0.00	0.05	0.39	1.32	3.12	6.10	10.54	16.74	24.99
ELEVATION	1350.00	1350.00	1350.01	1350.03	1350.07	1350.12	1350.19	1350.28	1350.38	1350.49
OUTFLOW	35.58	48.80	64.95	84.33	107.21	133.91	164.70	199.89	239.76	284.60
ELEVATION	1350.63	1350.77	1350.93	1351.11	1351.30	1351.51	1351.74	1351.98	1352.23	1352.50

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	0.00	0.03	0.07	0.12	0.20	0.28	0.39	0.51	0.65	0.81
OUTFLOW	0.00	0.39	1.32	3.12	6.10	10.54	16.74	24.98	35.58	48.80
ELEVATION	1350.00	1350.03	1350.07	1350.12	1350.19	1350.28	1350.38	1350.49	1350.63	1350.77
STORAGE	0.99	1.19	1.42	1.67	1.94	2.24	2.57	2.93		
OUTFLOW	64.95	84.32	107.21	133.91	164.70	199.89	239.76	284.60		
ELEVATION	1350.93	1351.11	1351.30	1351.51	1351.74	1351.98	1352.23	1352.50		

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HYDROGRAPH AT STATION POND8

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DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE
11	FEB	0600	1	0.	0.0	1350.0	11	FEB	1005	50	0.	0.0	1350.0	11	FEB	1410	99	21.	0.4	1350.4
11	FEB	0605	2	0.	0.0	1350.0	11	FEB	1010	51	0.	0.0	1350.0	11	FEB	1415	100	20.	0.4	1350.4
11	FEB	0610	3	0.	0.0	1350.0	11	FEB	1015	52	0.	0.0	1350.0	11	FEB	1420	101	19.	0.4	1350.4
11	FEB	0615	4	0.	0.0	1350.0	11	FEB	1020	53	0.	0.0	1350.0	11	FEB	1425	102	18.	0.4	1350.4
11	FEB	0620	5	0.	0.0	1350.0	11	FEB	1025	54	0.	0.0	1350.0	11	FEB	1430	103	17.	0.4	1350.4
11	FEB	0625	6	0.	0.0	1350.0	11	FEB	1030	55	0.	0.0	1350.0	11	FEB	1435	104	16.	0.4	1350.4
11	FEB	0630	7	0.	0.0	1350.0	11	FEB	1035	56	0.	0.0	1350.0	11	FEB	1440	105	15.	0.4	1350.4
11	FEB	0635	8	0.	0.0	1350.0	11	FEB	1040	57	0.	0.0	1350.0	11	FEB	1445	106	15.	0.4	1350.3
11	FEB	0640	9	0.	0.0	1350.0	11	FEB	1045	58	0.	0.0	1350.0	11	FEB	1450	107	14.	0.3	1350.3
11	FEB	0645	10	0.	0.0	1350.0	11	FEB	1050	59	1.	0.0	1350.0	11	FEB	1455	108	14.	0.3	1350.3
11	FEB	0650	11	0.	0.0	1350.0	11	FEB	1055	60	1.	0.0	1350.0	11	FEB	1500	109	13.	0.3	1350.3
11	FEB	0655	12	0.	0.0	1350.0	11	FEB	1100	61	1.	0.1	1350.1	11	FEB	1505	110	13.	0.3	1350.3
11	FEB	0700	13	0.	0.0	1350.0	11	FEB	1105	62	1.	0.1	1350.1	11	FEB	1510	111	13.	0.3	1350.3
11	FEB	0705	14	0.	0.0	1350.0	11	FEB	1110	63	2.	0.1	1350.1	11	FEB	1515	112	13.	0.3	1350.3
11	FEB	0710	15	0.	0.0	1350.0	11	FEB	1115	64	3.	0.1	1350.1	11	FEB	1520	113	13.	0.3	1350.3
11	FEB	0715	16	0.	0.0	1350.0	11	FEB	1120	65	3.	0.1	1350.1	11	FEB	1525	114	13.	0.3	1350.3
11	FEB	0720	17	0.	0.0	1350.0	11	FEB	1125	66	4.	0.1	1350.1	11	FEB	1530	115	13.	0.3	1350.3
11	FEB	0725	18	0.	0.0	1350.0	11	FEB	1130	67	5.	0.2	1350.2	11	FEB	1535	116	12.	0.3	1350.3
11	FEB	0730	19	0.	0.0	1350.0	11	FEB	1135	68	6.	0.2	1350.2	11	FEB	1540	117	12.	0.3	1350.3
11	FEB	0735	20	0.	0.0	1350.0	11	FEB	1140	69	9.	0.3	1350.2	11	FEB	1545	118	12.	0.3	1350.3
11	FEB	0740	21	0.	0.0	1350.0	11	FEB	1145	70	15.	0.3	1350.3	11	FEB	1550	119	12.	0.3	1350.3
11	FEB	0745	22	0.	0.0	1350.0	11	FEB	1150	71	25.	0.5	1350.5	11	FEB	1555	120	12.	0.3	1350.3
11	FEB	0750	23	0.	0.0	1350.0	11	FEB	1155	72	44.	0.8	1350.7	11	FEB	1600	121	12.	0.3	1350.3
11	FEB	0755	24	0.	0.0	1350.0	11	FEB	1200	73	70.	1.0	1351.0	11	FEB	1605	122	12.	0.3	1350.3
11	FEB	0800	25	0.	0.0	1350.0	11	FEB	1205	74	100.	1.4	1351.2	11	FEB	1610	123	12.	0.3	1350.3
11	FEB	0805	26	0.	0.0	1350.0	11	FEB	1210	75	129.	1.6	1351.5	11	FEB	1615	124	12.	0.3	1350.3

11 FEB	0810	27	0.	0.0	1350.0	*	11 FEB	1215	76	150.	1.8	1351.6	*	11 FEB	1620	125	12.	0.3	1350.3				
11 FEB	0815	28	0.	0.0	1350.0	*	11 FEB	1220	77	158.	1.9	1351.7	*	11 FEB	1625	126	12.	0.3	1350.3				
11 FEB	0820	29	0.	0.0	1350.0	*	11 FEB	1225	78	155.	1.9	1351.7	*	11 FEB	1630	127	11.	0.3	1350.3				
11 FEB	0825	30	0.	0.0	1350.0	*	11 FEB	1230	79	144.	1.8	1351.6	*	11 FEB	1635	128	11.	0.3	1350.3				
11 FEB	0830	31	0.	0.0	1350.0	*	11 FEB	1235	80	129.	1.6	1351.5	*	11 FEB	1640	129	10.	0.3	1350.3				
11 FEB	0835	32	0.	0.0	1350.0	*	11 FEB	1240	81	113.	1.5	1351.4	*	11 FEB	1645	130	10.	0.3	1350.3				
11 FEB	0840	33	0.	0.0	1350.0	*	11 FEB	1245	82	99.	1.3	1351.2	*	11 FEB	1650	131	10.	0.3	1350.3				
11 FEB	0845	34	0.	0.0	1350.0	*	11 FEB	1250	83	86.	1.2	1351.1	*	11 FEB	1655	132	9.	0.3	1350.3				
11 FEB	0850	35	0.	0.0	1350.0	*	11 FEB	1255	84	75.	1.1	1351.0	*	11 FEB	1700	133	9.	0.3	1350.3				
11 FEB	0855	36	0.	0.0	1350.0	*	11 FEB	1300	85	66.	1.0	1350.9	*	11 FEB	1705	134	9.	0.3	1350.2				
11 FEB	0900	37	0.	0.0	1350.0	*	11 FEB	1305	86	58.	0.9	1350.9	*	11 FEB	1710	135	9.	0.3	1350.2				
11 FEB	0905	38	0.	0.0	1350.0	*	11 FEB	1310	87	51.	0.8	1350.8	*	11 FEB	1715	136	9.	0.2	1350.2				
11 FEB	0910	39	0.	0.0	1350.0	*	11 FEB	1315	88	46.	0.8	1350.7	*	11 FEB	1720	137	9.	0.2	1350.2				
11 FEB	0915	40	0.	0.0	1350.0	*	11 FEB	1320	89	41.	0.7	1350.7	*	11 FEB	1725	138	9.	0.2	1350.2				
11 FEB	0920	41	0.	0.0	1350.0	*	11 FEB	1325	90	38.	0.7	1350.6	*	11 FEB	1730	139	9.	0.2	1350.2				
11 FEB	0925	42	0.	0.0	1350.0	*	11 FEB	1330	91	34.	0.6	1350.6	*	11 FEB	1735	140	9.	0.2	1350.2				
11 FEB	0930	43	0.	0.0	1350.0	*	11 FEB	1335	92	32.	0.6	1350.6	*	11 FEB	1740	141	8.	0.2	1350.2				
11 FEB	0935	44	0.	0.0	1350.0	*	11 FEB	1340	93	29.	0.6	1350.5	*	11 FEB	1745	142	8.	0.2	1350.2				
11 FEB	0940	45	0.	0.0	1350.0	*	11 FEB	1345	94	27.	0.5	1350.5	*	11 FEB	1750	143	8.	0.2	1350.2				
11 FEB	0945	46	0.	0.0	1350.0	*	11 FEB	1350	95	26.	0.5	1350.5	*	11 FEB	1755	144	8.	0.2	1350.2				
11 FEB	0950	47	0.	0.0	1350.0	*	11 FEB	1355	96	24.	0.5	1350.5	*	11 FEB	1800	145	8.	0.2	1350.2				
11 FEB	0955	48	0.	0.0	1350.0	*	11 FEB	1400	97	23.	0.5	1350.5	*										
11 FEB	1000	49	0.	0.0	1350.0	*	11 FEB	1405	98	22.	0.5	1350.4	*										

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PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	12.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 158.	6.33		35.	18.	18.	18.
		(INCHES)	3.970	4.072	4.072	4.072
		(AC-FT)	18.	18.	18.	18.

PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	12.00-HR
+ (AC-FT)	(HR)					
2.	6.33		1.	0.	0.	0.

PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	12.00-HR
+ (FEET)	(HR)					
1351.69	6.33		1350.56	1350.29	1350.29	1350.29

CUMULATIVE AREA = 0.08 SQ MI

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          *             *
41 KK     *     WEST    *    PART OF KASTEN'S PROP. - 1/4 AC. RES. LOTS. DRAINS TO TYLER
          *             *
          ***************

11 IN         TIME DATA FOR INPUT TIME SERIES
                   JXMIN        30  TIME INTERVAL IN MINUTES
                  JXDATE    11FEB93  STARTING DATE
                  JXTIME         600  STARTING TIME

            SUBBASIN RUNOFF DATA

42 BA         SUBBASIN CHARACTERISTICS
                   TAREA        0.01  SUBBASIN AREA

              PRECIPITATION DATA

43 PB              STORM        7.80  BASIN TOTAL PRECIPITATION

44 PI           INCREMENTAL PRECIPITATION PATTERN
                  0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00
                  0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00
                  0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00
                  0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00
                  0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00
                  0.00    0.00    0.00    0.00    0.01    0.01    0.01    0.01    0.01    0.01
                  0.01    0.01    0.01    0.01    0.01    0.01    0.06    0.06    0.06    0.06
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0.06	0.06	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00						

48 LS SCS LOSS RATE
STRTL 0.41 INITIAL ABSTRACTION
CRVNBR 83.00 CURVE NUMBER
RTIMP 0.00 PERCENT IMPERVIOUS AREA

49 UD SCS DIMENSIONLESS UNITGRAPH
TLAG 0.25 LAG

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WARNING *** TIME INTERVAL IS GREATER THAN .29*LAG

UNIT HYDROGRAPH
17 END-OF-PERIOD ORDINATES

4.	15.	23.	23.	18.	11.	7.	4.	3.	2.
1.	1.	0.	0.	0.	0.	0.			

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HYDROGRAPH AT STATION WEST

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DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	*	DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
11 FEB 0600	1	0.00	0.00	0.00	0.	*	11 FEB 1205	74	0.11	0.01	0.10	50.
11 FEB 0605	2	0.02	0.02	0.00	0.	*	11 FEB 1210	75	0.11	0.01	0.10	46.
11 FEB 0610	3	0.02	0.02	0.00	0.	*	11 FEB 1215	76	0.11	0.01	0.10	39.
11 FEB 0615	4	0.02	0.02	0.00	0.	*	11 FEB 1220	77	0.11	0.01	0.10	30.
11 FEB 0620	5	0.02	0.02	0.00	0.	*	11 FEB 1225	78	0.11	0.01	0.10	23.
11 FEB 0625	6	0.02	0.02	0.00	0.	*	11 FEB 1230	79	0.11	0.01	0.10	19.
11 FEB 0630	7	0.02	0.02	0.00	0.	*	11 FEB 1235	80	0.06	0.00	0.05	16.
11 FEB 0635	8	0.02	0.02	0.00	0.	*	11 FEB 1240	81	0.06	0.00	0.05	14.
11 FEB 0640	9	0.02	0.02	0.00	0.	*	11 FEB 1245	82	0.06	0.00	0.05	11.
11 FEB 0645	10	0.02	0.02	0.00	0.	*	11 FEB 1250	83	0.06	0.00	0.05	10.
11 FEB 0650	11	0.02	0.02	0.00	0.	*	11 FEB 1255	84	0.06	0.00	0.05	8.
11 FEB 0655	12	0.02	0.02	0.00	0.	*	11 FEB 1300	85	0.06	0.00	0.05	7.
11 FEB 0700	13	0.02	0.02	0.00	0.	*	11 FEB 1305	86	0.04	0.00	0.04	7.
11 FEB 0705	14	0.02	0.02	0.00	0.	*	11 FEB 1310	87	0.04	0.00	0.04	6.
11 FEB 0710	15	0.02	0.02	0.00	0.	*	11 FEB 1315	88	0.04	0.00	0.04	6.
11 FEB 0715	16	0.02	0.02	0.00	0.	*	11 FEB 1320	89	0.04	0.00	0.04	5.
11 FEB 0720	17	0.02	0.02	0.00	0.	*	11 FEB 1325	90	0.04	0.00	0.04	5.
11 FEB 0725	18	0.02	0.02	0.00	0.	*	11 FEB 1330	91	0.04	0.00	0.04	5.
11 FEB 0730	19	0.02	0.02	0.00	0.	*	11 FEB 1335	92	0.03	0.00	0.03	5.
11 FEB 0735	20	0.02	0.02	0.00	0.	*	11 FEB 1340	93	0.03	0.00	0.03	4.
11 FEB 0740	21	0.02	0.02	0.00	0.	*	11 FEB 1345	94	0.03	0.00	0.03	4.
11 FEB 0745	22	0.02	0.02	0.00	0.	*	11 FEB 1350	95	0.03	0.00	0.03	4.
11 FEB 0750	23	0.02	0.02	0.00	0.	*	11 FEB 1355	96	0.03	0.00	0.03	4.
11 FEB 0755	24	0.02	0.02	0.00	0.	*	11 FEB 1400	97	0.03	0.00	0.03	4.
11 FEB 0800	25	0.02	0.02	0.00	0.	*	11 FEB 1405	98	0.02	0.00	0.02	4.
11 FEB 0805	26	0.02	0.02	0.00	0.	*	11 FEB 1410	99	0.02	0.00	0.02	3.
11 FEB 0810	27	0.02	0.02	0.00	0.	*	11 FEB 1415	100	0.02	0.00	0.02	3.
11 FEB 0815	28	0.02	0.02	0.00	0.	*	11 FEB 1420	101	0.02	0.00	0.02	3.
11 FEB 0820	29	0.02	0.02	0.00	0.	*	11 FEB 1425	102	0.02	0.00	0.02	3.
11 FEB 0825	30	0.02	0.02	0.00	0.	*	11 FEB 1430	103	0.02	0.00	0.02	3.
11 FEB 0830	31	0.02	0.02	0.00	0.	*	11 FEB 1435	104	0.02	0.00	0.02	3.
11 FEB 0835	32	0.02	0.02	0.00	0.	*	11 FEB 1440	105	0.02	0.00	0.02	3.
11 FEB 0840	33	0.02	0.02	0.00	0.	*	11 FEB 1445	106	0.02	0.00	0.02	3.
11 FEB 0845	34	0.02	0.02	0.00	0.	*	11 FEB 1450	107	0.02	0.00	0.02	3.
11 FEB 0850	35	0.02	0.02	0.00	0.	*	11 FEB 1455	108	0.02	0.00	0.02	2.
11 FEB 0855	36	0.02	0.02	0.00	0.	*	11 FEB 1500	109	0.02	0.00	0.02	2.
11 FEB 0900	37	0.02	0.02	0.00	0.	*	11 FEB 1505	110	0.02	0.00	0.02	2.
11 FEB 0905	38	0.02	0.02	0.00	0.	*	11 FEB 1510	111	0.02	0.00	0.02	2.
11 FEB 0910	39	0.02	0.02	0.01	0.	*	11 FEB 1515	112	0.02	0.00	0.02	2.
11 FEB 0915	40	0.02	0.02	0.01	0.	*	11 FEB 1520	113	0.02	0.00	0.02	2.
11 FEB 0920	41	0.02	0.02	0.01	0.	*	11 FEB 1525	114	0.02	0.00	0.02	2.
11 FEB 0925	42	0.02	0.02	0.01	1.	*	11 FEB 1530	115	0.02	0.00	0.02	2.
11 FEB 0930	43	0.02	0.02	0.01	1.	*	11 FEB 1535	116	0.02	0.00	0.02	2.
11 FEB 0935	44	0.03	0.02	0.01	1.	*	11 FEB 1540	117	0.02	0.00	0.02	2.
11 FEB 0940	45	0.03	0.02	0.01	1.	*	11 FEB 1545	118	0.02	0.00	0.02	2.
11 FEB 0945	46	0.03	0.02	0.01	1.	*	11 FEB 1550	119	0.02	0.00	0.02	2.

11 FEB 0950	47	0.03	0.02	0.01	1.	*	11 FEB 1555	120	0.02	0.00	0.02	2.
11 FEB 0955	48	0.03	0.02	0.01	1.	*	11 FEB 1600	121	0.02	0.00	0.02	2.
11 FEB 1000	49	0.03	0.02	0.01	1.	*	11 FEB 1605	122	0.02	0.00	0.01	2.
11 FEB 1005	50	0.04	0.02	0.01	1.	*	11 FEB 1610	123	0.02	0.00	0.01	2.
11 FEB 1010	51	0.04	0.02	0.01	1.	*	11 FEB 1615	124	0.02	0.00	0.01	2.
11 FEB 1015	52	0.04	0.02	0.01	1.	*	11 FEB 1620	125	0.02	0.00	0.01	2.
11 FEB 1020	53	0.04	0.02	0.02	1.	*	11 FEB 1625	126	0.02	0.00	0.01	2.
11 FEB 1025	54	0.04	0.02	0.02	1.	*	11 FEB 1630	127	0.02	0.00	0.01	2.
11 FEB 1030	55	0.04	0.02	0.02	2.	*	11 FEB 1635	128	0.02	0.00	0.01	2.
11 FEB 1035	56	0.05	0.03	0.02	2.	*	11 FEB 1640	129	0.02	0.00	0.01	2.
11 FEB 1040	57	0.05	0.02	0.02	2.	*	11 FEB 1645	130	0.02	0.00	0.01	2.
11 FEB 1045	58	0.05	0.02	0.02	2.	*	11 FEB 1650	131	0.02	0.00	0.01	2.
11 FEB 1050	59	0.05	0.02	0.03	2.	*	11 FEB 1655	132	0.02	0.00	0.01	2.
11 FEB 1055	60	0.05	0.02	0.03	2.	*	11 FEB 1700	133	0.02	0.00	0.01	2.
11 FEB 1100	61	0.05	0.02	0.03	3.	*	11 FEB 1705	134	0.02	0.00	0.01	2.
11 FEB 1105	62	0.07	0.03	0.04	3.	*	11 FEB 1710	135	0.02	0.00	0.01	2.
11 FEB 1110	63	0.07	0.03	0.04	3.	*	11 FEB 1715	136	0.02	0.00	0.01	2.
11 FEB 1115	64	0.07	0.03	0.05	4.	*	11 FEB 1720	137	0.02	0.00	0.01	2.
11 FEB 1120	65	0.07	0.03	0.05	4.	*	11 FEB 1725	138	0.02	0.00	0.01	2.
11 FEB 1125	66	0.07	0.03	0.05	4.	*	11 FEB 1730	139	0.02	0.00	0.01	2.
11 FEB 1130	67	0.07	0.03	0.05	5.	*	11 FEB 1735	140	0.01	0.00	0.01	2.
11 FEB 1135	68	0.59	0.17	0.42	7.	*	11 FEB 1740	141	0.01	0.00	0.01	2.
11 FEB 1140	69	0.59	0.13	0.46	12.	*	11 FEB 1745	142	0.01	0.00	0.01	1.
11 FEB 1145	70	0.59	0.10	0.49	22.	*	11 FEB 1750	143	0.01	0.00	0.01	1.
11 FEB 1150	71	0.59	0.08	0.51	32.	*	11 FEB 1755	144	0.01	0.00	0.01	1.
11 FEB 1155	72	0.59	0.06	0.53	41.	*	11 FEB 1800	145	0.01	0.00	0.01	1.
11 FEB 1200	73	0.59	0.05	0.54	47.	*						
						*						

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TOTAL RAINFALL = 7.80, TOTAL LOSS = 2.01, TOTAL EXCESS = 5.79

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	12.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 50.	6.08		8.	4.	4.	4.
		(INCHES)	5.355	5.749	5.749	5.749
		(AC-FT)	4.	4.	4.	4.

CUMULATIVE AREA = 0.01 SQ MI

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          **************
          *            *
50 KK     *   BASIN1   *
          *            *
          **************

11 IN          TIME DATA FOR INPUT TIME SERIES
                  JXMIN           30  TIME INTERVAL IN MINUTES
                  JXDATE     11FEB93  STARTING DATE
                  JXTIME         600  STARTING TIME

             SUBBASIN RUNOFF DATA

51 BA          SUBBASIN CHARACTERISTICS
                  TAREA         0.00  SUBBASIN AREA

               PRECIPITATION DATA

52 PB             STORM         7.80  BASIN TOTAL PRECIPITATION

53 PI            INCREMENTAL PRECIPITATION PATTERN
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0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.06	0.06	0.06	0.06
0.06	0.06	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00						

57 LS SCS LOSS RATE

STRTL	0.53	INITIAL ABSTRACTION
CRVNBR	79.00	CURVE NUMBER
RTIMP	0.00	PERCENT IMPERVIOUS AREA

58 UD SCS DIMENSIONLESS UNITGRAPH

TLAG	0.25	LAG

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WARNING *** TIME INTERVAL IS GREATER THAN .29*LAG

UNIT HYDROGRAPH
17 END-OF-PERIOD ORDINATES

1.	5.	8.	8.	6.	4.	2.	1.	1.	1.
0.	0.	0.	0.	0.	0.	0.			

****

HYDROGRAPH AT STATION BASIN1

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DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
11 FEB 0600	1	0.00	0.00	0.00	0.	11 FEB 1205	74	0.11	0.01	0.10	15.
11 FEB 0605	2	0.02	0.02	0.00	0.	11 FEB 1210	75	0.11	0.01	0.10	14.
11 FEB 0610	3	0.02	0.02	0.00	0.	11 FEB 1215	76	0.11	0.01	0.10	12.
11 FEB 0615	4	0.02	0.02	0.00	0.	11 FEB 1220	77	0.11	0.01	0.10	9.
11 FEB 0620	5	0.02	0.02	0.00	0.	11 FEB 1225	78	0.11	0.01	0.10	7.
11 FEB 0625	6	0.02	0.02	0.00	0.	11 FEB 1230	79	0.11	0.01	0.10	6.
11 FEB 0630	7	0.02	0.02	0.00	0.	11 FEB 1235	80	0.06	0.01	0.05	5.
11 FEB 0635	8	0.02	0.02	0.00	0.	11 FEB 1240	81	0.06	0.01	0.05	4.
11 FEB 0640	9	0.02	0.02	0.00	0.	11 FEB 1245	82	0.06	0.01	0.05	4.
11 FEB 0645	10	0.02	0.02	0.00	0.	11 FEB 1250	83	0.06	0.01	0.05	3.
11 FEB 0650	11	0.02	0.02	0.00	0.	11 FEB 1255	84	0.06	0.01	0.05	3.
11 FEB 0655	12	0.02	0.02	0.00	0.	11 FEB 1300	85	0.06	0.01	0.05	2.
11 FEB 0700	13	0.02	0.02	0.00	0.	11 FEB 1305	86	0.04	0.00	0.04	2.
11 FEB 0705	14	0.02	0.02	0.00	0.	11 FEB 1310	87	0.04	0.00	0.04	2.
11 FEB 0710	15	0.02	0.02	0.00	0.	11 FEB 1315	88	0.04	0.00	0.04	2.
11 FEB 0715	16	0.02	0.02	0.00	0.	11 FEB 1320	89	0.04	0.00	0.04	2.
11 FEB 0720	17	0.02	0.02	0.00	0.	11 FEB 1325	90	0.04	0.00	0.04	2.
11 FEB 0725	18	0.02	0.02	0.00	0.	11 FEB 1330	91	0.04	0.00	0.04	1.
11 FEB 0730	19	0.02	0.02	0.00	0.	11 FEB 1335	92	0.03	0.00	0.03	1.
11 FEB 0735	20	0.02	0.02	0.00	0.	11 FEB 1340	93	0.03	0.00	0.03	1.
11 FEB 0740	21	0.02	0.02	0.00	0.	11 FEB 1345	94	0.03	0.00	0.03	1.
11 FEB 0745	22	0.02	0.02	0.00	0.	11 FEB 1350	95	0.03	0.00	0.03	1.
11 FEB 0750	23	0.02	0.02	0.00	0.	11 FEB 1355	96	0.03	0.00	0.03	1.
11 FEB 0755	24	0.02	0.02	0.00	0.	11 FEB 1400	97	0.03	0.00	0.03	1.
11 FEB 0800	25	0.02	0.02	0.00	0.	11 FEB 1405	98	0.02	0.00	0.02	1.
11 FEB 0805	26	0.02	0.02	0.00	0.	11 FEB 1410	99	0.02	0.00	0.02	1.
11 FEB 0810	27	0.02	0.02	0.00	0.	11 FEB 1415	100	0.02	0.00	0.02	1.
11 FEB 0815	28	0.02	0.02	0.00	0.	11 FEB 1420	101	0.02	0.00	0.02	1.
11 FEB 0820	29	0.02	0.02	0.00	0.	11 FEB 1425	102	0.02	0.00	0.02	1.
11 FEB 0825	30	0.02	0.02	0.00	0.	11 FEB 1430	103	0.02	0.00	0.02	1.
11 FEB 0830	31	0.02	0.02	0.00	0.	11 FEB 1435	104	0.02	0.00	0.02	1.
11 FEB 0835	32	0.02	0.02	0.00	0.	11 FEB 1440	105	0.02	0.00	0.02	1.
11 FEB 0840	33	0.02	0.02	0.00	0.	11 FEB 1445	106	0.02	0.00	0.02	1.
11 FEB 0845	34	0.02	0.02	0.00	0.	11 FEB 1450	107	0.02	0.00	0.02	1.
11 FEB 0850	35	0.02	0.02	0.00	0.	11 FEB 1455	108	0.02	0.00	0.02	1.
11 FEB 0855	36	0.02	0.02	0.00	0.	11 FEB 1500	109	0.02	0.00	0.02	1.
11 FEB 0900	37	0.02	0.02	0.00	0.	11 FEB 1505	110	0.02	0.00	0.02	1.
11 FEB 0905	38	0.02	0.02	0.00	0.	11 FEB 1510	111	0.02	0.00	0.02	1.
11 FEB 0910	39	0.02	0.02	0.00	0.	11 FEB 1515	112	0.02	0.00	0.02	1.
11 FEB 0915	40	0.02	0.02	0.00	0.	11 FEB 1520	113	0.02	0.00	0.02	1.
11 FEB 0920	41	0.02	0.02	0.00	0.	11 FEB 1525	114	0.02	0.00	0.02	1.
11 FEB 0925	42	0.02	0.02	0.00	0.	11 FEB 1530	115	0.02	0.00	0.02	1.
11 FEB 0930	43	0.02	0.02	0.00	0.	11 FEB 1535	116	0.02	0.00	0.02	1.
11 FEB 0935	44	0.03	0.02	0.00	0.	11 FEB 1540	117	0.02	0.00	0.02	1.
11 FEB 0940	45	0.03	0.02	0.01	0.	11 FEB 1545	118	0.02	0.00	0.02	1.
11 FEB 0945	46	0.03	0.02	0.01	0.	11 FEB 1550	119	0.02	0.00	0.02	1.
11 FEB 0950	47	0.03	0.02	0.01	0.	11 FEB 1555	120	0.02	0.00	0.02	1.
11 FEB 0955	48	0.03	0.02	0.01	0.	11 FEB 1600	121	0.02	0.00	0.02	1.
11 FEB 1000	49	0.03	0.02	0.01	0.	11 FEB 1605	122	0.02	0.00	0.01	1.
11 FEB 1005	50	0.04	0.03	0.01	0.	11 FEB 1610	123	0.02	0.00	0.01	1.

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66 LS          SCS LOSS RATE
                    STRTL       0.47  INITIAL ABSTRACTION
                   CRVNBR      81.00  CURVE NUMBER
                    RTIMP       0.00  PERCENT IMPERVIOUS AREA

67 UD          SCS DIMENSIONLESS UNITGRAPH
                    TLAG       0.25  LAG

                                                ***

WARNING *** TIME INTERVAL IS GREATER THAN .29*LAG

                                          UNIT HYDROGRAPH
                                      17 END-OF-PERIOD ORDINATES
            17.      58.      92.      92.      72.      43.      27.      17.      11.       7.
             4.       3.       2.       1.       1.       0.       0.
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HYDROGRAPH AT STATION BASIN2

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DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
11 FEB 0600	1	0.00	0.00	0.00	0.	11 FEB 1205	74	0.11	0.01	0.10	191.
11 FEB 0605	2	0.02	0.02	0.00	0.	11 FEB 1210	75	0.11	0.01	0.10	179.
11 FEB 0610	3	0.02	0.02	0.00	0.	11 FEB 1215	76	0.11	0.01	0.10	149.
11 FEB 0615	4	0.02	0.02	0.00	0.	11 FEB 1220	77	0.11	0.01	0.10	115.
11 FEB 0620	5	0.02	0.02	0.00	0.	11 FEB 1225	78	0.11	0.01	0.10	89.
11 FEB 0625	6	0.02	0.02	0.00	0.	11 FEB 1230	79	0.11	0.01	0.10	73.
11 FEB 0630	7	0.02	0.02	0.00	0.	11 FEB 1235	80	0.06	0.00	0.05	62.
11 FEB 0635	8	0.02	0.02	0.00	0.	11 FEB 1240	81	0.06	0.00	0.05	53.
11 FEB 0640	9	0.02	0.02	0.00	0.	11 FEB 1245	82	0.06	0.00	0.05	44.
11 FEB 0645	10	0.02	0.02	0.00	0.	11 FEB 1250	83	0.06	0.00	0.05	37.
11 FEB 0650	11	0.02	0.02	0.00	0.	11 FEB 1255	84	0.06	0.00	0.05	32.
11 FEB 0655	12	0.02	0.02	0.00	0.	11 FEB 1300	85	0.06	0.00	0.05	29.
11 FEB 0700	13	0.02	0.02	0.00	0.	11 FEB 1305	86	0.04	0.00	0.04	27.
11 FEB 0705	14	0.02	0.02	0.00	0.	11 FEB 1310	87	0.04	0.00	0.04	25.
11 FEB 0710	15	0.02	0.02	0.00	0.	11 FEB 1315	88	0.04	0.00	0.04	22.
11 FEB 0715	16	0.02	0.02	0.00	0.	11 FEB 1320	89	0.04	0.00	0.04	21.
11 FEB 0720	17	0.02	0.02	0.00	0.	11 FEB 1325	90	0.04	0.00	0.04	19.
11 FEB 0725	18	0.02	0.02	0.00	0.	11 FEB 1330	91	0.04	0.00	0.04	19.
11 FEB 0730	19	0.02	0.02	0.00	0.	11 FEB 1335	92	0.03	0.00	0.03	18.
11 FEB 0735	20	0.02	0.02	0.00	0.	11 FEB 1340	93	0.03	0.00	0.03	17.
11 FEB 0740	21	0.02	0.02	0.00	0.	11 FEB 1345	94	0.03	0.00	0.03	16.
11 FEB 0745	22	0.02	0.02	0.00	0.	11 FEB 1350	95	0.03	0.00	0.03	15.
11 FEB 0750	23	0.02	0.02	0.00	0.	11 FEB 1355	96	0.03	0.00	0.03	15.
11 FEB 0755	24	0.02	0.02	0.00	0.	11 FEB 1400	97	0.03	0.00	0.03	14.
11 FEB 0800	25	0.02	0.02	0.00	0.	11 FEB 1405	98	0.02	0.00	0.02	14.
11 FEB 0805	26	0.02	0.02	0.00	0.	11 FEB 1410	99	0.02	0.00	0.02	13.
11 FEB 0810	27	0.02	0.02	0.00	0.	11 FEB 1415	100	0.02	0.00	0.02	12.
11 FEB 0815	28	0.02	0.02	0.00	0.	11 FEB 1420	101	0.02	0.00	0.02	11.
11 FEB 0820	29	0.02	0.02	0.00	0.	11 FEB 1425	102	0.02	0.00	0.02	11.
11 FEB 0825	30	0.02	0.02	0.00	0.	11 FEB 1430	103	0.02	0.00	0.02	10.
11 FEB 0830	31	0.02	0.02	0.00	0.	11 FEB 1435	104	0.02	0.00	0.02	10.
11 FEB 0835	32	0.02	0.02	0.00	0.	11 FEB 1440	105	0.02	0.00	0.02	10.
11 FEB 0840	33	0.02	0.02	0.00	0.	11 FEB 1445	106	0.02	0.00	0.02	10.
11 FEB 0845	34	0.02	0.02	0.00	0.	11 FEB 1450	107	0.02	0.00	0.02	10.
11 FEB 0850	35	0.02	0.02	0.00	0.	11 FEB 1455	108	0.02	0.00	0.02	10.
11 FEB 0855	36	0.02	0.02	0.00	0.	11 FEB 1500	109	0.02	0.00	0.02	10.
11 FEB 0900	37	0.02	0.02	0.00	1.	11 FEB 1505	110	0.02	0.00	0.02	10.
11 FEB 0905	38	0.02	0.02	0.00	1.	11 FEB 1510	111	0.02	0.00	0.02	10.
11 FEB 0910	39	0.02	0.02	0.00	1.	11 FEB 1515	112	0.02	0.00	0.02	10.
11 FEB 0915	40	0.02	0.02	0.00	1.	11 FEB 1520	113	0.02	0.00	0.02	10.
11 FEB 0920	41	0.02	0.02	0.00	1.	11 FEB 1525	114	0.02	0.00	0.02	10.
11 FEB 0925	42	0.02	0.02	0.00	2.	11 FEB 1530	115	0.02	0.00	0.02	10.
11 FEB 0930	43	0.02	0.02	0.01	2.	11 FEB 1535	116	0.02	0.00	0.02	10.
11 FEB 0935	44	0.03	0.02	0.01	2.	11 FEB 1540	117	0.02	0.00	0.02	10.
11 FEB 0940	45	0.03	0.02	0.01	2.	11 FEB 1545	118	0.02	0.00	0.02	10.
11 FEB 0945	46	0.03	0.02	0.01	2.	11 FEB 1550	119	0.02	0.00	0.02	10.
11 FEB 0950	47	0.03	0.02	0.01	3.	11 FEB 1555	120	0.02	0.00	0.02	10.
11 FEB 0955	48	0.03	0.02	0.01	3.	11 FEB 1600	121	0.02	0.00	0.02	10.
11 FEB 1000	49	0.03	0.02	0.01	3.	11 FEB 1605	122	0.02	0.00	0.01	10.
11 FEB 1005	50	0.04	0.02	0.01	3.	11 FEB 1610	123	0.02	0.00	0.01	9.
11 FEB 1010	51	0.04	0.02	0.01	4.	11 FEB 1615	124	0.02	0.00	0.01	9.
11 FEB 1015	52	0.04	0.02	0.01	4.	11 FEB 1620	125	0.02	0.00	0.01	8.
11 FEB 1020	53	0.04	0.02	0.01	5.	11 FEB 1625	126	0.02	0.00	0.01	7.
11 FEB 1025	54	0.04	0.02	0.01	5.	11 FEB 1630	127	0.02	0.00	0.01	7.

11 FEB 1010	51	0.04	0.03	0.01	0.	*	11 FEB 1615	124	0.02	0.00	0.01	1.
11 FEB 1015	52	0.04	0.03	0.01	0.	*	11 FEB 1620	125	0.02	0.00	0.01	1.
11 FEB 1020	53	0.04	0.02	0.01	0.	*	11 FEB 1625	126	0.02	0.00	0.01	1.
11 FEB 1025	54	0.04	0.02	0.01	0.	*	11 FEB 1630	127	0.02	0.00	0.01	1.
11 FEB 1030	55	0.04	0.02	0.01	0.	*	11 FEB 1635	128	0.02	0.00	0.01	1.
11 FEB 1035	56	0.05	0.03	0.02	0.	*	11 FEB 1640	129	0.02	0.00	0.01	1.
11 FEB 1040	57	0.05	0.03	0.02	0.	*	11 FEB 1645	130	0.02	0.00	0.01	1.
11 FEB 1045	58	0.05	0.03	0.02	0.	*	11 FEB 1650	131	0.02	0.00	0.01	1.
11 FEB 1050	59	0.05	0.03	0.02	1.	*	11 FEB 1655	132	0.02	0.00	0.01	1.
11 FEB 1055	60	0.05	0.03	0.02	1.	*	11 FEB 1700	133	0.02	0.00	0.01	1.
11 FEB 1100	61	0.05	0.03	0.02	1.	*	11 FEB 1705	134	0.02	0.00	0.01	1.
11 FEB 1105	62	0.07	0.04	0.03	1.	*	11 FEB 1710	135	0.02	0.00	0.01	1.
11 FEB 1110	63	0.07	0.04	0.04	1.	*	11 FEB 1715	136	0.02	0.00	0.01	1.
11 FEB 1115	64	0.07	0.04	0.04	1.	*	11 FEB 1720	137	0.02	0.00	0.01	1.
11 FEB 1120	65	0.07	0.04	0.04	1.	*	11 FEB 1725	138	0.02	0.00	0.01	1.
11 FEB 1125	66	0.07	0.03	0.04	1.	*	11 FEB 1730	139	0.02	0.00	0.01	1.
11 FEB 1130	67	0.07	0.03	0.04	1.	*	11 FEB 1735	140	0.01	0.00	0.01	1.
11 FEB 1135	68	0.59	0.23	0.37	2.	*	11 FEB 1740	141	0.01	0.00	0.01	0.
11 FEB 1140	69	0.59	0.17	0.42	3.	*	11 FEB 1745	142	0.01	0.00	0.01	0.
11 FEB 1145	70	0.59	0.14	0.45	6.	*	11 FEB 1750	143	0.01	0.00	0.01	0.
11 FEB 1150	71	0.59	0.11	0.48	9.	*	11 FEB 1755	144	0.01	0.00	0.01	0.
11 FEB 1155	72	0.59	0.09	0.50	12.	*	11 FEB 1800	145	0.01	0.00	0.01	0.
11 FEB 1200	73	0.59	0.08	0.51	14.	*						

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TOTAL RAINFALL = 7.80, TOTAL LOSS = 2.48, TOTAL EXCESS = 5.32

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	12.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 15.	6.08		3.	1.	1.	1.
		(INCHES)	4.972	5.285	5.285	5.285
		(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = 0.00 SQ MI

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              **************
              *            *
59 KK         *   BASIN2   *
              *            *
              **************

11 IN         TIME DATA FOR INPUT TIME SERIES
                 JXMIN          30  TIME INTERVAL IN MINUTES
                 JXDATE    11FEB93  STARTING DATE
                 JXTIME        600  STARTING TIME

            SUBBASIN RUNOFF DATA

60 BA         SUBBASIN CHARACTERISTICS
                 TAREA        0.06  SUBBASIN AREA

              PRECIPITATION DATA

61 PB            STORM        7.80  BASIN TOTAL PRECIPITATION

62 PI           INCREMENTAL PRECIPITATION PATTERN
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0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.06	0.06	0.06	0.06
0.06	0.06	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00						

11 FEB 1030	55	0.04	0.02	0.01	5.	*	11 FEB 1635	128	0.02	0.00	0.01	7.		
11 FEB 1035	56	0.05	0.03	0.02	6.	*	11 FEB 1640	129	0.02	0.00	0.01	7.		
11 FEB 1040	57	0.05	0.03	0.02	6.	*	11 FEB 1645	130	0.02	0.00	0.01	7.		
11 FEB 1045	58	0.05	0.03	0.02	7.	*	11 FEB 1650	131	0.02	0.00	0.01	7.		
11 FEB 1050	59	0.05	0.03	0.02	8.	*	11 FEB 1655	132	0.02	0.00	0.01	7.		
11 FEB 1055	60	0.05	0.03	0.02	9.	*	11 FEB 1700	133	0.02	0.00	0.01	7.		
11 FEB 1100	61	0.05	0.02	0.02	9.	*	11 FEB 1705	134	0.02	0.00	0.01	7.		
11 FEB 1105	62	0.07	0.04	0.04	10.	*	11 FEB 1710	135	0.02	0.00	0.01	7.		
11 FEB 1110	63	0.07	0.03	0.04	11.	*	11 FEB 1715	136	0.02	0.00	0.01	7.		
11 FEB 1115	64	0.07	0.03	0.04	13.	*	11 FEB 1720	137	0.02	0.00	0.01	7.		
11 FEB 1120	65	0.07	0.03	0.04	15.	*	11 FEB 1725	138	0.02	0.00	0.01	7.		
11 FEB 1125	66	0.07	0.03	0.04	16.	*	11 FEB 1730	139	0.02	0.00	0.01	7.		
11 FEB 1130	67	0.07	0.03	0.05	17.	*	11 FEB 1735	140	0.01	0.00	0.01	6.		
11 FEB 1135	68	0.59	0.20	0.39	24.	*	11 FEB 1740	141	0.01	0.00	0.01	6.		
11 FEB 1140	69	0.59	0.15	0.44	46.	*	11 FEB 1745	142	0.01	0.00	0.01	6.		
11 FEB 1145	70	0.59	0.12	0.47	82.	*	11 FEB 1750	143	0.01	0.00	0.01	5.		
11 FEB 1150	71	0.59	0.10	0.50	121.	*	11 FEB 1755	144	0.01	0.00	0.01	5.		
11 FEB 1155	72	0.59	0.08	0.51	155.	*	11 FEB 1800	145	0.01	0.00	0.01	4.		
11 FEB 1200	73	0.59	0.07	0.52	180.	*								
						*								

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TOTAL RAINFALL = 7.80, TOTAL LOSS = 2.25, TOTAL EXCESS = 5.55

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	12.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 191.	6.08		32.	17.	17.	17.
		(INCHES)	5.165	5.516	5.516	5.516
		(AC-FT)	16.	17.	17.	17.

CUMULATIVE AREA = 0.06 SQ MI

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          *            *
68 KK     *    INTO2   *
          *            *
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69 HC HYDROGRAPH COMBINATION
ICOMP 5 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION INTO2
SUM OF 5 HYDROGRAPHS

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DA MON HRMN	ORD	FLOW	*	DA MON HRMN	ORD	FLOW	*	DA MON HRMN	ORD	FLOW	*	DA MON HRMN	ORD	FLOW
11 FEB 0600	1	0.	*	11 FEB 0905	38	1.	*	11 FEB 1210	75	424.	*	11 FEB 1515	112	48.
11 FEB 0605	2	0.	*	11 FEB 0910	39	1.	*	11 FEB 1215	76	407.	*	11 FEB 1520	113	47.
11 FEB 0610	3	0.	*	11 FEB 0915	40	2.	*	11 FEB 1220	77	373.	*	11 FEB 1525	114	45.
11 FEB 0615	4	0.	*	11 FEB 0920	41	2.	*	11 FEB 1225	78	336.	*	11 FEB 1530	115	44.
11 FEB 0620	5	0.	*	11 FEB 0925	42	2.	*	11 FEB 1230	79	304.	*	11 FEB 1535	116	43.
11 FEB 0625	6	0.	*	11 FEB 0930	43	2.	*	11 FEB 1235	80	274.	*	11 FEB 1540	117	42.
11 FEB 0630	7	0.	*	11 FEB 0935	44	3.	*	11 FEB 1240	81	246.	*	11 FEB 1545	118	41.
11 FEB 0635	8	0.	*	11 FEB 0940	45	3.	*	11 FEB 1245	82	220.	*	11 FEB 1550	119	40.
11 FEB 0640	9	0.	*	11 FEB 0945	46	3.	*	11 FEB 1250	83	197.	*	11 FEB 1555	120	40.
11 FEB 0645	10	0.	*	11 FEB 0950	47	4.	*	11 FEB 1255	84	179.	*	11 FEB 1600	121	39.
11 FEB 0650	11	0.	*	11 FEB 0955	48	4.	*	11 FEB 1300	85	165.	*	11 FEB 1605	122	38.
11 FEB 0655	12	0.	*	11 FEB 1000	49	4.	*	11 FEB 1305	86	153.	*	11 FEB 1610	123	37.
11 FEB 0700	13	0.	*	11 FEB 1005	50	5.	*	11 FEB 1310	87	142.	*	11 FEB 1615	124	36.
11 FEB 0705	14	0.	*	11 FEB 1010	51	5.	*	11 FEB 1315	88	133.	*	11 FEB 1620	125	34.
11 FEB 0710	15	0.	*	11 FEB 1015	52	6.	*	11 FEB 1320	89	125.	*	11 FEB 1625	126	33.
11 FEB 0715	16	0.	*	11 FEB 1020	53	6.	*	11 FEB 1325	90	118.	*	11 FEB 1630	127	31.
11 FEB 0720	17	0.	*	11 FEB 1025	54	7.	*	11 FEB 1330	91	113.	*	11 FEB 1635	128	30.
11 FEB 0725	18	0.	*	11 FEB 1030	55	7.	*	11 FEB 1335	92	108.	*	11 FEB 1640	129	29.
11 FEB 0730	19	0.	*	11 FEB 1035	56	8.	*	11 FEB 1340	93	104.	*	11 FEB 1645	130	28.
11 FEB 0735	20	0.	*	11 FEB 1040	57	9.	*	11 FEB 1345	94	99.	*	11 FEB 1650	131	28.

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 11 FEB 0740  21      0.  *  11 FEB 1045  58      10.  *  11 FEB 1350  95      95.  *  11 FEB 1655  132     27.
 11 FEB 0745  22      0.  *  11 FEB 1050  59      11.  *  11 FEB 1355  96      91.  *  11 FEB 1700  133     26.
 11 FEB 0750  23      0.  *  11 FEB 1055  60      12.  *  11 FEB 1400  97      88.  *  11 FEB 1705  134     26.
 11 FEB 0755  24      0.  *  11 FEB 1100  61      13.  *  11 FEB 1405  98      85.  *  11 FEB 1710  135     26.
 11 FEB 0800  25      0.  *  11 FEB 1105  62      15.  *  11 FEB 1410  99      82.  *  11 FEB 1715  136     25.
 11 FEB 0805  26      0.  *  11 FEB 1110  63      17.  *  11 FEB 1415  100     78.  *  11 FEB 1720  137     25.
 11 FEB 0810  27      0.  *  11 FEB 1115  64      21.  *  11 FEB 1420  101     75.  *  11 FEB 1725  138     25.
 11 FEB 0815  28      0.  *  11 FEB 1120  65      26.  *  11 FEB 1425  102     71.  *  11 FEB 1730  139     25.
 11 FEB 0820  29      0.  *  11 FEB 1125  66      31.  *  11 FEB 1430  103     68.  *  11 FEB 1735  140     24.
 11 FEB 0825  30      0.  *  11 FEB 1130  67      35.  *  11 FEB 1435  104     66.  *  11 FEB 1740  141     24.
 11 FEB 0830  31      0.  *  11 FEB 1135  68      48.  *  11 FEB 1440  105     64.  *  11 FEB 1745  142     23.
 11 FEB 0835  32      0.  *  11 FEB 1140  69      83.  *  11 FEB 1445  106     61.  *  11 FEB 1750  143     22.
 11 FEB 0840  33      0.  *  11 FEB 1145  70     144.  *  11 FEB 1450  107     59.  *  11 FEB 1755  144     21.
 11 FEB 0845  34      0.  *  11 FEB 1150  71     218.  *  11 FEB 1455  108     58.  *  11 FEB 1800  145     20.
 11 FEB 0850  35      0.  *  11 FEB 1155  72     289.  *  11 FEB 1500  109     56.  *
 11 FEB 0855  36      1.  *  11 FEB 1200  73     355.  *  11 FEB 1505  110     53.  *
 11 FEB 0900  37      1.  *  11 FEB 1205  74     405.  *  11 FEB 1510  111     50.  *
                          *                            *                            *
*****************************************************************************************************

  PEAK FLOW    TIME                      MAXIMUM AVERAGE FLOW
                                   6-HR        24-HR       72-HR      12.00-HR
+   (CFS)      (HR)
                          (CFS)
+     424.     6.17                110.          58.         58.          58.
                       (INCHES)   4.703        4.931       4.931        4.931
                        (AC-FT)     55.          57.         57.          57.

                          CUMULATIVE AREA =     0.22 SQ MI


*** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** ***

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              *            *
  70 KK       *   PON1$2   *
              *            *
              **************

                HYDROGRAPH ROUTING DATA

  71 RS           STORAGE ROUTING
                      NSTPS          1  NUMBER OF SUBREACHES
                       ITYP       ELEV  TYPE OF INITIAL CONDITION
                     RSVRIC    1346.50  INITIAL CONDITION
                          X       0.00  WORKING R AND D COEFFICIENT

  72 SA                AREA        2.8        3.9

  73 SE           ELEVATION    1346.50    1351.50

  74 SS           SPILLWAY
                       CREL    1346.50  SPILLWAY CREST ELEVATION
                      SPWID      30.00  SPILLWAY WIDTH
                       COQW       1.80  WEIR COEFFICIENT
                       EXPW       1.50  EXPONENT OF HEAD

                                                  ***

                                             COMPUTED STORAGE-ELEVATION DATA

             STORAGE       0.00      16.67
           ELEVATION    1346.50    1351.50

                                             COMPUTED OUTFLOW-ELEVATION DATA

             OUTFLOW       0.00       0.00       0.10       0.83       2.80       6.63      12.94      22.36      35.51      53.00
           ELEVATION    1346.50    1346.50    1346.52    1346.56    1346.64    1346.75    1346.89    1347.06    1347.26    1347.49

             OUTFLOW      75.47     103.52     137.79     178.89     227.44     284.06     349.39     424.02     508.60     603.74
           ELEVATION    1347.75    1348.04    1348.37    1348.72    1349.11    1349.52    1349.97    1350.45    1350.96    1351.50

                                          COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

             STORAGE       0.00       0.04       0.17       0.39       0.70       1.10       1.59       2.18       2.87       3.66
             OUTFLOW       0.00       0.10       0.83       2.80       6.63      12.94      22.36      35.51      53.00      75.47
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ELEVATION	1346.50	1346.52	1346.56	1346.64	1346.75	1346.89	1347.06	1347.26	1347.49	1347.75
STORAGE	4.57	5.59	6.73	8.01	9.43	10.99	12.71	14.60	16.67	
OUTFLOW	103.52	137.79	178.88	227.44	284.06	349.38	424.02	508.60	603.74	
ELEVATION	1348.04	1348.37	1348.72	1349.11	1349.52	1349.97	1350.45	1350.96	1351.50	

HYDROGRAPH AT STATION PON1$2

DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE
11	FEB	0600	1	0.	0.0	1346.5	11	FEB	1005	50	1.	0.2	1346.6	11	FEB	1410	99	101.	4.5	1348.0
11	FEB	0605	2	0.	0.0	1346.5	11	FEB	1010	51	1.	0.2	1346.6	11	FEB	1415	100	97.	4.3	1348.0
11	FEB	0610	3	0.	0.0	1346.5	11	FEB	1015	52	2.	0.3	1346.6	11	FEB	1420	101	93.	4.2	1347.9
11	FEB	0615	4	0.	0.0	1346.5	11	FEB	1020	53	2.	0.3	1346.6	11	FEB	1425	102	89.	4.1	1347.9
11	FEB	0620	5	0.	0.0	1346.5	11	FEB	1025	54	2.	0.3	1346.6	11	FEB	1430	103	85.	4.0	1347.9
11	FEB	0625	6	0.	0.0	1346.5	11	FEB	1030	55	2.	0.4	1346.6	11	FEB	1435	104	82.	3.9	1347.8
11	FEB	0630	7	0.	0.0	1346.5	11	FEB	1035	56	3.	0.4	1346.6	11	FEB	1440	105	78.	3.8	1347.8
11	FEB	0635	8	0.	0.0	1346.5	11	FEB	1040	57	3.	0.4	1346.7	11	FEB	1445	106	75.	3.7	1347.7
11	FEB	0640	9	0.	0.0	1346.5	11	FEB	1045	58	4.	0.5	1346.7	11	FEB	1450	107	73.	3.6	1347.7
11	FEB	0645	10	0.	0.0	1346.5	11	FEB	1050	59	4.	0.5	1346.7	11	FEB	1455	108	70.	3.5	1347.7
11	FEB	0650	11	0.	0.0	1346.5	11	FEB	1055	60	5.	0.6	1346.7	11	FEB	1500	109	68.	3.4	1347.7
11	FEB	0655	12	0.	0.0	1346.5	11	FEB	1100	61	6.	0.6	1346.7	11	FEB	1505	110	65.	3.3	1347.6
11	FEB	0700	13	0.	0.0	1346.5	11	FEB	1105	62	6.	0.7	1346.7	11	FEB	1510	111	63.	3.2	1347.6
11	FEB	0705	14	0.	0.0	1346.5	11	FEB	1110	63	7.	0.7	1346.8	11	FEB	1515	112	61.	3.1	1347.6
11	FEB	0710	15	0.	0.0	1346.5	11	FEB	1115	64	8.	0.8	1346.8	11	FEB	1520	113	58.	3.1	1347.5
11	FEB	0715	16	0.	0.0	1346.5	11	FEB	1120	65	10.	0.9	1346.8	11	FEB	1525	114	56.	3.0	1347.5
11	FEB	0720	17	0.	0.0	1346.5	11	FEB	1125	66	12.	1.0	1346.9	11	FEB	1530	115	54.	2.9	1347.5
11	FEB	0725	18	0.	0.0	1346.5	11	FEB	1130	67	14.	1.2	1346.9	11	FEB	1535	116	52.	2.8	1347.5
11	FEB	0730	19	0.	0.0	1346.5	11	FEB	1135	68	18.	1.3	1347.0	11	FEB	1540	117	51.	2.8	1347.5
11	FEB	0735	20	0.	0.0	1346.5	11	FEB	1140	69	24.	1.6	1347.1	11	FEB	1545	118	49.	2.7	1347.4
11	FEB	0740	21	0.	0.0	1346.5	11	FEB	1145	70	37.	2.2	1347.3	11	FEB	1550	119	48.	2.7	1347.4
11	FEB	0745	22	0.	0.0	1346.5	11	FEB	1150	71	61.	3.1	1347.6	11	FEB	1555	120	46.	2.6	1347.4
11	FEB	0750	23	0.	0.0	1346.5	11	FEB	1155	72	97.	4.3	1348.0	11	FEB	1600	121	45.	2.6	1347.4
11	FEB	0755	24	0.	0.0	1346.5	11	FEB	1200	73	143.	5.7	1348.4	11	FEB	1605	122	44.	2.5	1347.4
11	FEB	0800	25	0.	0.0	1346.5	11	FEB	1205	74	196.	7.2	1348.9	11	FEB	1610	123	43.	2.5	1347.4
11	FEB	0805	26	0.	0.0	1346.5	11	FEB	1210	75	247.	8.5	1349.3	11	FEB	1615	124	42.	2.4	1347.3
11	FEB	0810	27	0.	0.0	1346.5	11	FEB	1215	76	288.	9.5	1349.6	11	FEB	1620	125	41.	2.4	1347.3
11	FEB	0815	28	0.	0.0	1346.5	11	FEB	1220	77	314.	10.1	1349.7	11	FEB	1625	126	40.	2.3	1347.3
11	FEB	0820	29	0.	0.0	1346.5	11	FEB	1225	78	324.	10.4	1349.8	11	FEB	1630	127	39.	2.3	1347.3
11	FEB	0825	30	0.	0.0	1346.5	11	FEB	1230	79	323.	10.4	1349.8	11	FEB	1635	128	37.	2.2	1347.3
11	FEB	0830	31	0.	0.0	1346.5	11	FEB	1235	80	314.	10.2	1349.7	11	FEB	1640	129	36.	2.2	1347.3
11	FEB	0835	32	0.	0.0	1346.5	11	FEB	1240	81	301.	9.8	1349.6	11	FEB	1645	130	35.	2.2	1347.2
11	FEB	0840	33	0.	0.0	1346.5	11	FEB	1245	82	284.	9.4	1349.5	11	FEB	1650	131	34.	2.1	1347.2
11	FEB	0845	34	0.	0.0	1346.5	11	FEB	1250	83	266.	9.0	1349.4	11	FEB	1655	132	33.	2.1	1347.2
11	FEB	0850	35	0.	0.0	1346.5	11	FEB	1255	84	247.	8.5	1349.3	11	FEB	1700	133	32.	2.0	1347.2
11	FEB	0855	36	0.	0.0	1346.5	11	FEB	1300	85	229.	8.0	1349.1	11	FEB	1705	134	31.	2.0	1347.2
11	FEB	0900	37	0.	0.0	1346.5	11	FEB	1305	86	212.	7.6	1349.0	11	FEB	1710	135	31.	2.0	1347.2
11	FEB	0905	38	0.	0.0	1346.5	11	FEB	1310	87	197.	7.2	1348.9	11	FEB	1715	136	30.	1.9	1347.2
11	FEB	0910	39	0.	0.0	1346.5	11	FEB	1315	88	184.	6.9	1348.8	11	FEB	1720	137	29.	1.9	1347.2
11	FEB	0915	40	0.	0.0	1346.5	11	FEB	1320	89	171.	6.5	1348.7	11	FEB	1725	138	29.	1.9	1347.2
11	FEB	0920	41	0.	0.0	1346.5	11	FEB	1325	90	160.	6.2	1348.6	11	FEB	1730	139	28.	1.8	1347.1
11	FEB	0925	42	0.	0.1	1346.5	11	FEB	1330	91	151.	5.9	1348.5	11	FEB	1735	140	28.	1.8	1347.1
11	FEB	0930	43	0.	0.1	1346.5	11	FEB	1335	92	142.	5.7	1348.4	11	FEB	1740	141	27.	1.8	1347.1
11	FEB	0935	44	0.	0.1	1346.5	11	FEB	1340	93	134.	5.5	1348.3	11	FEB	1745	142	27.	1.8	1347.1
11	FEB	0940	45	0.	0.1	1346.5	11	FEB	1345	94	127.	5.3	1348.3	11	FEB	1750	143	26.	1.7	1347.1
11	FEB	0945	46	1.	0.1	1346.5	11	FEB	1350	95	121.	5.1	1348.2	11	FEB	1755	144	25.	1.7	1347.1
11	FEB	0950	47	1.	0.1	1346.6	11	FEB	1355	96	115.	4.9	1348.2	11	FEB	1800	145	25.	1.7	1347.1
11	FEB	0955	48	1.	0.2	1346.6	11	FEB	1400	97	110.	4.8	1348.1							
11	FEB	1000	49	1.	0.2	1346.6	11	FEB	1405	98	105.	4.6	1348.1							

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	12.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 324.	6.42		109.	56.	56.	56.
		(INCHES)	4.649	4.786	4.786	4.786
		(AC-FT)	54.	56.	56.	56.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	12.00-HR
+ (AC-FT)	(HR)				
10.	6.42	4.	2.	2.	2.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE

+ (FEET)	(HR)	6-HR	24-HR	72-HR	12.00-HR
1349.80	6.42	1347.99	1347.29	1347.29	1347.30

CUMULATIVE AREA = 0.22 SQ MI

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          **************
          *            *
 75 KK    *   BASIN3   *
          *            *
          **************

 11 IN        TIME DATA FOR INPUT TIME SERIES
                   JXMIN         30  TIME INTERVAL IN MINUTES
                  JXDATE     11FEB93  STARTING DATE
                  JXTIME        600  STARTING TIME

            SUBBASIN RUNOFF DATA

 76 BA        SUBBASIN CHARACTERISTICS
                   TAREA        0.15  SUBBASIN AREA

              PRECIPITATION DATA

 77 PB             STORM        7.80  BASIN TOTAL PRECIPITATION

 78 PI          INCREMENTAL PRECIPITATION PATTERN
                  0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00
                  0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00
                  0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00
                  0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00
                  0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00
                  0.00    0.00    0.00    0.00    0.01    0.01    0.01    0.01    0.01    0.01
                  0.01    0.01    0.01    0.01    0.01    0.01    0.06    0.06    0.06    0.06
                  0.06    0.06    0.01    0.01    0.01    0.01    0.01    0.01    0.01    0.01
                  0.01    0.01    0.01    0.01    0.00    0.00    0.00    0.00    0.00    0.00
                  0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00
                  0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00
                  0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00
                  0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00    0.00
                  0.00    0.00    0.00    0.00

 82 LS        SCS LOSS RATE
                   STRTL        0.44  INITIAL ABSTRACTION
                  CRVNBR       82.00  CURVE NUMBER
                   RTIMP        0.00  PERCENT IMPERVIOUS AREA

 83 UD        SCS DIMENSIONLESS UNITGRAPH
                    TLAG        0.25  LAG

                                                    ***

WARNING *** TIME INTERVAL IS GREATER THAN .29*LAG

                                   UNIT HYDROGRAPH
                                17 END-OF-PERIOD ORDINATES
            44.     151.     240.     240.     187.     112.      70.      45.      28.      18.
            11.       7.       4.       3.       2.       1.       0.
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****

HYDROGRAPH AT STATION BASIN3

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DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
11	FEB	0600	1	0.00	0.00	0.00	0.	11	FEB	1205	74	0.11	0.01	0.10	504.
11	FEB	0605	2	0.02	0.02	0.00	0.	11	FEB	1210	75	0.11	0.01	0.10	473.
11	FEB	0610	3	0.02	0.02	0.00	0.	11	FEB	1215	76	0.11	0.01	0.10	392.
11	FEB	0615	4	0.02	0.02	0.00	0.	11	FEB	1220	77	0.11	0.01	0.10	304.
11	FEB	0620	5	0.02	0.02	0.00	0.	11	FEB	1225	78	0.11	0.01	0.10	233.
11	FEB	0625	6	0.02	0.02	0.00	0.	11	FEB	1230	79	0.11	0.01	0.10	191.

11 FEB 0630	7	0.02	0.02	0.00	0.	*	11 FEB 1235	80	0.06	0.00	0.05	163.
11 FEB 0635	8	0.02	0.02	0.00	0.	*	11 FEB 1240	81	0.06	0.00	0.05	138.
11 FEB 0640	9	0.02	0.02	0.00	0.	*	11 FEB 1245	82	0.06	0.00	0.05	116.
11 FEB 0645	10	0.02	0.02	0.00	0.	*	11 FEB 1250	83	0.06	0.00	0.05	97.
11 FEB 0650	11	0.02	0.02	0.00	0.	*	11 FEB 1255	84	0.06	0.00	0.05	84.
11 FEB 0655	12	0.02	0.02	0.00	0.	*	11 FEB 1300	85	0.06	0.00	0.05	75.
11 FEB 0700	13	0.02	0.02	0.00	0.	*	11 FEB 1305	86	0.04	0.00	0.04	70.
11 FEB 0705	14	0.02	0.02	0.00	0.	*	11 FEB 1310	87	0.04	0.00	0.04	64.
11 FEB 0710	15	0.02	0.02	0.00	0.	*	11 FEB 1315	88	0.04	0.00	0.04	59.
11 FEB 0715	16	0.02	0.02	0.00	0.	*	11 FEB 1320	89	0.04	0.00	0.04	54.
11 FEB 0720	17	0.02	0.02	0.00	0.	*	11 FEB 1325	90	0.04	0.00	0.04	51.
11 FEB 0725	18	0.02	0.02	0.00	0.	*	11 FEB 1330	91	0.04	0.00	0.04	49.
11 FEB 0730	19	0.02	0.02	0.00	0.	*	11 FEB 1335	92	0.03	0.00	0.03	47.
11 FEB 0735	20	0.02	0.02	0.00	0.	*	11 FEB 1340	93	0.03	0.00	0.03	45.
11 FEB 0740	21	0.02	0.02	0.00	0.	*	11 FEB 1345	94	0.03	0.00	0.03	42.
11 FEB 0745	22	0.02	0.02	0.00	0.	*	11 FEB 1350	95	0.03	0.00	0.03	40.
11 FEB 0750	23	0.02	0.02	0.00	0.	*	11 FEB 1355	96	0.03	0.00	0.03	38.
11 FEB 0755	24	0.02	0.02	0.00	0.	*	11 FEB 1400	97	0.03	0.00	0.03	37.
11 FEB 0800	25	0.02	0.02	0.00	0.	*	11 FEB 1405	98	0.02	0.00	0.02	36.
11 FEB 0805	26	0.02	0.02	0.00	0.	*	11 FEB 1410	99	0.02	0.00	0.02	34.
11 FEB 0810	27	0.02	0.02	0.00	0.	*	11 FEB 1415	100	0.02	0.00	0.02	32.
11 FEB 0815	28	0.02	0.02	0.00	0.	*	11 FEB 1420	101	0.02	0.00	0.02	30.
11 FEB 0820	29	0.02	0.02	0.00	0.	*	11 FEB 1425	102	0.02	0.00	0.02	28.
11 FEB 0825	30	0.02	0.02	0.00	0.	*	11 FEB 1430	103	0.02	0.00	0.02	27.
11 FEB 0830	31	0.02	0.02	0.00	0.	*	11 FEB 1435	104	0.02	0.00	0.02	26.
11 FEB 0835	32	0.02	0.02	0.00	0.	*	11 FEB 1440	105	0.02	0.00	0.02	26.
11 FEB 0840	33	0.02	0.02	0.00	1.	*	11 FEB 1445	106	0.02	0.00	0.02	26.
11 FEB 0845	34	0.02	0.02	0.00	1.	*	11 FEB 1450	107	0.02	0.00	0.02	26.
11 FEB 0850	35	0.02	0.02	0.00	1.	*	11 FEB 1455	108	0.02	0.00	0.02	26.
11 FEB 0855	36	0.02	0.02	0.00	2.	*	11 FEB 1500	109	0.02	0.00	0.02	26.
11 FEB 0900	37	0.02	0.02	0.00	2.	*	11 FEB 1505	110	0.02	0.00	0.02	25.
11 FEB 0905	38	0.02	0.02	0.00	3.	*	11 FEB 1510	111	0.02	0.00	0.02	25.
11 FEB 0910	39	0.02	0.02	0.00	3.	*	11 FEB 1515	112	0.02	0.00	0.02	25.
11 FEB 0915	40	0.02	0.02	0.00	4.	*	11 FEB 1520	113	0.02	0.00	0.02	25.
11 FEB 0920	41	0.02	0.02	0.01	4.	*	11 FEB 1525	114	0.02	0.00	0.02	25.
11 FEB 0925	42	0.02	0.02	0.01	5.	*	11 FEB 1530	115	0.02	0.00	0.02	25.
11 FEB 0930	43	0.02	0.02	0.01	5.	*	11 FEB 1535	116	0.02	0.00	0.02	25.
11 FEB 0935	44	0.03	0.02	0.01	6.	*	11 FEB 1540	117	0.02	0.00	0.02	25.
11 FEB 0940	45	0.03	0.02	0.01	6.	*	11 FEB 1545	118	0.02	0.00	0.02	26.
11 FEB 0945	46	0.03	0.02	0.01	7.	*	11 FEB 1550	119	0.02	0.00	0.02	26.
11 FEB 0950	47	0.03	0.02	0.01	8.	*	11 FEB 1555	120	0.02	0.00	0.02	26.
11 FEB 0955	48	0.03	0.02	0.01	8.	*	11 FEB 1600	121	0.02	0.00	0.02	26.
11 FEB 1000	49	0.03	0.02	0.01	9.	*	11 FEB 1605	122	0.02	0.00	0.01	25.
11 FEB 1005	50	0.04	0.02	0.01	10.	*	11 FEB 1610	123	0.02	0.00	0.01	24.
11 FEB 1010	51	0.04	0.02	0.01	11.	*	11 FEB 1615	124	0.02	0.00	0.01	22.
11 FEB 1015	52	0.04	0.02	0.01	12.	*	11 FEB 1620	125	0.02	0.00	0.01	21.
11 FEB 1020	53	0.04	0.02	0.01	13.	*	11 FEB 1625	126	0.02	0.00	0.01	19.
11 FEB 1025	54	0.04	0.02	0.01	14.	*	11 FEB 1630	127	0.02	0.00	0.01	18.
11 FEB 1030	55	0.04	0.02	0.02	15.	*	11 FEB 1635	128	0.02	0.00	0.01	18.
11 FEB 1035	56	0.05	0.03	0.02	16.	*	11 FEB 1640	129	0.02	0.00	0.01	18.
11 FEB 1040	57	0.05	0.03	0.02	18.	*	11 FEB 1645	130	0.02	0.00	0.01	17.
11 FEB 1045	58	0.05	0.03	0.02	20.	*	11 FEB 1650	131	0.02	0.00	0.01	17.
11 FEB 1050	59	0.05	0.02	0.02	22.	*	11 FEB 1655	132	0.02	0.00	0.01	17.
11 FEB 1055	60	0.05	0.02	0.02	24.	*	11 FEB 1700	133	0.02	0.00	0.01	17.
11 FEB 1100	61	0.05	0.02	0.03	25.	*	11 FEB 1705	134	0.02	0.00	0.01	17.
11 FEB 1105	62	0.07	0.03	0.04	27.	*	11 FEB 1710	135	0.02	0.00	0.01	17.
11 FEB 1110	63	0.07	0.03	0.04	30.	*	11 FEB 1715	136	0.02	0.00	0.01	17.
11 FEB 1115	64	0.07	0.03	0.04	35.	*	11 FEB 1720	137	0.02	0.00	0.01	17.
11 FEB 1120	65	0.07	0.03	0.04	40.	*	11 FEB 1725	138	0.02	0.00	0.01	17.
11 FEB 1125	66	0.07	0.03	0.05	44.	*	11 FEB 1730	139	0.02	0.00	0.01	17.
11 FEB 1130	67	0.07	0.03	0.05	47.	*	11 FEB 1735	140	0.01	0.00	0.01	17.
11 FEB 1135	68	0.59	0.18	0.41	65.	*	11 FEB 1740	141	0.01	0.00	0.01	16.
11 FEB 1140	69	0.59	0.14	0.45	123.	*	11 FEB 1745	142	0.01	0.00	0.01	15.
11 FEB 1145	70	0.59	0.11	0.48	219.	*	11 FEB 1750	143	0.01	0.00	0.01	13.
11 FEB 1150	71	0.59	0.09	0.50	322.	*	11 FEB 1755	144	0.01	0.00	0.01	12.
11 FEB 1155	72	0.59	0.07	0.52	412.	*	11 FEB 1800	145	0.01	0.00	0.01	11.
11 FEB 1200	73	0.59	0.06	0.53	476.	*						
						*						

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TOTAL RAINFALL = 7.80, TOTAL LOSS = 2.13, TOTAL EXCESS = 5.67

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	12.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 504.	6.08		85.	45.	45.	45.
		(INCHES)	5.261	5.633	5.633	5.633
		(AC-FT)	42.	45.	45.	45.

CUMULATIVE AREA = 0.15 SQ MI

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84 KK     *   INTO3    *
          *            *
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85 KC        HYDROGRAPH COMBINATION
                  ICOMP          2  NUMBER OF HYDROGRAPHS TO COMBINE
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HYDROGRAPH AT STATION INTO3
SUM OF 2 HYDROGRAPHS

DA MON HRMN	ORD	FLOW	DA MON HRMN	ORD	FLOW	DA MON HRMN	ORD	FLOW	DA MON HRMN	ORD	FLOW
11 FEB 0600	1	0.	11 FEB 0905	38	3.	11 FEB 1210	75	720.	11 FEB 1515	112	86.
11 FEB 0605	2	0.	11 FEB 0910	39	3.	11 FEB 1215	76	681.	11 FEB 1520	113	84.
11 FEB 0610	3	0.	11 FEB 0915	40	4.	11 FEB 1220	77	618.	11 FEB 1525	114	82.
11 FEB 0615	4	0.	11 FEB 0920	41	4.	11 FEB 1225	78	557.	11 FEB 1530	115	79.
11 FEB 0620	5	0.	11 FEB 0925	42	5.	11 FEB 1230	79	514.	11 FEB 1535	116	78.
11 FEB 0625	6	0.	11 FEB 0930	43	6.	11 FEB 1235	80	477.	11 FEB 1540	117	76.
11 FEB 0630	7	0.	11 FEB 0935	44	6.	11 FEB 1240	81	439.	11 FEB 1545	118	75.
11 FEB 0635	8	0.	11 FEB 0940	45	7.	11 FEB 1245	82	400.	11 FEB 1550	119	73.
11 FEB 0640	9	0.	11 FEB 0945	46	8.	11 FEB 1250	83	363.	11 FEB 1555	120	72.
11 FEB 0645	10	0.	11 FEB 0950	47	8.	11 FEB 1255	84	331.	11 FEB 1600	121	71.
11 FEB 0650	11	0.	11 FEB 0955	48	9.	11 FEB 1300	85	304.	11 FEB 1605	122	69.
11 FEB 0655	12	0.	11 FEB 1000	49	10.	11 FEB 1305	86	282.	11 FEB 1610	123	67.
11 FEB 0700	13	0.	11 FEB 1005	50	11.	11 FEB 1310	87	262.	11 FEB 1615	124	65.
11 FEB 0705	14	0.	11 FEB 1010	51	12.	11 FEB 1315	88	242.	11 FEB 1620	125	62.
11 FEB 0710	15	0.	11 FEB 1015	52	13.	11 FEB 1320	89	225.	11 FEB 1625	126	59.
11 FEB 0715	16	0.	11 FEB 1020	53	15.	11 FEB 1325	90	211.	11 FEB 1630	127	57.
11 FEB 0720	17	0.	11 FEB 1025	54	16.	11 FEB 1330	91	199.	11 FEB 1635	128	55.
11 FEB 0725	18	0.	11 FEB 1030	55	17.	11 FEB 1335	92	189.	11 FEB 1640	129	54.
11 FEB 0730	19	0.	11 FEB 1035	56	19.	11 FEB 1340	93	179.	11 FEB 1645	130	52.
11 FEB 0735	20	0.	11 FEB 1040	57	21.	11 FEB 1345	94	170.	11 FEB 1650	131	51.
11 FEB 0740	21	0.	11 FEB 1045	58	23.	11 FEB 1350	95	161.	11 FEB 1655	132	50.
11 FEB 0745	22	0.	11 FEB 1050	59	26.	11 FEB 1355	96	153.	11 FEB 1700	133	49.
11 FEB 0750	23	0.	11 FEB 1055	60	29.	11 FEB 1400	97	147.	11 FEB 1705	134	48.
11 FEB 0755	24	0.	11 FEB 1100	61	31.	11 FEB 1405	98	141.	11 FEB 1710	135	48.
11 FEB 0800	25	0.	11 FEB 1105	62	33.	11 FEB 1410	99	135.	11 FEB 1715	136	47.
11 FEB 0805	26	0.	11 FEB 1110	63	38.	11 FEB 1415	100	129.	11 FEB 1720	137	46.
11 FEB 0810	27	0.	11 FEB 1115	64	43.	11 FEB 1420	101	123.	11 FEB 1725	138	46.
11 FEB 0815	28	0.	11 FEB 1120	65	50.	11 FEB 1425	102	117.	11 FEB 1730	139	45.
11 FEB 0820	29	0.	11 FEB 1125	66	56.	11 FEB 1430	103	112.	11 FEB 1735	140	44.
11 FEB 0825	30	0.	11 FEB 1130	67	61.	11 FEB 1435	104	108.	11 FEB 1740	141	43.
11 FEB 0830	31	0.	11 FEB 1135	68	83.	11 FEB 1440	105	105.	11 FEB 1745	142	41.
11 FEB 0835	32	0.	11 FEB 1140	69	147.	11 FEB 1445	106	101.	11 FEB 1750	143	39.
11 FEB 0840	33	1.	11 FEB 1145	70	256.	11 FEB 1450	107	98.	11 FEB 1755	144	37.
11 FEB 0845	34	1.	11 FEB 1150	71	383.	11 FEB 1455	108	96.	11 FEB 1800	145	36.
11 FEB 0850	35	1.	11 FEB 1155	72	509.	11 FEB 1500	109	93.			
11 FEB 0855	36	2.	11 FEB 1200	73	619.	11 FEB 1505	110	91.			
11 FEB 0900	37	2.	11 FEB 1205	74	700.	11 FEB 1510	111	88.			

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	12.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 720.	6.17		192.	102.	102.	102.
		(INCHES)	4.855	5.131	5.131	5.131
		(AC-FT)	95.	101.	101.	101.

CUMULATIVE AREA = 0.37 SQ MI

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            *            *
 86 KK      *    POND3   *
            *            *
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               HYDROGRAPH ROUTING DATA

 87 RS           STORAGE ROUTING
                       NSTPS          1  NUMBER OF SUBREACHES
                        ITYP       ELEV  TYPE OF INITIAL CONDITION
                      RSVRIC    1345.00  INITIAL CONDITION
                           X       0.00  WORKING R AND D COEFFICIENT

 88 SV             STORAGE        0.0       8.0      16.0      23.0      31.0      35.0

 89 SQ           DISCHARGE         0.       40.      220.      325.      400.      440.

 90 SE           ELEVATION    1344.70   1346.00   1347.00   1348.00   1349.00   1349.50

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HYDROGRAPH AT STATION POND3

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DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	*	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	*	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE
11	FEB	0600	1	9.	1.8	1345.0	*	11	FEB	1005	50	4.	0.8	1344.8	*	11	FEB	1410	99	237.	17.2	1347.2
11	FEB	0605	2	9.	1.8	1345.0	*	11	FEB	1010	51	4.	0.9	1344.8	*	11	FEB	1415	100	227.	16.5	1347.1
11	FEB	0610	3	9.	1.7	1345.0	*	11	FEB	1015	52	5.	0.9	1344.9	*	11	FEB	1420	101	216.	15.8	1347.0
11	FEB	0615	4	8.	1.7	1345.0	*	11	FEB	1020	53	5.	1.0	1344.9	*	11	FEB	1425	102	202.	15.2	1346.9
11	FEB	0620	5	8.	1.6	1345.0	*	11	FEB	1025	54	5.	1.1	1344.9	*	11	FEB	1430	103	189.	14.6	1346.8
11	FEB	0625	6	8.	1.6	1345.0	*	11	FEB	1030	55	6.	1.1	1344.9	*	11	FEB	1435	104	178.	14.1	1346.8
11	FEB	0630	7	8.	1.5	1344.9	*	11	FEB	1035	56	6.	1.2	1344.9	*	11	FEB	1440	105	168.	13.7	1346.7
11	FEB	0635	8	7.	1.5	1344.9	*	11	FEB	1040	57	7.	1.3	1344.9	*	11	FEB	1445	106	158.	13.3	1346.7
11	FEB	0640	9	7.	1.4	1344.9	*	11	FEB	1045	58	7.	1.4	1344.9	*	11	FEB	1450	107	150.	12.9	1346.6
11	FEB	0645	10	7.	1.4	1344.9	*	11	FEB	1050	59	8.	1.5	1345.0	*	11	FEB	1455	108	142.	12.5	1346.6
11	FEB	0650	11	7.	1.3	1344.9	*	11	FEB	1055	60	8.	1.7	1345.0	*	11	FEB	1500	109	135.	12.2	1346.5
11	FEB	0655	12	6.	1.3	1344.9	*	11	FEB	1100	61	9.	1.8	1345.0	*	11	FEB	1505	110	129.	12.0	1346.5
11	FEB	0700	13	6.	1.2	1344.9	*	11	FEB	1105	62	10.	2.0	1345.0	*	11	FEB	1510	111	124.	11.7	1346.5
11	FEB	0705	14	6.	1.2	1344.9	*	11	FEB	1110	63	11.	2.2	1345.0	*	11	FEB	1515	112	118.	11.5	1346.4
11	FEB	0710	15	6.	1.1	1344.9	*	11	FEB	1115	64	12.	2.4	1345.1	*	11	FEB	1520	113	114.	11.3	1346.4
11	FEB	0715	16	6.	1.1	1344.9	*	11	FEB	1120	65	13.	2.6	1345.1	*	11	FEB	1525	114	109.	11.1	1346.4
11	FEB	0720	17	5.	1.1	1344.9	*	11	FEB	1125	66	14.	2.9	1345.2	*	11	FEB	1530	115	105.	10.9	1346.4
11	FEB	0725	18	5.	1.0	1344.9	*	11	FEB	1130	67	16.	3.2	1345.2	*	11	FEB	1535	116	101.	10.7	1346.3
11	FEB	0730	19	5.	1.0	1344.9	*	11	FEB	1135	68	18.	3.5	1345.3	*	11	FEB	1540	117	98.	10.6	1346.3
11	FEB	0735	20	5.	1.0	1344.9	*	11	FEB	1140	69	21.	4.2	1345.4	*	11	FEB	1545	118	94.	10.4	1346.3
11	FEB	0740	21	5.	0.9	1344.9	*	11	FEB	1145	70	27.	5.4	1345.6	*	11	FEB	1550	119	92.	10.3	1346.3
11	FEB	0745	22	4.	0.9	1344.8	*	11	FEB	1150	71	37.	7.4	1345.9	*	11	FEB	1555	120	89.	10.2	1346.3
11	FEB	0750	23	4.	0.9	1344.8	*	11	FEB	1155	72	86.	10.0	1346.3	*	11	FEB	1600	121	86.	10.1	1346.3
11	FEB	0755	24	4.	0.8	1344.8	*	11	FEB	1200	73	155.	13.1	1346.6	*	11	FEB	1605	122	84.	10.0	1346.2
11	FEB	0800	25	4.	0.8	1344.8	*	11	FEB	1205	74	225.	16.3	1347.0	*	11	FEB	1610	123	82.	9.9	1346.2
11	FEB	0805	26	4.	0.8	1344.8	*	11	FEB	1210	75	273.	19.5	1347.5	*	11	FEB	1615	124	79.	9.8	1346.2
11	FEB	0810	27	4.	0.8	1344.8	*	11	FEB	1215	76	315.	22.3	1347.9	*	11	FEB	1620	125	77.	9.6	1346.2
11	FEB	0815	28	4.	0.7	1344.8	*	11	FEB	1220	77	339.	24.5	1348.2	*	11	FEB	1625	126	75.	9.5	1346.2
11	FEB	0820	29	4.	0.7	1344.8	*	11	FEB	1225	78	355.	26.2	1348.4	*	11	FEB	1630	127	72.	9.4	1346.2
11	FEB	0825	30	3.	0.7	1344.8	*	11	FEB	1230	79	366.	27.4	1348.5	*	11	FEB	1635	128	70.	9.3	1346.2
11	FEB	0830	31	3.	0.7	1344.8	*	11	FEB	1235	80	374.	28.3	1348.7	*	11	FEB	1640	129	68.	9.2	1346.2
11	FEB	0835	32	3.	0.6	1344.8	*	11	FEB	1240	81	379.	28.8	1348.7	*	11	FEB	1645	130	66.	9.1	1346.1
11	FEB	0840	33	3.	0.6	1344.8	*	11	FEB	1245	82	382.	29.1	1348.8	*	11	FEB	1650	131	64.	9.1	1346.1
11	FEB	0845	34	3.	0.6	1344.8	*	11	FEB	1250	83	382.	29.1	1348.8	*	11	FEB	1655	132	62.	9.0	1346.1
11	FEB	0850	35	3.	0.6	1344.8	*	11	FEB	1255	84	380.	28.8	1348.7	*	11	FEB	1700	133	60.	8.9	1346.1
11	FEB	0855	36	3.	0.6	1344.8	*	11	FEB	1300	85	376.	28.4	1348.7	*	11	FEB	1705	134	58.	8.8	1346.1
11	FEB	0900	37	3.	0.6	1344.8	*	11	FEB	1305	86	371.	27.9	1348.6	*	11	FEB	1710	135	57.	8.8	1346.1
11	FEB	0905	38	3.	0.6	1344.8	*	11	FEB	1310	87	364.	27.2	1348.5	*	11	FEB	1715	136	56.	8.7	1346.1
11	FEB	0910	39	3.	0.6	1344.8	*	11	FEB	1315	88	357.	26.5	1348.4	*	11	FEB	1720	137	54.	8.6	1346.1
11	FEB	0915	40	3.	0.6	1344.8	*	11	FEB	1320	89	350.	25.6	1348.3	*	11	FEB	1725	138	53.	8.6	1346.1
11	FEB	0920	41	3.	0.6	1344.8	*	11	FEB	1325	90	341.	24.8	1348.2	*	11	FEB	1730	139	52.	8.5	1346.1
11	FEB	0925	42	3.	0.6	1344.8	*	11	FEB	1330	91	333.	23.8	1348.1	*	11	FEB	1735	140	51.	8.5	1346.1
11	FEB	0930	43	3.	0.6	1344.8	*	11	FEB	1335	92	324.	22.9	1348.0	*	11	FEB	1740	141	50.	8.4	1346.1
11	FEB	0935	44	3.	0.6	1344.8	*	11	FEB	1340	93	310.	22.0	1347.9	*	11	FEB	1745	142	49.	8.4	1346.0
11	FEB	0940	45	3.	0.7	1344.8	*	11	FEB	1345	94	297.	21.1	1347.7	*	11	FEB	1750	143	47.	8.3	1346.0
11	FEB	0945	46	3.	0.7	1344.8	*	11	FEB	1350	95	284.	20.3	1347.6	*	11	FEB	1755	144	46.	8.3	1346.0

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  11 FEB 0950  47      4.     0.7  1344.8 * 11 FEB 1355  96      271.      19.4  1347.5 * 11 FEB 1800 145      45.      8.2  1346.0
  11 FEB 0955  48      4.     0.7  1344.8 * 11 FEB 1400  97      259.      18.6  1347.4 *
  11 FEB 1000  49      4.     0.8  1344.8 * 11 FEB 1405  98      248.      17.9  1347.3 *
                                          *                                       *
*****************************************************************************************************************

 PEAK FLOW     TIME                          MAXIMUM AVERAGE FLOW
                                  6-HR        24-HR       72-HR     12.00-HR

+  (CFS)       (HR)
                          (CFS)
+    382.      6.75                182.         95.         95.         95.
                       (INCHES)   4.611       4.807       4.807       4.807
                        (AC-FT)     90.         94.         94.         94.

PEAK STORAGE   TIME                          MAXIMUM AVERAGE STORAGE
                                  6-HR        24-HR       72-HR     12.00-HR
+ (AC-FT)      (HR)
      29.      6.75                 16.          9.          9.          9.

 PEAK STAGE    TIME                          MAXIMUM AVERAGE STAGE
                                  6-HR        24-HR       72-HR     12.00-HR
+  (FEET)      (HR)
   1348.76     6.75             1346.98     1345.96     1345.96     1345.96

                       CUMULATIVE AREA =    0.37 SQ MI


*** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** ***

              **************
              *            *
  91 KK       *   BASIN4   *
              *            *
              **************

  11 IN          TIME DATA FOR INPUT TIME SERIES
                      JXMIN          30  TIME INTERVAL IN MINUTES
                     JXDATE     11FEB93  STARTING DATE
                     JXTIME         600  STARTING TIME

              SUBBASIN RUNOFF DATA

  92 BA          SUBBASIN CHARACTERISTICS
                      TAREA        0.02  SUBBASIN AREA

                 PRECIPITATION DATA

  93 PB               STORM        7.80  BASIN TOTAL PRECIPITATION

  94 PI            INCREMENTAL PRECIPITATION PATTERN
                     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                     0.00     0.00     0.00     0.00     0.01     0.01     0.01     0.01     0.01     0.01
                     0.01     0.01     0.01     0.01     0.01     0.01     0.06     0.06     0.06     0.06
                     0.06     0.06     0.01     0.01     0.01     0.01     0.01     0.01     0.01     0.01
                     0.01     0.01     0.01     0.01     0.00     0.00     0.00     0.00     0.00     0.00
                     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                     0.00     0.00     0.00     0.00

  98 LS          SCS LOSS RATE
                      STRTL        0.63  INITIAL ABSTRACTION
                     CRVNBR       76.00  CURVE NUMBER
                      RTIMP        0.00  PERCENT IMPERVIOUS AREA

  99 UD          SCS DIMENSIONLESS UNITGRAPH
                       TLAG        0.25  LAG

                                         ***

WARNING *** TIME INTERVAL IS GREATER THAN .29*LAG
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UNIT HYDROGRAPH
17 END-OF-PERIOD ORDINATES

6.	19.	30.	30.	23.	14.	9.	6.	4.	2.
1.	1.	1.	0.	0.	0.	0.			

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HYDROGRAPH AT STATION BASIN4

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DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
11	FEB	0600	1	0.00	0.00	0.00	0.	11	FEB	1205	74	0.11	0.02	0.09	56.
11	FEB	0605	2	0.02	0.02	0.00	0.	11	FEB	1210	75	0.11	0.02	0.10	53.
11	FEB	0610	3	0.02	0.02	0.00	0.	11	FEB	1215	76	0.11	0.02	0.10	44.
11	FEB	0615	4	0.02	0.02	0.00	0.	11	FEB	1220	77	0.11	0.02	0.10	35.
11	FEB	0620	5	0.02	0.02	0.00	0.	11	FEB	1225	78	0.11	0.02	0.10	27.
11	FEB	0625	6	0.02	0.02	0.00	0.	11	FEB	1230	79	0.11	0.02	0.10	22.
11	FEB	0630	7	0.02	0.02	0.00	0.	11	FEB	1235	80	0.06	0.01	0.05	19.
11	FEB	0635	8	0.02	0.02	0.00	0.	11	FEB	1240	81	0.06	0.01	0.05	16.
11	FEB	0640	9	0.02	0.02	0.00	0.	11	FEB	1245	82	0.06	0.01	0.05	14.
11	FEB	0645	10	0.02	0.02	0.00	0.	11	FEB	1250	83	0.06	0.01	0.05	11.
11	FEB	0650	11	0.02	0.02	0.00	0.	11	FEB	1255	84	0.06	0.01	0.05	10.
11	FEB	0655	12	0.02	0.02	0.00	0.	11	FEB	1300	85	0.06	0.01	0.05	9.
11	FEB	0700	13	0.02	0.02	0.00	0.	11	FEB	1305	86	0.04	0.01	0.04	8.
11	FEB	0705	14	0.02	0.02	0.00	0.	11	FEB	1310	87	0.04	0.01	0.04	8.
11	FEB	0710	15	0.02	0.02	0.00	0.	11	FEB	1315	88	0.04	0.01	0.04	7.
11	FEB	0715	16	0.02	0.02	0.00	0.	11	FEB	1320	89	0.04	0.01	0.04	6.
11	FEB	0720	17	0.02	0.02	0.00	0.	11	FEB	1325	90	0.04	0.00	0.04	6.
11	FEB	0725	18	0.02	0.02	0.00	0.	11	FEB	1330	91	0.04	0.00	0.04	6.
11	FEB	0730	19	0.02	0.02	0.00	0.	11	FEB	1335	92	0.03	0.00	0.03	6.
11	FEB	0735	20	0.02	0.02	0.00	0.	11	FEB	1340	93	0.03	0.00	0.03	5.
11	FEB	0740	21	0.02	0.02	0.00	0.	11	FEB	1345	94	0.03	0.00	0.03	5.
11	FEB	0745	22	0.02	0.02	0.00	0.	11	FEB	1350	95	0.03	0.00	0.03	5.
11	FEB	0750	23	0.02	0.02	0.00	0.	11	FEB	1355	96	0.03	0.00	0.03	5.
11	FEB	0755	24	0.02	0.02	0.00	0.	11	FEB	1400	97	0.03	0.00	0.03	4.
11	FEB	0800	25	0.02	0.02	0.00	0.	11	FEB	1405	98	0.02	0.00	0.02	4.
11	FEB	0805	26	0.02	0.02	0.00	0.	11	FEB	1410	99	0.02	0.00	0.02	4.
11	FEB	0810	27	0.02	0.02	0.00	0.	11	FEB	1415	100	0.02	0.00	0.02	4.
11	FEB	0815	28	0.02	0.02	0.00	0.	11	FEB	1420	101	0.02	0.00	0.02	4.
11	FEB	0820	29	0.02	0.02	0.00	0.	11	FEB	1425	102	0.02	0.00	0.02	3.
11	FEB	0825	30	0.02	0.02	0.00	0.	11	FEB	1430	103	0.02	0.00	0.02	3.
11	FEB	0830	31	0.02	0.02	0.00	0.	11	FEB	1435	104	0.02	0.00	0.02	3.
11	FEB	0835	32	0.02	0.02	0.00	0.	11	FEB	1440	105	0.02	0.00	0.02	3.
11	FEB	0840	33	0.02	0.02	0.00	0.	11	FEB	1445	106	0.02	0.00	0.02	3.
11	FEB	0845	34	0.02	0.02	0.00	0.	11	FEB	1450	107	0.02	0.00	0.02	3.
11	FEB	0850	35	0.02	0.02	0.00	0.	11	FEB	1455	108	0.02	0.00	0.02	3.
11	FEB	0855	36	0.02	0.02	0.00	0.	11	FEB	1500	109	0.02	0.00	0.02	3.
11	FEB	0900	37	0.02	0.02	0.00	0.	11	FEB	1505	110	0.02	0.00	0.02	3.
11	FEB	0905	38	0.02	0.02	0.00	0.	11	FEB	1510	111	0.02	0.00	0.02	3.
11	FEB	0910	39	0.02	0.02	0.00	0.	11	FEB	1515	112	0.02	0.00	0.02	3.
11	FEB	0915	40	0.02	0.02	0.00	0.	11	FEB	1520	113	0.02	0.00	0.02	3.
11	FEB	0920	41	0.02	0.02	0.00	0.	11	FEB	1525	114	0.02	0.00	0.02	3.
11	FEB	0925	42	0.02	0.02	0.00	0.	11	FEB	1530	115	0.02	0.00	0.02	3.
11	FEB	0930	43	0.02	0.02	0.00	0.	11	FEB	1535	116	0.02	0.00	0.02	3.
11	FEB	0935	44	0.03	0.03	0.00	0.	11	FEB	1540	117	0.02	0.00	0.02	3.
11	FEB	0940	45	0.03	0.02	0.00	0.	11	FEB	1545	118	0.02	0.00	0.02	3.
11	FEB	0945	46	0.03	0.02	0.00	0.	11	FEB	1550	119	0.02	0.00	0.02	3.
11	FEB	0950	47	0.03	0.02	0.00	0.	11	FEB	1555	120	0.02	0.00	0.02	3.
11	FEB	0955	48	0.03	0.02	0.00	0.	11	FEB	1600	121	0.02	0.00	0.02	3.
11	FEB	1000	49	0.03	0.02	0.00	0.	11	FEB	1605	122	0.02	0.00	0.01	3.
11	FEB	1005	50	0.04	0.03	0.01	1.	11	FEB	1610	123	0.02	0.00	0.01	3.
11	FEB	1010	51	0.04	0.03	0.01	1.	11	FEB	1615	124	0.02	0.00	0.01	3.
11	FEB	1015	52	0.04	0.03	0.01	1.	11	FEB	1620	125	0.02	0.00	0.01	2.
11	FEB	1020	53	0.04	0.03	0.01	1.	11	FEB	1625	126	0.02	0.00	0.01	2.
11	FEB	1025	54	0.04	0.03	0.01	1.	11	FEB	1630	127	0.02	0.00	0.01	2.
11	FEB	1030	55	0.04	0.03	0.01	1.	11	FEB	1635	128	0.02	0.00	0.01	2.
11	FEB	1035	56	0.05	0.03	0.01	1.	11	FEB	1640	129	0.02	0.00	0.01	2.
11	FEB	1040	57	0.05	0.03	0.01	1.	11	FEB	1645	130	0.02	0.00	0.01	2.
11	FEB	1045	58	0.05	0.03	0.01	1.	11	FEB	1650	131	0.02	0.00	0.01	2.
11	FEB	1050	59	0.05	0.03	0.02	2.	11	FEB	1655	132	0.02	0.00	0.01	2.
11	FEB	1055	60	0.05	0.03	0.02	2.	11	FEB	1700	133	0.02	0.00	0.01	2.
11	FEB	1100	61	0.05	0.03	0.02	2.	11	FEB	1705	134	0.02	0.00	0.01	2.
11	FEB	1105	62	0.07	0.05	0.03	2.	11	FEB	1710	135	0.02	0.00	0.01	2.
11	FEB	1110	63	0.07	0.04	0.03	3.	11	FEB	1715	136	0.02	0.00	0.01	2.
11	FEB	1115	64	0.07	0.04	0.03	3.	11	FEB	1720	137	0.02	0.00	0.01	2.
11	FEB	1120	65	0.07	0.04	0.03	4.	11	FEB	1725	138	0.02	0.00	0.01	2.
11	FEB	1125	66	0.07	0.04	0.03	4.	11	FEB	1730	139	0.02	0.00	0.01	2.

11	FEB	1130	67	0.07	0.04	0.04	4.	*	11	FEB	1735	140	0.01	0.00	0.01	2.
11	FEB	1135	68	0.59	0.27	0.32	6.	*	11	FEB	1740	141	0.01	0.00	0.01	2.
11	FEB	1140	69	0.59	0.21	0.38	12.	*	11	FEB	1745	142	0.01	0.00	0.01	2.
11	FEB	1145	70	0.59	0.17	0.42	22.	*	11	FEB	1750	143	0.01	0.00	0.01	2.
11	FEB	1150	71	0.59	0.14	0.45	34.	*	11	FEB	1755	144	0.01	0.00	0.01	1.
11	FEB	1155	72	0.59	0.12	0.47	44.	*	11	FEB	1800	145	0.01	0.00	0.01	1.
11	FEB	1200	73	0.59	0.10	0.49	52.	*								
								*								

TOTAL RAINFALL = 7.80, TOTAL LOSS = 2.82, TOTAL EXCESS = 4.98

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	12.00-HR
(CFS)	(HR)				
	(CFS)				
56.	6.08	9.	5.	5.	5.
	(INCHES)	4.679	4.940	4.940	4.940
	(AC-FT)	5.	5.	5.	5.

CUMULATIVE AREA = .02 SQ MI

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          ***************
          *             *
100 KK    *     INTO4   *
          *             *
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101 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION INTO4
SUM OF 2 HYDROGRAPHS

DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW
11	FEB	0600	1	9.	11	FEB	0905	38	3.	11	FEB	1210	75	326.	11	FEB	1515	112	121.
11	FEB	0605	2	9.	11	FEB	0910	39	3.	11	FEB	1215	76	359.	11	FEB	1520	113	117.
11	FEB	0610	3	9.	11	FEB	0915	40	3.	11	FEB	1220	77	374.	11	FEB	1525	114	112.
11	FEB	0615	4	8.	11	FEB	0920	41	3.	11	FEB	1225	78	382.	11	FEB	1530	115	108.
11	FEB	0620	5	8.	11	FEB	0925	42	3.	11	FEB	1230	79	388.	11	FEB	1535	116	104.
11	FEB	0625	6	8.	11	FEB	0930	43	3.	11	FEB	1235	80	393.	11	FEB	1540	117	101.
11	FEB	0630	7	8.	11	FEB	0935	44	3.	11	FEB	1240	81	396.	11	FEB	1545	118	98.
11	FEB	0635	8	7.	11	FEB	0940	45	3.	11	FEB	1245	82	395.	11	FEB	1550	119	95.
11	FEB	0640	9	7.	11	FEB	0945	46	4.	11	FEB	1250	83	393.	11	FEB	1555	120	92.
11	FEB	0645	10	7.	11	FEB	0950	47	4.	11	FEB	1255	84	390.	11	FEB	1600	121	89.
11	FEB	0650	11	7.	11	FEB	0955	48	4.	11	FEB	1300	85	385.	11	FEB	1605	122	87.
11	FEB	0655	12	6.	11	FEB	1000	49	4.	11	FEB	1305	86	379.	11	FEB	1610	123	85.
11	FEB	0700	13	6.	11	FEB	1005	50	5.	11	FEB	1310	87	372.	11	FEB	1615	124	82.
11	FEB	0705	14	6.	11	FEB	1010	51	5.	11	FEB	1315	88	364.	11	FEB	1620	125	80.
11	FEB	0710	15	6.	11	FEB	1015	52	5.	11	FEB	1320	89	356.	11	FEB	1625	126	77.
11	FEB	0715	16	6.	11	FEB	1020	53	6.	11	FEB	1325	90	347.	11	FEB	1630	127	74.
11	FEB	0720	17	5.	11	FEB	1025	54	6.	11	FEB	1330	91	339.	11	FEB	1635	128	72.
11	FEB	0725	18	5.	11	FEB	1030	55	7.	11	FEB	1335	92	329.	11	FEB	1640	129	70.
11	FEB	0730	19	5.	11	FEB	1035	56	7.	11	FEB	1340	93	315.	11	FEB	1645	130	68.
11	FEB	0735	20	5.	11	FEB	1040	57	8.	11	FEB	1345	94	302.	11	FEB	1650	131	66.
11	FEB	0740	21	5.	11	FEB	1045	58	9.	11	FEB	1350	95	289.	11	FEB	1655	132	64.
11	FEB	0745	22	4.	11	FEB	1050	59	9.	11	FEB	1355	96	276.	11	FEB	1700	133	62.
11	FEB	0750	23	4.	11	FEB	1055	60	10.	11	FEB	1400	97	264.	11	FEB	1705	134	60.
11	FEB	0755	24	4.	11	FEB	1100	61	11.	11	FEB	1405	98	252.	11	FEB	1710	135	59.
11	FEB	0800	25	4.	11	FEB	1105	62	12.	11	FEB	1410	99	241.	11	FEB	1715	136	58.
11	FEB	0805	26	4.	11	FEB	1110	63	13.	11	FEB	1415	100	231.	11	FEB	1720	137	56.
11	FEB	0810	27	4.	11	FEB	1115	64	15.	11	FEB	1420	101	219.	11	FEB	1725	138	55.
11	FEB	0815	28	4.	11	FEB	1120	65	16.	11	FEB	1425	102	205.	11	FEB	1730	139	54.
11	FEB	0820	29	4.	11	FEB	1125	66	18.	11	FEB	1430	103	193.	11	FEB	1735	140	53.
11	FEB	0825	30	3.	11	FEB	1130	67	20.	11	FEB	1435	104	181.	11	FEB	1740	141	52.
11	FEB	0830	31	3.	11	FEB	1135	68	24.	11	FEB	1440	105	171.	11	FEB	1745	142	50.
11	FEB	0835	32	3.	11	FEB	1140	69	33.	11	FEB	1445	106	161.	11	FEB	1750	143	49.

11	FEB	0840	33	3.	*	11	FEB	1145	70	49.	*	11	FEB	1450	107	153.	*	11	FEB	1755	144	48.
11	FEB	0845	34	3.	*	11	FEB	1150	71	71.	*	11	FEB	1455	108	145.	*	11	FEB	1800	145	46.
11	FEB	0850	35	3.	*	11	FEB	1155	72	130.	*	11	FEB	1500	109	139.	*					
11	FEB	0855	36	3.	*	11	FEB	1200	73	207.	*	11	FEB	1505	110	132.	*					
11	FEB	0900	37	3.	*	11	FEB	1205	74	281.	*	11	FEB	1510	111	127.	*					

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PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	12.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 396.	6.67		191.	100.	100.	100.
		(INCHES)	4.599	4.813	4.813	4.813
		(AC-FT)	95.	99.	99.	99.

CUMULATIVE AREA = 0.39 SQ MI

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          *            *
102 KK    *    POND4   *
          *            *
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HYDROGRAPH ROUTING DATA

103 RS STORAGE ROUTING

NSTPS	1	NUMBER OF SUBREACHES
ITYP	ELEV	TYPE OF INITIAL CONDITION
RSVRIC	1344.70	INITIAL CONDITION
X	0.00	WORKING R AND D COEFFICIENT

104 SV	STORAGE	0.0	0.6	1.1	1.7	2.3	2.8
105 SQ	DISCHARGE	0.	40.	210.	350.	450.	530.
106 SE	ELEVATION	1344.70	1345.70	1346.70	1347.70	1348.70	1349.70

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*** WARNING *** MODIFIED PULS ROUTING MAY BE NUMERICALLY UNSTABLE FOR OUTFLOWS BETWEEN 40. TO 210.
THE ROUTED HYDROGRAPH SHOULD BE EXAMINED FOR OSCILLATIONS OR OUTFLOWS GREATER THAN PEAK INFLOWS.
THIS CAN BE CORRECTED BY DECREASING THE TIME INTERVAL OR INCREASING STORAGE (USE A LONGER REACH.)

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HYDROGRAPH AT STATION POND4

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DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE
11	FEB	0600	1	0.	0.0	1344.7	11	FEB	1005	50	4.	0.1	1344.8	11	FEB	1410	99	248.	1.3	1347.0
11	FEB	0605	2	3.	0.1	1344.8	11	FEB	1010	51	4.	0.1	1344.8	11	FEB	1415	100	237.	1.2	1346.9
11	FEB	0610	3	5.	0.1	1344.8	11	FEB	1015	52	5.	0.1	1344.8	11	FEB	1420	101	226.	1.2	1346.8
11	FEB	0615	4	7.	0.1	1344.9	11	FEB	1020	53	5.	0.1	1344.8	11	FEB	1425	102	214.	1.1	1346.7
11	FEB	0620	5	7.	0.1	1344.9	11	FEB	1025	54	5.	0.1	1344.8	11	FEB	1430	103	199.	1.1	1346.6
11	FEB	0625	6	7.	0.1	1344.9	11	FEB	1030	55	6.	0.1	1344.8	11	FEB	1435	104	186.	1.0	1346.6
11	FEB	0630	7	8.	0.1	1344.9	11	FEB	1035	56	6.	0.1	1344.9	11	FEB	1440	105	175.	1.0	1346.5
11	FEB	0635	8	7.	0.1	1344.9	11	FEB	1040	57	7.	0.1	1344.9	11	FEB	1445	106	165.	1.0	1346.4
11	FEB	0640	9	7.	0.1	1344.9	11	FEB	1045	58	7.	0.1	1344.9	11	FEB	1450	107	157.	0.9	1346.4
11	FEB	0645	10	7.	0.1	1344.9	11	FEB	1050	59	8.	0.1	1344.9	11	FEB	1455	108	149.	0.9	1346.3
11	FEB	0650	11	7.	0.1	1344.9	11	FEB	1055	60	9.	0.1	1344.9	11	FEB	1500	109	141.	0.9	1346.3
11	FEB	0655	12	7.	0.1	1344.9	11	FEB	1100	61	9.	0.1	1344.9	11	FEB	1505	110	135.	0.9	1346.3
11	FEB	0700	13	7.	0.1	1344.9	11	FEB	1105	62	10.	0.2	1345.0	11	FEB	1510	111	129.	0.9	1346.2
11	FEB	0705	14	6.	0.1	1344.9	11	FEB	1110	63	11.	0.2	1345.0	11	FEB	1515	112	124.	0.8	1346.2
11	FEB	0710	15	6.	0.1	1344.9	11	FEB	1115	64	12.	0.2	1345.0	11	FEB	1520	113	119.	0.8	1346.2
11	FEB	0715	16	6.	0.1	1344.8	11	FEB	1120	65	14.	0.2	1345.0	11	FEB	1525	114	114.	0.8	1346.1
11	FEB	0720	17	6.	0.1	1344.8	11	FEB	1125	66	15.	0.2	1345.1	11	FEB	1530	115	110.	0.8	1346.1
11	FEB	0725	18	6.	0.1	1344.8	11	FEB	1130	67	17.	0.2	1345.1	11	FEB	1535	116	106.	0.8	1346.1
11	FEB	0730	19	5.	0.1	1344.8	11	FEB	1135	68	19.	0.3	1345.2	11	FEB	1540	117	102.	0.8	1346.1
11	FEB	0735	20	5.	0.1	1344.8	11	FEB	1140	69	22.	0.3	1345.3	11	FEB	1545	118	99.	0.8	1346.0
11	FEB	0740	21	5.	0.1	1344.8	11	FEB	1145	70	29.	0.4	1345.4	11	FEB	1550	119	96.	0.8	1346.0
11	FEB	0745	22	5.	0.1	1344.8	11	FEB	1150	71	42.	0.6	1345.7	11	FEB	1555	120	93.	0.8	1346.0

11 FEB	0750	23	5.	0.1	1344.8	*	11 FEB	1155	72	105.	0.8	1346.1	*	11 FEB	1600	121	90.	0.7	1346.0
11 FEB	0755	24	5.	0.1	1344.8	*	11 FEB	1200	73	173.	1.0	1346.5	*	11 FEB	1605	122	88.	0.7	1346.0
11 FEB	0800	25	4.	0.1	1344.8	*	11 FEB	1205	74	243.	1.2	1346.9	*	11 FEB	1610	123	86.	0.7	1346.0
11 FEB	0805	26	4.	0.1	1344.8	*	11 FEB	1210	75	297.	1.5	1347.3	*	11 FEB	1615	124	83.	0.7	1346.0
11 FEB	0810	27	4.	0.1	1344.8	*	11 FEB	1215	76	337.	1.6	1347.6	*	11 FEB	1620	125	81.	0.7	1345.9
11 FEB	0815	28	4.	0.1	1344.8	*	11 FEB	1220	77	361.	1.8	1347.8	*	11 FEB	1625	126	78.	0.7	1345.9
11 FEB	0820	29	4.	0.1	1344.8	*	11 FEB	1225	78	373.	1.8	1347.9	*	11 FEB	1630	127	76.	0.7	1345.9
11 FEB	0825	30	4.	0.1	1344.8	*	11 FEB	1230	79	382.	1.9	1348.0	*	11 FEB	1635	128	73.	0.7	1345.9
11 FEB	0830	31	4.	0.1	1344.8	*	11 FEB	1235	80	388.	1.9	1348.1	*	11 FEB	1640	129	71.	0.7	1345.9
11 FEB	0835	32	3.	0.1	1344.8	*	11 FEB	1240	81	393.	2.0	1348.1	*	11 FEB	1645	130	69.	0.7	1345.9
11 FEB	0840	33	3.	0.0	1344.8	*	11 FEB	1245	82	395.	2.0	1348.1	*	11 FEB	1650	131	67.	0.7	1345.9
11 FEB	0845	34	3.	0.0	1344.8	*	11 FEB	1250	83	394.	2.0	1348.1	*	11 FEB	1655	132	65.	0.7	1345.8
11 FEB	0850	35	3.	0.0	1344.8	*	11 FEB	1255	84	392.	2.0	1348.1	*	11 FEB	1700	133	63.	0.7	1345.8
11 FEB	0855	36	3.	0.0	1344.8	*	11 FEB	1300	85	389.	1.9	1348.1	*	11 FEB	1705	134	61.	0.7	1345.8
11 FEB	0900	37	3.	0.0	1344.8	*	11 FEB	1305	86	384.	1.9	1348.0	*	11 FEB	1710	135	60.	0.7	1345.8
11 FEB	0905	38	3.	0.0	1344.8	*	11 FEB	1310	87	378.	1.9	1348.0	*	11 FEB	1715	136	58.	0.7	1345.8
11 FEB	0910	39	3.	0.0	1344.8	*	11 FEB	1315	88	371.	1.8	1347.9	*	11 FEB	1720	137	57.	0.6	1345.8
11 FEB	0915	40	3.	0.0	1344.8	*	11 FEB	1320	89	363.	1.8	1347.8	*	11 FEB	1725	138	56.	0.6	1345.8
11 FEB	0920	41	3.	0.0	1344.8	*	11 FEB	1325	90	355.	1.7	1347.7	*	11 FEB	1730	139	54.	0.6	1345.8
11 FEB	0925	42	3.	0.0	1344.8	*	11 FEB	1330	91	345.	1.7	1347.7	*	11 FEB	1735	140	53.	0.6	1345.8
11 FEB	0930	43	3.	0.0	1344.8	*	11 FEB	1335	92	335.	1.6	1347.6	*	11 FEB	1740	141	52.	0.6	1345.8
11 FEB	0935	44	3.	0.0	1344.8	*	11 FEB	1340	93	324.	1.6	1347.5	*	11 FEB	1745	142	51.	0.6	1345.8
11 FEB	0940	45	3.	0.0	1344.8	*	11 FEB	1345	94	310.	1.5	1347.4	*	11 FEB	1750	143	50.	0.6	1345.8
11 FEB	0945	46	3.	0.1	1344.8	*	11 FEB	1350	95	297.	1.5	1347.3	*	11 FEB	1755	144	48.	0.6	1345.7
11 FEB	0950	47	4.	0.1	1344.8	*	11 FEB	1355	96	284.	1.4	1347.2	*	11 FEB	1800	145	47.	0.6	1345.7
11 FEB	0955	48	4.	0.1	1344.8	*	11 FEB	1400	97	271.	1.4	1347.1	*						
11 FEB	1000	49	4.	0.1	1344.8	*	11 FEB	1405	98	260.	1.3	1347.1	*						

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PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	12.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 395.	6.75		191.	99.	99.	99.
		(INCHES)	4.594	4.783	4.783	4.783
		(AC-FT)	95.	99.	99.	99.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	12.00-HR
+ (AC-FT)	(HR)				
2.	6.75	1.	1.	1.	1.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	12.00-HR
+ (FEET)	(HR)				
1348.15	6.75	1346.67	1345.78	1345.78	1345.78

CUMULATIVE AREA = 0.39 SQ MI

1

RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

	OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD 6-HOUR	24-HOUR	72-HOUR	BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
+										
	HYDROGRAPH AT									
+		EAST	199.	6.08	33.	18.	18.	0.06		
	ROUTED TO									
+		PONDA	63.	6.58	33.	17.	17.	0.06		
+									1356.04	6.58
	HYDROGRAPH AT									
+		RRWEST	169.	6.25	35.	18.	18.	0.08		
	ROUTED TO									
+		PONDB	158.	6.33	35.	18.	18.	0.08		
+									1351.69	6.33
	HYDROGRAPH AT									
+		WEST	50.	6.08	8.	4.	4.	0.01		
	HYDROGRAPH AT									
+		BASIN1	15.	6.08	3.	1.	1.	0.00		
	HYDROGRAPH AT									

1355 ft

+		BASIN2	191.	6.08	32.	17.	17.	0.06	
	5 COMBINED AT								
+		INTO2	424.	6.17	110.	58.	58.	0.22	
	ROUTED TO								
+		POND$2	324.	6.42	109.	56.	56.	0.22	
+									1349.80 6.42
	HYDROGRAPH AT								
+		BASIN3	504.	6.08	85.	45.	45.	0.15	
	2 COMBINED AT								
+		INTO3	720.	6.17	192.	102.	102.	0.37	
	ROUTED TO								
+		POND3	382.	6.75	182.	95.	95.	0.37	
+									1348.76 6.75
	HYDROGRAPH AT								
+		BASIN4	56.	6.08	9.	5.	5.	0.02	
	2 COMBINED AT								
+		INTO4	396.	6.67	191.	100.	100.	0.39	
	ROUTED TO								
+		POND4	395.	6.75	191.	99.	99.	0.39	
+									1348.15 6.75

*** NORMAL END OF HEC-1 ***