SUBDIVISION COMMITTEE
METROPOLITAN AREA PLANNING COMMISSION

AGENDA ITEM NO. 5

May 18, 1995

STAFF REPORT
(Final Plat, Preliminary Plat approved 4/6/95)

CASE NUMBER: S/D 95-6 NORTHRIDGE LAKES ADDITION

OWNER/APPLICANT: Northridge Lakes, Inc., 7926 W. 21st Street, Wichita, KS 67205

OWNER: E. Leo and Burchie Kastens, 773 Westridge, Wichita, KS 67203

SURVEYOR/ENGINEER: P.E.C., P.A., 303 S. Topeka, Wichita, KS 67202

LOCATION: East of Tyler and south of 29th Street North

SITE SIZE: 76.5 Acres

NUMBER OF LOTS

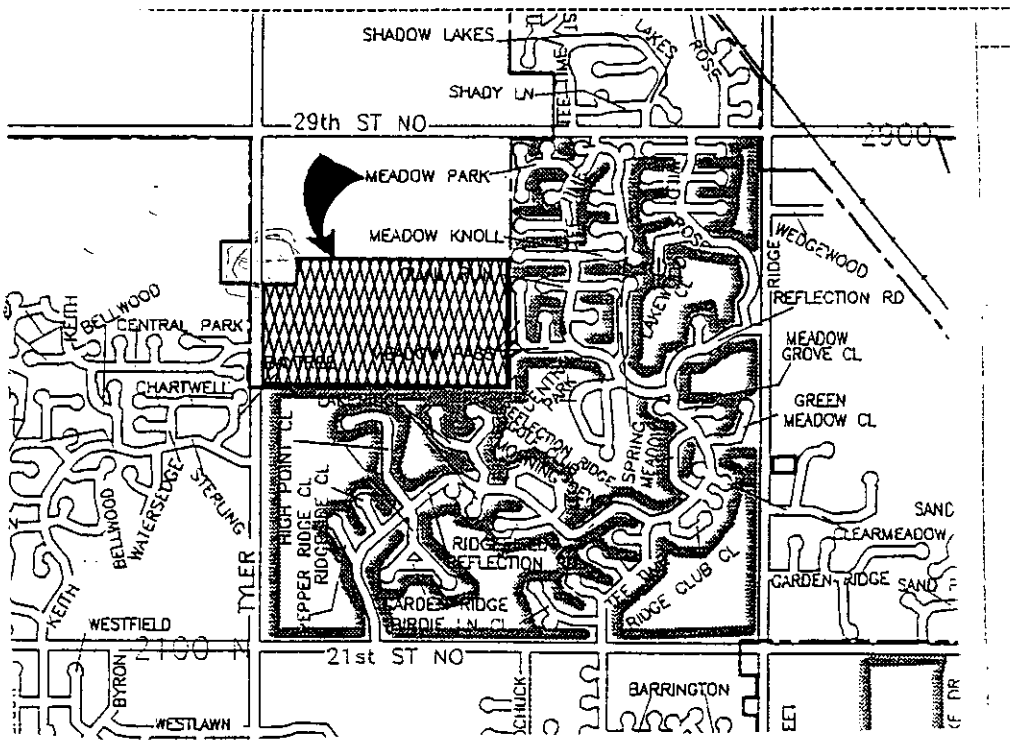
Residential:	140
Office:	
Commercial:	
Industrial:	
Total:	140

MINIMUM LOT AREA: 10,000 sq. ft.

CURRENT ZONING: R-1

PROPOSED ZONING: "AA" (Upon annexation) (This site will be annexed to the City of Wichita on 5/12/95)

VICINITY MAP:



NOTE: This site will be annexed to the City of Wichita on 5/12/95, and will be zoned "AA" One-family Dwelling District. The "AA" District has a minimum lot size of 6,000 square feet; the lots on this plat exceed that requirement.

STAFF COMMENTS:

A. This site will be annexed to the City of Wichita on 5/12/95. Upon annexation, the site will be zoned "AA" which allows for the lot sizes being indicated.

B. The applicant shall guarantee the extension of sanitary sewer to serve the lots being platted.

C. The applicant shall guarantee the extension of City water to serve the lots being platted. This guarantee shall also provide for any needed water line improvements along Tyler Road.

D. The applicant shall guarantee any drainage improvements required by the platting of this property.

E. The applicant shall guarantee construction of the storm sewers required by this plat.

F. The applicant shall guarantee the paving of the proposed interior streets. This guarantee shall also provide for sidewalks along one side of Meadow Pass and Meadow Grove/Lake Ridge. Further, as determined necessary by City Engineering, temporary turnarounds shall be provided for Meadow Pass Ct. adjacent to Block 2 and Pepper Ridge adjacent to Lot 1, Block 5.

G. A guarantee to participate in the paving of Tyler Road adjacent to this plat shall be provided. Staff has expressed a desire to appeal the Subcommittee's decision to not tie this plat to the "gap" paving issue on Tyler, just south of this plat.

H. As indicated by Traffic Engineering, guarantees shall be provided for a decel lane and left turn lane in Tyler Road and serve this site's entrance from Tyler Road.

I. If improvements are guaranteed by petition, a notarized certificate listing the petitions shall be submitted to the Planning Department for recording.

J. It appears that the court adjacent to Lots 16, 17 & 18 Block 5 shall be named Meadow Pass Court rather than Lake Ridge Circle.

K. That plattor's text indicates provisions shall be made for ownership and maintenance of the proposed reserves by the Homeowners' Associations. The applicant shall either form a lot owners' association prior to recording the plat or shall submit a covenant stating when the association will be formed, when the reserves will be deeded to the association and who is to own and maintain the reserves prior to the association taking over those responsibilities. The plattor's text also provides for the homeowner's association to maintain the "parking strip" area adjacent to the plat's west line, that is, the right-of-way area between this plat and the driving surface for Tyler Road.

L. For those reserves being platted for drainage purposes, the required covenant which provides for ownership and maintenance of the reserves shall grant, to the City, the authority to maintain the drainage reserves in the event the owner(s) fail to do so. The covenant shall provide for the cost of such maintenance to be charged back to the owner(s) by a method similar to special assessments.

M. The final plat shall state in the plattor's text the purposes of the proposed reserves as well as who is to own and maintain the reserves.

N. The applicant shall submit a covenant which provides for four (4) off-street parking spaces per dwelling unit on each lot which abuts a 58-foot street. The covenant shall inventory the affected lots by lot and block number and shall state that the covenant runs with the land and is binding on future owners and assigns.

O. The applicant shall submit a copy of the instrument which establishes the Arkla Energy Resources Easement on this property. The applicant's agent shall determine any setback requirements from the pipeline by researching the text of the pipeline agreement. If a setback from the pipeline easement is provided for in the pipeline easement agreement, it shall be indicated on the face of the plat.

P. Any relocation, lowering or encasement of the pipelines, made necessary by this development, will not be at the expense of the City.

Q. In regard to Reserve "E" proof shall be provided that access to this area, for maintenance, can be provided from the adjoining property. As shown as a part of this plat, this Reserve is landlocked.

R. The applicant shall install or guarantee the installation of all utilities and facilities which are applicable and described in Article 8 of the MAPC Subdivision Regulations. (Water service and fire hydrants required by Article 8 for fire protection shall be as per the direction and approval of the Chief of the Fire Department.)

S. The applicant's engineer is advised that the Register of Deeds is requiring the name(s) of the notary public, who acknowledges the signatures on this plat, to be printed beneath the notary's signature.

T. To receive mail delivery without delay, and to avoid unnecessary expense, the applicant is advised of the necessity to meet with the U.S. Postal Service Growth Management Coordinator (phone 316-946-4527) prior to development of the plat so that the type of delivery, and the tentative mailbox locations can be determined.

U. The representative from **City Engineering** should be prepared to comment on the status of the applicant's drainage plan.

V. The applicant is advised that various State and Federal requirements [specifically but not limited to the Army Corps of Engineers, David Hibbs, Kanopolis Project Office, Rt. 1, Box 30, Marquette, KS 67464 (913-546-2294) or Ron Little, Kansas Department of Wildlife and Parks,

P. O. Box 317, Valley Center, KS 67147] for the control of soil and wind erosion and the protection of wetlands may impact how this site can be developed. It is the applicant's responsibility to contact all appropriate agencies to determine any such requirements.

W. The final plat appears to be missing a utility easement requested by KG&E located between Lots 38 and 39, Block 4.

X. As noted by the Fire Department for the stub street in the area of Lots 16, 17, and 18, Block 1, a full turnaround should be provided, if the length of this Court exceeds the 150-foot limit for alternate turnarounds ("T", "L", etc.).

Y. Perimeter closure computations shall be submitted with the final plat tracing. Section 5-101(c).

Z. Recording of the plat within 30 days after approval by the City Council.

WICHITA-SEDGWICK COUNTY

METROPOLITAN AREA PLANNING DEPARTMENT

DATE: July 14, 1995

TO: Chris Cherches, City Manager

FROM: Marvin S. Krout, Director

SUBJECT: Northridge Lakes/arterial street paving

This memo concerns a proposed subdivision - Northridge Lakes Estates Addition - scheduled for the City Council agenda of July 25. As the greensheet states, staff and the developer have reached an agreement on a petition for paving a portion of Tyler Road leading to the proposed development. However, the discussion on this plat raises a larger policy issue on the funding of arterial streets in the City's fringe areas, and so I thought this more detailed explanation of the issue would be helpful for you and the City Council.

Background:

Up through the mid-1980s, the MAPC and City Council routinely approved plats for new residential subdivisions along unpaved mile line (arterial) streets which were not yet scheduled in the CIP for improvement. One of the impacts of this policy was that, after development occurred on these streets, the demands for improving the street became irresistable, and the CIP was adjusted to accommodate the needed improvement. In the process of adjusting the CIP, projects in the built-up portion of the city were being deferred in order to meet the new demands of the fringe developments.

Beginning with the plat for Bay Country Estates in 1987 (south and west of 119th/Central), city staff began requesting that developers of new subdivisions take some responsibility for extending a paved perimeter road to that subdivision. It seemed to be a natural extension of the established policies that required developer participation in the extension of water and sewer mains to serve new urban density developments. Last year, if you recall, the City Council even extended that policy to include subdivisions in the unincorporated area where the City is providing water and/or sewer: as a condition for City water, the City required the developer of Savannah at Castle Rock in the 4 Mile Creek area to guarantee the paving of 13th Street North, east of 143rd Street East.

The "rule of thumb" that evolved was that a typical subdivision

would be responsible for the equivalent of one lane of paving along its frontage on the perimeter mile line road. In addition, depending on the nature of the subdivision, additional guarantees for decel and/or left turn lanes at major entrances might be required. The "rule of thumb" for a typical subdivision, which has averaged about $1,000 per lot, does appear to easily meet the "rough proportionality" requirements of the courts for development exactions. By our rough calculations, a defensible exaction for road construction could be as high as $4,840.

This dollar figure is based on the following calculations that have been the basis for impact fees in other jurisdictions: the cost of paving and storm sewers for a lane-mile of roadway is about $500,000; the capacity of a single lane is about 5,000 Average Daily Trips (ADT); therefore, the proportional cost of building the lane-mile is $100 per trip. The average trip length is 5 miles, so the actual cost of a "trip" is $500. A single family home generates 10 ADT, so its proportional cost is $5,000. The average new home supports about $1,000 in debt service toward city capital improvements, and about 16% of this goes toward arterial street improvements, or $160. This contribution would require a reduction in the maximum possible exaction from $5,000 to $4,840.

In some cases, the configuration of a tract of land does not lend itself very well to this rule of thumb (e.g. a small single lot fronting the road would be assessed more than its "fair share" based on its traffic generation, and a large interior tract with only its access street fronting the road would be assessed far less than its "fair share"). Sometimes, when it was not possible to create a benefit district involving both sides of a street, the developer has been asked to pave two lanes for approximately 1/2 his frontage, with the expectation that the "gap" would later be filled in.

Planning staff had discussions over a year ago with WABA on this issue. WABA had concerns about the fact that this policy had evolved without formal adoption, that it was difficult for developers to estimate assessment costs, and that they were not clear on the street standards that would be used in each instance (when would the City require curbs and gutters, when would we require turn lanes, etc.). They felt that the subdivision policy was not consistent with the policy adopted several years ago for all arterial projects in the City's CIP (the City Council eliminated the use of assessments to help pay the cost of arterial streets programmed in the CIP, and now relies on 100% "at-large" funding). Our response was that unpaved roads like Tyler Road were not programmed in the CIP, and so they were not covered by that policy.

Shortly after this discussion, several lawsuits were filed in northeast Kansas on the issue of assessments for major roadways, and WABA agreed to wait until the suits were settled before

taking up their issues more formally. We understand that some of these lawsuits have been settled, in favor of the governing bodies.

In April of this year, WABA representatives met again with the Planning staff, and suggested again that the policies be refined and formalized. They also suggested that new subdivisions should not be assessed for perimeter road paving, but that these roads should be paved by the City at-large, just like projects funded in the CIP are paid by taxpayers at-large. In support of this position, they cited their cost/revenue study prepared last year by a WSU real estate professor. This disagreement remains an unsettled issue for WABA, and we expect that they will want to raise the issue with the City Council in the future.

Analysis:

Northridge Lakes Estates is planned for a tract of 76.5 acres with approximately 1000 feet of frontage along the east side of Tyler Road. Through the subdivision approval process, guarantees have been obtained for 2 lane paving for a distance of approximately 2000 feet north from 21st Street, from other abutting developers. In addition, a recent addition across Tyler Road from the subject tract, Bradford South, with 600 frontage along the southern portion of the frontage of the subject tract, is guaranteeing 2 lane paving along its frontage.

The developer of Northridge Lakes agreed at the MAPC meetings to guarantee 2 lane paving for the remaining 400 feet along the northern portion of its frontage, at an estimated $56,000. Storm sewers are not required in this particular road segment. This represents a per-lot cost of only $320-388, depending on whether the cost is spread over the 144 lots in the Addition, or also includes 31 more lots that are planned to the south. For comparison, the 117 lots in Bradford South Addition, across Tyler from Northridge Lakes, will be assessed approximately $966 each, and lots in Sterling Farms, which is being developed further south, will be assessed approximately $972 each.

Planning staff recognized that this developer had ownership interests in both Northridge Lakes and the as-yet unplatted property to the south, a part of the Reflection Ridge Residential CUP. The Northridge plat is shown with a street stubbing into this property to the south. The CUP shows the unplatted area will develop eventually with 28 single family lots, and the developer's latest plans call for 31 lots. We felt that it would be inequitable for those 31 lots to assume the burden for paving the "gap" of approximately 600 feet along their frontage, so it would be appropriate to suggest a petition now, from the Northridge Lakes property and the unplatted property, to complete the paving.

If the $90,000 cost of 2-lane paving for the 600 foot "gap" is added to the paving of the 400 feet of frontage, the per-lot

cost would increase to $834-1,014 (the developer will be separately responsible for drainage improvements along this segment of Tyler Road, regardless of whether the road is paved or not, so this is not included in the paving assessment calculation.

The developer and his agent argued at the Subdivision Committee and MAPC meetings that 1) he could not afford to spread the cost over the lots in Northlake Lakes, 2) the unplatted land to the south had overlapping but different ownership, and 3) the unplatted land should be "grandfathered" from assessments because it was part of the larger Reflection Ridge CUP, which was approved before the policy on assessments for arterial streets became the rule. Staff disagreed with the developer's position that the approval of a CUP constitutes a "grandfathering" of land from the standpoint of any new platting requirements. The assessments for Tyler Road paving as recommended by staff would be no higher than on the lots in nearby additions. The developer's overall assessments may be higher than in nearby additions, but that is because of his decision to plat fewer, larger lots over which to spread the costs.

The MAPC voted (8-1) to approve the plat, with a recommendation that "before the plat is recorded, the issue of paving will be resolved". At the meeting, that was interpreted by the maker of the motion to mean that one way or the other, the paving should be guaranteed before the plat is approved -- either the developer should be required to submit a guarantee, or the City Council should commit itself to paving the 600 foot "gap". Although the final motion was to approve the plat with this condition, two MAPC members qualified their vote by saying that they did not intend for the plat to be "held hostage" by the road paving issue, and they felt it should be the obligation of the City at-large to pave these arterial streets.

At the MAPC meeting, Planning staff admitted that this method of using a "patchwork" of guarantees to pave segments of these streets was cumbersome, difficult, and inefficient, but that returning to the old policy was even less desirable (allowing subdivisions again on unpaved streets, and then later adjusting the CIP to fix this problem, at the expense of deferring other projects that had been approved and programmed). It was pointed out that an impact fee system, whereby the City would collect a per-unit fee with building permits, and put the fee in a trust fund to pave longer road segments at one time, would be simpler to administer and result in the same charge for every lot. However, homebuilders have opposed and continue to oppose an impact fee system.

After the MAPC meeting, staff from Planning, Public Works, and Law met with the developer, and I suggested a possible compromise by which the developer's lots would be assessed for the cost of paving the 600 foot "gap" only. This would reduce

the per-lot assessments to about $514-625, exclusive of drainage improvemements. It will provide a paved Tyler Road up to the entrance of every platted subdivision, as recommended by MAPC. However, it only "postpones" the issue of the "gap", by leaving a new gap that will need to be filled somehow in the future, when properties to the north develop.

cc. Gary Rebenstorf
Doug Moshier
Steve Lackey
Mike Lindebak

CURRENT DATE: 10-10-1995
CURRENT TIME: 12:45:45

FILE DATE: 10-10-1995
FILE NAME: 2TO3

FHWA CULVERT ANALYSIS
HY-8, VERSION 3.2

2 to 3
36"

C U L V	SITE DATA: INLET ELEV. (FT)	SITE DATA: OUTLET ELEV. (FT)	SITE DATA: CULVERT LENGTH (FT)	CULVERT SHAPE, MATERIAL, INLET: BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	1339.00	1332.40	100.22	1 RCP	3.00	3.00	.012	CONVENTIONAL
2	1337.8	1332.5	92.1					
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (CFS) FILE: 2TO3 DATE: 10-10-1995

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
1342.40	0	0	0	0	0	0	0	0	1
1342.75	10	10	0	0	0	0	0	0	1
1343.13	20	20	0	0	0	0	0	0	1
1343.61	30	30	0	0	0	0	0	0	1
1344.20	40	40	0	0	0	0	0	0	1
1344.92	50	50	0	0	0	0	0	0	1
1345.75	60	60	0	0	0	0	0	0	1
1346.72	70	70	0	0	0	0	0	0	1
1347.80	80	80	0	0	0	0	0	0	1
1349.02	90	90	0	0	0	0	0	0	1
1350.37	100	100	0	0	0	0	0	0	1
1360.00	152	152	0	0	0	0	0	OVERTOPPING	

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: 2TO3 DATE: 10-10-1995

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
1342.40	0.00	0	0	0.00
1342.75	0.00	10	0	0.00
1343.13	0.00	20	0	0.00
1343.61	0.00	30	0	0.00
1344.20	0.00	40	0	0.00
1344.92	0.00	50	0	0.00
1345.75	0.00	60	0	0.00
1346.72	0.00	70	0	0.00
1347.80	0.00	80	0	0.00
1349.02	0.00	90	0	0.00
1350.37	0.00	100	0	0.00

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

CURRENT DATE: 10-10-1995 FILE DATE: 10-10-1995
CURRENT TIME: 12:45:45 FILE NAME: 2TO3

CULVERT # 1

PERFORMANCE CURVE FOR 1 BARREL(S)

Q (cfs)	HWE (ft)	TWE (ft)	ICH (ft)	OCH (ft)	FLOW TYPE	CCE (ft)	FCE (ft)	TCE (ft)	VO (fps)
0	1342.40	1342.40	0.00	3.40	0-NF	0.00	1339.00	0.00	0.00
10	1342.75	1342.70	1.31	3.75	4-FF	0.00	0.00	0.00	1.41
20	1343.13	1342.88	2.00	4.13	4-FF	0.00	0.00	0.00	2.83
30	1343.61	1343.03	2.60	4.61	4-FF	0.00	0.00	0.00	4.24
40	1344.20	1343.16	3.20	5.20	4-FF	0.00	0.00	0.00	5.66
50	1344.92	1343.29	3.90	5.92	4-FF	0.00	0.00	0.00	7.07
60	1345.75	1343.40	4.75	6.75	4-FF	0.00	0.00	0.00	8.49
70	1346.72	1343.51	5.78	7.72	4-FF	0.00	0.00	0.00	9.90
80	1347.80	1343.61	6.98	8.80	4-FF	0.00	0.00	0.00	11.32
90	1349.02	1343.71	8.35	10.02	4-FF	0.00	0.00	0.00	12.73
100	1350.37	1343.81	9.91	11.37	4-FF	0.00	0.00	0.00	14.15

El. inlet face invert 1339.00 ft El. outlet invert 1332.40 ft
El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

***** SITE DATA ***** CULVERT INVERT **********

INLET STATION (FT)	0.00
INLET ELEVATION (FT)	1339.00
OUTLET STATION (FT)	100.00
OUTLET ELEVATION (FT)	1332.40
NUMBER OF BARRELS	1.00
SLOPE (V-FT/H-FT)	0.0660
CULVERT LENGTH ALONG SLOPE (FT)	100.22

***** CULVERT DATA SUMMARY **********

BARREL SHAPE	CIRCULAR
BARREL DIAMETER	3.00 FT
BARREL MATERIAL	CONCRETE
BARREL MANNING'S N	0.012
INLET TYPE	CONVENTIONAL
INLET EDGE AND WALL	SQUARE EDGE WITH HEADWALL
INLET DEPRESSION	NONE

CURRENT DATE: 10-10-1995
CURRENT TIME: 12:45:45

FILE DATE: 10-10-1995
FILE NAME: 2TO3

TAILWATER

TAILWATER RATING CURVE

FLOW(CFS)	W.S.E.(FT)
0	1342.40
10	1342.70
20	1342.88
30	1343.03
40	1343.16
50	1343.29
60	1343.40
70	1343.51
80	1343.61
90	1343.71
100	1343.81

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH (FT)	30.00
CREST LENGTH (FT)	100.00
OVERTOPPING CREST ELEVATION (FT)	1360.00

CURRENT DATE: 10-10-1995
CURRENT TIME: 13:08:50

FILE DATE: 10-10-1995
FILE NAME: 5TO6

FHWA CULVERT ANALYSIS
HY-8, VERSION 3.2

CU LV	SITE DATA: INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	CULVERT SHAPE, MATERIAL, INLET: BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	1330.00	1328.80	250.00	1 RCP	4.00	4.00	.012	CONVENTIONAL
2	1328.5	1328.8	249					
3								
4								
5								
6								

Good

FILE: 5TO6 CULVERT HEADWATER ELEVATION (FT) DATE: 10-10-1995

DISCHARGE	1	2	3	4	5	6	ROADWAY
50	1336.52	0.00	0.00	0.00	0.00	0.00	1350.07
60	1336.90	0.00	0.00	0.00	0.00	0.00	1350.07
70	1337.34	0.00	0.00	0.00	0.00	0.00	1350.08
80	1337.81	0.00	0.00	0.00	0.00	0.00	1350.09
90	1338.34	0.00	0.00	0.00	0.00	0.00	1350.10
100	1338.91	0.00	0.00	0.00	0.00	0.00	1350.10
110	1339.53	0.00	0.00	0.00	0.00	0.00	1350.11
120	1340.19	0.00	0.00	0.00	0.00	0.00	1350.12
130	1340.90	0.00	0.00	0.00	0.00	0.00	1350.12
140	1341.66	0.00	0.00	0.00	0.00	0.00	1350.13
150	1342.47	0.00	0.00	0.00	0.00	0.00	1350.14

SQ SE

CURRENT DATE: 10-10-1995
CURRENT TIME: 13:08:50

FILE DATE: 10-10-1995
FILE NAME: 5TO6

CULVERT # 1

PERFORMANCE CURVE FOR 1 BARREL(S)

Q (cfs)	HWE (ft)	TWE (ft)	ICE (ft)	OCE (ft)	FLOW TYPE	CCE (ft)	FCE (ft)	TCE (ft)	VO (fps)
50	1336.52	1335.89	3.15	6.52	4-FF	0.00	0.00	0.00	3.98
60	1336.90	1336.00	3.53	6.90	4-FF	0.00	0.00	0.00	4.77
70	1337.34	1336.11	3.91	7.34	4-FF	0.00	0.00	0.00	5.57
80	1337.81	1336.21	4.31	7.81	4-FF	0.00	0.00	0.00	6.37
90	1338.34	1336.31	4.73	8.34	4-FF	0.00	0.00	0.00	7.16
100	1338.91	1336.41	5.20	8.91	4-FF	0.00	0.00	0.00	7.96
110	1339.53	1336.50	5.71	9.53	4-FF	0.00	0.00	0.00	8.75
120	1340.19	1336.59	6.27	10.19	4-FF	0.00	0.00	0.00	9.55
130	1340.90	1336.67	6.89	10.90	4-FF	0.00	0.00	0.00	10.35
140	1341.66	1336.76	7.57	11.66	4-FF	0.00	0.00	0.00	11.14
150	1342.47	1336.84	8.30	12.47	4-FF	0.00	0.00	0.00	11.94

El. inlet face invert 1330.00 ft El. outlet invert 1328.80 ft
El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

***** SITE DATA ***** CULVERT INVERT **********

INLET STATION (FT)	0.00
INLET ELEVATION (FT)	1330.00
OUTLET STATION (FT)	250.00
OUTLET ELEVATION (FT)	1328.80
NUMBER OF BARRELS	1.00
SLOPE (V-FT/H-FT)	0.0048
CULVERT LENGTH ALONG SLOPE (FT)	250.00

***** CULVERT DATA SUMMARY **********

BARREL SHAPE	CIRCULAR
BARREL DIAMETER	4.00 FT
BARREL MATERIAL	CONCRETE
BARREL MANNING'S N	0.012
INLET TYPE	CONVENTIONAL
INLET EDGE AND WALL	SQUARE EDGE WITH HEADWALL
INLET DEPRESSION	NONE

CURRENT DATE: 10-10-1995
CURRENT TIME: 13:08:50

FILE DATE: 10-10-1995
FILE NAME: 5TO6

TAILWATER

TAILWATER RATING CURVE

FLOW(CFS)	W.S.E.(FT)
50	1335.89
60	1336.00
70	1336.11
80	1336.21
90	1336.31
100	1336.41
110	1336.50
120	1336.59
130	1336.67
140	1336.76
150	1336.84

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH (FT)	30.00
CREST LENGTH (FT)	1000.00
OVERTOPPING CREST ELEVATION (FT)	1350.00

N½ Not Incl. 10-10-1995

```
1*****************************************
*                                       *
*   FLOOD HYDROGRAPH PACKAGE  (HEC-1)   *
*             MAY  1991                 *
*          VERSION 4.0.1E               *
*     Lahey F77L-EM/32 version 5.01     *
*       Dodson & Associates, Inc.       *
*  RUN DATE  10/10/95  TIME  14:59:12   *
*****************************************
```

```
*****************************************
*                                       *
*    U.S. ARMY CORPS OF ENGINEERS       *
*    HYDROLOGIC ENGINEERING CENTER      *
*          609 SECOND STREET            *
*        DAVIS, CALIFORNIA 95616        *
*          (916) 551-1748               *
*                                       *
*****************************************
```

```
X    X  XXXXXX   XXXX          X
X    X  X       X    X       XX
X    X  X            X        X
XXXXXX  XXX     X       XXXX  X
X    X  X       X            X
X    X  X       X    X       X
X    X  XXXXXX   XXXX        XXX
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM


```
         LINE          ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

           1           ID       BALTHROP ADDITION -- DETENTION STORAGE ANALYSIS, 100-YR STORM
                       *      T:\DAR\HEC1\KSTNS4.IH1
*** LIST ***
*** FREE ***
                       *DIAGRAM
           2           IT      6 29SEP92    0600       0 29SEP92    2400
           3           IN     30 29SEP92    0600
           4           IO      0       0
                       *       PARAMETERS FOR HYDROGRAPH FOR FLOW THROUGH 42" RCP

           5           KK      1
           6           BA   .0594
           7           PB    6.5
           8           PC   0.08   0.09   0.10   0.11   0.12   0.133  0.147  0.163  0.181  0.204
           9           PC  0.235  0.283  0.663  0.735  0.772  0.799  0.820  0.835  0.850  0.865
          10           PC  0.880  0.890  0.900  0.910  0.916  0.925  0.934  0.943  0.952  0.958
          11           PC  0.964  0.970  0.976  0.982  0.988  0.994  1.000
          12           LS      0     61     38
          13           UD   0.24
                       *       PARAMETERS FOR HYDROGRAPH FOR FLOW COLLECTED AT THE EXISTING POND

          14           KK      2
          15           BA   .0172
          16           PB    7.8
          17           PC   0.08   0.09   0.10   0.11   0.12   0.133  0.147  0.163  0.181  0.204
          18           PC  0.235  0.283  0.663  0.735  0.772  0.799  0.820  0.835  0.850  0.865
          19           PC  0.880  0.890  0.900  0.910  0.916  0.925  0.934  0.943  0.952  0.958
          20           PC  0.964  0.970  0.976  0.982  0.988  0.994  1.000
          21           LS      0     61     38
          22           UD   0.15
                       *       PARAMETERS FOR HYDROGRAPH FOR FLOW COLLECTED FROM 5.1 AC. BASIN

          23           KK   5.1AC
          24           BA  .00797
          25           PB    7.8
          26           PC   0.08   0.09   0.10   0.11   0.12   0.133  0.147  0.163  0.181  0.204
          27           PC  0.235  0.283  0.663  0.735  0.772  0.799  0.820  0.835  0.850  0.865
          28           PC  0.880  0.890  0.900  0.910  0.916  0.925  0.934  0.943  0.952  0.958
          29           PC  0.964  0.970  0.976  0.982  0.988  0.994  1.000
          30           LS      0     75      0
          31           UD   0.15
                       *       COMBINED FLOW INFLOW HYDROGRAPH AT POND NO. 2
```

```
                *       LAKES 1 & 2 ARE ONE LAKE

          32    KK   INTO2
          33    HC      3
                *       STAGE STORAGE RELATIONSHIP FOR POND NO. 2 FOR 42" RCP

          34    KK   POND2
          35    RS      1    ELEV  1345.4
          36    SA   1.20    1.60
          37    SE  1345.4  1349.0
          38    SQ      0      10      20      30      40      50      60      70      80      90
          39    SQ    100
          40    SE  1345.4  1345.7 1345.88 1346.03 1346.16 1346.29 1346.40 1346.72  1347.8 1349.02
1                                       HEC-1 INPUT                                          PAGE  2

        LINE    ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

          41    SE  1350.4
                *       PARAMETERS FOR HYDROGRAPH FOR FLOW COLLECTED FROM 2.2 AC. BASIN

          42    KK   2.2AC
          43    BA   .0034
          44    PB    7.8
          45    PC   0.08    0.09    0.10    0.11    0.12    0.133   0.147   0.163   0.181   0.204
          46    PC  0.235   0.283   0.663   0.735   0.772   0.799   0.820   0.835   0.850   0.865
          47    PC  0.880   0.890   0.900   0.910   0.916   0.925   0.934   0.943   0.952   0.958
          48    PC  0.964   0.970   0.976   0.982   0.988   0.994   1.000
          49    LS      0      88       0
          50    UD   0.15
                *       PARAMETERS FOR HYDROGRAPH FOR FLOW COLLECTED FROM N. PART 5.3 AC. BASIN

          51    KK  N5.3AC
          52    BA   0.005
          53    PB    5.0
          54    PC   0.08    0.09    0.10    0.11    0.12    0.133   0.147   0.163   0.181   0.204
          55    PC  0.235   0.283   0.663   0.735   0.772   0.799   0.820   0.835   0.850   0.865
          56    PC  0.880   0.890   0.900   0.910   0.916   0.925   0.934   0.943   0.952   0.958
          57    PC  0.964   0.970   0.976   0.982   0.988   0.994   1.000
          58    LS      0      75       0
          59    UD   0.15
                *       COMBINED FLOW INFLOW HYDROGRAPH AT POND. NO. 3

          60    KK   INTO3
          61    HC      3
                *       STAGE STORAGE RELATIONSHIP FOR POND. NO. 3. FOR 42" RCP OUTLET

          62    KK   POND3
          63    RS      1    ELEV  1342.4
          64    SA   0.26    0.40    0.53    0.66    0.79
          65    SE  1342.4  1343.3  1344.2  1345.1  1346.0
          66    SQ      0      10      20      30      40      50      60      70      80      90
          67    SQ    100
          68    SE  1342.4  1342.7 1342.88 1343.03 1343.16 1343.29 1343.40 1343.51 1343.61 1343.71
          69    SE  1343.8
                *       PARAMETERS FOR HYDROGRAPH FOR FLOW COLLECTED FROM 23.3 AC. BASIN

          70    KK  23.3AC
          71    BA  .03641
          72    PB    7.8
          73    PC   0.08    0.09    0.10    0.11    0.12    0.133   0.147   0.163   0.181   0.204
          74    PC  0.235   0.283   0.663   0.735   0.772   0.799   0.820   0.835   0.850   0.865
          75    PC  0.880   0.890   0.900   0.910   0.916   0.925   0.934   0.943   0.952   0.958
          76    PC  0.964   0.970   0.976   0.982   0.988   0.994   1.000
          77    LS      0      75
          78    UD   0.15
                *       STAGE STORAGE RELATIONSHIP FOR POND NO. 4 FOR 18" OUTLET
1                                       HEC-1 INPUT                                          PAGE  3

        LINE    ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

          79    KK   POND4
          80    RS      1    ELEV  1345.0
          81    SA    1.0    1.35
          82    SE  1345.0  1349.0
          83    SQ      0      15      18      20      24
          84    SE  1345.0 1345.86 1346.88  1351.2 1356.57
                *       PARAMETERS FRO HYDROGRAPH FOR FLOW COLLECTED FROM 8.3 AC. BASIN

          85    KK   8.3AC
```

```
 86          BA  .01297
 87          PB    7.8
 88          PC   0.08   0.09   0.10   0.11   0.12   0.133  0.147  0.163  0.181  0.204
 89          PC  0.235  0.283  0.663  0.735  0.772  0.799  0.820  0.835  0.850  0.865
 90          PC  0.880  0.890  0.900  0.910  0.916  0.925  0.934  0.943  0.952  0.958
 91          PC  0.964  0.970  0.976  0.982  0.988  0.994  1.000
 92          LS      0     85
 93          UD    .15
             *          COMBINED INFLOW HYDROGRAPH FOR FLOW INTO POND NO. 5

 94          KK  INTO5
 95          HC      3
             *      STAGE STORAGE RELATIONSHIP FOR POND NO. 5 FOR 48" PIPE

 96          KK  POND5
 97          RS      1    ELEV  1335.0
 98          SA   1.96    3.33
 99          SE 1335.0  1340.0
100          SQ      0      50      60      70      80      90     100     110     120     130
101          SQ    140     150
102          SE 1335.0  1336.5 1336.90 1337.34 1337.81 1338.34 1338.91 1339.53 1340.19 1340.90
103          SE 1341.6  1342.5
             *      PARAMETERS FOR HYDROGRAPH FOR FLOW COLLECTED FROM S. PART 5.3 AC. BASIN

104          KK  S5.3AC
105          BA  .00328
106          PB    5.0
107          PC   0.08   0.09   0.10   0.11   0.12   0.133  0.147  0.163  0.181  0.204
108          PC  0.235  0.283  0.663  0.735  0.772  0.799  0.820  0.835  0.850  0.865
109          PC  0.880  0.890  0.900  0.910  0.916  0.925  0.934  0.943  0.952  0.958
110          PC  0.964  0.970  0.976  0.982  0.988  0.994  1.000
111          LS      0     75
112          UD   0.15
             *      COMBINED INFLOW HYDROGRAPH FOR FLOW INTO POND NO. 6

113          KK  INTO6
114          HC      2
             *      STAGE STORAGE RELATIONSHIP FOR POND NO. 6 FOR 8' WIER

115          KK  POND6
116          RS      1    ELEV  1335.0
117          SA   0.25   0.29   0.33   0.37   0.41
118          SE 1335.0  1336.0 1337.0 1338.0 1339.0
119          SS 1335.0     20     3.0    1.5
120          ZZ
1
          SCHEMATIC DIAGRAM OF STREAM NETWORK

 INPUT
  LINE     (V) ROUTING          (--->) DIVERSION OR PUMP FLOW

   NO.     (.) CONNECTOR        (<---) RETURN OF DIVERTED OR PUMPED FLOW

    5          1
               .
               .
   14          .           2
               .           .
               .           .
   23          .           .       5.1AC
               .           .          .
               .           .          .
   32       INTO2.....................
               V
               V
   34       POND2
               .
               .
   42          .       2.2AC
               .           .
               .           .
   51          .           .     N5.3AC
               .           .          .
               .           .          .
   60       INTO3.....................
               V
               V
   62       POND3
               .
               .
   70          .      23.3AC
```

```
                .          V
                .          V
   79           .       POND4
                .          .
                .          .
   85           .          .       8.3AC
                .          .          .
                .          .          .
   94        INTO5.........................
                V
                V
   96        POND5
                .
                .
  104           .       S5.3AC
                .          .
                .          .
  113        INTO6............
                V
                V
  115        POND6

 (***) RUNOFF ALSO COMPUTED AT THIS LOCATION
1*****************************************
*                                       *
*   FLOOD HYDROGRAPH PACKAGE  (HEC-1)   *
*             MAY  1991                 *
*           VERSION 4.0.1E              *
*     Lahey F77L-EM/32 version 5.01     *
*       Dodson & Associates, Inc.       *
*  RUN DATE  10/10/95  TIME  14:59:12   *
*****************************************

*****************************************
*                                       *
*    U.S. ARMY CORPS OF ENGINEERS       *
*    HYDROLOGIC ENGINEERING CENTER      *
*         609 SECOND STREET             *
*       DAVIS, CALIFORNIA 95616         *
*           (916) 551-1748              *
*                                       *
*****************************************

                          BALTHROP ADDITION -- DETENTION STORAGE ANALYSIS, 100-YR STORM

   4 IO          OUTPUT CONTROL VARIABLES
                      IPRNT          0  PRINT CONTROL
                      IPLOT          0  PLOT CONTROL
                      QSCAL         0.  HYDROGRAPH PLOT SCALE

     IT          HYDROGRAPH TIME DATA
                       NMIN          6  MINUTES IN COMPUTATION INTERVAL
                      IDATE    29SEP92  STARTING DATE
                      ITIME       0600  STARTING TIME
                         NQ        181  NUMBER OF HYDROGRAPH ORDINATES
                      NDDATE   30SEP92  ENDING DATE
                      NDTIME       0000  ENDING TIME
                      ICENT         19  CENTURY MARK

                    COMPUTATION INTERVAL    0.10 HOURS
                        TOTAL TIME BASE   18.00 HOURS

          ENGLISH UNITS
              DRAINAGE AREA         SQUARE MILES
              PRECIPITATION DEPTH   INCHES
              LENGTH, ELEVATION     FEET
              FLOW                  CUBIC FEET PER SECOND
              STORAGE VOLUME        ACRE-FEET
              SURFACE AREA          ACRES
              TEMPERATURE           DEGREES FAHRENHEIT


*** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** ***


          **************
          *            *
   5 KK   *          1 *
          *            *
          **************

   3 IN          TIME DATA FOR INPUT TIME SERIES
                      JXMIN         30  TIME INTERVAL IN MINUTES
                     JXDATE    29SEP92  STARTING DATE
                     JXTIME        600  STARTING TIME
```

SUBBASIN RUNOFF DATA

6 BA SUBBASIN CHARACTERISTICS
TAREA 0.06 SUBBASIN AREA

PRECIPITATION DATA

7 PB STORM 6.50 BASIN TOTAL PRECIPITATION

8 PI INCREMENTAL PRECIPITATION PATTERN

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.08	0.08	0.08	0.08	0.08
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

12 LS SCS LOSS RATE
STRTL 1.28 INITIAL ABSTRACTION
CRVNBR 61.00 CURVE NUMBER
RTIMP 38.00 PERCENT IMPERVIOUS AREA

13 UD SCS DIMENSIONLESS UNITGRAPH
TLAG 0.24 LAG

***

WARNING *** TIME INTERVAL IS GREATER THAN .29*LAG

UNIT HYDROGRAPH
14 END-OF-PERIOD ORDINATES

24.	80.	99.	79.	44.	25.	14.	8.	5.	3.
2.	1.	1.	0.						

****

HYDROGRAPH AT STATION 1

****

DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	*	DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
29 SEP 0600	1	0.00	0.00	0.00	0.	*	29 SEP 1506	92	0.02	0.00	0.02	6.
29 SEP 0606	2	0.01	0.01	0.01	0.	*	29 SEP 1512	93	0.02	0.00	0.02	6.
29 SEP 0612	3	0.01	0.01	0.01	1.	*	29 SEP 1518	94	0.02	0.00	0.02	6.
29 SEP 0618	4	0.01	0.01	0.01	1.	*	29 SEP 1524	95	0.02	0.00	0.02	6.
29 SEP 0624	5	0.01	0.01	0.01	2.	*	29 SEP 1530	96	0.02	0.00	0.02	6.
29 SEP 0630	6	0.01	0.01	0.01	2.	*	29 SEP 1536	97	0.02	0.00	0.02	6.
29 SEP 0636	7	0.01	0.01	0.01	2.	*	29 SEP 1542	98	0.02	0.00	0.02	6.
29 SEP 0642	8	0.01	0.01	0.01	2.	*	29 SEP 1548	99	0.02	0.00	0.02	6.
29 SEP 0648	9	0.01	0.01	0.01	2.	*	29 SEP 1554	100	0.02	0.00	0.02	6.
29 SEP 0654	10	0.01	0.01	0.01	2.	*	29 SEP 1600	101	0.02	0.00	0.02	6.
29 SEP 0700	11	0.01	0.01	0.01	2.	*	29 SEP 1606	102	0.01	0.00	0.01	6.
29 SEP 0706	12	0.01	0.01	0.01	2.	*	29 SEP 1612	103	0.01	0.00	0.01	6.
29 SEP 0712	13	0.01	0.01	0.01	2.	*	29 SEP 1618	104	0.01	0.00	0.01	5.
29 SEP 0718	14	0.01	0.01	0.01	2.	*	29 SEP 1624	105	0.01	0.00	0.01	5.
29 SEP 0724	15	0.01	0.01	0.01	2.	*	29 SEP 1630	106	0.01	0.00	0.01	5.
29 SEP 0730	16	0.01	0.01	0.01	2.	*	29 SEP 1636	107	0.01	0.00	0.01	4.
29 SEP 0736	17	0.01	0.01	0.01	2.	*	29 SEP 1642	108	0.01	0.00	0.01	4.
29 SEP 0742	18	0.01	0.01	0.01	2.	*	29 SEP 1648	109	0.01	0.00	0.01	4.
29 SEP 0748	19	0.01	0.01	0.01	2.	*	29 SEP 1654	110	0.01	0.00	0.01	4.
29 SEP 0754	20	0.01	0.01	0.01	2.	*	29 SEP 1700	111	0.01	0.00	0.01	4.
29 SEP 0800	21	0.01	0.01	0.01	2.	*	29 SEP 1706	112	0.01	0.00	0.01	4.
29 SEP 0806	22	0.02	0.01	0.01	2.	*	29 SEP 1712	113	0.01	0.00	0.01	4.
29 SEP 0812	23	0.02	0.01	0.01	2.	*	29 SEP 1718	114	0.01	0.00	0.01	4.
29 SEP 0818	24	0.02	0.01	0.01	2.	*	29 SEP 1724	115	0.01	0.00	0.01	4.
29 SEP 0824	25	0.02	0.01	0.01	3.	*	29 SEP 1730	116	0.01	0.00	0.01	4.

29 SEP 0830	26	0.02	0.01	0.01	3.	*	29 SEP 1736	117	0.01	0.00	0.01	4.
29 SEP 0836	27	0.02	0.01	0.01	3.	*	29 SEP 1742	118	0.01	0.00	0.01	4.
29 SEP 0842	28	0.02	0.01	0.01	3.	*	29 SEP 1748	119	0.01	0.00	0.01	3.
29 SEP 0848	29	0.02	0.01	0.01	3.	*	29 SEP 1754	120	0.01	0.00	0.01	3.
29 SEP 0854	30	0.02	0.01	0.01	3.	*	29 SEP 1800	121	0.01	0.00	0.01	3.
29 SEP 0900	31	0.02	0.01	0.01	3.	*	29 SEP 1806	122	0.01	0.00	0.01	3.
29 SEP 0906	32	0.02	0.01	0.01	3.	*	29 SEP 1812	123	0.01	0.00	0.01	3.
29 SEP 0912	33	0.02	0.01	0.01	3.	*	29 SEP 1818	124	0.01	0.00	0.01	3.
29 SEP 0918	34	0.02	0.01	0.01	3.	*	29 SEP 1824	125	0.01	0.00	0.01	4.
29 SEP 0924	35	0.02	0.01	0.01	3.	*	29 SEP 1830	126	0.01	0.00	0.01	4.
29 SEP 0930	36	0.02	0.01	0.01	3.	*	29 SEP 1836	127	0.01	0.00	0.01	4.
29 SEP 0936	37	0.03	0.02	0.01	3.	*	29 SEP 1842	128	0.01	0.00	0.01	4.
29 SEP 0942	38	0.03	0.02	0.01	3.	*	29 SEP 1848	129	0.01	0.00	0.01	4.
29 SEP 0948	39	0.03	0.02	0.01	3.	*	29 SEP 1854	130	0.01	0.00	0.01	4.
29 SEP 0954	40	0.03	0.02	0.01	4.	*	29 SEP 1900	131	0.01	0.00	0.01	4.
29 SEP 1000	41	0.03	0.02	0.01	4.	*	29 SEP 1906	132	0.01	0.00	0.01	4.
29 SEP 1006	42	0.03	0.02	0.01	4.	*	29 SEP 1912	133	0.01	0.00	0.01	4.
29 SEP 1012	43	0.03	0.02	0.01	4.	*	29 SEP 1918	134	0.01	0.00	0.01	4.
29 SEP 1018	44	0.03	0.02	0.01	4.	*	29 SEP 1924	135	0.01	0.00	0.01	4.
29 SEP 1024	45	0.03	0.02	0.01	4.	*	29 SEP 1930	136	0.01	0.00	0.01	4.
29 SEP 1030	46	0.03	0.02	0.01	5.	*	29 SEP 1936	137	0.01	0.00	0.01	4.
29 SEP 1036	47	0.04	0.03	0.02	5.	*	29 SEP 1942	138	0.01	0.00	0.01	4.
29 SEP 1042	48	0.04	0.03	0.02	5.	*	29 SEP 1948	139	0.01	0.00	0.01	4.
29 SEP 1048	49	0.04	0.03	0.02	6.	*	29 SEP 1954	140	0.01	0.00	0.01	4.
29 SEP 1054	50	0.04	0.03	0.02	6.	*	29 SEP 2000	141	0.01	0.00	0.01	4.
29 SEP 1100	51	0.04	0.03	0.02	6.	*	29 SEP 2006	142	0.01	0.00	0.01	4.
29 SEP 1106	52	0.07	0.04	0.03	6.	*	29 SEP 2012	143	0.01	0.00	0.01	4.
29 SEP 1112	53	0.07	0.04	0.03	7.	*	29 SEP 2018	144	0.01	0.00	0.01	3.
29 SEP 1118	54	0.07	0.04	0.03	8.	*	29 SEP 2024	145	0.01	0.00	0.01	3.
29 SEP 1124	55	0.07	0.04	0.03	9.	*	29 SEP 2030	146	0.01	0.00	0.01	3.
29 SEP 1130	56	0.07	0.04	0.03	9.	*	29 SEP 2036	147	0.01	0.00	0.01	3.
29 SEP 1136	57	0.54	0.29	0.24	15.	*	29 SEP 2042	148	0.01	0.00	0.01	3.
29 SEP 1142	58	0.54	0.25	0.29	34.	*	29 SEP 2048	149	0.01	0.00	0.01	3.
29 SEP 1148	59	0.54	0.22	0.32	59.	*	29 SEP 2054	150	0.01	0.00	0.01	3.
29 SEP 1154	60	0.54	0.19	0.35	84.	*	29 SEP 2100	151	0.01	0.00	0.01	3.
29 SEP 1200	61	0.54	0.17	0.37	102.	*	29 SEP 2106	152	0.01	0.00	0.01	3.
29 SEP 1206	62	0.10	0.03	0.07	110.	*	29 SEP 2112	153	0.01	0.00	0.01	3.
29 SEP 1212	63	0.10	0.03	0.07	96.	*	29 SEP 2118	154	0.01	0.00	0.01	3.
29 SEP 1218	64	0.10	0.03	0.07	73.	*	29 SEP 2124	155	0.01	0.00	0.01	3.
29 SEP 1224	65	0.10	0.03	0.07	53.	*	29 SEP 2130	156	0.01	0.00	0.01	3.
29 SEP 1230	66	0.10	0.03	0.07	43.	*	29 SEP 2136	157	0.01	0.00	0.01	3.
29 SEP 1236	67	0.05	0.01	0.04	36.	*	29 SEP 2142	158	0.01	0.00	0.01	3.
29 SEP 1242	68	0.05	0.01	0.04	29.	*	29 SEP 2148	159	0.01	0.00	0.01	3.
29 SEP 1248	69	0.05	0.01	0.04	24.	*	29 SEP 2154	160	0.01	0.00	0.01	3.
29 SEP 1254	70	0.05	0.01	0.04	20.	*	29 SEP 2200	161	0.01	0.00	0.01	3.
29 SEP 1300	71	0.05	0.01	0.04	18.	*	29 SEP 2206	162	0.01	0.00	0.01	3.
29 SEP 1306	72	0.04	0.01	0.03	16.	*	29 SEP 2212	163	0.01	0.00	0.01	3.
29 SEP 1312	73	0.04	0.01	0.03	15.	*	29 SEP 2218	164	0.01	0.00	0.01	3.
29 SEP 1318	74	0.04	0.01	0.03	13.	*	29 SEP 2224	165	0.01	0.00	0.01	3.
29 SEP 1324	75	0.04	0.01	0.03	12.	*	29 SEP 2230	166	0.01	0.00	0.01	3.
29 SEP 1330	76	0.04	0.01	0.03	12.	*	29 SEP 2236	167	0.01	0.00	0.01	3.
29 SEP 1336	77	0.03	0.01	0.02	11.	*	29 SEP 2242	168	0.01	0.00	0.01	3.
29 SEP 1342	78	0.03	0.01	0.02	11.	*	29 SEP 2248	169	0.01	0.00	0.01	3.
29 SEP 1348	79	0.03	0.01	0.02	10.	*	29 SEP 2254	170	0.01	0.00	0.01	3.
29 SEP 1354	80	0.03	0.01	0.02	9.	*	29 SEP 2300	171	0.01	0.00	0.01	3.
29 SEP 1400	81	0.03	0.01	0.02	9.	*	29 SEP 2306	172	0.01	0.00	0.01	3.
29 SEP 1406	82	0.02	0.01	0.02	9.	*	29 SEP 2312	173	0.01	0.00	0.01	3.
29 SEP 1412	83	0.02	0.00	0.02	8.	*	29 SEP 2318	174	0.01	0.00	0.01	3.
29 SEP 1418	84	0.02	0.00	0.02	7.	*	29 SEP 2324	175	0.01	0.00	0.01	3.
29 SEP 1424	85	0.02	0.00	0.02	7.	*	29 SEP 2330	176	0.01	0.00	0.01	3.
29 SEP 1430	86	0.02	0.00	0.02	7.	*	29 SEP 2336	177	0.01	0.00	0.01	3.
29 SEP 1436	87	0.02	0.00	0.02	6.	*	29 SEP 2342	178	0.01	0.00	0.01	3.
29 SEP 1442	88	0.02	0.00	0.02	6.	*	29 SEP 2348	179	0.01	0.00	0.01	3.
29 SEP 1448	89	0.02	0.00	0.02	6.	*	29 SEP 2354	180	0.01	0.00	0.01	3.
29 SEP 1454	90	0.02	0.00	0.02	6.	*	30 SEP 0000	181	0.01	0.00	0.01	3.
29 SEP 1500	91	0.02	0.00	0.02	6.	*						
						*						

****

TOTAL RAINFALL = 6.50, TOTAL LOSS = 2.57, TOTAL EXCESS = 3.93

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	18.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 110.	6.10		19.	8.	8.	8.
		(INCHES)	2.974	3.903	3.903	3.903
		(AC-FT)	9.	12.	12.	12.

CUMULATIVE AREA = 0.06 SQ MI

*** ***

```
          **************
          *            *
 14 KK    *        2   *
          *            *
          **************

  3 IN        TIME DATA FOR INPUT TIME SERIES
                JXMIN         30  TIME INTERVAL IN MINUTES
                JXDATE    29SEP92  STARTING DATE
                JXTIME       600  STARTING TIME

            SUBBASIN RUNOFF DATA

 15 BA        SUBBASIN CHARACTERISTICS
                TAREA       0.02  SUBBASIN AREA

              PRECIPITATION DATA

 16 PB          STORM       7.80  BASIN TOTAL PRECIPITATION

 17 PI          INCREMENTAL PRECIPITATION PATTERN
```

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.08	0.08	0.08	0.08	0.08
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

```
 21 LS        SCS LOSS RATE
                STRTL       1.28  INITIAL ABSTRACTION
                CRVNBR     61.00  CURVE NUMBER
                RTIMP      38.00  PERCENT IMPERVIOUS AREA

 22 UD        SCS DIMENSIONLESS UNITGRAPH
                TLAG        0.15  LAG

                                        ***

WARNING *** TIME INTERVAL IS GREATER THAN .29*LAG

                                   UNIT HYDROGRAPH
                               10 END-OF-PERIOD ORDINATES
        20.      42.      28.      12.       5.       2.       1.       0.       0.       0.
```

****

HYDROGRAPH AT STATION 2

****

DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	*	DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
29 SEP 0600	1	0.00	0.00	0.00	0.	*	29 SEP 1506	92	0.03	0.00	0.02	2.
29 SEP 0606	2	0.02	0.01	0.01	0.	*	29 SEP 1512	93	0.03	0.00	0.02	2.
29 SEP 0612	3	0.02	0.01	0.01	0.	*	29 SEP 1518	94	0.03	0.00	0.02	2.
29 SEP 0618	4	0.02	0.01	0.01	1.	*	29 SEP 1524	95	0.03	0.00	0.02	2.
29 SEP 0624	5	0.02	0.01	0.01	1.	*	29 SEP 1530	96	0.03	0.00	0.02	2.
29 SEP 0630	6	0.02	0.01	0.01	1.	*	29 SEP 1536	97	0.03	0.00	0.02	2.
29 SEP 0636	7	0.02	0.01	0.01	1.	*	29 SEP 1542	98	0.03	0.00	0.02	2.
29 SEP 0642	8	0.02	0.01	0.01	1.	*	29 SEP 1548	99	0.03	0.00	0.02	2.
29 SEP 0648	9	0.02	0.01	0.01	1.	*	29 SEP 1554	100	0.03	0.00	0.02	2.

29 SEP 0654	10	0.02	0.01	0.01	1.	*	29 SEP 1600	101	0.03	0.00	0.02	2.
29 SEP 0700	11	0.02	0.01	0.01	1.	*	29 SEP 1606	102	0.02	0.00	0.01	2.
29 SEP 0706	12	0.02	0.01	0.01	1.	*	29 SEP 1612	103	0.02	0.00	0.01	2.
29 SEP 0712	13	0.02	0.01	0.01	1.	*	29 SEP 1618	104	0.02	0.00	0.01	2.
29 SEP 0718	14	0.02	0.01	0.01	1.	*	29 SEP 1624	105	0.02	0.00	0.01	2.
29 SEP 0724	15	0.02	0.01	0.01	1.	*	29 SEP 1630	106	0.02	0.00	0.01	2.
29 SEP 0730	16	0.02	0.01	0.01	1.	*	29 SEP 1636	107	0.02	0.00	0.01	2.
29 SEP 0736	17	0.02	0.01	0.01	1.	*	29 SEP 1642	108	0.02	0.00	0.01	2.
29 SEP 0742	18	0.02	0.01	0.01	1.	*	29 SEP 1648	109	0.02	0.00	0.01	2.
29 SEP 0748	19	0.02	0.01	0.01	1.	*	29 SEP 1654	110	0.02	0.00	0.01	2.
29 SEP 0754	20	0.02	0.01	0.01	1.	*	29 SEP 1700	111	0.02	0.00	0.01	2.
29 SEP 0800	21	0.02	0.01	0.01	1.	*	29 SEP 1706	112	0.02	0.00	0.01	2.
29 SEP 0806	22	0.02	0.01	0.01	1.	*	29 SEP 1712	113	0.02	0.00	0.01	2.
29 SEP 0812	23	0.02	0.01	0.01	1.	*	29 SEP 1718	114	0.02	0.00	0.01	2.
29 SEP 0818	24	0.02	0.01	0.01	1.	*	29 SEP 1724	115	0.02	0.00	0.01	2.
29 SEP 0824	25	0.02	0.01	0.01	1.	*	29 SEP 1730	116	0.02	0.00	0.01	2.
29 SEP 0830	26	0.02	0.01	0.01	1.	*	29 SEP 1736	117	0.01	0.00	0.01	1.
29 SEP 0836	27	0.02	0.01	0.01	1.	*	29 SEP 1742	118	0.01	0.00	0.01	1.
29 SEP 0842	28	0.02	0.01	0.01	1.	*	29 SEP 1748	119	0.01	0.00	0.01	1.
29 SEP 0848	29	0.02	0.01	0.01	1.	*	29 SEP 1754	120	0.01	0.00	0.01	1.
29 SEP 0854	30	0.02	0.01	0.01	1.	*	29 SEP 1800	121	0.01	0.00	0.01	1.
29 SEP 0900	31	0.02	0.01	0.01	1.	*	29 SEP 1806	122	0.02	0.00	0.01	1.
29 SEP 0906	32	0.03	0.02	0.01	1.	*	29 SEP 1812	123	0.02	0.00	0.01	1.
29 SEP 0912	33	0.03	0.02	0.01	1.	*	29 SEP 1818	124	0.02	0.00	0.01	1.
29 SEP 0918	34	0.03	0.02	0.01	1.	*	29 SEP 1824	125	0.02	0.00	0.01	1.
29 SEP 0924	35	0.03	0.02	0.01	1.	*	29 SEP 1830	126	0.02	0.00	0.01	1.
29 SEP 0930	36	0.03	0.02	0.01	1.	*	29 SEP 1836	127	0.02	0.00	0.01	1.
29 SEP 0936	37	0.03	0.02	0.01	1.	*	29 SEP 1842	128	0.02	0.00	0.01	1.
29 SEP 0942	38	0.03	0.02	0.01	1.	*	29 SEP 1848	129	0.02	0.00	0.01	1.
29 SEP 0948	39	0.03	0.02	0.01	1.	*	29 SEP 1854	130	0.02	0.00	0.01	1.
29 SEP 0954	40	0.03	0.02	0.01	1.	*	29 SEP 1900	131	0.02	0.00	0.01	1.
29 SEP 1000	41	0.03	0.02	0.01	1.	*	29 SEP 1906	132	0.02	0.00	0.01	1.
29 SEP 1006	42	0.04	0.02	0.01	1.	*	29 SEP 1912	133	0.02	0.00	0.01	1.
29 SEP 1012	43	0.04	0.02	0.01	1.	*	29 SEP 1918	134	0.02	0.00	0.01	1.
29 SEP 1018	44	0.04	0.02	0.01	2.	*	29 SEP 1924	135	0.02	0.00	0.01	1.
29 SEP 1024	45	0.04	0.02	0.01	2.	*	29 SEP 1930	136	0.02	0.00	0.01	1.
29 SEP 1030	46	0.04	0.02	0.01	2.	*	29 SEP 1936	137	0.02	0.00	0.01	1.
29 SEP 1036	47	0.05	0.03	0.02	2.	*	29 SEP 1942	138	0.02	0.00	0.01	1.
29 SEP 1042	48	0.05	0.03	0.02	2.	*	29 SEP 1948	139	0.02	0.00	0.01	1.
29 SEP 1048	49	0.05	0.03	0.02	2.	*	29 SEP 1954	140	0.02	0.00	0.01	1.
29 SEP 1054	50	0.05	0.03	0.02	2.	*	29 SEP 2000	141	0.02	0.00	0.01	1.
29 SEP 1100	51	0.05	0.03	0.02	2.	*	29 SEP 2006	142	0.01	0.00	0.01	1.
29 SEP 1106	52	0.08	0.05	0.03	2.	*	29 SEP 2012	143	0.01	0.00	0.01	1.
29 SEP 1112	53	0.08	0.05	0.03	3.	*	29 SEP 2018	144	0.01	0.00	0.01	1.
29 SEP 1118	54	0.08	0.05	0.03	3.	*	29 SEP 2024	145	0.01	0.00	0.01	1.
29 SEP 1124	55	0.08	0.05	0.04	4.	*	29 SEP 2030	146	0.01	0.00	0.01	1.
29 SEP 1130	56	0.08	0.04	0.04	4.	*	29 SEP 2036	147	0.01	0.00	0.01	1.
29 SEP 1136	57	0.64	0.32	0.32	10.	*	29 SEP 2042	148	0.01	0.00	0.01	1.
29 SEP 1142	58	0.64	0.27	0.38	23.	*	29 SEP 2048	149	0.01	0.00	0.01	1.
29 SEP 1148	59	0.64	0.23	0.42	34.	*	29 SEP 2054	150	0.01	0.00	0.01	1.
29 SEP 1154	60	0.64	0.20	0.45	41.	*	29 SEP 2100	151	0.01	0.00	0.01	1.
29 SEP 1200	61	0.64	0.17	0.47	46.	*	29 SEP 2106	152	0.01	0.00	0.01	1.
29 SEP 1206	62	0.12	0.03	0.09	42.	*	29 SEP 2112	153	0.01	0.00	0.01	1.
29 SEP 1212	63	0.12	0.03	0.09	28.	*	29 SEP 2118	154	0.01	0.00	0.01	1.
29 SEP 1218	64	0.12	0.03	0.09	18.	*	29 SEP 2124	155	0.01	0.00	0.01	1.
29 SEP 1224	65	0.12	0.03	0.09	14.	*	29 SEP 2130	156	0.01	0.00	0.01	1.
29 SEP 1230	66	0.12	0.03	0.09	12.	*	29 SEP 2136	157	0.01	0.00	0.01	1.
29 SEP 1236	67	0.06	0.01	0.05	10.	*	29 SEP 2142	158	0.01	0.00	0.01	1.
29 SEP 1242	68	0.06	0.01	0.05	8.	*	29 SEP 2148	159	0.01	0.00	0.01	1.
29 SEP 1248	69	0.06	0.01	0.05	6.	*	29 SEP 2154	160	0.01	0.00	0.01	1.
29 SEP 1254	70	0.06	0.01	0.05	6.	*	29 SEP 2200	161	0.01	0.00	0.01	1.
29 SEP 1300	71	0.06	0.01	0.05	6.	*	29 SEP 2206	162	0.01	0.00	0.01	1.
29 SEP 1306	72	0.05	0.01	0.04	5.	*	29 SEP 2212	163	0.01	0.00	0.01	1.
29 SEP 1312	73	0.05	0.01	0.04	5.	*	29 SEP 2218	164	0.01	0.00	0.01	1.
29 SEP 1318	74	0.05	0.01	0.04	4.	*	29 SEP 2224	165	0.01	0.00	0.01	1.
29 SEP 1324	75	0.05	0.01	0.04	4.	*	29 SEP 2230	166	0.01	0.00	0.01	1.
29 SEP 1330	76	0.05	0.01	0.04	4.	*	29 SEP 2236	167	0.01	0.00	0.01	1.
29 SEP 1336	77	0.04	0.01	0.03	4.	*	29 SEP 2242	168	0.01	0.00	0.01	1.
29 SEP 1342	78	0.04	0.01	0.03	4.	*	29 SEP 2248	169	0.01	0.00	0.01	1.
29 SEP 1348	79	0.04	0.01	0.03	3.	*	29 SEP 2254	170	0.01	0.00	0.01	1.
29 SEP 1354	80	0.04	0.01	0.03	3.	*	29 SEP 2300	171	0.01	0.00	0.01	1.
29 SEP 1400	81	0.04	0.01	0.03	3.	*	29 SEP 2306	172	0.01	0.00	0.01	1.
29 SEP 1406	82	0.03	0.00	0.02	3.	*	29 SEP 2312	173	0.01	0.00	0.01	1.
29 SEP 1412	83	0.03	0.00	0.02	3.	*	29 SEP 2318	174	0.01	0.00	0.01	1.
29 SEP 1418	84	0.03	0.00	0.02	2.	*	29 SEP 2324	175	0.01	0.00	0.01	1.
29 SEP 1424	85	0.03	0.00	0.02	2.	*	29 SEP 2330	176	0.01	0.00	0.01	1.
29 SEP 1430	86	0.03	0.00	0.02	2.	*	29 SEP 2336	177	0.01	0.00	0.01	1.
29 SEP 1436	87	0.03	0.00	0.02	2.	*	29 SEP 2342	178	0.01	0.00	0.01	1.
29 SEP 1442	88	0.03	0.00	0.02	2.	*	29 SEP 2348	179	0.01	0.00	0.01	1.
29 SEP 1448	89	0.03	0.00	0.02	2.	*	29 SEP 2354	180	0.01	0.00	0.01	1.

```
      29 SEP 1454   90    0.03    0.00    0.02         2.      *      30 SEP 0000  181    0.01    0.00    0.01         1.
      29 SEP 1500   91    0.03    0.00    0.02         2.      *
                                                                *
*******************************************************************************************************************************

    TOTAL RAINFALL =    7.80, TOTAL LOSS =    2.79, TOTAL EXCESS =    5.01

  PEAK FLOW     TIME                        MAXIMUM AVERAGE FLOW
                                 6-HR       24-HR      72-HR      18.00-HR
+   (CFS)       (HR)
                          (CFS)
+      46.       6.00                7.         3.         3.          3.
                        (INCHES)  3.828      4.987      4.987       4.987
                         (AC-FT)     4.         5.         5.          5.

                      CUMULATIVE AREA =    0.02 SQ MI



*** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** ***


            **************
            *            *
   23 KK    *    5.1AC   *
            *            *
            **************

    3 IN         TIME DATA FOR INPUT TIME SERIES
                       JXMIN          30  TIME INTERVAL IN MINUTES
                      JXDATE     29SEP92  STARTING DATE
                      JXTIME         600  STARTING TIME

               SUBBASIN RUNOFF DATA

   24 BA         SUBBASIN CHARACTERISTICS
                       TAREA        0.01  SUBBASIN AREA

                 PRECIPITATION DATA

   25 PB               STORM        7.80  BASIN TOTAL PRECIPITATION

   26 PI           INCREMENTAL PRECIPITATION PATTERN
                      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                      0.00      0.00      0.00      0.00      0.00      0.01      0.01      0.01      0.01      0.01
                      0.01      0.01      0.01      0.01      0.01      0.08      0.08      0.08      0.08      0.08
                      0.01      0.01      0.01      0.01      0.01      0.01      0.01      0.01      0.01      0.01
                      0.01      0.01      0.01      0.01      0.01      0.00      0.00      0.00      0.00      0.00
                      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00

   30 LS         SCS LOSS RATE
                       STRTL        0.67  INITIAL ABSTRACTION
                      CRVNBR       75.00  CURVE NUMBER
                       RTIMP        0.00  PERCENT IMPERVIOUS AREA

   31 UD         SCS DIMENSIONLESS UNITGRAPH
                        TLAG        0.15  LAG

                                                                ***

WARNING *** TIME INTERVAL IS GREATER THAN .29*LAG

                                                          UNIT HYDROGRAPH
                                                      10 END-OF-PERIOD ORDINATES
                 9.        19.        13.         5.         2.         1.         0.         0.         0.         0.
*******************************************************************************************************************************
```

HYDROGRAPH AT STATION 5.1AC

DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
29 SEP 0600	1	0.00	0.00	0.00	0.	29 SEP 1506	92	0.03	0.00	0.02	1.
29 SEP 0606	2	0.02	0.02	0.00	0.	29 SEP 1512	93	0.03	0.00	0.02	1.
29 SEP 0612	3	0.02	0.02	0.00	0.	29 SEP 1518	94	0.03	0.00	0.02	1.
29 SEP 0618	4	0.02	0.02	0.00	0.	29 SEP 1524	95	0.03	0.00	0.02	1.
29 SEP 0624	5	0.02	0.02	0.00	0.	29 SEP 1530	96	0.03	0.00	0.02	1.
29 SEP 0630	6	0.02	0.02	0.00	0.	29 SEP 1536	97	0.03	0.00	0.02	1.
29 SEP 0636	7	0.02	0.02	0.00	0.	29 SEP 1542	98	0.03	0.00	0.02	1.
29 SEP 0642	8	0.02	0.02	0.00	0.	29 SEP 1548	99	0.03	0.00	0.02	1.
29 SEP 0648	9	0.02	0.02	0.00	0.	29 SEP 1554	100	0.03	0.00	0.02	1.
29 SEP 0654	10	0.02	0.02	0.00	0.	29 SEP 1600	101	0.03	0.00	0.02	1.
29 SEP 0700	11	0.02	0.02	0.00	0.	29 SEP 1606	102	0.02	0.00	0.01	1.
29 SEP 0706	12	0.02	0.02	0.00	0.	29 SEP 1612	103	0.02	0.00	0.01	1.
29 SEP 0712	13	0.02	0.02	0.00	0.	29 SEP 1618	104	0.02	0.00	0.01	1.
29 SEP 0718	14	0.02	0.02	0.00	0.	29 SEP 1624	105	0.02	0.00	0.01	1.
29 SEP 0724	15	0.02	0.02	0.00	0.	29 SEP 1630	106	0.02	0.00	0.01	1.
29 SEP 0730	16	0.02	0.02	0.00	0.	29 SEP 1636	107	0.02	0.00	0.01	1.
29 SEP 0736	17	0.02	0.02	0.00	0.	29 SEP 1642	108	0.02	0.00	0.01	1.
29 SEP 0742	18	0.02	0.02	0.00	0.	29 SEP 1648	109	0.02	0.00	0.01	1.
29 SEP 0748	19	0.02	0.02	0.00	0.	29 SEP 1654	110	0.02	0.00	0.01	1.
29 SEP 0754	20	0.02	0.02	0.00	0.	29 SEP 1700	111	0.02	0.00	0.01	1.
29 SEP 0800	21	0.02	0.02	0.00	0.	29 SEP 1706	112	0.02	0.00	0.01	1.
29 SEP 0806	22	0.02	0.02	0.00	0.	29 SEP 1712	113	0.02	0.00	0.01	1.
29 SEP 0812	23	0.02	0.02	0.00	0.	29 SEP 1718	114	0.02	0.00	0.01	1.
29 SEP 0818	24	0.02	0.02	0.00	0.	29 SEP 1724	115	0.02	0.00	0.01	1.
29 SEP 0824	25	0.02	0.02	0.00	0.	29 SEP 1730	116	0.02	0.00	0.01	1.
29 SEP 0830	26	0.02	0.02	0.00	0.	29 SEP 1736	117	0.01	0.00	0.01	1.
29 SEP 0836	27	0.02	0.02	0.00	0.	29 SEP 1742	118	0.01	0.00	0.01	1.
29 SEP 0842	28	0.02	0.02	0.00	0.	29 SEP 1748	119	0.01	0.00	0.01	1.
29 SEP 0848	29	0.02	0.02	0.00	0.	29 SEP 1754	120	0.01	0.00	0.01	0.
29 SEP 0854	30	0.02	0.02	0.00	0.	29 SEP 1800	121	0.01	0.00	0.01	0.
29 SEP 0900	31	0.02	0.02	0.00	0.	29 SEP 1806	122	0.02	0.00	0.01	1.
29 SEP 0906	32	0.03	0.03	0.00	0.	29 SEP 1812	123	0.02	0.00	0.01	1.
29 SEP 0912	33	0.03	0.03	0.00	0.	29 SEP 1818	124	0.02	0.00	0.01	1.
29 SEP 0918	34	0.03	0.03	0.00	0.	29 SEP 1824	125	0.02	0.00	0.01	1.
29 SEP 0924	35	0.03	0.03	0.00	0.	29 SEP 1830	126	0.02	0.00	0.01	1.
29 SEP 0930	36	0.03	0.03	0.00	0.	29 SEP 1836	127	0.02	0.00	0.01	1.
29 SEP 0936	37	0.03	0.03	0.00	0.	29 SEP 1842	128	0.02	0.00	0.01	1.
29 SEP 0942	38	0.03	0.03	0.00	0.	29 SEP 1848	129	0.02	0.00	0.01	1.
29 SEP 0948	39	0.03	0.03	0.00	0.	29 SEP 1854	130	0.02	0.00	0.01	1.
29 SEP 0954	40	0.03	0.03	0.00	0.	29 SEP 1900	131	0.02	0.00	0.01	1.
29 SEP 1000	41	0.03	0.03	0.00	0.	29 SEP 1906	132	0.02	0.00	0.01	1.
29 SEP 1006	42	0.04	0.03	0.00	0.	29 SEP 1912	133	0.02	0.00	0.01	1.
29 SEP 1012	43	0.04	0.03	0.01	0.	29 SEP 1918	134	0.02	0.00	0.01	1.
29 SEP 1018	44	0.04	0.03	0.01	0.	29 SEP 1924	135	0.02	0.00	0.01	1.
29 SEP 1024	45	0.04	0.03	0.01	0.	29 SEP 1930	136	0.02	0.00	0.01	1.
29 SEP 1030	46	0.04	0.03	0.01	0.	29 SEP 1936	137	0.02	0.00	0.01	1.
29 SEP 1036	47	0.05	0.04	0.01	0.	29 SEP 1942	138	0.02	0.00	0.01	1.
29 SEP 1042	48	0.05	0.04	0.01	0.	29 SEP 1948	139	0.02	0.00	0.01	1.
29 SEP 1048	49	0.05	0.04	0.01	1.	29 SEP 1954	140	0.02	0.00	0.01	1.
29 SEP 1054	50	0.05	0.04	0.01	1.	29 SEP 2000	141	0.02	0.00	0.01	1.
29 SEP 1100	51	0.05	0.04	0.02	1.	29 SEP 2006	142	0.01	0.00	0.01	1.
29 SEP 1106	52	0.08	0.06	0.03	1.	29 SEP 2012	143	0.01	0.00	0.01	1.
29 SEP 1112	53	0.08	0.05	0.03	1.	29 SEP 2018	144	0.01	0.00	0.01	1.
29 SEP 1118	54	0.08	0.05	0.03	1.	29 SEP 2024	145	0.01	0.00	0.01	0.
29 SEP 1124	55	0.08	0.05	0.03	1.	29 SEP 2030	146	0.01	0.00	0.01	0.
29 SEP 1130	56	0.08	0.05	0.03	2.	29 SEP 2036	147	0.01	0.00	0.01	0.
29 SEP 1136	57	0.64	0.32	0.32	4.	29 SEP 2042	148	0.01	0.00	0.01	0.
29 SEP 1142	58	0.64	0.25	0.39	11.	29 SEP 2048	149	0.01	0.00	0.01	0.
29 SEP 1148	59	0.64	0.20	0.44	16.	29 SEP 2054	150	0.01	0.00	0.01	0.
29 SEP 1154	60	0.64	0.16	0.48	20.	29 SEP 2100	151	0.01	0.00	0.01	0.
29 SEP 1200	61	0.64	0.14	0.51	23.	29 SEP 2106	152	0.01	0.00	0.01	0.
29 SEP 1206	62	0.12	0.02	0.10	21.	29 SEP 2112	153	0.01	0.00	0.01	0.
29 SEP 1212	63	0.12	0.02	0.10	14.	29 SEP 2118	154	0.01	0.00	0.01	0.
29 SEP 1218	64	0.12	0.02	0.10	9.	29 SEP 2124	155	0.01	0.00	0.01	0.
29 SEP 1224	65	0.12	0.02	0.10	7.	29 SEP 2130	156	0.01	0.00	0.01	0.
29 SEP 1230	66	0.12	0.02	0.10	6.	29 SEP 2136	157	0.01	0.00	0.01	0.
29 SEP 1236	67	0.06	0.01	0.05	5.	29 SEP 2142	158	0.01	0.00	0.01	0.
29 SEP 1242	68	0.06	0.01	0.05	4.	29 SEP 2148	159	0.01	0.00	0.01	0.
29 SEP 1248	69	0.06	0.01	0.05	3.	29 SEP 2154	160	0.01	0.00	0.01	0.
29 SEP 1254	70	0.06	0.01	0.05	3.	29 SEP 2200	161	0.01	0.00	0.01	0.
29 SEP 1300	71	0.06	0.01	0.05	3.	29 SEP 2206	162	0.01	0.00	0.01	0.
29 SEP 1306	72	0.05	0.01	0.04	3.	29 SEP 2212	163	0.01	0.00	0.01	0.
29 SEP 1312	73	0.05	0.01	0.04	2.	29 SEP 2218	164	0.01	0.00	0.01	0.

29	SEP	1318	74	0.05	0.01	0.04	2.	*	29	SEP	2224	165	0.01	0.00	0.01	0.
29	SEP	1324	75	0.05	0.01	0.04	2.	*	29	SEP	2230	166	0.01	0.00	0.01	0.
29	SEP	1330	76	0.05	0.01	0.04	2.	*	29	SEP	2236	167	0.01	0.00	0.01	0.
29	SEP	1336	77	0.04	0.01	0.03	2.	*	29	SEP	2242	168	0.01	0.00	0.01	0.
29	SEP	1342	78	0.04	0.01	0.03	2.	*	29	SEP	2248	169	0.01	0.00	0.01	0.
29	SEP	1348	79	0.04	0.01	0.03	2.	*	29	SEP	2254	170	0.01	0.00	0.01	0.
29	SEP	1354	80	0.04	0.01	0.03	2.	*	29	SEP	2300	171	0.01	0.00	0.01	0.
29	SEP	1400	81	0.04	0.00	0.03	2.	*	29	SEP	2306	172	0.01	0.00	0.01	0.
29	SEP	1406	82	0.03	0.00	0.02	2.	*	29	SEP	2312	173	0.01	0.00	0.01	0.
29	SEP	1412	83	0.03	0.00	0.02	1.	*	29	SEP	2318	174	0.01	0.00	0.01	0.
29	SEP	1418	84	0.03	0.00	0.02	1.	*	29	SEP	2324	175	0.01	0.00	0.01	0.
29	SEP	1424	85	0.03	0.00	0.02	1.	*	29	SEP	2330	176	0.01	0.00	0.01	0.
29	SEP	1430	86	0.03	0.00	0.02	1.	*	29	SEP	2336	177	0.01	0.00	0.01	0.
29	SEP	1436	87	0.03	0.00	0.02	1.	*	29	SEP	2342	178	0.01	0.00	0.01	0.
29	SEP	1442	88	0.03	0.00	0.02	1.	*	29	SEP	2348	179	0.01	0.00	0.01	0.
29	SEP	1448	89	0.03	0.00	0.02	1.	*	29	SEP	2354	180	0.01	0.00	0.01	0.
29	SEP	1454	90	0.03	0.00	0.02	1.	*	30	SEP	0000	181	0.01	0.00	0.01	0.
29	SEP	1500	91	0.03	0.00	0.02	1.	*								

****

TOTAL RAINFALL = 7.80, TOTAL LOSS = 2.94, TOTAL EXCESS = 4.86

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	18.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 23.	6.00		3.	1.	1.	1.
		(INCHES)	4.000	4.842	4.842	4.842
		(AC-FT)	2.	2.	2.	2.

CUMULATIVE AREA = 0.01 SQ MI

*** ***

```
          **************
          *            *
32 KK     *    INTO2   *
          *            *
          **************
```

33 HC HYDROGRAPH COMBINATION
ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

***

****

HYDROGRAPH AT STATION INTO2
SUM OF 3 HYDROGRAPHS

****

DA MON HRMN	ORD	FLOW	DA MON HRMN	ORD	FLOW	DA MON HRMN	ORD	FLOW	DA MON HRMN	ORD	FLOW
29 SEP 0600	1	0.	29 SEP 1036	47	7.	29 SEP 1512	93	10.	29 SEP 1948	139	6.
29 SEP 0606	2	0.	29 SEP 1042	48	8.	29 SEP 1518	94	10.	29 SEP 1954	140	6.
29 SEP 0612	3	1.	29 SEP 1048	49	8.	29 SEP 1524	95	10.	29 SEP 2000	141	6.
29 SEP 0618	4	2.	29 SEP 1054	50	9.	29 SEP 1530	96	10.	29 SEP 2006	142	6.
29 SEP 0624	5	2.	29 SEP 1100	51	9.	29 SEP 1536	97	10.	29 SEP 2012	143	5.
29 SEP 0630	6	2.	29 SEP 1106	52	10.	29 SEP 1542	98	10.	29 SEP 2018	144	5.
29 SEP 0636	7	3.	29 SEP 1112	53	11.	29 SEP 1548	99	10.	29 SEP 2024	145	4.
29 SEP 0642	8	3.	29 SEP 1118	54	13.	29 SEP 1554	100	10.	29 SEP 2030	146	4.
29 SEP 0648	9	3.	29 SEP 1124	55	14.	29 SEP 1600	101	10.	29 SEP 2036	147	4.
29 SEP 0654	10	3.	29 SEP 1130	56	15.	29 SEP 1606	102	9.	29 SEP 2042	148	4.
29 SEP 0700	11	3.	29 SEP 1136	57	29.	29 SEP 1612	103	9.	29 SEP 2048	149	4.
29 SEP 0706	12	3.	29 SEP 1142	58	67.	29 SEP 1618	104	8.	29 SEP 2054	150	4.
29 SEP 0712	13	3.	29 SEP 1148	59	109.	29 SEP 1624	105	7.	29 SEP 2100	151	4.
29 SEP 0718	14	3.	29 SEP 1154	60	145.	29 SEP 1630	106	7.	29 SEP 2106	152	4.
29 SEP 0724	15	3.	29 SEP 1200	61	171.	29 SEP 1636	107	7.	29 SEP 2112	153	4.
29 SEP 0730	16	3.	29 SEP 1206	62	172.	29 SEP 1642	108	7.	29 SEP 2118	154	4.
29 SEP 0736	17	3.	29 SEP 1212	63	138.	29 SEP 1648	109	7.	29 SEP 2124	155	4.
29 SEP 0742	18	3.	29 SEP 1218	64	100.	29 SEP 1654	110	7.	29 SEP 2130	156	4.
29 SEP 0748	19	3.	29 SEP 1224	65	74.	29 SEP 1700	111	7.	29 SEP 2136	157	4.
29 SEP 0754	20	3.	29 SEP 1230	66	60.	29 SEP 1706	112	7.	29 SEP 2142	158	4.
29 SEP 0800	21	3.	29 SEP 1236	67	51.	29 SEP 1712	113	7.	29 SEP 2148	159	4.

29 SEP 0806	22	3.	*	29 SEP 1242	68	41.	*	29 SEP 1718	114	7.	*	29 SEP 2154	160	4.
29 SEP 0812	23	3.	*	29 SEP 1248	69	34.	*	29 SEP 1724	115	7.	*	29 SEP 2200	161	4.
29 SEP 0818	24	3.	*	29 SEP 1254	70	29.	*	29 SEP 1730	116	7.	*	29 SEP 2206	162	4.
29 SEP 0824	25	3.	*	29 SEP 1300	71	26.	*	29 SEP 1736	117	6.	*	29 SEP 2212	163	4.
29 SEP 0830	26	4.	*	29 SEP 1306	72	24.	*	29 SEP 1742	118	6.	*	29 SEP 2218	164	4.
29 SEP 0836	27	4.	*	29 SEP 1312	73	22.	*	29 SEP 1748	119	5.	*	29 SEP 2224	165	4.
29 SEP 0842	28	4.	*	29 SEP 1318	74	20.	*	29 SEP 1754	120	4.	*	29 SEP 2230	166	4.
29 SEP 0848	29	4.	*	29 SEP 1324	75	18.	*	29 SEP 1800	121	4.	*	29 SEP 2236	167	4.
29 SEP 0854	30	4.	*	29 SEP 1330	76	18.	*	29 SEP 1806	122	4.	*	29 SEP 2242	168	4.
29 SEP 0900	31	4.	*	29 SEP 1336	77	17.	*	29 SEP 1812	123	5.	*	29 SEP 2248	169	4.
29 SEP 0906	32	4.	*	29 SEP 1342	78	16.	*	29 SEP 1818	124	5.	*	29 SEP 2254	170	4.
29 SEP 0912	33	4.	*	29 SEP 1348	79	15.	*	29 SEP 1824	125	6.	*	29 SEP 2300	171	4.
29 SEP 0918	34	4.	*	29 SEP 1354	80	14.	*	29 SEP 1830	126	6.	*	29 SEP 2306	172	4.
29 SEP 0924	35	4.	*	29 SEP 1400	81	14.	*	29 SEP 1836	127	6.	*	29 SEP 2312	173	4.
29 SEP 0930	36	4.	*	29 SEP 1406	82	13.	*	29 SEP 1842	128	6.	*	29 SEP 2318	174	4.
29 SEP 0936	37	4.	*	29 SEP 1412	83	12.	*	29 SEP 1848	129	6.	*	29 SEP 2324	175	4.
29 SEP 0942	38	5.	*	29 SEP 1418	84	11.	*	29 SEP 1854	130	6.	*	29 SEP 2330	176	4.
29 SEP 0948	39	5.	*	29 SEP 1424	85	10.	*	29 SEP 1900	131	6.	*	29 SEP 2336	177	4.
29 SEP 0954	40	5.	*	29 SEP 1430	86	10.	*	29 SEP 1906	132	6.	*	29 SEP 2342	178	4.
29 SEP 1000	41	5.	*	29 SEP 1436	87	10.	*	29 SEP 1912	133	6.	*	29 SEP 2348	179	4.
29 SEP 1006	42	5.	*	29 SEP 1442	88	10.	*	29 SEP 1918	134	6.	*	29 SEP 2354	180	4.
29 SEP 1012	43	6.	*	29 SEP 1448	89	10.	*	29 SEP 1924	135	6.	*	30 SEP 0000	181	4.
29 SEP 1018	44	6.	*	29 SEP 1454	90	10.	*	29 SEP 1930	136	6.	*			
29 SEP 1024	45	6.	*	29 SEP 1500	91	10.	*	29 SEP 1936	137	6.	*			
29 SEP 1030	46	7.	*	29 SEP 1506	92	10.	*	29 SEP 1942	138	6.	*			
			*				*				*			

****

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	18.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 172.	6.10		29.	13.	13.	13.
		(INCHES)	3.242	4.212	4.212	4.212
		(AC-FT)	15.	19.	19.	19.

CUMULATIVE AREA = 0.08 SQ MI

*** ***

```
          **************
          *            *
34 KK     *    POND2   *
          *            *
          **************
```

HYDROGRAPH ROUTING DATA

35 RS STORAGE ROUTING

NSTPS	1	NUMBER OF SUBREACHES
ITYP	ELEV	TYPE OF INITIAL CONDITION
RSVRIC	1345.40	INITIAL CONDITION
X	0.00	WORKING R AND D COEFFICIENT

36 SA	AREA	1.2	1.6								
37 SE	ELEVATION	1345.40	1349.00								
38 SQ	DISCHARGE	0.	10.	20.	30.	40.	50.	60.	70.	80.	90.
		100.									
40 SE	ELEVATION	1345.40	1345.70	1345.88	1346.03	1346.16	1346.29	1346.40	1346.72	1347.80	1349.02
		1350.40									

***

COMPUTED STORAGE-ELEVATION DATA

STORAGE	0.00	5.02
ELEVATION	1345.40	1349.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	0.00	0.36	0.59	0.78	0.94	1.11	1.25	1.68	3.19	5.02
OUTFLOW	0.00	10.00	20.00	30.00	40.00	50.00	60.00	70.00	80.00	89.84
ELEVATION	1345.40	1345.70	1345.88	1346.03	1346.16	1346.29	1346.40	1346.72	1347.80	1349.00

STORAGE	5.05	7.38
OUTFLOW	90.00	100.00
ELEVATION	1349.02	1350.40

HYDROGRAPH AT STATION POND2

DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE
29	SEP	0600	1	0.	0.0	1345.4	29	SEP	1206	62	80.	3.2	1347.8	29	SEP	1812	123	5.	0.2	1345.6
29	SEP	0606	2	0.	0.0	1345.4	29	SEP	1212	63	83.	3.8	1348.2	29	SEP	1818	124	5.	0.2	1345.6
29	SEP	0612	3	0.	0.0	1345.4	29	SEP	1218	64	85.	4.1	1348.4	29	SEP	1824	125	5.	0.2	1345.6
29	SEP	0618	4	0.	0.0	1345.4	29	SEP	1224	65	85.	4.1	1348.4	29	SEP	1830	126	5.	0.2	1345.6
29	SEP	0624	5	1.	0.0	1345.4	29	SEP	1230	66	84.	3.9	1348.3	29	SEP	1836	127	5.	0.2	1345.6
29	SEP	0630	6	1.	0.0	1345.4	29	SEP	1236	67	83.	3.7	1348.1	29	SEP	1842	128	6.	0.2	1345.6
29	SEP	0636	7	1.	0.0	1345.4	29	SEP	1242	68	81.	3.4	1347.9	29	SEP	1848	129	6.	0.2	1345.6
29	SEP	0642	8	2.	0.1	1345.4	29	SEP	1248	69	79.	3.0	1347.7	29	SEP	1854	130	6.	0.2	1345.6
29	SEP	0648	9	2.	0.1	1345.5	29	SEP	1254	70	77.	2.7	1347.4	29	SEP	1900	131	6.	0.2	1345.6
29	SEP	0654	10	2.	0.1	1345.5	29	SEP	1300	71	74.	2.3	1347.1	29	SEP	1906	132	6.	0.2	1345.6
29	SEP	0700	11	2.	0.1	1345.5	29	SEP	1306	72	71.	1.9	1346.9	29	SEP	1912	133	6.	0.2	1345.6
29	SEP	0706	12	2.	0.1	1345.5	29	SEP	1312	73	66.	1.5	1346.6	29	SEP	1918	134	6.	0.2	1345.6
29	SEP	0712	13	2.	0.1	1345.5	29	SEP	1318	74	54.	1.2	1346.3	29	SEP	1924	135	6.	0.2	1345.6
29	SEP	0718	14	2.	0.1	1345.5	29	SEP	1324	75	40.	0.9	1346.2	29	SEP	1930	136	6.	0.2	1345.6
29	SEP	0724	15	3.	0.1	1345.5	29	SEP	1330	76	31.	0.8	1346.0	29	SEP	1936	137	6.	0.2	1345.6
29	SEP	0730	16	3.	0.1	1345.5	29	SEP	1336	77	26.	0.7	1346.0	29	SEP	1942	138	6.	0.2	1345.6
29	SEP	0736	17	3.	0.1	1345.5	29	SEP	1342	78	23.	0.6	1345.9	29	SEP	1948	139	6.	0.2	1345.6
29	SEP	0742	18	3.	0.1	1345.5	29	SEP	1348	79	20.	0.6	1345.9	29	SEP	1954	140	6.	0.2	1345.6
29	SEP	0748	19	3.	0.1	1345.5	29	SEP	1354	80	18.	0.6	1345.8	29	SEP	2000	141	6.	0.2	1345.6
29	SEP	0754	20	3.	0.1	1345.5	29	SEP	1400	81	17.	0.5	1345.8	29	SEP	2006	142	6.	0.2	1345.6
29	SEP	0800	21	3.	0.1	1345.5	29	SEP	1406	82	16.	0.5	1345.8	29	SEP	2012	143	6.	0.2	1345.6
29	SEP	0806	22	3.	0.1	1345.5	29	SEP	1412	83	15.	0.5	1345.8	29	SEP	2018	144	6.	0.2	1345.6
29	SEP	0812	23	3.	0.1	1345.5	29	SEP	1418	84	14.	0.5	1345.8	29	SEP	2024	145	5.	0.2	1345.6
29	SEP	0818	24	3.	0.1	1345.5	29	SEP	1424	85	13.	0.4	1345.8	29	SEP	2030	146	5.	0.2	1345.6
29	SEP	0824	25	3.	0.1	1345.5	29	SEP	1430	86	12.	0.4	1345.7	29	SEP	2036	147	5.	0.2	1345.6
29	SEP	0830	26	3.	0.1	1345.5	29	SEP	1436	87	11.	0.4	1345.7	29	SEP	2042	148	5.	0.2	1345.5
29	SEP	0836	27	3.	0.1	1345.5	29	SEP	1442	88	11.	0.4	1345.7	29	SEP	2048	149	5.	0.2	1345.5
29	SEP	0842	28	3.	0.1	1345.5	29	SEP	1448	89	11.	0.4	1345.7	29	SEP	2054	150	5.	0.2	1345.5
29	SEP	0848	29	3.	0.1	1345.5	29	SEP	1454	90	10.	0.4	1345.7	29	SEP	2100	151	4.	0.2	1345.5
29	SEP	0854	30	3.	0.1	1345.5	29	SEP	1500	91	10.	0.4	1345.7	29	SEP	2106	152	4.	0.2	1345.5
29	SEP	0900	31	4.	0.1	1345.5	29	SEP	1506	92	10.	0.4	1345.7	29	SEP	2112	153	4.	0.2	1345.5
29	SEP	0906	32	4.	0.1	1345.5	29	SEP	1512	93	10.	0.4	1345.7	29	SEP	2118	154	4.	0.2	1345.5
29	SEP	0912	33	4.	0.1	1345.5	29	SEP	1518	94	10.	0.4	1345.7	29	SEP	2124	155	4.	0.2	1345.5
29	SEP	0918	34	4.	0.1	1345.5	29	SEP	1524	95	10.	0.4	1345.7	29	SEP	2130	156	4.	0.2	1345.5
29	SEP	0924	35	4.	0.1	1345.5	29	SEP	1530	96	10.	0.4	1345.7	29	SEP	2136	157	4.	0.2	1345.5
29	SEP	0930	36	4.	0.1	1345.5	29	SEP	1536	97	10.	0.4	1345.7	29	SEP	2142	158	4.	0.2	1345.5
29	SEP	0936	37	4.	0.1	1345.5	29	SEP	1542	98	10.	0.4	1345.7	29	SEP	2148	159	4.	0.1	1345.5
29	SEP	0942	38	4.	0.2	1345.5	29	SEP	1548	99	10.	0.4	1345.7	29	SEP	2154	160	4.	0.1	1345.5
29	SEP	0948	39	4.	0.2	1345.5	29	SEP	1554	100	10.	0.4	1345.7	29	SEP	2200	161	4.	0.1	1345.5
29	SEP	0954	40	4.	0.2	1345.5	29	SEP	1600	101	10.	0.4	1345.7	29	SEP	2206	162	4.	0.1	1345.5
29	SEP	1000	41	5.	0.2	1345.5	29	SEP	1606	102	10.	0.4	1345.7	29	SEP	2212	163	4.	0.1	1345.5
29	SEP	1006	42	5.	0.2	1345.5	29	SEP	1612	103	10.	0.3	1345.7	29	SEP	2218	164	4.	0.1	1345.5
29	SEP	1012	43	5.	0.2	1345.5	29	SEP	1618	104	9.	0.3	1345.7	29	SEP	2224	165	4.	0.1	1345.5
29	SEP	1018	44	5.	0.2	1345.6	29	SEP	1624	105	9.	0.3	1345.7	29	SEP	2230	166	4.	0.1	1345.5
29	SEP	1024	45	5.	0.2	1345.6	29	SEP	1630	106	9.	0.3	1345.7	29	SEP	2236	167	4.	0.1	1345.5
29	SEP	1030	46	5.	0.2	1345.6	29	SEP	1636	107	8.	0.3	1345.6	29	SEP	2242	168	4.	0.1	1345.5
29	SEP	1036	47	6.	0.2	1345.6	29	SEP	1642	108	8.	0.3	1345.6	29	SEP	2248	169	4.	0.1	1345.5
29	SEP	1042	48	6.	0.2	1345.6	29	SEP	1648	109	8.	0.3	1345.6	29	SEP	2254	170	4.	0.1	1345.5
29	SEP	1048	49	6.	0.2	1345.6	29	SEP	1654	110	7.	0.3	1345.6	29	SEP	2300	171	4.	0.1	1345.5
29	SEP	1054	50	7.	0.2	1345.6	29	SEP	1700	111	7.	0.3	1345.6	29	SEP	2306	172	4.	0.1	1345.5
29	SEP	1100	51	7.	0.3	1345.6	29	SEP	1706	112	7.	0.3	1345.6	29	SEP	2312	173	4.	0.1	1345.5
29	SEP	1106	52	8.	0.3	1345.6	29	SEP	1712	113	7.	0.3	1345.6	29	SEP	2318	174	4.	0.1	1345.5
29	SEP	1112	53	8.	0.3	1345.6	29	SEP	1718	114	7.	0.3	1345.6	29	SEP	2324	175	4.	0.1	1345.5
29	SEP	1118	54	9.	0.3	1345.7	29	SEP	1724	115	7.	0.3	1345.6	29	SEP	2330	176	4.	0.1	1345.5
29	SEP	1124	55	10.	0.4	1345.7	29	SEP	1730	116	7.	0.2	1345.6	29	SEP	2336	177	4.	0.1	1345.5
29	SEP	1130	56	11.	0.4	1345.7	29	SEP	1736	117	7.	0.2	1345.6	29	SEP	2342	178	4.	0.1	1345.5
29	SEP	1136	57	15.	0.5	1345.8	29	SEP	1742	118	7.	0.2	1345.6	29	SEP	2348	179	4.	0.1	1345.5
29	SEP	1142	58	26.	0.7	1346.0	29	SEP	1748	119	6.	0.2	1345.6	29	SEP	2354	180	4.	0.1	1345.5
29	SEP	1148	59	50.	1.1	1346.3	29	SEP	1754	120	6.	0.2	1345.6	30	SEP	0000	181	4.	0.1	1345.5
29	SEP	1154	60	70.	1.7	1346.7	29	SEP	1800	121	6.	0.2	1345.6							
29	SEP	1200	61	75.	2.4	1347.2	29	SEP	1806	122	5.	0.2	1345.6							

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	18.00-HR
+ (CFS)	(HR)				

```
                              (CFS)
+     85.      6.40                  29.        13.        13.        13.
                            (INCHES)  3.231      4.179      4.179      4.179
                             (AC-FT)  15.        19.        19.        19.

 PEAK STORAGE   TIME                  MAXIMUM AVERAGE STORAGE
                                    6-HR      24-HR      72-HR     18.00-HR
+  (AC-FT)      (HR)
     4.         6.40                 1.         0.         0.         0.

  PEAK STAGE    TIME                  MAXIMUM AVERAGE STAGE
                                    6-HR      24-HR      72-HR     18.00-HR
+   (FEET)      (HR)
   1348.38      6.40             1346.20    1345.75    1345.75    1345.75

                            CUMULATIVE AREA =     0.08 SQ MI


*** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** ***


              **************
              *            *
   42 KK      *    2.2AC   *
              *            *
              **************

    3 IN        TIME DATA FOR INPUT TIME SERIES
                      JXMIN          30  TIME INTERVAL IN MINUTES
                      JXDATE    29SEP92  STARTING DATE
                      JXTIME        600  STARTING TIME

              SUBBASIN RUNOFF DATA

   43 BA        SUBBASIN CHARACTERISTICS
                      TAREA        0.00  SUBBASIN AREA

                PRECIPITATION DATA

   44 PB              STORM        7.80  BASIN TOTAL PRECIPITATION

   45 PI          INCREMENTAL PRECIPITATION PATTERN
                   0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                   0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                   0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                   0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                   0.00     0.00     0.00     0.00     0.00     0.01     0.01     0.01     0.01     0.01
                   0.01     0.01     0.01     0.01     0.01     0.08     0.08     0.08     0.08     0.08
                   0.01     0.01     0.01     0.01     0.01     0.01     0.01     0.01     0.01     0.01
                   0.01     0.01     0.01     0.01     0.01     0.00     0.00     0.00     0.00     0.00
                   0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                   0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                   0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                   0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                   0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                   0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                   0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                   0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                   0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00
                   0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00     0.00

   49 LS        SCS LOSS RATE
                      STRTL        0.27  INITIAL ABSTRACTION
                     CRVNBR       88.00  CURVE NUMBER
                      RTIMP        0.00  PERCENT IMPERVIOUS AREA

   50 UD        SCS DIMENSIONLESS UNITGRAPH
                       TLAG        0.15  LAG

                                                  ***

 WARNING *** TIME INTERVAL IS GREATER THAN .29*LAG

                                              UNIT HYDROGRAPH
                                           10 END-OF-PERIOD ORDINATES
               4.       8.       6.       2.       1.       0.       0.       0.       0.       0.

*****************************************************************************************************
```

HYDROGRAPH AT STATION 2.2AC

DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
29	SEP	0600	1	0.00	0.00	0.00	0.	29	SEP	1506	92	0.03	0.00	0.02	1.
29	SEP	0606	2	0.02	0.02	0.00	0.	29	SEP	1512	93	0.03	0.00	0.02	1.
29	SEP	0612	3	0.02	0.02	0.00	0.	29	SEP	1518	94	0.03	0.00	0.02	1.
29	SEP	0618	4	0.02	0.02	0.00	0.	29	SEP	1524	95	0.03	0.00	0.02	1.
29	SEP	0624	5	0.02	0.02	0.00	0.	29	SEP	1530	96	0.03	0.00	0.02	1.
29	SEP	0630	6	0.02	0.02	0.00	0.	29	SEP	1536	97	0.03	0.00	0.02	1.
29	SEP	0636	7	0.02	0.02	0.00	0.	29	SEP	1542	98	0.03	0.00	0.02	1.
29	SEP	0642	8	0.02	0.02	0.00	0.	29	SEP	1548	99	0.03	0.00	0.02	1.
29	SEP	0648	9	0.02	0.02	0.00	0.	29	SEP	1554	100	0.03	0.00	0.02	1.
29	SEP	0654	10	0.02	0.02	0.00	0.	29	SEP	1600	101	0.03	0.00	0.02	1.
29	SEP	0700	11	0.02	0.02	0.00	0.	29	SEP	1606	102	0.02	0.00	0.02	1.
29	SEP	0706	12	0.02	0.02	0.00	0.	29	SEP	1612	103	0.02	0.00	0.02	0.
29	SEP	0712	13	0.02	0.02	0.00	0.	29	SEP	1618	104	0.02	0.00	0.02	0.
29	SEP	0718	14	0.02	0.02	0.00	0.	29	SEP	1624	105	0.02	0.00	0.02	0.
29	SEP	0724	15	0.02	0.02	0.00	0.	29	SEP	1630	106	0.02	0.00	0.02	0.
29	SEP	0730	16	0.02	0.02	0.00	0.	29	SEP	1636	107	0.02	0.00	0.02	0.
29	SEP	0736	17	0.02	0.02	0.00	0.	29	SEP	1642	108	0.02	0.00	0.02	0.
29	SEP	0742	18	0.02	0.02	0.00	0.	29	SEP	1648	109	0.02	0.00	0.02	0.
29	SEP	0748	19	0.02	0.02	0.00	0.	29	SEP	1654	110	0.02	0.00	0.02	0.
29	SEP	0754	20	0.02	0.02	0.00	0.	29	SEP	1700	111	0.02	0.00	0.02	0.
29	SEP	0800	21	0.02	0.02	0.00	0.	29	SEP	1706	112	0.02	0.00	0.02	0.
29	SEP	0806	22	0.02	0.02	0.00	0.	29	SEP	1712	113	0.02	0.00	0.02	0.
29	SEP	0812	23	0.02	0.02	0.00	0.	29	SEP	1718	114	0.02	0.00	0.02	0.
29	SEP	0818	24	0.02	0.02	0.00	0.	29	SEP	1724	115	0.02	0.00	0.02	0.
29	SEP	0824	25	0.02	0.02	0.00	0.	29	SEP	1730	116	0.02	0.00	0.02	0.
29	SEP	0830	26	0.02	0.02	0.00	0.	29	SEP	1736	117	0.01	0.00	0.01	0.
29	SEP	0836	27	0.02	0.02	0.01	0.	29	SEP	1742	118	0.01	0.00	0.01	0.
29	SEP	0842	28	0.02	0.02	0.01	0.	29	SEP	1748	119	0.01	0.00	0.01	0.
29	SEP	0848	29	0.02	0.02	0.01	0.	29	SEP	1754	120	0.01	0.00	0.01	0.
29	SEP	0854	30	0.02	0.02	0.01	0.	29	SEP	1800	121	0.01	0.00	0.01	0.
29	SEP	0900	31	0.02	0.02	0.01	0.	29	SEP	1806	122	0.02	0.00	0.01	0.
29	SEP	0906	32	0.03	0.02	0.01	0.	29	SEP	1812	123	0.02	0.00	0.01	0.
29	SEP	0912	33	0.03	0.02	0.01	0.	29	SEP	1818	124	0.02	0.00	0.01	0.
29	SEP	0918	34	0.03	0.02	0.01	0.	29	SEP	1824	125	0.02	0.00	0.01	0.
29	SEP	0924	35	0.03	0.02	0.01	0.	29	SEP	1830	126	0.02	0.00	0.01	0.
29	SEP	0930	36	0.03	0.02	0.01	0.	29	SEP	1836	127	0.02	0.00	0.01	0.
29	SEP	0936	37	0.03	0.02	0.01	0.	29	SEP	1842	128	0.02	0.00	0.01	0.
29	SEP	0942	38	0.03	0.02	0.01	0.	29	SEP	1848	129	0.02	0.00	0.01	0.
29	SEP	0948	39	0.03	0.02	0.01	0.	29	SEP	1854	130	0.02	0.00	0.01	0.
29	SEP	0954	40	0.03	0.02	0.01	0.	29	SEP	1900	131	0.02	0.00	0.01	0.
29	SEP	1000	41	0.03	0.02	0.02	0.	29	SEP	1906	132	0.02	0.00	0.01	0.
29	SEP	1006	42	0.04	0.02	0.02	0.	29	SEP	1912	133	0.02	0.00	0.01	0.
29	SEP	1012	43	0.04	0.02	0.02	0.	29	SEP	1918	134	0.02	0.00	0.01	0.
29	SEP	1018	44	0.04	0.02	0.02	0.	29	SEP	1924	135	0.02	0.00	0.01	0.
29	SEP	1024	45	0.04	0.02	0.02	0.	29	SEP	1930	136	0.02	0.00	0.01	0.
29	SEP	1030	46	0.04	0.02	0.02	0.	29	SEP	1936	137	0.02	0.00	0.01	0.
29	SEP	1036	47	0.05	0.02	0.03	1.	29	SEP	1942	138	0.02	0.00	0.01	0.
29	SEP	1042	48	0.05	0.02	0.03	1.	29	SEP	1948	139	0.02	0.00	0.01	0.
29	SEP	1048	49	0.05	0.02	0.03	1.	29	SEP	1954	140	0.02	0.00	0.01	0.
29	SEP	1054	50	0.05	0.02	0.03	1.	29	SEP	2000	141	0.02	0.00	0.01	0.
29	SEP	1100	51	0.05	0.02	0.04	1.	29	SEP	2006	142	0.01	0.00	0.01	0.
29	SEP	1106	52	0.08	0.03	0.06	1.	29	SEP	2012	143	0.01	0.00	0.01	0.
29	SEP	1112	53	0.08	0.02	0.06	1.	29	SEP	2018	144	0.01	0.00	0.01	0.
29	SEP	1118	54	0.08	0.02	0.06	1.	29	SEP	2024	145	0.01	0.00	0.01	0.
29	SEP	1124	55	0.08	0.02	0.06	1.	29	SEP	2030	146	0.01	0.00	0.01	0.
29	SEP	1130	56	0.08	0.02	0.06	1.	29	SEP	2036	147	0.01	0.00	0.01	0.
29	SEP	1136	57	0.64	0.12	0.52	3.	29	SEP	2042	148	0.01	0.00	0.01	0.
29	SEP	1142	58	0.64	0.08	0.56	7.	29	SEP	2048	149	0.01	0.00	0.01	0.
29	SEP	1148	59	0.64	0.06	0.58	10.	29	SEP	2054	150	0.01	0.00	0.01	0.
29	SEP	1154	60	0.64	0.05	0.60	12.	29	SEP	2100	151	0.01	0.00	0.01	0.
29	SEP	1200	61	0.64	0.04	0.61	12.	29	SEP	2106	152	0.01	0.00	0.01	0.
29	SEP	1206	62	0.12	0.01	0.12	11.	29	SEP	2112	153	0.01	0.00	0.01	0.
29	SEP	1212	63	0.12	0.01	0.12	7.	29	SEP	2118	154	0.01	0.00	0.01	0.
29	SEP	1218	64	0.12	0.01	0.12	5.	29	SEP	2124	155	0.01	0.00	0.01	0.
29	SEP	1224	65	0.12	0.01	0.12	3.	29	SEP	2130	156	0.01	0.00	0.01	0.
29	SEP	1230	66	0.12	0.01	0.12	3.	29	SEP	2136	157	0.01	0.00	0.01	0.
29	SEP	1236	67	0.06	0.00	0.06	3.	29	SEP	2142	158	0.01	0.00	0.01	0.
29	SEP	1242	68	0.06	0.00	0.06	2.	29	SEP	2148	159	0.01	0.00	0.01	0.
29	SEP	1248	69	0.06	0.00	0.06	2.	29	SEP	2154	160	0.01	0.00	0.01	0.
29	SEP	1254	70	0.06	0.00	0.06	1.	29	SEP	2200	161	0.01	0.00	0.01	0.
29	SEP	1300	71	0.06	0.00	0.06	1.	29	SEP	2206	162	0.01	0.00	0.01	0.
29	SEP	1306	72	0.05	0.00	0.04	1.	29	SEP	2212	163	0.01	0.00	0.01	0.
29	SEP	1312	73	0.05	0.00	0.04	1.	29	SEP	2218	164	0.01	0.00	0.01	0.

29 SEP 1318	74	0.05	0.00	0.04	1.	*
29 SEP 1324	75	0.05	0.00	0.04	1.	*
29 SEP 1330	76	0.05	0.00	0.04	1.	*
29 SEP 1336	77	0.04	0.00	0.03	1.	*
29 SEP 1342	78	0.04	0.00	0.03	1.	*
29 SEP 1348	79	0.04	0.00	0.03	1.	*
29 SEP 1354	80	0.04	0.00	0.03	1.	*
29 SEP 1400	81	0.04	0.00	0.03	1.	*
29 SEP 1406	82	0.03	0.00	0.02	1.	*
29 SEP 1412	83	0.03	0.00	0.02	1.	*
29 SEP 1418	84	0.03	0.00	0.02	1.	*
29 SEP 1424	85	0.03	0.00	0.02	1.	*
29 SEP 1430	86	0.03	0.00	0.02	1.	*
29 SEP 1436	87	0.03	0.00	0.02	1.	*
29 SEP 1442	88	0.03	0.00	0.02	1.	*
29 SEP 1448	89	0.03	0.00	0.02	1.	*
29 SEP 1454	90	0.03	0.00	0.02	1.	*
29 SEP 1500	91	0.03	0.00	0.02	1.	*
29 SEP 2224	165	0.01	0.00	0.01	0.	
29 SEP 2230	166	0.01	0.00	0.01	0.	
29 SEP 2236	167	0.01	0.00	0.01	0.	
29 SEP 2242	168	0.01	0.00	0.01	0.	
29 SEP 2248	169	0.01	0.00	0.01	0.	
29 SEP 2254	170	0.01	0.00	0.01	0.	
29 SEP 2300	171	0.01	0.00	0.01	0.	
29 SEP 2306	172	0.01	0.00	0.01	0.	
29 SEP 2312	173	0.01	0.00	0.01	0.	
29 SEP 2318	174	0.01	0.00	0.01	0.	
29 SEP 2324	175	0.01	0.00	0.01	0.	
29 SEP 2330	176	0.01	0.00	0.01	0.	
29 SEP 2336	177	0.01	0.00	0.01	0.	
29 SEP 2342	178	0.01	0.00	0.01	0.	
29 SEP 2348	179	0.01	0.00	0.01	0.	
29 SEP 2354	180	0.01	0.00	0.01	0.	
30 SEP 0000	181	0.01	0.00	0.01	0.	

****

TOTAL RAINFALL = 7.80, TOTAL LOSS = 1.43, TOTAL EXCESS = 6.37

	PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
				6-HR	24-HR	72-HR	18.00-HR
+	(CFS)	(HR)					
			(CFS)				
+	12.	6.00		2.	1.	1.	1.
			(INCHES)	5.201	6.352	6.352	6.352
			(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = 0.00 SQ MI

*** ***

```
          **************
          *            *
51 KK     *   N5.3AC   *
          *            *
          **************
```

3 IN TIME DATA FOR INPUT TIME SERIES
JXMIN 30 TIME INTERVAL IN MINUTES
JXDATE 29SEP92 STARTING DATE
JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

52 BA SUBBASIN CHARACTERISTICS
TAREA 0.00 SUBBASIN AREA

PRECIPITATION DATA

53 PB STORM 5.00 BASIN TOTAL PRECIPITATION

54 PI INCREMENTAL PRECIPITATION PATTERN

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.08	0.08	0.08	0.08	0.08
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

58 LS SCS LOSS RATE

	STRTL	0.67 INITIAL ABSTRACTION
	CRVNBR	75.00 CURVE NUMBER
	RTIMP	0.00 PERCENT IMPERVIOUS AREA

59 UD SCS DIMENSIONLESS UNITGRAPH
TLAG 0.15 LAG

***

WARNING *** TIME INTERVAL IS GREATER THAN .29*LAG

UNIT HYDROGRAPH
10 END-OF-PERIOD ORDINATES
6. 12. 8. 3. 2. 1. 0. 0. 0. 0.

****

HYDROGRAPH AT STATION N5.3AC

****

DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
29 SEP 0600	1	0.00	0.00	0.00	0.	29 SEP 1506	92	0.02	0.00	0.01	0.
29 SEP 0606	2	0.01	0.01	0.00	0.	29 SEP 1512	93	0.02	0.00	0.01	0.
29 SEP 0612	3	0.01	0.01	0.00	0.	29 SEP 1518	94	0.02	0.00	0.01	0.
29 SEP 0618	4	0.01	0.01	0.00	0.	29 SEP 1524	95	0.02	0.00	0.01	0.
29 SEP 0624	5	0.01	0.01	0.00	0.	29 SEP 1530	96	0.02	0.00	0.01	0.
29 SEP 0630	6	0.01	0.01	0.00	0.	29 SEP 1536	97	0.02	0.00	0.01	0.
29 SEP 0636	7	0.01	0.01	0.00	0.	29 SEP 1542	98	0.02	0.00	0.01	0.
29 SEP 0642	8	0.01	0.01	0.00	0.	29 SEP 1548	99	0.02	0.00	0.01	0.
29 SEP 0648	9	0.01	0.01	0.00	0.	29 SEP 1554	100	0.02	0.00	0.01	0.
29 SEP 0654	10	0.01	0.01	0.00	0.	29 SEP 1600	101	0.02	0.00	0.01	0.
29 SEP 0700	11	0.01	0.01	0.00	0.	29 SEP 1606	102	0.01	0.00	0.01	0.
29 SEP 0706	12	0.01	0.01	0.00	0.	29 SEP 1612	103	0.01	0.00	0.01	0.
29 SEP 0712	13	0.01	0.01	0.00	0.	29 SEP 1618	104	0.01	0.00	0.01	0.
29 SEP 0718	14	0.01	0.01	0.00	0.	29 SEP 1624	105	0.01	0.00	0.01	0.
29 SEP 0724	15	0.01	0.01	0.00	0.	29 SEP 1630	106	0.01	0.00	0.01	0.
29 SEP 0730	16	0.01	0.01	0.00	0.	29 SEP 1636	107	0.01	0.00	0.01	0.
29 SEP 0736	17	0.01	0.01	0.00	0.	29 SEP 1642	108	0.01	0.00	0.01	0.
29 SEP 0742	18	0.01	0.01	0.00	0.	29 SEP 1648	109	0.01	0.00	0.01	0.
29 SEP 0748	19	0.01	0.01	0.00	0.	29 SEP 1654	110	0.01	0.00	0.01	0.
29 SEP 0754	20	0.01	0.01	0.00	0.	29 SEP 1700	111	0.01	0.00	0.01	0.
29 SEP 0800	21	0.01	0.01	0.00	0.	29 SEP 1706	112	0.01	0.00	0.01	0.
29 SEP 0806	22	0.01	0.01	0.00	0.	29 SEP 1712	113	0.01	0.00	0.01	0.
29 SEP 0812	23	0.01	0.01	0.00	0.	29 SEP 1718	114	0.01	0.00	0.01	0.
29 SEP 0818	24	0.01	0.01	0.00	0.	29 SEP 1724	115	0.01	0.00	0.01	0.
29 SEP 0824	25	0.01	0.01	0.00	0.	29 SEP 1730	116	0.01	0.00	0.01	0.
29 SEP 0830	26	0.01	0.01	0.00	0.	29 SEP 1736	117	0.01	0.00	0.01	0.
29 SEP 0836	27	0.02	0.02	0.00	0.	29 SEP 1742	118	0.01	0.00	0.01	0.
29 SEP 0842	28	0.02	0.02	0.00	0.	29 SEP 1748	119	0.01	0.00	0.01	0.
29 SEP 0848	29	0.02	0.02	0.00	0.	29 SEP 1754	120	0.01	0.00	0.01	0.
29 SEP 0854	30	0.02	0.02	0.00	0.	29 SEP 1800	121	0.01	0.00	0.01	0.
29 SEP 0900	31	0.02	0.02	0.00	0.	29 SEP 1806	122	0.01	0.00	0.01	0.
29 SEP 0906	32	0.02	0.02	0.00	0.	29 SEP 1812	123	0.01	0.00	0.01	0.
29 SEP 0912	33	0.02	0.02	0.00	0.	29 SEP 1818	124	0.01	0.00	0.01	0.
29 SEP 0918	34	0.02	0.02	0.00	0.	29 SEP 1824	125	0.01	0.00	0.01	0.
29 SEP 0924	35	0.02	0.02	0.00	0.	29 SEP 1830	126	0.01	0.00	0.01	0.
29 SEP 0930	36	0.02	0.02	0.00	0.	29 SEP 1836	127	0.01	0.00	0.01	0.
29 SEP 0936	37	0.02	0.02	0.00	0.	29 SEP 1842	128	0.01	0.00	0.01	0.
29 SEP 0942	38	0.02	0.02	0.00	0.	29 SEP 1848	129	0.01	0.00	0.01	0.
29 SEP 0948	39	0.02	0.02	0.00	0.	29 SEP 1854	130	0.01	0.00	0.01	0.
29 SEP 0954	40	0.02	0.02	0.00	0.	29 SEP 1900	131	0.01	0.00	0.01	0.
29 SEP 1000	41	0.02	0.02	0.00	0.	29 SEP 1906	132	0.01	0.00	0.01	0.
29 SEP 1006	42	0.03	0.03	0.00	0.	29 SEP 1912	133	0.01	0.00	0.01	0.
29 SEP 1012	43	0.03	0.03	0.00	0.	29 SEP 1918	134	0.01	0.00	0.01	0.
29 SEP 1018	44	0.02	0.02	0.00	0.	29 SEP 1924	135	0.01	0.00	0.01	0.
29 SEP 1024	45	0.03	0.03	0.00	0.	29 SEP 1930	136	0.01	0.00	0.01	0.
29 SEP 1030	46	0.03	0.02	0.00	0.	29 SEP 1936	137	0.01	0.00	0.01	0.
29 SEP 1036	47	0.03	0.03	0.00	0.	29 SEP 1942	138	0.01	0.00	0.01	0.
29 SEP 1042	48	0.03	0.03	0.00	0.	29 SEP 1948	139	0.01	0.00	0.01	0.
29 SEP 1048	49	0.03	0.03	0.00	0.	29 SEP 1954	140	0.01	0.00	0.01	0.
29 SEP 1054	50	0.03	0.03	0.00	0.	29 SEP 2000	141	0.01	0.00	0.01	0.
29 SEP 1100	51	0.03	0.03	0.00	0.	29 SEP 2006	142	0.01	0.00	0.01	0.
29 SEP 1106	52	0.05	0.05	0.01	0.	29 SEP 2012	143	0.01	0.00	0.01	0.
29 SEP 1112	53	0.05	0.05	0.01	0.	29 SEP 2018	144	0.01	0.00	0.01	0.
29 SEP 1118	54	0.05	0.04	0.01	0.	29 SEP 2024	145	0.01	0.00	0.01	0.
29 SEP 1124	55	0.05	0.04	0.01	0.	29 SEP 2030	146	0.01	0.00	0.01	0.
29 SEP 1130	56	0.05	0.04	0.01	0.	29 SEP 2036	147	0.01	0.00	0.01	0.
29 SEP 1136	57	0.41	0.29	0.12	1.	29 SEP 2042	148	0.01	0.00	0.01	0.

29 SEP 1142	58	0.41	0.24	0.17	3.	*	29 SEP 2048	149	0.01	0.00	0.01	0.
29 SEP 1148	59	0.41	0.20	0.21	4.	*	29 SEP 2054	150	0.01	0.00	0.01	0.
29 SEP 1154	60	0.41	0.17	0.24	6.	*	29 SEP 2100	151	0.01	0.00	0.01	0.
29 SEP 1200	61	0.41	0.15	0.27	7.	*	29 SEP 2106	152	0.01	0.00	0.01	0.
29 SEP 1206	62	0.08	0.03	0.05	7.	*	29 SEP 2112	153	0.01	0.00	0.01	0.
29 SEP 1212	63	0.08	0.02	0.05	4.	*	29 SEP 2118	154	0.01	0.00	0.01	0.
29 SEP 1218	64	0.08	0.02	0.05	3.	*	29 SEP 2124	155	0.01	0.00	0.01	0.
29 SEP 1224	65	0.08	0.02	0.05	2.	*	29 SEP 2130	156	0.01	0.00	0.01	0.
29 SEP 1230	66	0.08	0.02	0.06	2.	*	29 SEP 2136	157	0.01	0.00	0.01	0.
29 SEP 1236	67	0.04	0.01	0.03	2.	*	29 SEP 2142	158	0.01	0.00	0.01	0.
29 SEP 1242	68	0.04	0.01	0.03	1.	*	29 SEP 2148	159	0.01	0.00	0.01	0.
29 SEP 1248	69	0.04	0.01	0.03	1.	*	29 SEP 2154	160	0.01	0.00	0.01	0.
29 SEP 1254	70	0.04	0.01	0.03	1.	*	29 SEP 2200	161	0.01	0.00	0.01	0.
29 SEP 1300	71	0.04	0.01	0.03	1.	*	29 SEP 2206	162	0.01	0.00	0.01	0.
29 SEP 1306	72	0.03	0.01	0.02	1.	*	29 SEP 2212	163	0.01	0.00	0.01	0.
29 SEP 1312	73	0.03	0.01	0.02	1.	*	29 SEP 2218	164	0.01	0.00	0.01	0.
29 SEP 1318	74	0.03	0.01	0.02	1.	*	29 SEP 2224	165	0.01	0.00	0.01	0.
29 SEP 1324	75	0.03	0.01	0.02	1.	*	29 SEP 2230	166	0.01	0.00	0.01	0.
29 SEP 1330	76	0.03	0.01	0.02	1.	*	29 SEP 2236	167	0.01	0.00	0.01	0.
29 SEP 1336	77	0.02	0.01	0.02	1.	*	29 SEP 2242	168	0.01	0.00	0.01	0.
29 SEP 1342	78	0.02	0.01	0.02	1.	*	29 SEP 2248	169	0.01	0.00	0.01	0.
29 SEP 1348	79	0.02	0.01	0.02	1.	*	29 SEP 2254	170	0.01	0.00	0.01	0.
29 SEP 1354	80	0.02	0.01	0.02	1.	*	29 SEP 2300	171	0.01	0.00	0.01	0.
29 SEP 1400	81	0.02	0.01	0.02	1.	*	29 SEP 2306	172	0.01	0.00	0.01	0.
29 SEP 1406	82	0.02	0.00	0.01	1.	*	29 SEP 2312	173	0.01	0.00	0.01	0.
29 SEP 1412	83	0.02	0.00	0.01	0.	*	29 SEP 2318	174	0.01	0.00	0.01	0.
29 SEP 1418	84	0.02	0.00	0.01	0.	*	29 SEP 2324	175	0.01	0.00	0.01	0.
29 SEP 1424	85	0.02	0.00	0.01	0.	*	29 SEP 2330	176	0.01	0.00	0.01	0.
29 SEP 1430	86	0.02	0.00	0.01	0.	*	29 SEP 2336	177	0.01	0.00	0.01	0.
29 SEP 1436	87	0.02	0.00	0.01	0.	*	29 SEP 2342	178	0.01	0.00	0.01	0.
29 SEP 1442	88	0.02	0.00	0.01	0.	*	29 SEP 2348	179	0.01	0.00	0.01	0.
29 SEP 1448	89	0.02	0.00	0.01	0.	*	29 SEP 2354	180	0.01	0.00	0.01	0.
29 SEP 1454	90	0.02	0.00	0.01	0.	*	30 SEP 0000	181	0.01	0.00	0.01	0.
29 SEP 1500	91	0.02	0.00	0.01	0.	*						
						*						

****

TOTAL RAINFALL = 5.00, TOTAL LOSS = 2.55, TOTAL EXCESS = 2.45

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	18.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 7.	6.00		1.	0.	0.	0.
		(INCHES)	2.011	2.438	2.438	2.438
		(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = 0.00 SQ MI

*** ***

```
          **************
          *            *
60 KK     *     INTO3  *
          *            *
          **************
```

61 HC HYDROGRAPH COMBINATION
ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

***

****

HYDROGRAPH AT STATION INTO3
SUM OF 3 HYDROGRAPHS

****

DA MON HRMN	ORD	FLOW	*	DA MON HRMN	ORD	FLOW	*	DA MON HRMN	ORD	FLOW	*	DA MON HRMN	ORD	FLOW
29 SEP 0600	1	0.	*	29 SEP 1036	47	6.	*	29 SEP 1512	93	11.	*	29 SEP 1948	139	7.
29 SEP 0606	2	0.	*	29 SEP 1042	48	7.	*	29 SEP 1518	94	11.	*	29 SEP 1954	140	7.
29 SEP 0612	3	0.	*	29 SEP 1048	49	7.	*	29 SEP 1524	95	11.	*	29 SEP 2000	141	7.
29 SEP 0618	4	0.	*	29 SEP 1054	50	8.	*	29 SEP 1530	96	11.	*	29 SEP 2006	142	7.
29 SEP 0624	5	1.	*	29 SEP 1100	51	8.	*	29 SEP 1536	97	11.	*	29 SEP 2012	143	6.

29 SEP	0630	6	1.	*	29 SEP	1106	52	9.	*	29 SEP	1542	98	11.	*	29 SEP	2018	144	6.					
29 SEP	0636	7	1.	*	29 SEP	1112	53	9.	*	29 SEP	1548	99	11.	*	29 SEP	2024	145	6.					
29 SEP	0642	8	2.	*	29 SEP	1118	54	10.	*	29 SEP	1554	100	11.	*	29 SEP	2030	146	6.					
29 SEP	0648	9	2.	*	29 SEP	1124	55	11.	*	29 SEP	1600	101	11.	*	29 SEP	2036	147	5.					
29 SEP	0654	10	2.	*	29 SEP	1130	56	13.	*	29 SEP	1606	102	11.	*	29 SEP	2042	148	5.					
29 SEP	0700	11	2.	*	29 SEP	1136	57	19.	*	29 SEP	1612	103	10.	*	29 SEP	2048	149	5.					
29 SEP	0706	12	2.	*	29 SEP	1142	58	35.	*	29 SEP	1618	104	10.	*	29 SEP	2054	150	5.					
29 SEP	0712	13	2.	*	29 SEP	1148	59	65.	*	29 SEP	1624	105	10.	*	29 SEP	2100	151	5.					
29 SEP	0718	14	2.	*	29 SEP	1154	60	87.	*	29 SEP	1630	106	9.	*	29 SEP	2106	152	5.					
29 SEP	0724	15	3.	*	29 SEP	1200	61	94.	*	29 SEP	1636	107	9.	*	29 SEP	2112	153	5.					
29 SEP	0730	16	3.	*	29 SEP	1206	62	97.	*	29 SEP	1642	108	9.	*	29 SEP	2118	154	5.					
29 SEP	0736	17	3.	*	29 SEP	1212	63	95.	*	29 SEP	1648	109	8.	*	29 SEP	2124	155	5.					
29 SEP	0742	18	3.	*	29 SEP	1218	64	92.	*	29 SEP	1654	110	8.	*	29 SEP	2130	156	5.					
29 SEP	0748	19	3.	*	29 SEP	1224	65	90.	*	29 SEP	1700	111	8.	*	29 SEP	2136	157	5.					
29 SEP	0754	20	3.	*	29 SEP	1230	66	89.	*	29 SEP	1706	112	8.	*	29 SEP	2142	158	5.					
29 SEP	0800	21	3.	*	29 SEP	1236	67	87.	*	29 SEP	1712	113	8.	*	29 SEP	2148	159	4.					
29 SEP	0806	22	3.	*	29 SEP	1242	68	84.	*	29 SEP	1718	114	8.	*	29 SEP	2154	160	4.					
29 SEP	0812	23	3.	*	29 SEP	1248	69	82.	*	29 SEP	1724	115	7.	*	29 SEP	2200	161	4.					
29 SEP	0818	24	3.	*	29 SEP	1254	70	79.	*	29 SEP	1730	116	7.	*	29 SEP	2206	162	4.					
29 SEP	0824	25	3.	*	29 SEP	1300	71	76.	*	29 SEP	1736	117	7.	*	29 SEP	2212	163	4.					
29 SEP	0830	26	3.	*	29 SEP	1306	72	74.	*	29 SEP	1742	118	7.	*	29 SEP	2218	164	4.					
29 SEP	0836	27	3.	*	29 SEP	1312	73	68.	*	29 SEP	1748	119	7.	*	29 SEP	2224	165	4.					
29 SEP	0842	28	3.	*	29 SEP	1318	74	56.	*	29 SEP	1754	120	6.	*	29 SEP	2230	166	4.					
29 SEP	0848	29	3.	*	29 SEP	1324	75	42.	*	29 SEP	1800	121	6.	*	29 SEP	2236	167	4.					
29 SEP	0854	30	4.	*	29 SEP	1330	76	33.	*	29 SEP	1806	122	6.	*	29 SEP	2242	168	4.					
29 SEP	0900	31	4.	*	29 SEP	1336	77	28.	*	29 SEP	1812	123	6.	*	29 SEP	2248	169	4.					
29 SEP	0906	32	4.	*	29 SEP	1342	78	24.	*	29 SEP	1818	124	6.	*	29 SEP	2254	170	4.					
29 SEP	0912	33	4.	*	29 SEP	1348	79	21.	*	29 SEP	1824	125	6.	*	29 SEP	2300	171	4.					
29 SEP	0918	34	4.	*	29 SEP	1354	80	20.	*	29 SEP	1830	126	6.	*	29 SEP	2306	172	4.					
29 SEP	0924	35	4.	*	29 SEP	1400	81	18.	*	29 SEP	1836	127	6.	*	29 SEP	2312	173	4.					
29 SEP	0930	36	4.	*	29 SEP	1406	82	17.	*	29 SEP	1842	128	6.	*	29 SEP	2318	174	4.					
29 SEP	0936	37	4.	*	29 SEP	1412	83	16.	*	29 SEP	1848	129	6.	*	29 SEP	2324	175	4.					
29 SEP	0942	38	4.	*	29 SEP	1418	84	15.	*	29 SEP	1854	130	6.	*	29 SEP	2330	176	4.					
29 SEP	0948	39	5.	*	29 SEP	1424	85	14.	*	29 SEP	1900	131	6.	*	29 SEP	2336	177	4.					
29 SEP	0954	40	5.	*	29 SEP	1430	86	13.	*	29 SEP	1906	132	6.	*	29 SEP	2342	178	4.					
29 SEP	1000	41	5.	*	29 SEP	1436	87	12.	*	29 SEP	1912	133	6.	*	29 SEP	2348	179	4.					
29 SEP	1006	42	5.	*	29 SEP	1442	88	12.	*	29 SEP	1918	134	6.	*	29 SEP	2354	180	4.					
29 SEP	1012	43	5.	*	29 SEP	1448	89	11.	*	29 SEP	1924	135	6.	*	30 SEP	0000	181	4.					
29 SEP	1018	44	5.	*	29 SEP	1454	90	11.	*	29 SEP	1930	136	6.	*									
29 SEP	1024	45	6.	*	29 SEP	1500	91	11.	*	29 SEP	1936	137	7.	*									
29 SEP	1030	46	6.	*	29 SEP	1506	92	11.	*	29 SEP	1942	138	7.	*									

****

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	18.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 97.	6.10		32.	14.	14.	14.
		(INCHES)	3.234	4.165	4.165	4.165
		(AC-FT)	16.	21.	21.	21.

COMULATIVE AREA = 0.09 SQ MI

*** ***

```
          **************
          *            *
62 KK     *    POND3   *
          *            *
          **************
```

HYDROGRAPH ROUTING DATA

63 RS STORAGE ROUTING
NSTPS 1 NUMBER OF SUBREACHES
ITYP ELEV TYPE OF INITIAL CONDITION
RSVRIC 1342.40 INITIAL CONDITION
X 0.00 WORKING R AND D COEFFICIENT

64 SA	AREA	0.3	0.4	0.5	0.7	0.8	
65 SE	ELEVATION	1342.40	1343.30	1344.20	1345.10	1346.00	
66 SQ	DISCHARGE	0.	10.	20.	30.	40.	50. 60. 70. 80. 90. 100.

68 SE ELEVATION 1342.40 1342.70 1342.88 1343.03 1343.16 1343.29 1343.40 1343.51 1343.61 1343.71 1343.80

***

COMPUTED STORAGE-ELEVATION DATA

STORAGE	0.00	0.29	0.71	1.25	1.90
ELEVATION	1342.40	1343.30	1344.20	1345.10	1346.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	0.00	0.08	0.14	0.19	0.24	0.29	0.34	0.38	0.43	0.47
OUTFLOW	0.00	10.00	20.00	30.00	40.00	50.00	60.00	70.00	80.00	90.00
ELEVATION	1342.40	1342.70	1342.88	1343.03	1343.16	1343.29	1343.40	1343.51	1343.61	1343.71

STORAGE	0.51	0.71	1.25	1.90
OUTFLOW	100.00	144.39	244.30	344.20
ELEVATION	1343.80	1344.20	1345.10	1346.00

****

HYDROGRAPH AT STATION POND3

****

DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE
29	SEP	0600	1	0.	0.0	1342.4	29	SEP	1206	62	96.	0.5	1343.8	29	SEP	1812	123	6.	0.0	1342.6
29	SEP	0606	2	0.	0.0	1342.4	29	SEP	1212	63	96.	0.5	1343.8	29	SEP	1818	124	6.	0.0	1342.6
29	SEP	0612	3	0.	0.0	1342.4	29	SEP	1218	64	93.	0.5	1343.7	29	SEP	1824	125	6.	0.0	1342.6
29	SEP	0618	4	0.	0.0	1342.4	29	SEP	1224	65	91.	0.5	1343.7	29	SEP	1830	126	6.	0.0	1342.6
29	SEP	0624	5	0.	0.0	1342.4	29	SEP	1230	66	90.	0.5	1343.7	29	SEP	1836	127	6.	0.0	1342.6
29	SEP	0630	6	1.	0.0	1342.4	29	SEP	1236	67	88.	0.5	1343.7	29	SEP	1842	128	6.	0.1	1342.6
29	SEP	0636	7	1.	0.0	1342.4	29	SEP	1242	68	86.	0.5	1343.7	29	SEP	1848	129	6.	0.1	1342.6
29	SEP	0642	8	1.	0.0	1342.4	29	SEP	1248	69	83.	0.4	1343.6	29	SEP	1854	130	6.	0.1	1342.6
29	SEP	0648	9	2.	0.0	1342.4	29	SEP	1254	70	80.	0.4	1343.6	29	SEP	1900	131	6.	0.1	1342.6
29	SEP	0654	10	2.	0.0	1342.5	29	SEP	1300	71	78.	0.4	1343.6	29	SEP	1906	132	6.	0.1	1342.6
29	SEP	0700	11	2.	0.0	1342.5	29	SEP	1306	72	75.	0.4	1343.6	29	SEP	1912	133	6.	0.1	1342.6
29	SEP	0706	12	2.	0.0	1342.5	29	SEP	1312	73	71.	0.4	1343.5	29	SEP	1918	134	6.	0.1	1342.6
29	SEP	0712	13	2.	0.0	1342.5	29	SEP	1318	74	62.	0.3	1343.4	29	SEP	1924	135	6.	0.1	1342.6
29	SEP	0718	14	2.	0.0	1342.5	29	SEP	1324	75	50.	0.3	1343.3	29	SEP	1930	136	6.	0.1	1342.6
29	SEP	0724	15	2.	0.0	1342.5	29	SEP	1330	76	38.	0.2	1343.1	29	SEP	1936	137	6.	0.1	1342.6
29	SEP	0730	16	3.	0.0	1342.5	29	SEP	1336	77	31.	0.2	1343.0	29	SEP	1942	138	6.	0.1	1342.6
29	SEP	0736	17	3.	0.0	1342.5	29	SEP	1342	78	26.	0.2	1343.0	29	SEP	1948	139	7.	0.1	1342.6
29	SEP	0742	18	3.	0.0	1342.5	29	SEP	1348	79	23.	0.2	1342.9	29	SEP	1954	140	7.	0.1	1342.6
29	SEP	0748	19	3.	0.0	1342.5	29	SEP	1354	80	21.	0.1	1342.9	29	SEP	2000	141	7.	0.1	1342.6
29	SEP	0754	20	3.	0.0	1342.5	29	SEP	1400	81	19.	0.1	1342.9	29	SEP	2006	142	7.	0.1	1342.6
29	SEP	0800	21	3.	0.0	1342.5	29	SEP	1406	82	18.	0.1	1342.8	29	SEP	2012	143	6.	0.1	1342.6
29	SEP	0806	22	3.	0.0	1342.5	29	SEP	1412	83	17.	0.1	1342.8	29	SEP	2018	144	6.	0.1	1342.6
29	SEP	0812	23	3.	0.0	1342.5	29	SEP	1418	84	16.	0.1	1342.8	29	SEP	2024	145	6.	0.1	1342.6
29	SEP	0818	24	3.	0.0	1342.5	29	SEP	1424	85	15.	0.1	1342.8	29	SEP	2030	146	6.	0.0	1342.6
29	SEP	0824	25	3.	0.0	1342.5	29	SEP	1430	86	14.	0.1	1342.8	29	SEP	2036	147	6.	0.0	1342.6
29	SEP	0830	26	3.	0.0	1342.5	29	SEP	1436	87	13.	0.1	1342.8	29	SEP	2042	148	5.	0.0	1342.6
29	SEP	0836	27	3.	0.0	1342.5	29	SEP	1442	88	12.	0.1	1342.7	29	SEP	2048	149	5.	0.0	1342.6
29	SEP	0842	28	3.	0.0	1342.5	29	SEP	1448	89	12.	0.1	1342.7	29	SEP	2054	150	5.	0.0	1342.6
29	SEP	0848	29	3.	0.0	1342.5	29	SEP	1454	90	11.	0.1	1342.7	29	SEP	2100	151	5.	0.0	1342.5
29	SEP	0854	30	3.	0.0	1342.5	29	SEP	1500	91	11.	0.1	1342.7	29	SEP	2106	152	5.	0.0	1342.5
29	SEP	0900	31	4.	0.0	1342.5	29	SEP	1506	92	11.	0.1	1342.7	29	SEP	2112	153	5.	0.0	1342.5
29	SEP	0906	32	4.	0.0	1342.5	29	SEP	1512	93	11.	0.1	1342.7	29	SEP	2118	154	5.	0.0	1342.5
29	SEP	0912	33	4.	0.0	1342.5	29	SEP	1518	94	11.	0.1	1342.7	29	SEP	2124	155	5.	0.0	1342.5
29	SEP	0918	34	4.	0.0	1342.5	29	SEP	1524	95	11.	0.1	1342.7	29	SEP	2130	156	5.	0.0	1342.5
29	SEP	0924	35	4.	0.0	1342.5	29	SEP	1530	96	11.	0.1	1342.7	29	SEP	2136	157	5.	0.0	1342.5
29	SEP	0930	36	4.	0.0	1342.5	29	SEP	1536	97	11.	0.1	1342.7	29	SEP	2142	158	5.	0.0	1342.5
29	SEP	0936	37	4.	0.0	1342.5	29	SEP	1542	98	11.	0.1	1342.7	29	SEP	2148	159	5.	0.0	1342.5
29	SEP	0942	38	4.	0.0	1342.5	29	SEP	1548	99	11.	0.1	1342.7	29	SEP	2154	160	4.	0.0	1342.5
29	SEP	0948	39	4.	0.0	1342.5	29	SEP	1554	100	11.	0.1	1342.7	29	SEP	2200	161	4.	0.0	1342.5
29	SEP	0954	40	5.	0.0	1342.5	29	SEP	1600	101	11.	0.1	1342.7	29	SEP	2206	162	4.	0.0	1342.5
29	SEP	1000	41	5.	0.0	1342.5	29	SEP	1606	102	11.	0.1	1342.7	29	SEP	2212	163	4.	0.0	1342.5
29	SEP	1006	42	5.	0.0	1342.5	29	SEP	1612	103	11.	0.1	1342.7	29	SEP	2218	164	4.	0.0	1342.5
29	SEP	1012	43	5.	0.0	1342.6	29	SEP	1618	104	10.	0.1	1342.7	29	SEP	2224	165	4.	0.0	1342.5
29	SEP	1018	44	5.	0.0	1342.6	29	SEP	1624	105	10.	0.1	1342.7	29	SEP	2230	166	4.	0.0	1342.5
29	SEP	1024	45	5.	0.0	1342.6	29	SEP	1630	106	10.	0.1	1342.7	29	SEP	2236	167	4.	0.0	1342.5
29	SEP	1030	46	6.	0.0	1342.6	29	SEP	1636	107	9.	0.1	1342.7	29	SEP	2242	168	4.	0.0	1342.5
29	SEP	1036	47	6.	0.1	1342.6	29	SEP	1642	108	9.	0.1	1342.7	29	SEP	2248	169	4.	0.0	1342.5
29	SEP	1042	48	6.	0.1	1342.6	29	SEP	1648	109	9.	0.1	1342.7	29	SEP	2254	170	4.	0.0	1342.5
29	SEP	1048	49	7.	0.1	1342.6	29	SEP	1654	110	8.	0.1	1342.6	29	SEP	2300	171	4.	0.0	1342.5
29	SEP	1054	50	7.	0.1	1342.6	29	SEP	1700	111	8.	0.1	1342.6	29	SEP	2306	172	4.	0.0	1342.5
29	SEP	1100	51	8.	0.1	1342.6	29	SEP	1706	112	8.	0.1	1342.6	29	SEP	2312	173	4.	0.0	1342.5

29 SEP 1106	52	8.	0.1	1342.6	*	29 SEP 1712	113	8.	0.1	1342.6	*	29 SEP 2318	174	4.	0.0	1342.5	
29 SEP 1112	53	9.	0.1	1342.7	*	29 SEP 1718	114	8.	0.1	1342.6	*	29 SEP 2324	175	4.	0.0	1342.5	
29 SEP 1118	54	10.	0.1	1342.7	*	29 SEP 1724	115	8.	0.1	1342.6	*	29 SEP 2330	176	4.	0.0	1342.5	
29 SEP 1124	55	11.	0.1	1342.7	*	29 SEP 1730	116	8.	0.1	1342.6	*	29 SEP 2336	177	4.	0.0	1342.5	
29 SEP 1130	56	12.	0.1	1342.7	*	29 SEP 1736	117	7.	0.1	1342.6	*	29 SEP 2342	178	4.	0.0	1342.5	
29 SEP 1136	57	15.	0.1	1342.8	*	29 SEP 1742	118	7.	0.1	1342.6	*	29 SEP 2348	179	4.	0.0	1342.5	
29 SEP 1142	58	25.	0.2	1343.0	*	29 SEP 1748	119	7.	0.1	1342.6	*	29 SEP 2354	180	4.	0.0	1342.5	
29 SEP 1148	59	48.	0.3	1343.3	*	29 SEP 1754	120	7.	0.1	1342.6	*	30 SEP 0000	181	4.	0.0	1342.5	
29 SEP 1154	60	75.	0.4	1343.6	*	29 SEP 1800	121	6.	0.1	1342.6	*						
29 SEP 1200	61	90.	0.5	1343.7	*	29 SEP 1806	122	6.	0.1	1342.6	*						
					*						*						

****

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	18.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 96.	6.20		32.	14.	14.	14.
		(INCHES)	3.234	4.157	4.157	4.157
		(AC-FT)	16.	21.	21.	21.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	18.00-HR
+ (AC-FT)	(HR)				
0.	6.20	0.	0.	0.	0.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	18.00-HR
+ (FEET)	(HR)				
1343.77	6.20	1343.00	1342.69	1342.69	1342.69

CUMULATIVE AREA = 0.09 SQ MI

*** ***

```
              **************
              *            *
   70 KK      *   23.3AC   *
              *            *
              **************
```

3 IN TIME DATA FOR INPUT TIME SERIES

JXMIN	30	TIME INTERVAL IN MINUTES
JXDATE	29SEP92	STARTING DATE
JXTIME	600	STARTING TIME

SUBBASIN RUNOFF DATA

71 BA SUBBASIN CHARACTERISTICS

TAREA	0.04	SUBBASIN AREA

PRECIPITATION DATA

72 PB	STORM	7.80	BASIN TOTAL PRECIPITATION

73 PI INCREMENTAL PRECIPITATION PATTERN

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.08	0.08	0.08	0.08	0.08
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

77 LS SCS LOSS RATE

```
                STRTL       0.67  INITIAL ABSTRACTION
                CRVNBR     75.00  CURVE NUMBER
                RTIMP       0.00  PERCENT IMPERVIOUS AREA

 78 UD        SCS DIMENSIONLESS UNITGRAPH
                TLAG        0.15  LAG

                                                ***

WARNING *** TIME INTERVAL IS GREATER THAN .29*LAG

                                          UNIT HYDROGRAPH
                                      10 END-OF-PERIOD ORDINATES
            42.      89.      60.      25.      11.       5.       2.       1.       0.       0.

************************************************************************************************************************

                                      HYDROGRAPH AT STATION   23.3AC

************************************************************************************************************************
```

DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
29 SEP 0600	1	0.00	0.00	0.00	0.	29 SEP 1506	92	0.03	0.00	0.02	5.
29 SEP 0606	2	0.02	0.02	0.00	0.	29 SEP 1512	93	0.03	0.00	0.02	5.
29 SEP 0612	3	0.02	0.02	0.00	0.	29 SEP 1518	94	0.03	0.00	0.02	5.
29 SEP 0618	4	0.02	0.02	0.00	0.	29 SEP 1524	95	0.03	0.00	0.02	5.
29 SEP 0624	5	0.02	0.02	0.00	0.	29 SEP 1530	96	0.03	0.00	0.02	5.
29 SEP 0630	6	0.02	0.02	0.00	0.	29 SEP 1536	97	0.03	0.00	0.02	5.
29 SEP 0636	7	0.02	0.02	0.00	0.	29 SEP 1542	98	0.03	0.00	0.02	5.
29 SEP 0642	8	0.02	0.02	0.00	0.	29 SEP 1548	99	0.03	0.00	0.02	5.
29 SEP 0648	9	0.02	0.02	0.00	0.	29 SEP 1554	100	0.03	0.00	0.02	5.
29 SEP 0654	10	0.02	0.02	0.00	0.	29 SEP 1600	101	0.03	0.00	0.02	5.
29 SEP 0700	11	0.02	0.02	0.00	0.	29 SEP 1606	102	0.02	0.00	0.01	5.
29 SEP 0706	12	0.02	0.02	0.00	0.	29 SEP 1612	103	0.02	0.00	0.01	4.
29 SEP 0712	13	0.02	0.02	0.00	0.	29 SEP 1618	104	0.02	0.00	0.01	4.
29 SEP 0718	14	0.02	0.02	0.00	0.	29 SEP 1624	105	0.02	0.00	0.01	4.
29 SEP 0724	15	0.02	0.02	0.00	0.	29 SEP 1630	106	0.02	0.00	0.01	4.
29 SEP 0730	16	0.02	0.02	0.00	0.	29 SEP 1636	107	0.02	0.00	0.01	4.
29 SEP 0736	17	0.02	0.02	0.00	0.	29 SEP 1642	108	0.02	0.00	0.01	4.
29 SEP 0742	18	0.02	0.02	0.00	0.	29 SEP 1648	109	0.02	0.00	0.01	4.
29 SEP 0748	19	0.02	0.02	0.00	0.	29 SEP 1654	110	0.02	0.00	0.01	4.
29 SEP 0754	20	0.02	0.02	0.00	0.	29 SEP 1700	111	0.02	0.00	0.01	4.
29 SEP 0800	21	0.02	0.02	0.00	0.	29 SEP 1706	112	0.02	0.00	0.01	4.
29 SEP 0806	22	0.02	0.02	0.00	0.	29 SEP 1712	113	0.02	0.00	0.01	4.
29 SEP 0812	23	0.02	0.02	0.00	0.	29 SEP 1718	114	0.02	0.00	0.01	4.
29 SEP 0818	24	0.02	0.02	0.00	0.	29 SEP 1724	115	0.02	0.00	0.01	4.
29 SEP 0824	25	0.02	0.02	0.00	0.	29 SEP 1730	116	0.02	0.00	0.01	4.
29 SEP 0830	26	0.02	0.02	0.00	0.	29 SEP 1736	117	0.01	0.00	0.01	3.
29 SEP 0836	27	0.02	0.02	0.00	0.	29 SEP 1742	118	0.01	0.00	0.01	3.
29 SEP 0842	28	0.02	0.02	0.00	0.	29 SEP 1748	119	0.01	0.00	0.01	2.
29 SEP 0848	29	0.02	0.02	0.00	0.	29 SEP 1754	120	0.01	0.00	0.01	2.
29 SEP 0854	30	0.02	0.02	0.00	0.	29 SEP 1800	121	0.01	0.00	0.01	2.
29 SEP 0900	31	0.02	0.02	0.00	0.	29 SEP 1806	122	0.02	0.00	0.01	2.
29 SEP 0906	32	0.03	0.03	0.00	0.	29 SEP 1812	123	0.02	0.00	0.01	3.
29 SEP 0912	33	0.03	0.03	0.00	0.	29 SEP 1818	124	0.02	0.00	0.01	3.
29 SEP 0918	34	0.03	0.03	0.00	0.	29 SEP 1824	125	0.02	0.00	0.01	3.
29 SEP 0924	35	0.03	0.03	0.00	0.	29 SEP 1830	126	0.02	0.00	0.01	3.
29 SEP 0930	36	0.03	0.03	0.00	0.	29 SEP 1836	127	0.02	0.00	0.01	3.
29 SEP 0936	37	0.03	0.03	0.00	0.	29 SEP 1842	128	0.02	0.00	0.01	3.
29 SEP 0942	38	0.03	0.03	0.00	0.	29 SEP 1848	129	0.02	0.00	0.01	3.
29 SEP 0948	39	0.03	0.03	0.00	0.	29 SEP 1854	130	0.02	0.00	0.01	3.
29 SEP 0954	40	0.03	0.03	0.00	0.	29 SEP 1900	131	0.02	0.00	0.01	3.
29 SEP 1000	41	0.03	0.03	0.00	1.	29 SEP 1906	132	0.02	0.00	0.01	3.
29 SEP 1006	42	0.04	0.03	0.00	1.	29 SEP 1912	133	0.02	0.00	0.01	3.
29 SEP 1012	43	0.04	0.03	0.01	1.	29 SEP 1918	134	0.02	0.00	0.01	3.
29 SEP 1018	44	0.04	0.03	0.01	1.	29 SEP 1924	135	0.02	0.00	0.01	3.
29 SEP 1024	45	0.04	0.03	0.01	1.	29 SEP 1930	136	0.02	0.00	0.01	3.
29 SEP 1030	46	0.04	0.03	0.01	1.	29 SEP 1936	137	0.02	0.00	0.01	3.
29 SEP 1036	47	0.05	0.04	0.01	2.	29 SEP 1942	138	0.02	0.00	0.01	3.
29 SEP 1042	48	0.05	0.04	0.01	2.	29 SEP 1948	139	0.02	0.00	0.01	3.
29 SEP 1048	49	0.05	0.04	0.01	3.	29 SEP 1954	140	0.02	0.00	0.01	3.
29 SEP 1054	50	0.05	0.04	0.01	3.	29 SEP 2000	141	0.02	0.00	0.01	3.
29 SEP 1100	51	0.05	0.04	0.02	3.	29 SEP 2006	142	0.01	0.00	0.01	3.
29 SEP 1106	52	0.08	0.06	0.03	4.	29 SEP 2012	143	0.01	0.00	0.01	3.
29 SEP 1112	53	0.08	0.05	0.03	5.	29 SEP 2018	144	0.01	0.00	0.01	2.
29 SEP 1118	54	0.08	0.05	0.03	6.	29 SEP 2024	145	0.01	0.00	0.01	2.
29 SEP 1124	55	0.08	0.05	0.03	7.	29 SEP 2030	146	0.01	0.00	0.01	2.
29 SEP 1130	56	0.08	0.05	0.03	7.	29 SEP 2036	147	0.01	0.00	0.01	2.
29 SEP 1136	57	0.64	0.32	0.32	19.	29 SEP 2042	148	0.01	0.00	0.01	2.

29 SEP 1142	58	0.64	0.25	0.39	48.	*	29 SEP 2048	149	0.01	0.00	0.01	2.
29 SEP 1148	59	0.64	0.20	0.44	74.	*	29 SEP 2054	150	0.01	0.00	0.01	2.
29 SEP 1154	60	0.64	0.16	0.48	92.	*	29 SEP 2100	151	0.01	0.00	0.01	2.
29 SEP 1200	61	0.64	0.14	0.51	104.	*	29 SEP 2106	152	0.01	0.00	0.01	2.
29 SEP 1206	62	0.12	0.02	0.10	95.	*	29 SEP 2112	153	0.01	0.00	0.01	2.
29 SEP 1212	63	0.12	0.02	0.10	63.	*	29 SEP 2118	154	0.01	0.00	0.01	2.
29 SEP 1218	64	0.12	0.02	0.10	40.	*	29 SEP 2124	155	0.01	0.00	0.01	2.
29 SEP 1224	65	0.12	0.02	0.10	31.	*	29 SEP 2130	156	0.01	0.00	0.01	2.
29 SEP 1230	66	0.12	0.02	0.10	27.	*	29 SEP 2136	157	0.01	0.00	0.01	2.
29 SEP 1236	67	0.06	0.01	0.05	23.	*	29 SEP 2142	158	0.01	0.00	0.01	2.
29 SEP 1242	68	0.06	0.01	0.05	18.	*	29 SEP 2148	159	0.01	0.00	0.01	2.
29 SEP 1248	69	0.06	0.01	0.05	15.	*	29 SEP 2154	160	0.01	0.00	0.01	2.
29 SEP 1254	70	0.06	0.01	0.05	13.	*	29 SEP 2200	161	0.01	0.00	0.01	2.
29 SEP 1300	71	0.06	0.01	0.05	13.	*	29 SEP 2206	162	0.01	0.00	0.01	2.
29 SEP 1306	72	0.05	0.01	0.04	12.	*	29 SEP 2212	163	0.01	0.00	0.01	2.
29 SEP 1312	73	0.05	0.01	0.04	11.	*	29 SEP 2218	164	0.01	0.00	0.01	2.
29 SEP 1318	74	0.05	0.01	0.04	10.	*	29 SEP 2224	165	0.01	0.00	0.01	2.
29 SEP 1324	75	0.05	0.01	0.04	9.	*	29 SEP 2230	166	0.01	0.00	0.01	2.
29 SEP 1330	76	0.05	0.01	0.04	9.	*	29 SEP 2236	167	0.01	0.00	0.01	2.
29 SEP 1336	77	0.04	0.01	0.03	9.	*	29 SEP 2242	168	0.01	0.00	0.01	2.
29 SEP 1342	78	0.04	0.01	0.03	8.	*	29 SEP 2248	169	0.01	0.00	0.01	2.
29 SEP 1348	79	0.04	0.01	0.03	8.	*	29 SEP 2254	170	0.01	0.00	0.01	2.
29 SEP 1354	80	0.04	0.01	0.03	7.	*	29 SEP 2300	171	0.01	0.00	0.01	2.
29 SEP 1400	81	0.04	0.00	0.03	7.	*	29 SEP 2306	172	0.01	0.00	0.01	2.
29 SEP 1406	82	0.03	0.00	0.02	7.	*	29 SEP 2312	173	0.01	0.00	0.01	2.
29 SEP 1412	83	0.03	0.00	0.02	6.	*	29 SEP 2318	174	0.01	0.00	0.01	2.
29 SEP 1418	84	0.03	0.00	0.02	6.	*	29 SEP 2324	175	0.01	0.00	0.01	2.
29 SEP 1424	85	0.03	0.00	0.02	5.	*	29 SEP 2330	176	0.01	0.00	0.01	2.
29 SEP 1430	86	0.03	0.00	0.02	5.	*	29 SEP 2336	177	0.01	0.00	0.01	2.
29 SEP 1436	87	0.03	0.00	0.02	5.	*	29 SEP 2342	178	0.01	0.00	0.01	2.
29 SEP 1442	88	0.03	0.00	0.02	5.	*	29 SEP 2348	179	0.01	0.00	0.01	2.
29 SEP 1448	89	0.03	0.00	0.02	5.	*	29 SEP 2354	180	0.01	0.00	0.01	2.
29 SEP 1454	90	0.03	0.00	0.02	5.	*	30 SEP 0000	181	0.01	0.00	0.01	2.
29 SEP 1500	91	0.03	0.00	0.02	5.	*						
						*						

****

TOTAL RAINFALL = 7.80, TOTAL LOSS = 2.94, TOTAL EXCESS = 4.86

	PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
				6-HR	24-HR	72-HR	18.00-HR
+	(CFS)	(HR)					
			(CFS)				
+	104.	6.00		16.	6.	6.	6.
			(INCHES)	4.000	4.842	4.842	4.842
			(AC-FT)	8.	9.	9.	9.

CUMULATIVE AREA = 0.04 SQ MI

*** ***

```
          **************
          *            *
79 KK     *    POND4   *
          *            *
          **************
```

HYDROGRAPH ROUTING DATA

```
80 RS       STORAGE ROUTING
                 NSTPS          1  NUMBER OF SUBREACHES
                  ITYP       ELEV  TYPE OF INITIAL CONDITION
                 RSVRIC    1345.00  INITIAL CONDITION
                     X        0.00 WORKING R AND D COEFFICIENT

81 SA            AREA         1.0       1.4

82 SE         ELEVATION    1345.00   1349.00

83 SQ         DISCHARGE          0.       15.       18.       20.       24.

84 SE         ELEVATION    1345.00   1345.86   1348.88   1351.20   1356.57
```

***

COMPUTED STORAGE-ELEVATION DATA

STORAGE	0.00	4.68
ELEVATION	1345.00	1349.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	0.00	0.89	4.52	4.68	7.89	17.83
OUTFLOW	0.00	15.00	18.00	18.10	20.00	24.00
ELEVATION	1345.00	1345.86	1348.88	1349.00	1351.20	1356.57

****

HYDROGRAPH AT STATION POND4

****

DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE
29	SEP	0600	1	0.	0.0	1345.0	29	SEP	1206	62	17.	2.8	1347.5	29	SEP	1812	123	4.	0.2	1345.2
29	SEP	0606	2	0.	0.0	1345.0	29	SEP	1212	63	17.	3.4	1347.9	29	SEP	1818	124	4.	0.2	1345.2
29	SEP	0612	3	0.	0.0	1345.0	29	SEP	1218	64	17.	3.6	1348.2	29	SEP	1824	125	4.	0.2	1345.2
29	SEP	0618	4	0.	0.0	1345.0	29	SEP	1224	65	17.	3.8	1348.3	29	SEP	1830	126	4.	0.2	1345.2
29	SEP	0624	5	0.	0.0	1345.0	29	SEP	1230	66	17.	3.9	1348.4	29	SEP	1836	127	4.	0.2	1345.2
29	SEP	0630	6	0.	0.0	1345.0	29	SEP	1236	67	18.	4.0	1348.4	29	SEP	1842	128	4.	0.2	1345.2
29	SEP	0636	7	0.	0.0	1345.0	29	SEP	1242	68	18.	4.0	1348.4	29	SEP	1848	129	4.	0.2	1345.2
29	SEP	0642	8	0.	0.0	1345.0	29	SEP	1248	69	18.	4.0	1348.4	29	SEP	1854	130	4.	0.2	1345.2
29	SEP	0648	9	0.	0.0	1345.0	29	SEP	1254	70	18.	3.9	1348.4	29	SEP	1900	131	3.	0.2	1345.2
29	SEP	0654	10	0.	0.0	1345.0	29	SEP	1300	71	17.	3.9	1348.4	29	SEP	1906	132	3.	0.2	1345.2
29	SEP	0700	11	0.	0.0	1345.0	29	SEP	1306	72	17.	3.9	1348.3	29	SEP	1912	133	3.	0.2	1345.2
29	SEP	0706	12	0.	0.0	1345.0	29	SEP	1312	73	17.	3.8	1348.3	29	SEP	1918	134	3.	0.2	1345.2
29	SEP	0712	13	0.	0.0	1345.0	29	SEP	1318	74	17.	3.8	1348.2	29	SEP	1924	135	3.	0.2	1345.2
29	SEP	0718	14	0.	0.0	1345.0	29	SEP	1324	75	17.	3.7	1348.2	29	SEP	1930	136	3.	0.2	1345.2
29	SEP	0724	15	0.	0.0	1345.0	29	SEP	1330	76	17.	3.6	1348.1	29	SEP	1936	137	3.	0.2	1345.2
29	SEP	0730	16	0.	0.0	1345.0	29	SEP	1336	77	17.	3.6	1348.1	29	SEP	1942	138	3.	0.2	1345.2
29	SEP	0736	17	0.	0.0	1345.0	29	SEP	1342	78	17.	3.5	1348.0	29	SEP	1948	139	3.	0.2	1345.2
29	SEP	0742	18	0.	0.0	1345.0	29	SEP	1348	79	17.	3.4	1348.0	29	SEP	1954	140	3.	0.2	1345.2
29	SEP	0748	19	0.	0.0	1345.0	29	SEP	1354	80	17.	3.3	1347.9	29	SEP	2000	141	3.	0.2	1345.2
29	SEP	0754	20	0.	0.0	1345.0	29	SEP	1400	81	17.	3.3	1347.8	29	SEP	2006	142	3.	0.2	1345.2
29	SEP	0800	21	0.	0.0	1345.0	29	SEP	1406	82	17.	3.2	1347.8	29	SEP	2012	143	3.	0.2	1345.2
29	SEP	0806	22	0.	0.0	1345.0	29	SEP	1412	83	17.	3.1	1347.7	29	SEP	2018	144	3.	0.2	1345.2
29	SEP	0812	23	0.	0.0	1345.0	29	SEP	1418	84	17.	3.0	1347.6	29	SEP	2024	145	3.	0.2	1345.2
29	SEP	0818	24	0.	0.0	1345.0	29	SEP	1424	85	17.	2.9	1347.5	29	SEP	2030	146	3.	0.2	1345.2
29	SEP	0824	25	0.	0.0	1345.0	29	SEP	1430	86	17.	2.8	1347.5	29	SEP	2036	147	3.	0.2	1345.2
29	SEP	0830	26	0.	0.0	1345.0	29	SEP	1436	87	17.	2.7	1347.4	29	SEP	2042	148	3.	0.2	1345.2
29	SEP	0836	27	0.	0.0	1345.0	29	SEP	1442	88	16.	2.6	1347.3	29	SEP	2048	149	3.	0.2	1345.2
29	SEP	0842	28	0.	0.0	1345.0	29	SEP	1448	89	16.	2.5	1347.2	29	SEP	2054	150	3.	0.2	1345.1
29	SEP	0848	29	0.	0.0	1345.0	29	SEP	1454	90	16.	2.4	1347.1	29	SEP	2100	151	3.	0.1	1345.1
29	SEP	0854	30	0.	0.0	1345.0	29	SEP	1500	91	16.	2.3	1347.1	29	SEP	2106	152	2.	0.1	1345.1
29	SEP	0900	31	0.	0.0	1345.0	29	SEP	1506	92	16.	2.3	1347.0	29	SEP	2112	153	2.	0.1	1345.1
29	SEP	0906	32	0.	0.0	1345.0	29	SEP	1512	93	16.	2.2	1346.9	29	SEP	2118	154	2.	0.1	1345.1
29	SEP	0912	33	0.	0.0	1345.0	29	SEP	1518	94	16.	2.1	1346.8	29	SEP	2124	155	2.	0.1	1345.1
29	SEP	0918	34	0.	0.0	1345.0	29	SEP	1524	95	16.	2.0	1346.8	29	SEP	2130	156	2.	0.1	1345.1
29	SEP	0924	35	0.	0.0	1345.0	29	SEP	1530	96	16.	1.9	1346.7	29	SEP	2136	157	2.	0.1	1345.1
29	SEP	0930	36	0.	0.0	1345.0	29	SEP	1536	97	16.	1.8	1346.6	29	SEP	2142	158	2.	0.1	1345.1
29	SEP	0936	37	0.	0.0	1345.0	29	SEP	1542	98	16.	1.7	1346.6	29	SEP	2148	159	2.	0.1	1345.1
29	SEP	0942	38	0.	0.0	1345.0	29	SEP	1548	99	16.	1.6	1346.5	29	SEP	2154	160	2.	0.1	1345.1
29	SEP	0948	39	0.	0.0	1345.0	29	SEP	1554	100	16.	1.6	1346.4	29	SEP	2200	161	2.	0.1	1345.1
29	SEP	0954	40	0.	0.0	1345.0	29	SEP	1600	101	15.	1.5	1346.3	29	SEP	2206	162	2.	0.1	1345.1
29	SEP	1000	41	0.	0.0	1345.0	29	SEP	1606	102	15.	1.4	1346.3	29	SEP	2212	163	2.	0.1	1345.1
29	SEP	1006	42	0.	0.0	1345.0	29	SEP	1612	103	15.	1.3	1346.2	29	SEP	2218	164	2.	0.1	1345.1
29	SEP	1012	43	0.	0.0	1345.0	29	SEP	1618	104	15.	1.2	1346.1	29	SEP	2224	165	2.	0.1	1345.1
29	SEP	1018	44	0.	0.0	1345.0	29	SEP	1624	105	15.	1.1	1346.0	29	SEP	2230	166	2.	0.1	1345.1
29	SEP	1024	45	0.	0.0	1345.0	29	SEP	1630	106	15.	1.0	1346.0	29	SEP	2236	167	2.	0.1	1345.1
29	SEP	1030	46	1.	0.0	1345.0	29	SEP	1636	107	15.	0.9	1345.9	29	SEP	2242	168	2.	0.1	1345.1
29	SEP	1036	47	1.	0.0	1345.0	29	SEP	1642	108	14.	0.8	1345.8	29	SEP	2248	169	2.	0.1	1345.1
29	SEP	1042	48	1.	0.1	1345.1	29	SEP	1648	109	13.	0.7	1345.7	29	SEP	2254	170	2.	0.1	1345.1
29	SEP	1048	49	1.	0.1	1345.1	29	SEP	1654	110	11.	0.7	1345.6	29	SEP	2300	171	2.	0.1	1345.1
29	SEP	1054	50	1.	0.1	1345.1	29	SEP	1700	111	10.	0.6	1345.6	29	SEP	2306	172	2.	0.1	1345.1
29	SEP	1100	51	2.	0.1	1345.1	29	SEP	1706	112	9.	0.6	1345.5	29	SEP	2312	173	2.	0.1	1345.1
29	SEP	1106	52	2.	0.1	1345.1	29	SEP	1712	113	9.	0.5	1345.5	29	SEP	2318	174	2.	0.1	1345.1
29	SEP	1112	53	2.	0.1	1345.1	29	SEP	1718	114	8.	0.5	1345.5	29	SEP	2324	175	2.	0.1	1345.1
29	SEP	1118	54	3.	0.2	1345.1	29	SEP	1724	115	7.	0.4	1345.4	29	SEP	2330	176	2.	0.1	1345.1
29	SEP	1124	55	3.	0.2	1345.2	29	SEP	1730	116	7.	0.4	1345.4	29	SEP	2336	177	2.	0.1	1345.1
29	SEP	1130	56	4.	0.2	1345.2	29	SEP	1736	117	6.	0.4	1345.4	29	SEP	2342	178	2.	0.1	1345.1
29	SEP	1136	57	5.	0.3	1345.3	29	SEP	1742	118	6.	0.4	1345.3	29	SEP	2348	179	2.	0.1	1345.1
29	SEP	1142	58	9.	0.5	1345.5	29	SEP	1748	119	6.	0.3	1345.3	29	SEP	2354	180	2.	0.1	1345.1
29	SEP	1148	59	15.	0.9	1345.9	29	SEP	1754	120	5.	0.3	1345.3	30	SEP	0000	181	2.	0.1	1345.1
29	SEP	1154	60	15.	1.5	1346.3	29	SEP	1800	121	5.	0.3	1345.3							
29	SEP	1200	61	16.	2.2	1346.9	29	SEP	1806	122	4.	0.3	1345.3							

```
*********************************************************************************************************

  PEAK FLOW     TIME                              MAXIMUM AVERAGE FLOW
                                         6-HR       24-HR      72-HR     18.00-HR
 +  (CFS)       (HR)
                           (CFS)
 +     18.      6.70                      15.          6.         6.          6.
                         (INCHES)        3.870      4.777      4.777       4.777
                          (AC-FT)          8.          9.         9.          9.

 PEAK STORAGE   TIME                            MAXIMUM AVERAGE STORAGE
                                         6-HR       24-HR      72-HR     18.00-HR
 + (AC-FT)      (HR)
        4.      6.70                       2.          1.         1.          1.

  PEAK STAGE    TIME                             MAXIMUM AVERAGE STAGE
                                         6-HR       24-HR      72-HR     18.00-HR
 +  (FEET)      (HR)
   1348.43      6.70                   1347.01    1345.74    1345.74     1345.74

                         CUMULATIVE AREA =     0.04 SQ MI


*** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** ***


              **************
              *            *
  85 KK       *    8.3AC   *
              *            *
              **************

   3 IN          TIME DATA FOR INPUT TIME SERIES
                       JXMIN          30  TIME INTERVAL IN MINUTES
                      JXDATE     29SEP92  STARTING DATE
                      JXTIME         600  STARTING TIME

               SUBBASIN RUNOFF DATA

  86 BA          SUBBASIN CHARACTERISTICS
                       TAREA        0.01  SUBBASIN AREA

                 PRECIPITATION DATA

  87 PB                STORM        7.80  BASIN TOTAL PRECIPITATION

  88 PI            INCREMENTAL PRECIPITATION PATTERN
                        0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                        0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                        0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                        0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                        0.00      0.00      0.00      0.00      0.00      0.01      0.01      0.01      0.01      0.01
                        0.01      0.01      0.01      0.01      0.01      0.08      0.08      0.08      0.08      0.08
                        0.01      0.01      0.01      0.01      0.01      0.01      0.01      0.01      0.01      0.01
                        0.01      0.01      0.01      0.01      0.01      0.00      0.00      0.00      0.00      0.00
                        0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                        0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                        0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                        0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                        0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                        0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                        0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                        0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                        0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00
                        0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00      0.00

  92 LS          SCS LOSS RATE
                       STRTL        0.35  INITIAL ABSTRACTION
                      CRVNBR       85.00  CURVE NUMBER
                       RTIMP        0.00  PERCENT IMPERVIOUS AREA

  93 UD          SCS DIMENSIONLESS UNITGRAPH
                        TLAG        0.15  LAG

                                          ***

 WARNING *** TIME INTERVAL IS GREATER THAN .29*LAG
```

UNIT HYDROGRAPH
10 END-OF-PERIOD ORDINATES

15. 32. 21. 9. 4. 2. 1. 0. 0. 0.

HYDROGRAPH AT STATION 8.3AC

DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
29	SEP	0600	1	0.00	0.00	0.00	0.	29	SEP	1506	92	0.03	0.00	0.02	2.
29	SEP	0606	2	0.02	0.02	0.00	0.	29	SEP	1512	93	0.03	0.00	0.02	2.
29	SEP	0612	3	0.02	0.02	0.00	0.	29	SEP	1518	94	0.03	0.00	0.02	2.
29	SEP	0618	4	0.02	0.02	0.00	0.	29	SEP	1524	95	0.03	0.00	0.02	2.
29	SEP	0624	5	0.02	0.02	0.00	0.	29	SEP	1530	96	0.03	0.00	0.02	2.
29	SEP	0630	6	0.02	0.02	0.00	0.	29	SEP	1536	97	0.03	0.00	0.02	2.
29	SEP	0636	7	0.02	0.02	0.00	0.	29	SEP	1542	98	0.03	0.00	0.02	2.
29	SEP	0642	8	0.02	0.02	0.00	0.	29	SEP	1548	99	0.03	0.00	0.02	2.
29	SEP	0648	9	0.02	0.02	0.00	0.	29	SEP	1554	100	0.03	0.00	0.02	2.
29	SEP	0654	10	0.02	0.02	0.00	0.	29	SEP	1600	101	0.03	0.00	0.02	2.
29	SEP	0700	11	0.02	0.02	0.00	0.	29	SEP	1606	102	0.02	0.00	0.02	2.
29	SEP	0706	12	0.02	0.02	0.00	0.	29	SEP	1612	103	0.02	0.00	0.02	2.
29	SEP	0712	13	0.02	0.02	0.00	0.	29	SEP	1618	104	0.02	0.00	0.02	1.
29	SEP	0718	14	0.02	0.02	0.00	0.	29	SEP	1624	105	0.02	0.00	0.02	1.
29	SEP	0724	15	0.02	0.02	0.00	0.	29	SEP	1630	106	0.02	0.00	0.02	1.
29	SEP	0730	16	0.02	0.02	0.00	0.	29	SEP	1636	107	0.02	0.00	0.02	1.
29	SEP	0736	17	0.02	0.02	0.00	0.	29	SEP	1642	108	0.02	0.00	0.02	1.
29	SEP	0742	18	0.02	0.02	0.00	0.	29	SEP	1648	109	0.02	0.00	0.02	1.
29	SEP	0748	19	0.02	0.02	0.00	0.	29	SEP	1654	110	0.02	0.00	0.02	1.
29	SEP	0754	20	0.02	0.02	0.00	0.	29	SEP	1700	111	0.02	0.00	0.02	1.
29	SEP	0800	21	0.02	0.02	0.00	0.	29	SEP	1706	112	0.02	0.00	0.02	1.
29	SEP	0806	22	0.02	0.02	0.00	0.	29	SEP	1712	113	0.02	0.00	0.02	1.
29	SEP	0812	23	0.02	0.02	0.00	0.	29	SEP	1718	114	0.02	0.00	0.02	1.
29	SEP	0818	24	0.02	0.02	0.00	0.	29	SEP	1724	115	0.02	0.00	0.02	1.
29	SEP	0824	25	0.02	0.02	0.00	0.	29	SEP	1730	116	0.02	0.00	0.02	1.
29	SEP	0830	26	0.02	0.02	0.00	0.	29	SEP	1736	117	0.01	0.00	0.01	1.
29	SEP	0836	27	0.02	0.02	0.00	0.	29	SEP	1742	118	0.01	0.00	0.01	1.
29	SEP	0842	28	0.02	0.02	0.00	0.	29	SEP	1748	119	0.01	0.00	0.01	1.
29	SEP	0848	29	0.02	0.02	0.00	0.	29	SEP	1754	120	0.01	0.00	0.01	1.
29	SEP	0854	30	0.02	0.02	0.00	0.	29	SEP	1800	121	0.01	0.00	0.01	1.
29	SEP	0900	31	0.02	0.02	0.00	0.	29	SEP	1806	122	0.02	0.00	0.01	1.
29	SEP	0906	32	0.03	0.02	0.01	0.	29	SEP	1812	123	0.02	0.00	0.01	1.
29	SEP	0912	33	0.03	0.02	0.01	0.	29	SEP	1818	124	0.02	0.00	0.01	1.
29	SEP	0918	34	0.03	0.02	0.01	1.	29	SEP	1824	125	0.02	0.00	0.01	1.
29	SEP	0924	35	0.03	0.02	0.01	1.	29	SEP	1830	126	0.02	0.00	0.01	1.
29	SEP	0930	36	0.03	0.02	0.01	1.	29	SEP	1836	127	0.02	0.00	0.01	1.
29	SEP	0936	37	0.03	0.02	0.01	1.	29	SEP	1842	128	0.02	0.00	0.01	1.
29	SEP	0942	38	0.03	0.02	0.01	1.	29	SEP	1848	129	0.02	0.00	0.01	1.
29	SEP	0948	39	0.03	0.02	0.01	1.	29	SEP	1854	130	0.02	0.00	0.01	1.
29	SEP	0954	40	0.03	0.02	0.01	1.	29	SEP	1900	131	0.02	0.00	0.01	1.
29	SEP	1000	41	0.03	0.02	0.01	1.	29	SEP	1906	132	0.02	0.00	0.01	1.
29	SEP	1006	42	0.04	0.02	0.02	1.	29	SEP	1912	133	0.02	0.00	0.01	1.
29	SEP	1012	43	0.04	0.02	0.02	1.	29	SEP	1918	134	0.02	0.00	0.01	1.
29	SEP	1018	44	0.04	0.02	0.02	1.	29	SEP	1924	135	0.02	0.00	0.01	1.
29	SEP	1024	45	0.04	0.02	0.02	1.	29	SEP	1930	136	0.02	0.00	0.01	1.
29	SEP	1030	46	0.04	0.02	0.02	1.	29	SEP	1936	137	0.02	0.00	0.01	1.
29	SEP	1036	47	0.05	0.03	0.03	2.	29	SEP	1942	138	0.02	0.00	0.01	1.
29	SEP	1042	48	0.05	0.03	0.03	2.	29	SEP	1948	139	0.02	0.00	0.01	1.
29	SEP	1048	49	0.05	0.02	0.03	2.	29	SEP	1954	140	0.02	0.00	0.01	1.
29	SEP	1054	50	0.05	0.02	0.03	2.	29	SEP	2000	141	0.02	0.00	0.01	1.
29	SEP	1100	51	0.05	0.02	0.03	2.	29	SEP	2006	142	0.01	0.00	0.01	1.
29	SEP	1106	52	0.08	0.03	0.05	3.	29	SEP	2012	143	0.01	0.00	0.01	1.
29	SEP	1112	53	0.08	0.03	0.05	3.	29	SEP	2018	144	0.01	0.00	0.01	1.
29	SEP	1118	54	0.08	0.03	0.05	4.	29	SEP	2024	145	0.01	0.00	0.01	1.
29	SEP	1124	55	0.08	0.03	0.05	4.	29	SEP	2030	146	0.01	0.00	0.01	1.
29	SEP	1130	56	0.08	0.03	0.05	4.	29	SEP	2036	147	0.01	0.00	0.01	1.
29	SEP	1136	57	0.64	0.17	0.47	11.	29	SEP	2042	148	0.01	0.00	0.01	1.
29	SEP	1142	58	0.64	0.12	0.52	25.	29	SEP	2048	149	0.01	0.00	0.01	1.
29	SEP	1148	59	0.64	0.09	0.55	36.	29	SEP	2054	150	0.01	0.00	0.01	1.
29	SEP	1154	60	0.64	0.07	0.57	42.	29	SEP	2100	151	0.01	0.00	0.01	1.
29	SEP	1200	61	0.64	0.06	0.59	45.	29	SEP	2106	152	0.01	0.00	0.01	1.
29	SEP	1206	62	0.12	0.01	0.11	40.	29	SEP	2112	153	0.01	0.00	0.01	1.
29	SEP	1212	63	0.12	0.01	0.11	26.	29	SEP	2118	154	0.01	0.00	0.01	1.
29	SEP	1218	64	0.12	0.01	0.11	17.	29	SEP	2124	155	0.01	0.00	0.01	1.
29	SEP	1224	65	0.12	0.01	0.11	13.	29	SEP	2130	156	0.01	0.00	0.01	1.
29	SEP	1230	66	0.12	0.01	0.11	11.	29	SEP	2136	157	0.01	0.00	0.01	1.
29	SEP	1236	67	0.06	0.00	0.06	9.	29	SEP	2142	158	0.01	0.00	0.01	1.
29	SEP	1242	68	0.06	0.00	0.06	7.	29	SEP	2148	159	0.01	0.00	0.01	1.

29 SEP 1248	69	0.06	0.00	0.06	6.	*	29 SEP 2154	160	0.01	0.00	0.01	1.
29 SEP 1254	70	0.06	0.00	0.06	5.	*	29 SEP 2200	161	0.01	0.00	0.01	1.
29 SEP 1300	71	0.06	0.00	0.06	5.	*	29 SEP 2206	162	0.01	0.00	0.01	1.
29 SEP 1306	72	0.05	0.00	0.04	5.	*	29 SEP 2212	163	0.01	0.00	0.01	1.
29 SEP 1312	73	0.05	0.00	0.04	4.	*	29 SEP 2218	164	0.01	0.00	0.01	1.
29 SEP 1318	74	0.05	0.00	0.04	4.	*	29 SEP 2224	165	0.01	0.00	0.01	1.
29 SEP 1324	75	0.05	0.00	0.04	4.	*	29 SEP 2230	166	0.01	0.00	0.01	1.
29 SEP 1330	76	0.05	0.00	0.04	4.	*	29 SEP 2236	167	0.01	0.00	0.01	1.
29 SEP 1336	77	0.04	0.00	0.03	3.	*	29 SEP 2242	168	0.01	0.00	0.01	1.
29 SEP 1342	78	0.04	0.00	0.03	3.	*	29 SEP 2248	169	0.01	0.00	0.01	1.
29 SEP 1348	79	0.04	0.00	0.03	3.	*	29 SEP 2254	170	0.01	0.00	0.01	1.
29 SEP 1354	80	0.04	0.00	0.03	3.	*	29 SEP 2300	171	0.01	0.00	0.01	1.
29 SEP 1400	81	0.04	0.00	0.03	3.	*	29 SEP 2306	172	0.01	0.00	0.01	1.
29 SEP 1406	82	0.03	0.00	0.02	3.	*	29 SEP 2312	173	0.01	0.00	0.01	1.
29 SEP 1412	83	0.03	0.00	0.02	2.	*	29 SEP 2318	174	0.01	0.00	0.01	1.
29 SEP 1418	84	0.03	0.00	0.02	2.	*	29 SEP 2324	175	0.01	0.00	0.01	1.
29 SEP 1424	85	0.03	0.00	0.02	2.	*	29 SEP 2330	176	0.01	0.00	0.01	1.
29 SEP 1430	86	0.03	0.00	0.02	2.	*	29 SEP 2336	177	0.01	0.00	0.01	1.
29 SEP 1436	87	0.03	0.00	0.02	2.	*	29 SEP 2342	178	0.01	0.00	0.01	1.
29 SEP 1442	88	0.03	0.00	0.02	2.	*	29 SEP 2348	179	0.01	0.00	0.01	1.
29 SEP 1448	89	0.03	0.00	0.02	2.	*	29 SEP 2354	180	0.01	0.00	0.01	1.
29 SEP 1454	90	0.03	0.00	0.02	2.	*	30 SEP 0000	181	0.01	0.00	0.01	1.
29 SEP 1500	91	0.03	0.00	0.02	2.	*						

****

TOTAL RAINFALL = 7.80, TOTAL LOSS = 1.78, TOTAL EXCESS = 6.02

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	18.00-HR
+ (CFS)	(HR)				
		(CFS)			
+ 45.	6.00	7.	3.	3.	3.
		(INCHES) 4.931	6.000	6.000	6.000
		(AC-FT) 3.	4.	4.	4.

CUMULATIVE AREA = 0.01 SQ MI

*** ***

```
          ***************
          *             *
94 KK     *     INTO5   *
          *             *
          ***************
```

95 HC HYDROGRAPH COMBINATION
ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

***

****

HYDROGRAPH AT STATION INTO5
SUM OF 3 HYDROGRAPHS

****

DA MON HRMN	ORD	FLOW	*	DA MON HRMN	ORD	FLOW	*	DA MON HRMN	ORD	FLOW	*	DA MON HRMN	ORD	FLOW
29 SEP 0600	1	0.	*	29 SEP 1036	47	8.	*	29 SEP 1512	93	29.	*	29 SEP 1948	139	11.
29 SEP 0606	2	0.	*	29 SEP 1042	48	9.	*	29 SEP 1518	94	29.	*	29 SEP 1954	140	11.
29 SEP 0612	3	0.	*	29 SEP 1048	49	10.	*	29 SEP 1524	95	29.	*	29 SEP 2000	141	11.
29 SEP 0618	4	0.	*	29 SEP 1054	50	11.	*	29 SEP 1530	96	29.	*	29 SEP 2006	142	11.
29 SEP 0624	5	0.	*	29 SEP 1100	51	11.	*	29 SEP 1536	97	29.	*	29 SEP 2012	143	11.
29 SEP 0630	6	1.	*	29 SEP 1106	52	13.	*	29 SEP 1542	98	28.	*	29 SEP 2018	144	10.
29 SEP 0636	7	1.	*	29 SEP 1112	53	14.	*	29 SEP 1548	99	28.	*	29 SEP 2024	145	10.
29 SEP 0642	8	1.	*	29 SEP 1118	54	16.	*	29 SEP 1554	100	28.	*	29 SEP 2030	146	10.
29 SEP 0648	9	2.	*	29 SEP 1124	55	18.	*	29 SEP 1600	101	28.	*	29 SEP 2036	147	9.
29 SEP 0654	10	2.	*	29 SEP 1130	56	20.	*	29 SEP 1606	102	28.	*	29 SEP 2042	148	9.
29 SEP 0700	11	2.	*	29 SEP 1136	57	31.	*	29 SEP 1612	103	28.	*	29 SEP 2048	149	9.
29 SEP 0706	12	2.	*	29 SEP 1142	58	59.	*	29 SEP 1618	104	27.	*	29 SEP 2054	150	8.
29 SEP 0712	13	2.	*	29 SEP 1148	59	99.	*	29 SEP 1624	105	26.	*	29 SEP 2100	151	8.
29 SEP 0718	14	2.	*	29 SEP 1154	60	132.	*	29 SEP 1630	106	26.	*	29 SEP 2106	152	8.
29 SEP 0724	15	2.	*	29 SEP 1200	61	152.	*	29 SEP 1636	107	26.	*	29 SEP 2112	153	8.
29 SEP 0730	16	3.	*	29 SEP 1206	62	153.	*	29 SEP 1642	108	24.	*	29 SEP 2118	154	8.

29 SEP 0736	17	3.	*	29 SEP 1212	63	140.	*	29 SEP 1648	109	22.	*	29 SEP 2124	155	8.
29 SEP 0742	18	3.	*	29 SEP 1218	64	127.	*	29 SEP 1654	110	21.	*	29 SEP 2130	156	8.
29 SEP 0748	19	3.	*	29 SEP 1224	65	121.	*	29 SEP 1700	111	20.	*	29 SEP 2136	157	8.
29 SEP 0754	20	3.	*	29 SEP 1230	66	118.	*	29 SEP 1706	112	19.	*	29 SEP 2142	158	8.
29 SEP 0800	21	3.	*	29 SEP 1236	67	115.	*	29 SEP 1712	113	18.	*	29 SEP 2148	159	8.
29 SEP 0806	22	3.	*	29 SEP 1242	68	111.	*	29 SEP 1718	114	17.	*	29 SEP 2154	160	8.
29 SEP 0812	23	3.	*	29 SEP 1248	69	107.	*	29 SEP 1724	115	16.	*	29 SEP 2200	161	8.
29 SEP 0818	24	3.	*	29 SEP 1254	70	103.	*	29 SEP 1730	116	16.	*	29 SEP 2206	162	7.
29 SEP 0824	25	3.	*	29 SEP 1300	71	100.	*	29 SEP 1736	117	15.	*	29 SEP 2212	163	7.
29 SEP 0830	26	3.	*	29 SEP 1306	72	97.	*	29 SEP 1742	118	14.	*	29 SEP 2218	164	7.
29 SEP 0836	27	3.	*	29 SEP 1312	73	92.	*	29 SEP 1748	119	13.	*	29 SEP 2224	165	7.
29 SEP 0842	28	3.	*	29 SEP 1318	74	84.	*	29 SEP 1754	120	13.	*	29 SEP 2230	166	7.
29 SEP 0848	29	4.	*	29 SEP 1324	75	71.	*	29 SEP 1800	121	12.	*	29 SEP 2236	167	7.
29 SEP 0854	30	4.	*	29 SEP 1330	76	59.	*	29 SEP 1806	122	11.	*	29 SEP 2242	168	7.
29 SEP 0900	31	4.	*	29 SEP 1336	77	52.	*	29 SEP 1812	123	11.	*	29 SEP 2248	169	7.
29 SEP 0906	32	4.	*	29 SEP 1342	78	47.	*	29 SEP 1818	124	11.	*	29 SEP 2254	170	7.
29 SEP 0912	33	4.	*	29 SEP 1348	79	43.	*	29 SEP 1824	125	11.	*	29 SEP 2300	171	7.
29 SEP 0918	34	4.	*	29 SEP 1354	80	41.	*	29 SEP 1830	126	11.	*	29 SEP 2306	172	7.
29 SEP 0924	35	5.	*	29 SEP 1400	81	39.	*	29 SEP 1836	127	11.	*	29 SEP 2312	173	7.
29 SEP 0930	36	5.	*	29 SEP 1406	82	38.	*	29 SEP 1842	128	11.	*	29 SEP 2318	174	7.
29 SEP 0936	37	5.	*	29 SEP 1412	83	36.	*	29 SEP 1848	129	11.	*	29 SEP 2324	175	7.
29 SEP 0942	38	5.	*	29 SEP 1418	84	35.	*	29 SEP 1854	130	11.	*	29 SEP 2330	176	7.
29 SEP 0948	39	5.	*	29 SEP 1424	85	33.	*	29 SEP 1900	131	11.	*	29 SEP 2336	177	7.
29 SEP 0954	40	6.	*	29 SEP 1430	86	32.	*	29 SEP 1906	132	11.	*	29 SEP 2342	178	7.
29 SEP 1000	41	6.	*	29 SEP 1436	87	31.	*	29 SEP 1912	133	11.	*	29 SEP 2348	179	7.
29 SEP 1006	42	6.	*	29 SEP 1442	88	31.	*	29 SEP 1918	134	11.	*	29 SEP 2354	180	7.
29 SEP 1012	43	6.	*	29 SEP 1448	89	30.	*	29 SEP 1924	135	11.	*	30 SEP 0000	181	7.
29 SEP 1018	44	7.	*	29 SEP 1454	90	30.	*	29 SEP 1930	136	11.	*			
29 SEP 1024	45	7.	*	29 SEP 1500	91	29.	*	29 SEP 1936	137	11.	*			
29 SEP 1030	46	8.	*	29 SEP 1506	92	29.	*	29 SEP 1942	138	11.	*			

```
*********************************************************************************************************************************

  PEAK FLOW     TIME                      MAXIMUM AVERAGE FLOW
                                 6-HR      24-HR      72-HR     18.00-HR
+   (CFS)       (HR)
                         (CFS)
+    153.       6.10                54.        23.        23.        23.
                       (INCHES)  3.528      4.484      4.484      4.484
                        (AC-FT)    27.        34.        34.        34.

                       CUMULATIVE AREA =    0.14 SQ MI


*** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** ***

              **************
              *            *
  96 KK       *    POND5   *
              *            *
              **************

               HYDROGRAPH ROUTING DATA

  97 RS          STORAGE ROUTING
                       NSTPS          1  NUMBER OF SUBREACHES
                        ITYP       ELEV  TYPE OF INITIAL CONDITION
                      RSVRIC    1335.00  INITIAL CONDITION
                           X       0.00  WORKING R AND D COEFFICIENT

  98 SA                 AREA        2.0       3.3

  99 SE          ELEVATION    1335.00   1340.00

 100 SQ          DISCHARGE         0.        50.       60.       70.       80.       90.      100.      110.      120.      130.
                                 140.       150.

 102 SE          ELEVATION    1335.00   1336.50   1336.90   1337.34   1337.81   1338.34   1338.91   1339.53   1340.19   1340.90
                              1341.60   1342.50

                                                          ***

                                                  COMPUTED STORAGE-ELEVATION DATA

            STORAGE      0.00     13.07
          ELEVATION   1335.00   1340.00
```

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	0.00	3.22	4.17	5.27	6.50	7.96	9.63	11.54	13.07	13.71
OUTFLOW	0.00	50.00	60.00	70.00	80.00	90.00	100.00	110.00	117.12	120.00
ELEVATION	1335.00	1336.50	1336.90	1337.34	1337.81	1338.34	1338.91	1339.53	1340.00	1340.19
STORAGE	16.20	18.81	22.41							
OUTFLOW	130.00	140.00	150.00							
ELEVATION	1340.90	1341.60	1342.50							

HYDROGRAPH AT STATION POND5

DA MON HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA MON HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA MON HRMN	ORD	OUTFLOW	STORAGE	STAGE
29 SEP 0600	1	0.	0.0	1335.0	29 SEP 1206	62	57.	3.9	1336.8	29 SEP 1812	123	17.	1.1	1335.5
29 SEP 0606	2	0.	0.0	1335.0	29 SEP 1212	63	64.	4.6	1337.1	29 SEP 1818	124	16.	1.0	1335.5
29 SEP 0612	3	0.	0.0	1335.0	29 SEP 1218	64	69.	5.2	1337.3	29 SEP 1824	125	15.	1.0	1335.5
29 SEP 0618	4	0.	0.0	1335.0	29 SEP 1224	65	73.	5.6	1337.5	29 SEP 1830	126	15.	1.0	1335.4
29 SEP 0624	5	0.	0.0	1335.0	29 SEP 1230	66	76.	6.0	1337.6	29 SEP 1836	127	14.	0.9	1335.4
29 SEP 0630	6	0.	0.0	1335.0	29 SEP 1236	67	79.	6.3	1337.7	29 SEP 1842	128	14.	0.9	1335.4
29 SEP 0636	7	0.	0.0	1335.0	29 SEP 1242	68	81.	6.6	1337.8	29 SEP 1848	129	14.	0.9	1335.4
29 SEP 0642	8	0.	0.0	1335.0	29 SEP 1248	69	82.	6.8	1337.9	29 SEP 1854	130	13.	0.9	1335.4
29 SEP 0648	9	0.	0.0	1335.0	29 SEP 1254	70	83.	7.0	1338.0	29 SEP 1900	131	13.	0.8	1335.4
29 SEP 0654	10	1.	0.0	1335.0	29 SEP 1300	71	84.	7.1	1338.0	29 SEP 1906	132	13.	0.8	1335.4
29 SEP 0700	11	1.	0.0	1335.0	29 SEP 1306	72	85.	7.3	1338.1	29 SEP 1912	133	13.	0.8	1335.4
29 SEP 0706	12	1.	0.1	1335.0	29 SEP 1312	73	86.	7.3	1338.1	29 SEP 1918	134	12.	0.8	1335.4
29 SEP 0712	13	1.	0.1	1335.0	29 SEP 1318	74	86.	7.4	1338.1	29 SEP 1924	135	12.	0.8	1335.4
29 SEP 0718	14	1.	0.1	1335.0	29 SEP 1324	75	85.	7.3	1338.1	29 SEP 1930	136	12.	0.8	1335.4
29 SEP 0724	15	1.	0.1	1335.0	29 SEP 1330	76	84.	7.1	1338.0	29 SEP 1936	137	12.	0.8	1335.4
29 SEP 0730	16	1.	0.1	1335.0	29 SEP 1336	77	83.	6.9	1338.0	29 SEP 1942	138	12.	0.8	1335.4
29 SEP 0736	17	2.	0.1	1335.0	29 SEP 1342	78	81.	6.6	1337.9	29 SEP 1948	139	12.	0.8	1335.4
29 SEP 0742	18	2.	0.1	1335.1	29 SEP 1348	79	79.	6.3	1337.7	29 SEP 1954	140	12.	0.7	1335.3
29 SEP 0748	19	2.	0.1	1335.1	29 SEP 1354	80	76.	6.0	1337.6	29 SEP 2000	141	12.	0.7	1335.3
29 SEP 0754	20	2.	0.1	1335.1	29 SEP 1400	81	74.	5.8	1337.5	29 SEP 2006	142	11.	0.7	1335.3
29 SEP 0800	21	2.	0.1	1335.1	29 SEP 1406	82	72.	5.5	1337.4	29 SEP 2012	143	11.	0.7	1335.3
29 SEP 0806	22	2.	0.1	1335.1	29 SEP 1412	83	69.	5.2	1337.3	29 SEP 2018	144	11.	0.7	1335.3
29 SEP 0812	23	2.	0.1	1335.1	29 SEP 1418	84	67.	4.9	1337.2	29 SEP 2024	145	11.	0.7	1335.3
29 SEP 0818	24	2.	0.1	1335.1	29 SEP 1424	85	64.	4.7	1337.1	29 SEP 2030	146	11.	0.7	1335.3
29 SEP 0824	25	2.	0.2	1335.1	29 SEP 1430	86	62.	4.4	1337.0	29 SEP 2036	147	11.	0.7	1335.3
29 SEP 0830	26	2.	0.2	1335.1	29 SEP 1436	87	60.	4.2	1336.9	29 SEP 2042	148	11.	0.7	1335.3
29 SEP 0836	27	3.	0.2	1335.1	29 SEP 1442	88	58.	3.9	1336.8	29 SEP 2048	149	10.	0.7	1335.3
29 SEP 0842	28	3.	0.2	1335.1	29 SEP 1448	89	55.	3.7	1336.7	29 SEP 2054	150	10.	0.7	1335.3
29 SEP 0848	29	3.	0.2	1335.1	29 SEP 1454	90	53.	3.5	1336.6	29 SEP 2100	151	10.	0.6	1335.3
29 SEP 0854	30	3.	0.2	1335.1	29 SEP 1500	91	51.	3.3	1336.5	29 SEP 2106	152	10.	0.6	1335.3
29 SEP 0900	31	3.	0.2	1335.1	29 SEP 1506	92	49.	3.2	1336.5	29 SEP 2112	153	10.	0.6	1335.3
29 SEP 0906	32	3.	0.2	1335.1	29 SEP 1512	93	47.	3.0	1336.4	29 SEP 2118	154	9.	0.6	1335.3
29 SEP 0912	33	3.	0.2	1335.1	29 SEP 1518	94	45.	2.9	1336.3	29 SEP 2124	155	9.	0.6	1335.3
29 SEP 0918	34	3.	0.2	1335.1	29 SEP 1524	95	43.	2.7	1336.3	29 SEP 2130	156	9.	0.6	1335.3
29 SEP 0924	35	3.	0.2	1335.1	29 SEP 1530	96	41.	2.6	1336.2	29 SEP 2136	157	9.	0.6	1335.3
29 SEP 0930	36	4.	0.2	1335.1	29 SEP 1536	97	39.	2.5	1336.2	29 SEP 2142	158	9.	0.6	1335.3
29 SEP 0936	37	4.	0.2	1335.1	29 SEP 1542	98	38.	2.5	1336.1	29 SEP 2148	159	9.	0.6	1335.3
29 SEP 0942	38	4.	0.3	1335.1	29 SEP 1548	99	37.	2.4	1336.1	29 SEP 2154	160	8.	0.5	1335.3
29 SEP 0948	39	4.	0.3	1335.1	29 SEP 1554	100	36.	2.3	1336.1	29 SEP 2200	161	8.	0.5	1335.2
29 SEP 0954	40	4.	0.3	1335.1	29 SEP 1600	101	35.	2.3	1336.1	29 SEP 2206	162	8.	0.5	1335.2
29 SEP 1000	41	4.	0.3	1335.1	29 SEP 1606	102	34.	2.2	1336.0	29 SEP 2212	163	8.	0.5	1335.2
29 SEP 1006	42	5.	0.3	1335.1	29 SEP 1612	103	33.	2.1	1336.0	29 SEP 2218	164	8.	0.5	1335.2
29 SEP 1012	43	5.	0.3	1335.1	29 SEP 1618	104	33.	2.1	1336.0	29 SEP 2224	165	8.	0.5	1335.2
29 SEP 1018	44	5.	0.3	1335.1	29 SEP 1624	105	32.	2.1	1336.0	29 SEP 2230	166	8.	0.5	1335.2
29 SEP 1024	45	5.	0.3	1335.2	29 SEP 1630	106	31.	2.0	1335.9	29 SEP 2236	167	8.	0.5	1335.2
29 SEP 1030	46	6.	0.4	1335.2	29 SEP 1636	107	31.	2.0	1335.9	29 SEP 2242	168	8.	0.5	1335.2
29 SEP 1036	47	6.	0.4	1335.2	29 SEP 1642	108	30.	1.9	1335.9	29 SEP 2248	169	8.	0.5	1335.2
29 SEP 1042	48	6.	0.4	1335.2	29 SEP 1648	109	29.	1.9	1335.9	29 SEP 2254	170	8.	0.5	1335.2
29 SEP 1048	49	7.	0.4	1335.2	29 SEP 1654	110	28.	1.8	1335.8	29 SEP 2300	171	8.	0.5	1335.2
29 SEP 1054	50	7.	0.5	1335.2	29 SEP 1700	111	27.	1.8	1335.8	29 SEP 2306	172	8.	0.5	1335.2
29 SEP 1100	51	8.	0.5	1335.2	29 SEP 1706	112	26.	1.7	1335.8	29 SEP 2312	173	8.	0.5	1335.2
29 SEP 1106	52	8.	0.5	1335.2	29 SEP 1712	113	25.	1.6	1335.8	29 SEP 2318	174	8.	0.5	1335.2
29 SEP 1112	53	9.	0.6	1335.3	29 SEP 1718	114	24.	1.6	1335.7	29 SEP 2324	175	8.	0.5	1335.2
29 SEP 1118	54	9.	0.6	1335.3	29 SEP 1724	115	23.	1.5	1335.7	29 SEP 2330	176	8.	0.5	1335.2
29 SEP 1124	55	10.	0.7	1335.3	29 SEP 1730	116	23.	1.4	1335.7	29 SEP 2336	177	8.	0.5	1335.2
29 SEP 1130	56	11.	0.7	1335.3	29 SEP 1736	117	22.	1.4	1335.7	29 SEP 2342	178	8.	0.5	1335.2
29 SEP 1136	57	13.	0.8	1335.4	29 SEP 1742	118	21.	1.3	1335.6	29 SEP 2348	179	8.	0.5	1335.2
29 SEP 1142	58	17.	1.1	1335.5	29 SEP 1748	119	20.	1.3	1335.6	29 SEP 2354	180	7.	0.5	1335.2
29 SEP 1148	59	24.	1.6	1335.7	29 SEP 1754	120	19.	1.2	1335.6	30 SEP 0000	181	7.	0.5	1335.2
29 SEP 1154	60	35.	2.3	1336.1	29 SEP 1800	121	18.	1.2	1335.6					
29 SEP 1200	61	48.	3.1	1336.4	29 SEP 1806	122	18.	1.1	1335.5					

****

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	18.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 86.	7.30		53.	23.	23.	23.
		(INCHES)	3.448	4.420	4.420	4.420
		(AC-FT)	26.	34.	34.	34.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	18.00-HR
+ (AC-FT)	(HR)				
7.	7.30	4.	2.	2.	2.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	18.00-HR
+ (FEET)	(HR)				
1338.12	7.30	1336.74	1335.73	1335.73	1335.73

CUMULATIVE AREA = 0.14 SQ MI

*** ***

```
           **************
           *            *
104 KK     *   S5.3AC   *
           *            *
           **************
```

3 IN TIME DATA FOR INPUT TIME SERIES

JXMIN	30	TIME INTERVAL IN MINUTES
JXDATE	29SEP92	STARTING DATE
JXTIME	600	STARTING TIME

SUBBASIN RUNOFF DATA

105 BA SUBBASIN CHARACTERISTICS

TAREA	0.00	SUBBASIN AREA

PRECIPITATION DATA

106 PB STORM 5.00 BASIN TOTAL PRECIPITATION

107 PI INCREMENTAL PRECIPITATION PATTERN

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.08	0.08	0.08	0.08	0.08
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

111 LS SCS LOSS RATE

STRTL	0.67	INITIAL ABSTRACTION
CRVNBR	75.00	CURVE NUMBER
RTIMP	0.00	PERCENT IMPERVIOUS AREA

112 UD SCS DIMENSIONLESS UNITGRAPH

TLAG	0.15	LAG

***

WARNING *** TIME INTERVAL IS GREATER THAN .29*LAG

UNIT HYDROGRAPH
10 END-OF-PERIOD ORDINATES

4. 8. 5. 2. 1. 0. 0. 0. 0. 0.

HYDROGRAPH AT STATION S5.3AC

DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	DA MON HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
29 SEP 0600	1	0.00	0.00	0.00	0.	29 SEP 1506	92	0.02	0.00	0.01	0.
29 SEP 0606	2	0.01	0.01	0.00	0.	29 SEP 1512	93	0.02	0.00	0.01	0.
29 SEP 0612	3	0.01	0.01	0.00	0.	29 SEP 1518	94	0.02	0.00	0.01	0.
29 SEP 0618	4	0.01	0.01	0.00	0.	29 SEP 1524	95	0.02	0.00	0.01	0.
29 SEP 0624	5	0.01	0.01	0.00	0.	29 SEP 1530	96	0.02	0.00	0.01	0.
29 SEP 0630	6	0.01	0.01	0.00	0.	29 SEP 1536	97	0.02	0.00	0.01	0.
29 SEP 0636	7	0.01	0.01	0.00	0.	29 SEP 1542	98	0.02	0.00	0.01	0.
29 SEP 0642	8	0.01	0.01	0.00	0.	29 SEP 1548	99	0.02	0.00	0.01	0.
29 SEP 0648	9	0.01	0.01	0.00	0.	29 SEP 1554	100	0.02	0.00	0.01	0.
29 SEP 0654	10	0.01	0.01	0.00	0.	29 SEP 1600	101	0.02	0.00	0.01	0.
29 SEP 0700	11	0.01	0.01	0.00	0.	29 SEP 1606	102	0.01	0.00	0.01	0.
29 SEP 0706	12	0.01	0.01	0.00	0.	29 SEP 1612	103	0.01	0.00	0.01	0.
29 SEP 0712	13	0.01	0.01	0.00	0.	29 SEP 1618	104	0.01	0.00	0.01	0.
29 SEP 0718	14	0.01	0.01	0.00	0.	29 SEP 1624	105	0.01	0.00	0.01	0.
29 SEP 0724	15	0.01	0.01	0.00	0.	29 SEP 1630	106	0.01	0.00	0.01	0.
29 SEP 0730	16	0.01	0.01	0.00	0.	29 SEP 1636	107	0.01	0.00	0.01	0.
29 SEP 0736	17	0.01	0.01	0.00	0.	29 SEP 1642	108	0.01	0.00	0.01	0.
29 SEP 0742	18	0.01	0.01	0.00	0.	29 SEP 1648	109	0.01	0.00	0.01	0.
29 SEP 0748	19	0.01	0.01	0.00	0.	29 SEP 1654	110	0.01	0.00	0.01	0.
29 SEP 0754	20	0.01	0.01	0.00	0.	29 SEP 1700	111	0.01	0.00	0.01	0.
29 SEP 0800	21	0.01	0.01	0.00	0.	29 SEP 1706	112	0.01	0.00	0.01	0.
29 SEP 0806	22	0.01	0.01	0.00	0.	29 SEP 1712	113	0.01	0.00	0.01	0.
29 SEP 0812	23	0.01	0.01	0.00	0.	29 SEP 1718	114	0.01	0.00	0.01	0.
29 SEP 0818	24	0.01	0.01	0.00	0.	29 SEP 1724	115	0.01	0.00	0.01	0.
29 SEP 0824	25	0.01	0.01	0.00	0.	29 SEP 1730	116	0.01	0.00	0.01	0.
29 SEP 0830	26	0.01	0.01	0.00	0.	29 SEP 1736	117	0.01	0.00	0.01	0.
29 SEP 0836	27	0.02	0.02	0.00	0.	29 SEP 1742	118	0.01	0.00	0.01	0.
29 SEP 0842	28	0.02	0.02	0.00	0.	29 SEP 1748	119	0.01	0.00	0.01	0.
29 SEP 0848	29	0.02	0.02	0.00	0.	29 SEP 1754	120	0.01	0.00	0.01	0.
29 SEP 0854	30	0.02	0.02	0.00	0.	29 SEP 1800	121	0.01	0.00	0.01	0.
29 SEP 0900	31	0.02	0.02	0.00	0.	29 SEP 1806	122	0.01	0.00	0.01	0.
29 SEP 0906	32	0.02	0.02	0.00	0.	29 SEP 1812	123	0.01	0.00	0.01	0.
29 SEP 0912	33	0.02	0.02	0.00	0.	29 SEP 1818	124	0.01	0.00	0.01	0.
29 SEP 0918	34	0.02	0.02	0.00	0.	29 SEP 1824	125	0.01	0.00	0.01	0.
29 SEP 0924	35	0.02	0.02	0.00	0.	29 SEP 1830	126	0.01	0.00	0.01	0.
29 SEP 0930	36	0.02	0.02	0.00	0.	29 SEP 1836	127	0.01	0.00	0.01	0.
29 SEP 0936	37	0.02	0.02	0.00	0.	29 SEP 1842	128	0.01	0.00	0.01	0.
29 SEP 0942	38	0.02	0.02	0.00	0.	29 SEP 1848	129	0.01	0.00	0.01	0.
29 SEP 0948	39	0.02	0.02	0.00	0.	29 SEP 1854	130	0.01	0.00	0.01	0.
29 SEP 0954	40	0.02	0.02	0.00	0.	29 SEP 1900	131	0.01	0.00	0.01	0.
29 SEP 1000	41	0.02	0.02	0.00	0.	29 SEP 1906	132	0.01	0.00	0.01	0.
29 SEP 1006	42	0.03	0.03	0.00	0.	29 SEP 1912	133	0.01	0.00	0.01	0.
29 SEP 1012	43	0.03	0.03	0.00	0.	29 SEP 1918	134	0.01	0.00	0.01	0.
29 SEP 1018	44	0.02	0.02	0.00	0.	29 SEP 1924	135	0.01	0.00	0.01	0.
29 SEP 1024	45	0.03	0.03	0.00	0.	29 SEP 1930	136	0.01	0.00	0.01	0.
29 SEP 1030	46	0.03	0.02	0.00	0.	29 SEP 1936	137	0.01	0.00	0.01	0.
29 SEP 1036	47	0.03	0.03	0.00	0.	29 SEP 1942	138	0.01	0.00	0.01	0.
29 SEP 1042	48	0.03	0.03	0.00	0.	29 SEP 1948	139	0.01	0.00	0.01	0.
29 SEP 1048	49	0.03	0.03	0.00	0.	29 SEP 1954	140	0.01	0.00	0.01	0.
29 SEP 1054	50	0.03	0.03	0.00	0.	29 SEP 2000	141	0.01	0.00	0.01	0.
29 SEP 1100	51	0.03	0.03	0.00	0.	29 SEP 2006	142	0.01	0.00	0.01	0.
29 SEP 1106	52	0.05	0.05	0.01	0.	29 SEP 2012	143	0.01	0.00	0.01	0.
29 SEP 1112	53	0.05	0.05	0.01	0.	29 SEP 2018	144	0.01	0.00	0.01	0.
29 SEP 1118	54	0.05	0.04	0.01	0.	29 SEP 2024	145	0.01	0.00	0.01	0.
29 SEP 1124	55	0.05	0.04	0.01	0.	29 SEP 2030	146	0.01	0.00	0.01	0.
29 SEP 1130	56	0.05	0.04	0.01	0.	29 SEP 2036	147	0.01	0.00	0.01	0.
29 SEP 1136	57	0.41	0.29	0.12	1.	29 SEP 2042	148	0.01	0.00	0.01	0.
29 SEP 1142	58	0.41	0.24	0.17	2.	29 SEP 2048	149	0.01	0.00	0.01	0.
29 SEP 1148	59	0.41	0.20	0.21	3.	29 SEP 2054	150	0.01	0.00	0.01	0.
29 SEP 1154	60	0.41	0.17	0.24	4.	29 SEP 2100	151	0.01	0.00	0.01	0.
29 SEP 1200	61	0.41	0.15	0.27	5.	29 SEP 2106	152	0.01	0.00	0.01	0.
29 SEP 1206	62	0.08	0.03	0.05	4.	29 SEP 2112	153	0.01	0.00	0.01	0.
29 SEP 1212	63	0.08	0.02	0.05	3.	29 SEP 2118	154	0.01	0.00	0.01	0.
29 SEP 1218	64	0.08	0.02	0.05	2.	29 SEP 2124	155	0.01	0.00	0.01	0.
29 SEP 1224	65	0.08	0.02	0.05	1.	29 SEP 2130	156	0.01	0.00	0.01	0.
29 SEP 1230	66	0.08	0.02	0.06	1.	29 SEP 2136	157	0.01	0.00	0.01	0.
29 SEP 1236	67	0.04	0.01	0.03	1.	29 SEP 2142	158	0.01	0.00	0.01	0.
29 SEP 1242	68	0.04	0.01	0.03	1.	29 SEP 2148	159	0.01	0.00	0.01	0.

29 SEP 1248	69	0.04	0.01	0.03	1.	*	29 SEP 2154	160	0.01	0.00	0.01	0.
29 SEP 1254	70	0.04	0.01	0.03	1.	*	29 SEP 2200	161	0.01	0.00	0.01	0.
29 SEP 1300	71	0.04	0.01	0.03	1.	*	29 SEP 2206	162	0.01	0.00	0.01	0.
29 SEP 1306	72	0.03	0.01	0.02	1.	*	29 SEP 2212	163	0.01	0.00	0.01	0.
29 SEP 1312	73	0.03	0.01	0.02	1.	*	29 SEP 2218	164	0.01	0.00	0.01	0.
29 SEP 1318	74	0.03	0.01	0.02	0.	*	29 SEP 2224	165	0.01	0.00	0.01	0.
29 SEP 1324	75	0.03	0.01	0.02	0.	*	29 SEP 2230	166	0.01	0.00	0.01	0.
29 SEP 1330	76	0.03	0.01	0.02	0.	*	29 SEP 2236	167	0.01	0.00	0.01	0.
29 SEP 1336	77	0.02	0.01	0.02	0.	*	29 SEP 2242	168	0.01	0.00	0.01	0.
29 SEP 1342	78	0.02	0.01	0.02	0.	*	29 SEP 2248	169	0.01	0.00	0.01	0.
29 SEP 1348	79	0.02	0.01	0.02	0.	*	29 SEP 2254	170	0.01	0.00	0.01	0.
29 SEP 1354	80	0.02	0.01	0.02	0.	*	29 SEP 2300	171	0.01	0.00	0.01	0.
29 SEP 1400	81	0.02	0.01	0.02	0.	*	29 SEP 2306	172	0.01	0.00	0.01	0.
29 SEP 1406	82	0.02	0.00	0.01	0.	*	29 SEP 2312	173	0.01	0.00	0.01	0.
29 SEP 1412	83	0.02	0.00	0.01	0.	*	29 SEP 2318	174	0.01	0.00	0.01	0.
29 SEP 1418	84	0.02	0.00	0.01	0.	*	29 SEP 2324	175	0.01	0.00	0.01	0.
29 SEP 1424	85	0.02	0.00	0.01	0.	*	29 SEP 2330	176	0.01	0.00	0.01	0.
29 SEP 1430	86	0.02	0.00	0.01	0.	*	29 SEP 2336	177	0.01	0.00	0.01	0.
29 SEP 1436	87	0.02	0.00	0.01	0.	*	29 SEP 2342	178	0.01	0.00	0.01	0.
29 SEP 1442	88	0.02	0.00	0.01	0.	*	29 SEP 2348	179	0.01	0.00	0.01	0.
29 SEP 1448	89	0.02	0.00	0.01	0.	*	29 SEP 2354	180	0.01	0.00	0.01	0.
29 SEP 1454	90	0.02	0.00	0.01	0.	*	30 SEP 0000	181	0.01	0.00	0.01	0.
29 SEP 1500	91	0.02	0.00	0.01	0.	*						

****

TOTAL RAINFALL = 5.00, TOTAL LOSS = 2.55, TOTAL EXCESS = 2.45

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	18.00-HR
+ (CFS)	(HR)	(CFS)				
+ 5.	6.00		1.	0.	0.	0.
		(INCHES)	2.011	2.438	2.438	2.438
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

*** ***

```
          **************
          *            *
113 KK    *    INTO6   *
          *            *
          **************
```

114 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

***

****

HYDROGRAPH AT STATION INTO6
SUM OF 2 HYDROGRAPHS

****

DA MON HRMN	ORD	FLOW	*	DA MON HRMN	ORD	FLOW	*	DA MON HRMN	ORD	FLOW	*	DA MON HRMN	ORD	FLOW
29 SEP 0600	1	0.	*	29 SEP 1036	47	6.	*	29 SEP 1512	93	47.	*	29 SEP 1948	139	12.
29 SEP 0606	2	0.	*	29 SEP 1042	48	6.	*	29 SEP 1518	94	45.	*	29 SEP 1954	140	12.
29 SEP 0612	3	0.	*	29 SEP 1048	49	7.	*	29 SEP 1524	95	43.	*	29 SEP 2000	141	12.
29 SEP 0618	4	0.	*	29 SEP 1054	50	7.	*	29 SEP 1530	96	41.	*	29 SEP 2006	142	12.
29 SEP 0624	5	0.	*	29 SEP 1100	51	8.	*	29 SEP 1536	97	40.	*	29 SEP 2012	143	12.
29 SEP 0630	6	0.	*	29 SEP 1106	52	8.	*	29 SEP 1542	98	38.	*	29 SEP 2018	144	11.
29 SEP 0636	7	0.	*	29 SEP 1112	53	9.	*	29 SEP 1548	99	37.	*	29 SEP 2024	145	11.
29 SEP 0642	8	0.	*	29 SEP 1118	54	10.	*	29 SEP 1554	100	36.	*	29 SEP 2030	146	11.
29 SEP 0648	9	0.	*	29 SEP 1124	55	11.	*	29 SEP 1600	101	35.	*	29 SEP 2036	147	11.
29 SEP 0654	10	1.	*	29 SEP 1130	56	12.	*	29 SEP 1606	102	34.	*	29 SEP 2042	148	11.
29 SEP 0700	11	1.	*	29 SEP 1136	57	14.	*	29 SEP 1612	103	34.	*	29 SEP 2048	149	10.
29 SEP 0706	12	1.	*	29 SEP 1142	58	19.	*	29 SEP 1618	104	33.	*	29 SEP 2054	150	10.
29 SEP 0712	13	1.	*	29 SEP 1148	59	27.	*	29 SEP 1624	105	32.	*	29 SEP 2100	151	10.
29 SEP 0718	14	1.	*	29 SEP 1154	60	39.	*	29 SEP 1630	106	31.	*	29 SEP 2106	152	10.
29 SEP 0724	15	1.	*	29 SEP 1200	61	53.	*	29 SEP 1636	107	31.	*	29 SEP 2112	153	10.
29 SEP 0730	16	1.	*	29 SEP 1206	62	62.	*	29 SEP 1642	108	30.	*	29 SEP 2118	154	9.

29 SEP 0736	17	2.	*	29 SEP 1212	63	67.	*	29 SEP 1648	109	29.	*	29 SEP 2124	155	9.					
29 SEP 0742	18	2.	*	29 SEP 1218	64	71.	*	29 SEP 1654	110	28.	*	29 SEP 2130	156	9.					
29 SEP 0748	19	2.	*	29 SEP 1224	65	74.	*	29 SEP 1700	111	27.	*	29 SEP 2136	157	9.					
29 SEP 0754	20	2.	*	29 SEP 1230	66	77.	*	29 SEP 1706	112	26.	*	29 SEP 2142	158	9.					
29 SEP 0800	21	2.	*	29 SEP 1236	67	80.	*	29 SEP 1712	113	25.	*	29 SEP 2148	159	9.					
29 SEP 0806	22	2.	*	29 SEP 1242	68	82.	*	29 SEP 1718	114	25.	*	29 SEP 2154	160	9.					
29 SEP 0812	23	2.	*	29 SEP 1248	69	83.	*	29 SEP 1724	115	24.	*	29 SEP 2200	161	8.					
29 SEP 0818	24	2.	*	29 SEP 1254	70	84.	*	29 SEP 1730	116	23.	*	29 SEP 2206	162	8.					
29 SEP 0824	25	2.	*	29 SEP 1300	71	85.	*	29 SEP 1736	117	22.	*	29 SEP 2212	163	8.					
29 SEP 0830	26	2.	*	29 SEP 1306	72	86.	*	29 SEP 1742	118	21.	*	29 SEP 2218	164	8.					
29 SEP 0836	27	3.	*	29 SEP 1312	73	86.	*	29 SEP 1748	119	20.	*	29 SEP 2224	165	8.					
29 SEP 0842	28	3.	*	29 SEP 1318	74	86.	*	29 SEP 1754	120	19.	*	29 SEP 2230	166	8.					
29 SEP 0848	29	3.	*	29 SEP 1324	75	86.	*	29 SEP 1800	121	18.	*	29 SEP 2236	167	8.					
29 SEP 0854	30	3.	*	29 SEP 1330	76	85.	*	29 SEP 1806	122	18.	*	29 SEP 2242	168	8.					
29 SEP 0900	31	3.	*	29 SEP 1336	77	83.	*	29 SEP 1812	123	17.	*	29 SEP 2248	169	8.					
29 SEP 0906	32	3.	*	29 SEP 1342	78	81.	*	29 SEP 1818	124	16.	*	29 SEP 2254	170	8.					
29 SEP 0912	33	3.	*	29 SEP 1348	79	79.	*	29 SEP 1824	125	16.	*	29 SEP 2300	171	8.					
29 SEP 0918	34	3.	*	29 SEP 1354	80	77.	*	29 SEP 1830	126	15.	*	29 SEP 2306	172	8.					
29 SEP 0924	35	3.	*	29 SEP 1400	81	74.	*	29 SEP 1836	127	15.	*	29 SEP 2312	173	8.					
29 SEP 0930	36	4.	*	29 SEP 1406	82	72.	*	29 SEP 1842	128	14.	*	29 SEP 2318	174	8.					
29 SEP 0936	37	4.	*	29 SEP 1412	83	70.	*	29 SEP 1848	129	14.	*	29 SEP 2324	175	8.					
29 SEP 0942	38	4.	*	29 SEP 1418	84	67.	*	29 SEP 1854	130	13.	*	29 SEP 2330	176	8.					
29 SEP 0948	39	4.	*	29 SEP 1424	85	65.	*	29 SEP 1900	131	13.	*	29 SEP 2336	177	8.					
29 SEP 0954	40	4.	*	29 SEP 1430	86	62.	*	29 SEP 1906	132	13.	*	29 SEP 2342	178	8.					
29 SEP 1000	41	4.	*	29 SEP 1436	87	60.	*	29 SEP 1912	133	13.	*	29 SEP 2348	179	8.					
29 SEP 1006	42	5.	*	29 SEP 1442	88	58.	*	29 SEP 1918	134	12.	*	29 SEP 2354	180	8.					
29 SEP 1012	43	5.	*	29 SEP 1448	89	56.	*	29 SEP 1924	135	12.	*	30 SEP 0000	181	8.					
29 SEP 1018	44	5.	*	29 SEP 1454	90	53.	*	29 SEP 1930	136	12.	*								
29 SEP 1024	45	5.	*	29 SEP 1500	91	51.	*	29 SEP 1936	137	12.	*								
29 SEP 1030	46	6.	*	29 SEP 1506	92	49.	*	29 SEP 1942	138	12.	*								
			*				*				*								

****

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	18.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 86.	7.30		53.	23.	23.	23.
		(INCHES)	3.414	4.376	4.376	4.376
		(AC-FT)	27.	34.	34.	34.

CUMULATIVE AREA = 0.15 SQ MI

*** ***

```
          **************
          *            *
115 KK    *     POND6  *
          *            *
          **************
```

HYDROGRAPH ROUTING DATA

116 RS STORAGE ROUTING

NSTPS	1	NUMBER OF SUBREACHES
ITYP	ELEV	TYPE OF INITIAL CONDITION
RSVRIC	1335.00	INITIAL CONDITION
X	0.00	WORKING R AND D COEFFICIENT

117 SA	AREA	0.3	0.3	0.3	0.4	0.4
118 SE	ELEVATION	1335.00	1336.00	1337.00	1338.00	1339.00

119 SS SPILLWAY

CREL	1335.00	SPILLWAY CREST ELEVATION
SPWID	20.00	SPILLWAY WIDTH
COQW	3.00	WEIR COEFFICIENT
EXPW	1.50	EXPONENT OF HEAD

***

COMPUTED STORAGE-ELEVATION DATA

STORAGE	0.00	0.27	0.58	0.93	1.32
ELEVATION	1335.00	1336.00	1337.00	1338.00	1339.00

COMPUTED OUTFLOW-ELEVATION DATA

OUTFLOW	0.00	0.00	0.08	0.66	2.22	5.27	10.29	17.78	28.23	42.14
ELEVATION	1335.00	1335.00	1335.01	1335.05	1335.11	1335.20	1335.31	1335.44	1335.60	1335.79
OUTFLOW	60.00	82.30	109.55	142.22	180.82	225.84	277.78	337.12	404.36	480.00
ELEVATION	1336.00	1336.23	1336.49	1336.78	1337.09	1337.42	1337.78	1338.16	1338.57	1339.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	0.00	0.00	0.01	0.03	0.05	0.08	0.11	0.16	0.21	0.27
OUTFLOW	0.00	0.08	0.66	2.22	5.27	10.29	17.78	28.23	42.14	60.00
ELEVATION	1335.00	1335.01	1335.05	1335.11	1335.20	1335.31	1335.44	1335.60	1335.79	1336.00
STORAGE	0.34	0.42	0.51	0.58	0.61	0.72	0.85	0.93	0.99	1.15
OUTFLOW	82.31	109.54	142.23	169.71	180.82	225.85	277.79	311.77	337.12	404.36
ELEVATION	1336.23	1336.49	1336.78	1337.00	1337.09	1337.42	1337.78	1338.00	1338.16	1338.57
STORAGE	1.32									
OUTFLOW	480.00									
ELEVATION	1339.00									

*** WARNING *** MODIFIED PULS ROUTING MAY BE NUMERICALLY UNSTABLE FOR OUTFLOWS BETWEEN 28. TO 480.
THE ROUTED HYDROGRAPH SHOULD BE EXAMINED FOR OSCILLATIONS OR OUTFLOWS GREATER THAN PEAK INFLOWS.
THIS CAN BE CORRECTED BY DECREASING THE TIME INTERVAL OR INCREASING STORAGE (USE A LONGER REACH.)

****

HYDROGRAPH AT STATION POND6

****

DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE
29	SEP	0600	1	0.	0.0	1335.0	29	SEP	1206	62	58.	0.3	1336.0	29	SEP	1812	123	17.	0.1	1335.4
29	SEP	0606	2	0.	0.0	1335.0	29	SEP	1212	63	65.	0.3	1336.1	29	SEP	1818	124	17.	0.1	1335.4
29	SEP	0612	3	0.	0.0	1335.0	29	SEP	1218	64	70.	0.3	1336.1	29	SEP	1824	125	16.	0.1	1335.4
29	SEP	0618	4	0.	0.0	1335.0	29	SEP	1224	65	73.	0.3	1336.1	29	SEP	1830	126	15.	0.1	1335.4
29	SEP	0624	5	0.	0.0	1335.0	29	SEP	1230	66	76.	0.3	1336.2	29	SEP	1836	127	15.	0.1	1335.4
29	SEP	0630	6	0.	0.0	1335.0	29	SEP	1236	67	79.	0.3	1336.2	29	SEP	1842	128	14.	0.1	1335.4
29	SEP	0636	7	0.	0.0	1335.0	29	SEP	1242	68	81.	0.3	1336.2	29	SEP	1848	129	14.	0.1	1335.4
29	SEP	0642	8	0.	0.0	1335.0	29	SEP	1248	69	82.	0.3	1336.2	29	SEP	1854	130	14.	0.1	1335.4
29	SEP	0648	9	0.	0.0	1335.0	29	SEP	1254	70	84.	0.3	1336.2	29	SEP	1900	131	13.	0.1	1335.4
29	SEP	0654	10	0.	0.0	1335.0	29	SEP	1300	71	85.	0.3	1336.3	29	SEP	1906	132	13.	0.1	1335.4
29	SEP	0700	11	0.	0.0	1335.0	29	SEP	1306	72	86.	0.3	1336.3	29	SEP	1912	133	13.	0.1	1335.4
29	SEP	0706	12	1.	0.0	1335.0	29	SEP	1312	73	86.	0.3	1336.3	29	SEP	1918	134	13.	0.1	1335.4
29	SEP	0712	13	1.	0.0	1335.1	29	SEP	1318	74	86.	0.4	1336.3	29	SEP	1924	135	12.	0.1	1335.3
29	SEP	0718	14	1.	0.0	1335.1	29	SEP	1324	75	86.	0.3	1336.3	29	SEP	1930	136	12.	0.1	1335.3
29	SEP	0724	15	1.	0.0	1335.1	29	SEP	1330	76	85.	0.3	1336.3	29	SEP	1936	137	12.	0.1	1335.3
29	SEP	0730	16	1.	0.0	1335.1	29	SEP	1336	77	84.	0.3	1336.2	29	SEP	1942	138	12.	0.1	1335.3
29	SEP	0736	17	1.	0.0	1335.1	29	SEP	1342	78	82.	0.3	1336.2	29	SEP	1948	139	12.	0.1	1335.3
29	SEP	0742	18	2.	0.0	1335.1	29	SEP	1348	79	80.	0.3	1336.2	29	SEP	1954	140	12.	0.1	1335.3
29	SEP	0748	19	2.	0.0	1335.1	29	SEP	1354	80	78.	0.3	1336.2	29	SEP	2000	141	12.	0.1	1335.3
29	SEP	0754	20	2.	0.0	1335.1	29	SEP	1400	81	75.	0.3	1336.2	29	SEP	2006	142	12.	0.1	1335.3
29	SEP	0800	21	2.	0.0	1335.1	29	SEP	1406	82	73.	0.3	1336.1	29	SEP	2012	143	12.	0.1	1335.3
29	SEP	0806	22	2.	0.0	1335.1	29	SEP	1412	83	70.	0.3	1336.1	29	SEP	2018	144	11.	0.1	1335.3
29	SEP	0812	23	2.	0.0	1335.1	29	SEP	1418	84	68.	0.3	1336.1	29	SEP	2024	145	11.	0.1	1335.3
29	SEP	0818	24	2.	0.0	1335.1	29	SEP	1424	85	66.	0.3	1336.1	29	SEP	2030	146	11.	0.1	1335.3
29	SEP	0824	25	2.	0.0	1335.1	29	SEP	1430	86	63.	0.3	1336.0	29	SEP	2036	147	11.	0.1	1335.3
29	SEP	0830	26	2.	0.0	1335.1	29	SEP	1436	87	61.	0.3	1336.0	29	SEP	2042	148	11.	0.1	1335.3
29	SEP	0836	27	2.	0.0	1335.1	29	SEP	1442	88	59.	0.3	1336.0	29	SEP	2048	149	11.	0.1	1335.3
29	SEP	0842	28	3.	0.0	1335.1	29	SEP	1448	89	56.	0.3	1336.0	29	SEP	2054	150	10.	0.1	1335.3
29	SEP	0848	29	3.	0.0	1335.1	29	SEP	1454	90	54.	0.3	1335.9	29	SEP	2100	151	10.	0.1	1335.3
29	SEP	0854	30	3.	0.0	1335.1	29	SEP	1500	91	52.	0.2	1335.9	29	SEP	2106	152	10.	0.1	1335.3
29	SEP	0900	31	3.	0.0	1335.1	29	SEP	1506	92	50.	0.2	1335.9	29	SEP	2112	153	10.	0.1	1335.3
29	SEP	0906	32	3.	0.0	1335.1	29	SEP	1512	93	48.	0.2	1335.9	29	SEP	2118	154	10.	0.1	1335.3
29	SEP	0912	33	3.	0.0	1335.1	29	SEP	1518	94	46.	0.2	1335.8	29	SEP	2124	155	9.	0.1	1335.3
29	SEP	0918	34	3.	0.0	1335.1	29	SEP	1524	95	44.	0.2	1335.8	29	SEP	2130	156	9.	0.1	1335.3
29	SEP	0924	35	3.	0.0	1335.1	29	SEP	1530	96	42.	0.2	1335.8	29	SEP	2136	157	9.	0.1	1335.3
29	SEP	0930	36	3.	0.0	1335.1	29	SEP	1536	97	40.	0.2	1335.8	29	SEP	2142	158	9.	0.1	1335.3
29	SEP	0936	37	4.	0.0	1335.2	29	SEP	1542	98	39.	0.2	1335.7	29	SEP	2148	159	9.	0.1	1335.3
29	SEP	0942	38	4.	0.0	1335.2	29	SEP	1548	99	38.	0.2	1335.7	29	SEP	2154	160	9.	0.1	1335.3
29	SEP	0948	39	4.	0.0	1335.2	29	SEP	1554	100	37.	0.2	1335.7	29	SEP	2200	161	9.	0.1	1335.3
29	SEP	0954	40	4.	0.0	1335.2	29	SEP	1600	101	36.	0.2	1335.7	29	SEP	2206	162	8.	0.1	1335.3
29	SEP	1000	41	4.	0.0	1335.2	29	SEP	1606	102	35.	0.2	1335.7	29	SEP	2212	163	8.	0.1	1335.3
29	SEP	1006	42	4.	0.0	1335.2	29	SEP	1612	103	34.	0.2	1335.7	29	SEP	2218	164	8.	0.1	1335.3
29	SEP	1012	43	5.	0.0	1335.2	29	SEP	1618	104	33.	0.2	1335.7	29	SEP	2224	165	8.	0.1	1335.3
29	SEP	1018	44	5.	0.0	1335.2	29	SEP	1624	105	32.	0.2	1335.7	29	SEP	2230	166	8.	0.1	1335.3
29	SEP	1024	45	5.	0.0	1335.2	29	SEP	1630	106	32.	0.2	1335.7	29	SEP	2236	167	8.	0.1	1335.3

29 SEP	1030	46	5.	0.1	1335.2	*	29 SEP	1636	107	31.	0.2	1335.6	*	29 SEP	2242	168	8.	0.1	1335.3
29 SEP	1036	47	6.	0.1	1335.2	*	29 SEP	1642	108	30.	0.2	1335.6	*	29 SEP	2248	169	8.	0.1	1335.3
29 SEP	1042	48	6.	0.1	1335.2	*	29 SEP	1648	109	30.	0.2	1335.6	*	29 SEP	2254	170	8.	0.1	1335.3
29 SEP	1048	49	6.	0.1	1335.2	*	29 SEP	1654	110	29.	0.2	1335.6	*	29 SEP	2300	171	8.	0.1	1335.3
29 SEP	1054	50	7.	0.1	1335.2	*	29 SEP	1700	111	28.	0.2	1335.6	*	29 SEP	2306	172	8.	0.1	1335.3
29 SEP	1100	51	7.	0.1	1335.2	*	29 SEP	1706	112	27.	0.2	1335.6	*	29 SEP	2312	173	8.	0.1	1335.3
29 SEP	1106	52	8.	0.1	1335.3	*	29 SEP	1712	113	26.	0.1	1335.6	*	29 SEP	2318	174	8.	0.1	1335.3
29 SEP	1112	53	8.	0.1	1335.3	*	29 SEP	1718	114	25.	0.1	1335.6	*	29 SEP	2324	175	8.	0.1	1335.3
29 SEP	1118	54	9.	0.1	1335.3	*	29 SEP	1724	115	24.	0.1	1335.5	*	29 SEP	2330	176	8.	0.1	1335.3
29 SEP	1124	55	10.	0.1	1335.3	*	29 SEP	1730	116	23.	0.1	1335.5	*	29 SEP	2336	177	8.	0.1	1335.3
29 SEP	1130	56	11.	0.1	1335.3	*	29 SEP	1736	117	22.	0.1	1335.5	*	29 SEP	2342	178	8.	0.1	1335.3
29 SEP	1136	57	12.	0.1	1335.3	*	29 SEP	1742	118	21.	0.1	1335.5	*	29 SEP	2348	179	8.	0.1	1335.2
29 SEP	1142	58	16.	0.1	1335.4	*	29 SEP	1748	119	21.	0.1	1335.5	*	29 SEP	2354	180	8.	0.1	1335.2
29 SEP	1148	59	23.	0.1	1335.5	*	29 SEP	1754	120	20.	0.1	1335.5	*	30 SEP	0000	181	8.	0.1	1335.2
29 SEP	1154	60	33.	0.2	1335.7	*	29 SEP	1800	121	19.	0.1	1335.5	*						
29 SEP	1200	61	47.	0.2	1335.8	*	29 SEP	1806	122	18.	0.1	1335.4	*						
						*							*						

****

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	18.00-HR
+ (CFS)	(HR)					
		(CFS)				
+ 86.	7.30		53.	23.	23.	23.
		(INCHES)	3.413	4.367	4.367	4.367
		(AC-FT)	27.	34.	34.	34.

PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	18.00-HR
+ (AC-FT)	(HR)					
0.	7.20		0.	0.	0.	0.

PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	18.00-HR
+ (FEET)	(HR)					
1336.27	7.30		1335.91	1335.46	1335.46	1335.46

CUMULATIVE AREA = 0.15 SQ MI

1

RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

	OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
+					6-HOUR	24-HOUR	72-HOUR			
	HYDROGRAPH AT									
+		1	110.	6.10	19.	8.	8.	0.06		
	HYDROGRAPH AT									
+		2	46.	6.00	7.	3.	3.	0.02		
	HYDROGRAPH AT									
+		5.1AC	23.	6.00	3.	1.	1.	0.01		
	3 COMBINED AT									
+		INTO2	172.	6.10	29.	13.	13.	0.08		
	ROUTED TO									
+		POND2	85.	6.40	29.	13.	13.	0.08		
+									1348.38	6.40
	HYDROGRAPH AT									
+		2.2AC	12.	6.00	2.	1.	1.	0.00		
	HYDROGRAPH AT									
+		N5.3AC	7.	6.00	1.	0.	0.	0.00		
	3 COMBINED AT									
+		INTO3	97.	6.10	32.	14.	14.	0.09		
	ROUTED TO									
+		POND3	96.	6.20	32.	14.	14.	0.09		
+									1343.77	6.20
	HYDROGRAPH AT									
+		23.3AC	104.	6.00	16.	6.	6.	0.04		

	ROUTED TO								
+		POND4	18.	6.70	15.	6.	6.	0.04	
+								1348.43	6.70
	HYDROGRAPH AT								
+		S.3AC	45.	6.00	7.	3.	3.	0.01	
	3 COMBINED AT								
+		INTO5	153.	6.10	54.	23.	23.	0.14	
	ROUTED TO								
+		POND5	86.	7.30	53.	23.	23.	0.14	
+								1338.12	7.30
	HYDROGRAPH AT								
+		S5.3AC	5.	6.00	1.	0.	0.	0.00	
	2 COMBINED AT								
+		INTO6	86.	7.30	53.	23.	23.	0.15	
	ROUTED TO								
+		POND6	86.	7.30	53.	23.	23.	0.15	
+								1336.27	7.30

*** NORMAL END OF HEC-1 ***

REFLECTION RIDGE
"Life as it Should Be"

CONFIDENTIAL

FACSIMILE TRANSMITTAL

FROM:

Name: Marvin Schlegel

Address: 7926 W. 21st Street

Telephone: (316) 721-2153

Fax: (316)721-0620

Date/Time Sent: _____

DELIVER TO:

Company: City Engineering

Name: Vickey

Telephone: _____

Fax: 268-4114

Number of pages following this cover sheet: 5

SPECIAL INSTRUCTIONS: Vicky, Following is the N.P.D.E.S. permit for Northridge Lakes. Thanks for keeping us on schedule.

Marv Schlegel

Please print or type in the unshaded areas only
(fill—in areas are spaced for elite type, i.e., 12 characters/inch).

Form Approved. OMB No. 2040-0086 Approval expires 7-31-88

FORM 1 GENERAL

U.S. ENVIRONMENTAL PROTECTION AGENCY

GENERAL INFORMATION

Consolidated Permits Program

(Read the "General Instructions" before starting.)

I. EPA I.D. NUMBER: F NOT REQUIRED

LABEL ITEMS

I. EPA I.D. NUMBER

III. FACILITY NAME

V. FACILITY MAILING ADDRESS

VI. FACILITY LOCATION

PLEASE PLACE LABEL IN THIS SPACE

GENERAL INSTRUCTIONS

If a preprinted label has been provided, affix it in the designated space. Review the information carefully; if any of it is incorrect, cross through it and enter the correct data in the appropriate fill—in area below. Also, if any of the preprinted data is absent (the area to the left of the label space lists the information that should appear), please provide it in the proper fill—in area(s) below. If the label is complete and correct, you need not complete items I, III, V, and VI (except VI-B which must be completed regardless). Complete all items if no label has been provided. Refer to the instructions for detailed item descriptions and for the legal authorizations under which this data is collected.

II. POLLUTANT CHARACTERISTICS

INSTRUCTIONS: Complete A through J to determine whether you need to submit any permit application forms to the EPA. If you answer "yes" to any questions, you must submit this form and the supplemental form listed in the parenthesis following the question. Mark "X" in the box in the third column if the supplemental form is attached. If you answer "no" to each question, you need not submit any of these forms. You may answer "no" if your activity is excluded from permit requirements; see Section C of the instructions. See also, Section D of the instructions for definitions of bold—faced terms.

SPECIFIC QUESTIONS	MARK 'X' YES	NO	FORM ATTACHED
A. Is this facility a publicly owned treatment works which results in a discharge to waters of the U.S.? (FORM 2A)		X	
B. Does or will this facility (either existing or proposed) include a concentrated animal feeding operation or aquatic animal production facility which results in a discharge to waters of the U.S.? (FORM 2B)		X	
C. Is this a facility which currently results in discharges to waters of the U.S. other than those described in A or B above? (FORM 2C)		X	
D. Is this a proposed facility (other than those described in A or B above) which will result in a discharge to waters of the U.S.? (FORM 2D)		X	
E. Does or will this facility treat, store, or dispose of hazardous wastes? (FORM 3)		X	
F. Do you or will you inject at this facility industrial or municipal effluent below the lowermost stratum containing, within one quarter mile of the well bore, underground sources of drinking water? (FORM 4)		X	
G. Do you or will you inject at this facility any produced water or other fluids which are brought to the surface in connection with conventional oil or natural gas production, inject fluids used for enhanced recovery of oil or natural gas, or inject fluids for storage of liquid hydrocarbons? (FORM 4)		X	
H. Do you or will you inject at this facility fluids for special processes such as mining of sulfur by the Frasch process, solution mining of minerals, in situ combustion of fossil fuel, or recovery of geothermal energy? (FORM 4)		X	
I. Is this facility a proposed stationary source which is one of the 28 industrial categories listed in the instructions and which will potentially emit 100 tons per year of any air pollutant regulated under the Clean Air Act and may affect or be located in an attainment area? (FORM 5)		X	
J. Is this facility a proposed stationary source which is NOT one of the 28 industrial categories listed in the instructions and which will potentially emit 250 tons per year of any air pollutant regulated under the Clean Air Act and may affect or be located in an attainment area? (FORM 5)		X	

III. NAME OF FACILITY

1 SKIP NORTHRIDGE LAKES, INC.

IV. FACILITY CONTACT

A. NAME & TITLE (last, first, & title)	B. PHONE (area code & no.)
2 SCHELLENBERG, MARVIN - PRESIDENT	316 721 2153

V. FACILITY MAILING ADDRESS

A. STREET OR P.O. BOX	B. CITY OR TOWN	C. STATE	D. ZIP CODE
3 7926 W 21 N	4 WICHITA	KS	67205

VI. FACILITY LOCATION

A. STREET, ROUTE NO. OR OTHER SPECIFIC IDENTIFIER	B. COUNTY NAME	C. CITY OR TOWN	D. STATE	E. ZIP CODE	F. COUNTY CODE (if known)
5 NORTHRIDGE LAKES ADD	SEDGWICK	6 WICHITA	KS	67205	

CONTINUED FROM THE FRONT

VII. SIC CODES *(4-digit, in order of priority)*

A. FIRST: 7 | (specify) N/A

B. SECOND: 7 | (specify)

C. THIRD: 7 | (specify)

D. FOURTH: 7 | (specify)

VIII. OPERATOR INFORMATION

A. NAME: 8

B. Is the name listed in Item VIII-A also the owner? ☐ YES ☐ NO

C. STATUS OF OPERATOR *(Enter the appropriate letter into the answer box; if "Other", specify.)*
F = FEDERAL; M = PUBLIC *(other than federal or state)*; $ = STATE; O = OTHER *(specify)*; P = PRIVATE

(specify)

D. PHONE *(area code & no.)*: A

E. STREET OR P.O. BOX

F. CITY OR TOWN: B

G. STATE

H. ZIP CODE

IX. INDIAN LAND

Is the facility located on Indian lands? ☐ YES ☐ NO

X. EXISTING ENVIRONMENTAL PERMITS

A. NPDES *(Discharges to Surface Water)*: 9 N

B. UIC *(Underground Injection of Fluids)*: 9 U

C. RCRA *(Hazardous Wastes)*: 9 R

D. PSD *(Air Emissions from Proposed Sources)*: 9 P

E. OTHER *(specify)*: 9 | (specify)

F. OTHER *(specify)*: 9 | (specify)

XI. MAP

Attach to this application a topographic map of the area extending to at least one mile beyond property boundaries. The map must show the outline of the facility, the location of each of its existing and proposed intake and discharge structures, each of its hazardous waste treatment, storage, or disposal facilities, and each well where it injects fluids underground. Include all springs, rivers and other surface water bodies in the map area. See instructions for precise requirements.

XII. NATURE OF BUSINESS *(provide a brief description)*

NORTHRIDGE LAKES IS A SINGLE FAMILY URBAN RESIDENTIAL DEVELOPMENT WHICH ULTIMATELY WILL CONTAIN 138 UNITS ON APPROX. 76 ACRES. THE DEVELOPMENT IS LOCATED ON UPLAND AREAS. THERE IS NO KNOWN CONTAMINATION ON SITE, WHICH HAS BEEN IN CULTIVATION FOR MANY YEARS.

XIII. CERTIFICATION *(see instructions)*

I certify under penalty of law that I have personally examined and am familiar with the information submitted in this application and all attachments and that, based on my inquiry of those persons immediately responsible for obtaining the information contained in the application, I believe that the information is true, accurate and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment.

A. NAME & OFFICIAL TITLE *(type or print)*	B. SIGNATURE	C. DATE SIGNED
MARVIN SCHELLENBERG PRESIDENT	Marvin Schellenberg Pres.	9/18/95

COMMENTS FOR OFFICIAL USE ONLY

C

EPA Form 3510-1 (Rev. 10-80) Reverse

* U.S. Government Printing Office : 1985 - 486-765/32991

NORTHRIDGE LAKES
NPDES PERMIT APPLICATION FOR CONSTRUCTION ACTIVITY
SUPPLEMENTAL INFORMATION

A. NorthRidge Lakes is an urban single family residential development in northwest Wichita, Ks. It will ultimately consist of 138 housing units on approximately 76 acres. Construction activities on the site include the following:
- Infrastructure improvements to be built by the City of Wichita, including sanitary sewers, water distribution systems, storm water sewers. paving, and sidewalks.
- Utility construction by the utility companies
- Pond construction by the Developer
- Housing construction by individual lot owners/Builders.

B. The site comprises 76 acres. During the life of the project, it is estimated that 75% of the land will be disturbed.

C. BMP's during construction of the project include the following:
- Seeding and mulching of the site after each City infrastructure project
- Seeding of building lots after utility installation
- Installation of sediment control barriers at strategic site locations, including all city drainage inlets.

No state or local regulations regarding stormwater runoff quality apply during construction.

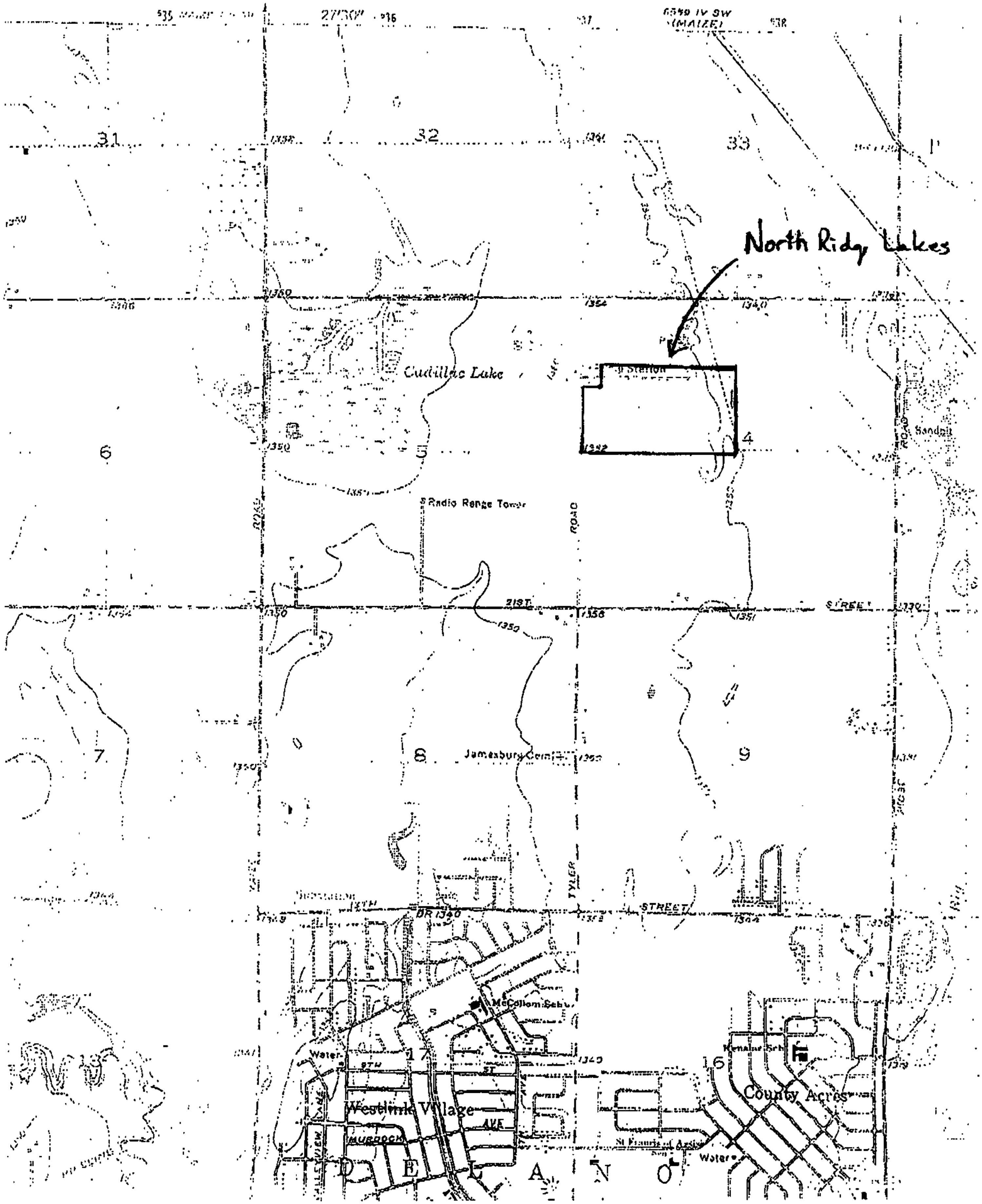
D. At the completion of construction, the following BMP's will be in place:
- Stormwater detention ponds will limit the runoff from the developed site to a level compatible with downstream drainage facilities.
- Stormwater detention pond will serve to trap sediment before it leaves the site.
- Each building lot will be turfed.
- All common areas and open space will be turfed.
- Pond banks will be protected with stone riprap at the static water level. All pond banks will be turfed.

Local requirements dictate that the post-developed peak runoff discharge rate be reduced to that existing prior to development.

E. The existing site is in cultivation with an estimated runoff coefficient C=0.3. The estimated proposed conditions runoff coefficient C=0.5.

F. The site discharges into the City of Wichita storm sewer system, and ultimately to an unnamed tributary of the Big Slough near the East 1/4 Corner of Section 4, T.27 S., R 1 W.

STATE OF KANSAS



STORMWATER POLLUTION PREVENTION PLAN CERTIFICATION

I, the undersigned, certify that a Stormwater Pollution Prevention Plan (SWPPP) will be or has been developed for the indicated construction project. I also certify that the SWPPP will be implemented at the time construction begins.

NORTH RIDGE LAKES ADDITION

Name of Construction Project

NORTH RIDGE LAKES, INC.

Owner's Signature

BY: MARVIN SCHELLENBERG, PRES.

9/12/95

Date

Kansas Department of Health and Environment
Bureau of Water - Industrial Programs Section
Forbes Field - Bldg. 283
Topeka, KS 66620-0001
(913)296-5524

SWPPP.CRT

HEC-1 & CULVERT FOR RE-ANALYSIS 10-10-1995

OF NORTHRIDGE LAKES - EAST 1/2 DRAINAGE

CURRENT DATE: 10-10-1995
CURRENT TIME: 11:40:12

FILE DATE: 10-10-1995
FILE NAME: 3TO5

FHWA CULVERT ANALYSIS
HY-8, VERSION 3.2

Good

CU LV	SITE DATA: INLET ELEV. (FT)	SITE DATA: OUTLET ELEV. (FT)	SITE DATA: CULVERT LENGTH (FT)	CULVERT SHAPE, MATERIAL, INLET: BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	146.00	145.00	340.00	1 RCP	3.50	3.50	.012	CONVENTIONAL
2	147.8	143.8	314					
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (CFS) FILE: 3TO5 DATE: 10-10-1995

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
150.20	0	0	0	0	0	0	0	0	1
150.25	10	10	0	0	0	0	0	0	1
150.41	20	20	0	0	0	0	0	0	1
150.68	30	30	0	0	0	0	0	0	1
151.06	40	40	0	0	0	0	0	0	1
151.54	50	50	0	0	0	0	0	0	1
152.13	60	60	0	0	0	0	0	0	1
152.83	70	70	0	0	0	0	0	0	1
153.63	80	80	0	0	0	0	0	0	1
154.54	90	90	0	0	0	0	0	0	1
155.56	100	100	0	0	0	0	0	0	1
160.00	135	135	0	0	0	0	0	OVERTOPPING	

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: 3TO5 DATE: 10-10-1995

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
150.20	0.00	0	0	0.00
150.25	0.00	10	0	0.00
150.41	0.00	20	0	0.00
150.68	0.00	30	0	0.00
151.06	0.00	40	0	0.00
151.54	0.00	50	0	0.00
152.13	0.00	60	0	0.00
152.83	0.00	70	0	0.00
153.63	0.00	80	0	0.00
154.54	0.00	90	0	0.00
155.56	0.00	100	0	0.00

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

CURRENT DATE: 10-10-1995 FILE DATE: 10-10-1995
CURRENT TIME: 11:40:12 FILE NAME: 3TO5

CULVERT # 1

PERFORMANCE CURVE FOR 1 BARREL(S)

Q (cfs)	HWE (ft)	TWE (ft)	ICH (ft)	OCH (ft)	FLOW TYPE	CCE (ft)	FCE (ft)	TCE (ft)	VO (fps)
0	150.20	150.20	0.00	4.20	0-NF	0.00	146.00	0.00	0.00
10	150.25	150.20	1.31	4.25	4-FF	0.00	0.00	0.00	1.04
20	150.41	150.20	1.93	4.41	4-FF	0.00	0.00	0.00	2.08
30	150.68	150.20	2.48	4.68	4-FF	0.00	0.00	0.00	3.12
40	151.06	150.20	2.96	5.06	4-FF	0.00	0.00	0.00	4.16
50	151.54	150.20	3.42	5.54	4-FF	0.00	0.00	0.00	5.20
60	152.13	150.20	3.91	6.13	4-FF	0.00	0.00	0.00	6.24
70	152.83	150.20	4.45	6.83	4-FF	0.00	0.00	0.00	7.28
80	153.63	150.20	5.08	7.63	4-FF	0.00	0.00	0.00	8.32
90	154.54	150.20	5.79	8.54	4-FF	0.00	0.00	0.00	9.35
100	155.56	150.20	6.60	9.56	4-FF	0.00	0.00	0.00	10.39

El. inlet face invert 146.00 ft El. outlet invert 145.00 ft
El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

***** SITE DATA ***** CULVERT INVERT **********

INLET STATION (FT)	0.00
INLET ELEVATION (FT)	146.00
OUTLET STATION (FT)	340.00
OUTLET ELEVATION (FT)	145.00
NUMBER OF BARRELS	1.00
SLOPE (V-FT/H-FT)	0.0029
CULVERT LENGTH ALONG SLOPE (FT)	340.00

***** CULVERT DATA SUMMARY **********

BARREL SHAPE	CIRCULAR
BARREL DIAMETER	3.50 FT
BARREL MATERIAL	CONCRETE
BARREL MANNING'S N	0.012
INLET TYPE	CONVENTIONAL
INLET EDGE AND WALL	SQUARE EDGE WITH HEADWALL
INLET DEPRESSION	NONE

CURRENT DATE: 10-10-1995
CURRENT TIME: 11:40:12

FILE DATE: 10-10-1995
FILE NAME: 3TO5

TAILWATER

CONSTANT WATER SURFACE ELEVATION
150.20

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH (FT)	30.00
CREST LENGTH (FT)	100.00
OVERTOPPING CREST ELEVATION (FT)	160.00

20-01-01-13
20-01-04-06
20-01-04-29

AFFIDAVIT

STATE OF KANSAS, COUNTY OF SEDGWICK: ss.

Michael E. Lindebak, P.E., City Engineer for the City of Wichita, Kansas, being first duly sworn, on oath states:

I have examined the recorded plats of Northridge Lakes and Northridge Lakes 2nd Addition to Wichita, Sedgwick County Kansas, and have found that three street names should be changed as follows:

MEADOW GROVE ST, from N Tyler Rd to Lake Ridge St; adjacent to lot 2 Block 1, and lots 2 & 3 Block 2, in the Northridge Lakes 2nd Addition; lots 3-13 Block 3, lots 38 & 39 Block 4, and lots 49-53 Block 4 in the Northridge Lakes Addition should be changed to **W NORTHRIDGE ST**.

MEADOW GROVE CT; adjacent to lots 1 & 2 Block 1; and lots 1 & 2 Block 2 in the Northridge Lakes 2nd Addition should be changed to **W NORTHRIDGE CT**.

MEADOW GROVE CT; adjacent to lots 39-49 Block 4 in the Northridge Lakes Addition should be changed to **W NORTHRIDGE CT**.

FURTHER AFFIANT SAITH NOT.

Michael E. Lindebak, P.E.

Dated this 16th day of June, 1997

(Seal)

ATTEST:

Taylor Levins, Office of Central Inspection
Permits Examiner

Lori Wilkerson, City of Wichita
Address Subcommittee Chairperson

STATE OF KANSAS, COUNTY OF SEDGWICK: ss.

Be it remembered that on this 16th, day of June, 1997, before me a notary public in and for said County and State, came Michael E. Lindebak, to me known to be the same person who executed the foregoing instrument duly acknowledged by me. In testimony whereof, I have hereunto set my hand and affixed my Notarial Seal the day and year above written.

JACK L. LOVE
Notary Public - State of Kansas
My Appt. Expires 1-5-99

My Appointment Expires 1/5/99