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CONSULTANTS
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SUPPLEMENT TO
"DRAINAGE PLAN & SUPPORTING CALCULATIONS"

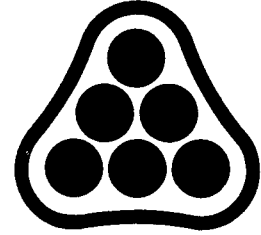
FOR
AMARADO ESTATES THIRD ADDITION
TO WICHITA, SEDGWICK COUNTY, KANSAS

PREPARED BY
PROFESSIONAL ENGINEERING CONSULTANTS, P.A.
ENGINEERS
WICHITA, KANSAS

FEBRUARY 25, 1987

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February 25, 1987

Michael E. Lindebak, P.E., City Engineer
 7th Floor - City Hall
 455 North Main
 Wichita, Kansas 67202

Attention: Mr. Carl Gipson, P.E.

Reference: Amarado Estates 3rd Addition
 Drainage Plan
 PEC File No: 36-87053-1047

Dear Mr. Gipson:

As requested, we are transmitting herewith two (2) copies of the Supplement to the Drainage Plan and Supporting Calculations for Amarado Estates 3rd Addition.

The plan has been revised to divert the 100-year runoff from the southwesterly portion of the plat (Nodes 211-214) to 18th Street. Also, the outfall pipe of System 100 was increased from 48" to 54" to handle 100% of the 100-year storm runoff.

Please review and advise our office of your comments.

Very truly yours,

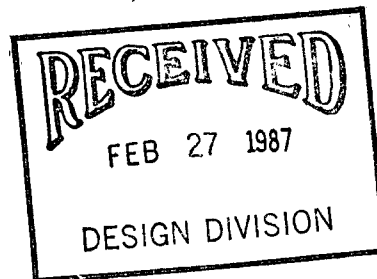
PROFESSIONAL ENGINEERING CONSULTANTS, P.A.

Charles S. Brown
 Charles S. Brown, P.E.
 Project Engineer

enclosures

CSB/mkm

xc: Randy Voth





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Project Amarado 3rd

Item Revised Drainage Plan

100 Year flow from 17th Street Area only
into System 200 (Nodes 200-210)

All remaining areas to System 100 (Nodes 100-116
plus 211-214)

| SYSTEM 200 | <u>Node</u> | <u>Q₁₀₀</u> | |
|------------|-------------|------------------------|-----|
| | 210 | 3.1 | cfs |
| | 209 | 16.0 | |
| | 208 | 6.3 | |
| | 207 | 3.4 | |
| | 206 | 2.9 | |
| | 205 | 7.9 | |
| | 204 | 3.5 | |
| | 203 | 3.6 | |
| | 202 | 10.2 | |
| | 201 | 0.6 | |
| | 200 | - | |
| | TOTAL | 65.5 | cfs |



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Project Amarado 3rd.

Item Revised Drainage Plan

| <u>SYSTEM</u> | <u>100</u> | <u>Node</u> | <u>Q₁₀₀</u> |
|---------------|------------|-------------|------------------------|
| | | 116 | 16.1 |
| | | 115 | 23.7 |
| | | 114 | 19.5 |
| | | 113 | 8.3 |
| | | 112 | 1.0 |
| | | 111 | 13.4 |
| | | 110 | 3.4 |
| | | 109 | 3.8 |
| | | 108 | 8.4 |
| | | 107 | 4.6 |
| | | 106 | 4.0 |
| | | 105 | 21.7 |
| | | 104 | 13.8 |
| | | 103 | 2.5 |
| | | 102 | 6.4 |
| | | 101 | 3.9 |
| | | 100 | - |
| | | 214 | 44.4 |
| | | 213 | 2.2 |
| | | 212 | 10.4 |
| | | 211 | 9.5 |
| | | | <u>77.10</u> cfs |



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Project Amarado 3rd

Item Revised Drainage Plan.

CHECK STREET FLOW 17th STREET (SYSTEM 200)

$$Q_{\text{street}} = Q_{100} - Q_{2(\text{pipes})}$$

$$Q_{\text{street}} = 65.5 - (Q_2 \text{ nodes } 200-210)$$

$$= 65.5 - (23.8)$$

$$= 41.7 \text{ cfs}$$

$$\text{From Page 4, } Q_{\text{max}} = 1,262.0 \text{ s}^{1/2}$$

$$= 1,262.0 \times 0.0031^{1/2}$$

$$= 70.3 \text{ cfs}$$

$$Q_{\text{street}} < Q_{\text{max}}$$

Street Flow OK

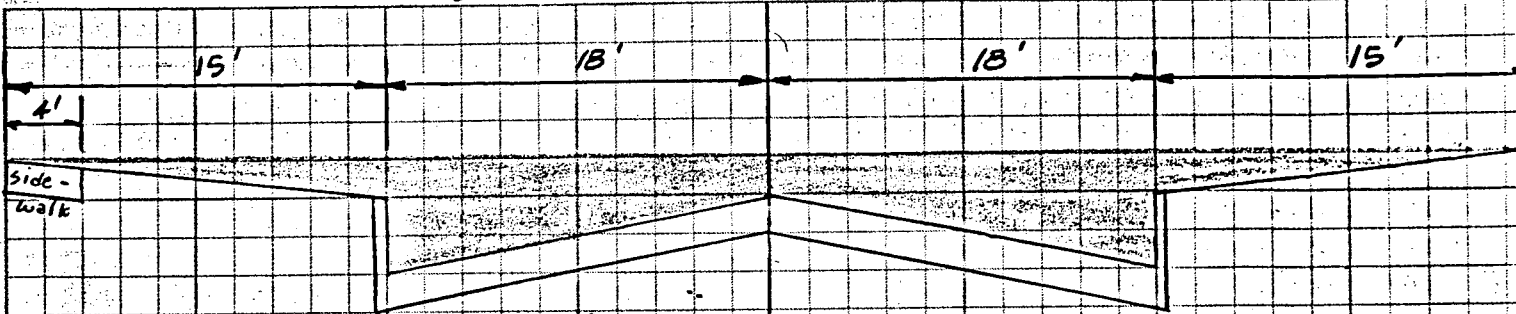


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Project Amavado 3rd Addition

Item Drainage Plan - System 200

STREET FLOW - 100-YR



Use Manning's Eq'n

$$Q = \frac{1.486}{n} A R^{2/3} S^{1/2}$$

$$n = \frac{(4' \times 0.04) + (10.5 \times 0.03) + 2(1.05 \times 0.013) + (36 \times 0.016) + (14.5 \times 0.016)}{67.1}$$

$$= 0.021$$

$$A = (2 \times \frac{1}{2} \times 15 \times 0.4) + (36 \times 0.4) + (2 \times \frac{1}{2} \times 18 \times 0.55)$$

$$= 30.3$$

$$P = (2 \times 15) + (2 \times 0.55) + (2 \times 18)$$

$$= 67.1$$

$$R = A/P = 0.451565$$

$$R^{2/3} = 0.5886$$

$$Q = \frac{1.486}{0.021} \times 30.3 \times 0.5886 \times S^{1/2}$$

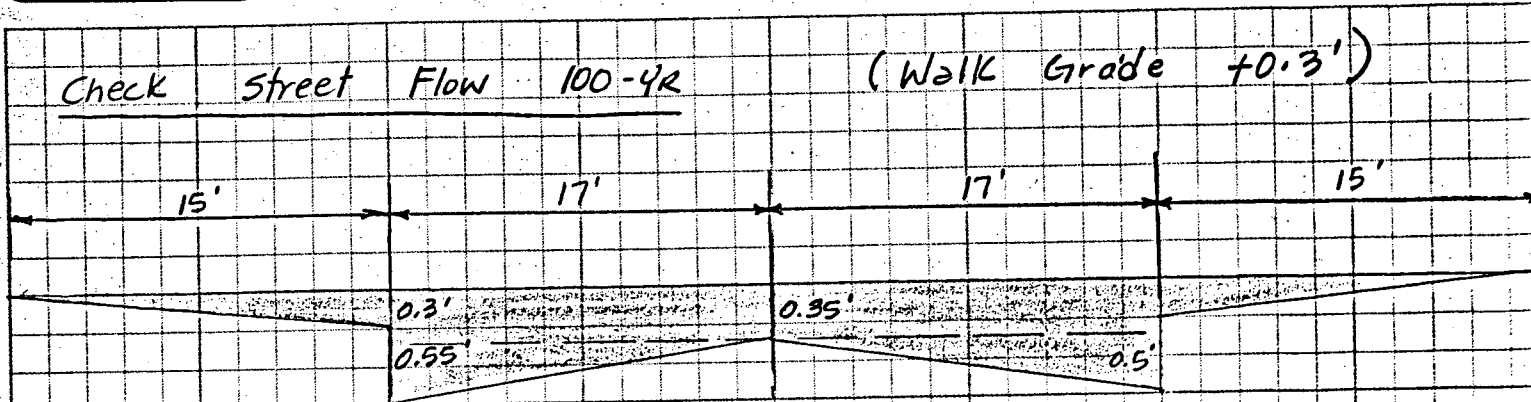
$$Q = 1,262.0 S^{1/2}$$



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Project Amarado 3rd

Item Drainage Plan - System 100



Determine Q_{max} in Street R-O-W

Use Mannings Eq'n $Q = \frac{1.486}{n} A R^{2/3} S^{1/2}$

$$n = \frac{2(14.5 \times 0.030) + 2(1.05' \times 0.013) + 2(17 \times 0.016)}{65.1}$$

$$n = \frac{1.4413}{65.1} = 0.0221$$

$$A = 2\left(\frac{1}{2} \times 15 \times 0.3\right) + (34 \times 0.35) + 2\left(\frac{1}{2} \times 0.5 \times 17\right)$$

$$= 24.90 \text{ SF}$$

$$p = (2 \times 15) + (2 \times 17) + (2 \times 0.55)$$

$$= 65.1'$$

$$R = A/p = 24.9/65.1 = 0.38249$$

$$R^{2/3} = 0.527$$

$$Q = \frac{1.486}{0.0221} \times 24.90 \times 0.527 \times 5^{1/2}$$

$$Q = 882.3 \times 5^{1/2}$$

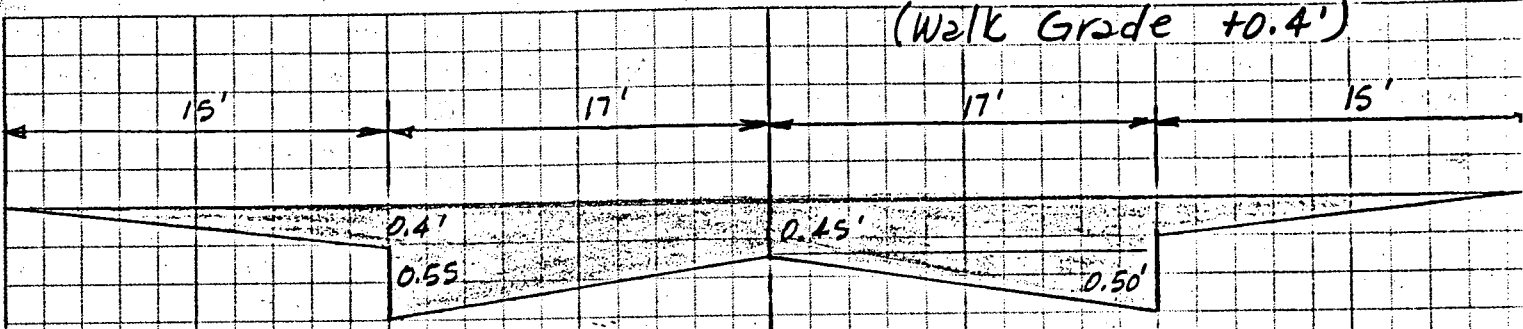


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Project Amarado 3rd Addition

Item Drainage Plan - System 100

(Walk Grade +0.4')



$n = 0.0221$ (see previous sheet)

$$A = 2\left(\frac{1}{2} \times 15' \times 0.4'\right) + (34 \times 0.45') + 2\left(\frac{1}{2} \times 17' \times 0.5'\right)$$

$$= 29.8 \text{ SF}$$

$$P = 65.1'$$

$$R = A/P = 29.8/65.1 = 0.4577$$

$$R^{2/3} = 0.594$$

$$Q = \frac{1.486}{0.0221} \times 29.8 \times 0.594 \times 5^{1/2}$$

$$Q = 1,190.2 \text{ s}^{1/2}$$

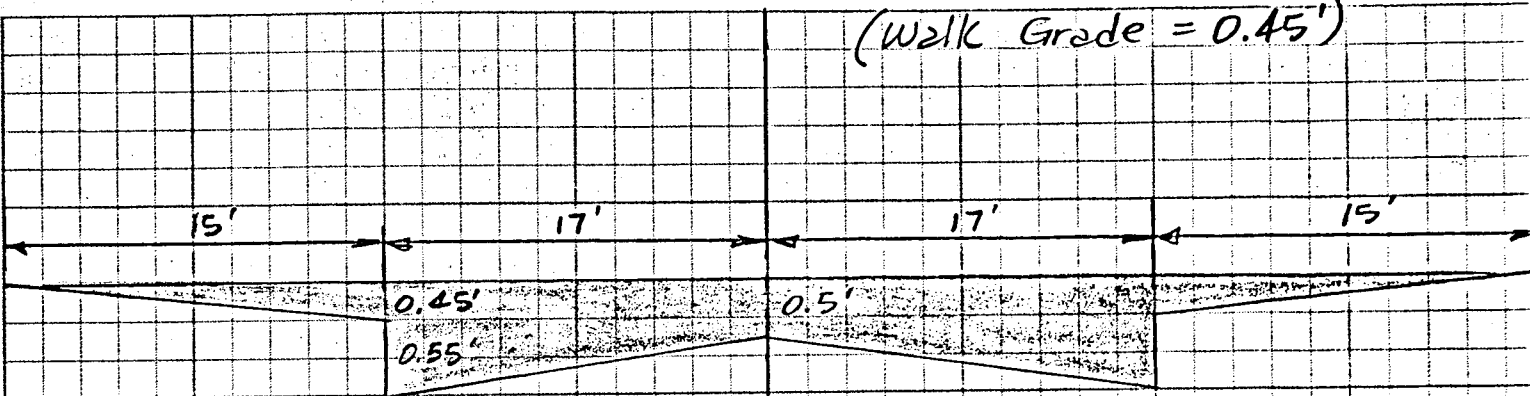


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Project Amarado 3rd

Item Drainage Plan - System 100

(Walk Grade = 0.45')



$$n: 0.0221 \text{ (see previous sheet)}$$

$$A = 2\left(\frac{1}{2} \times 15' \times 0.45'\right) + (34' \times 0.5) + 2\left(\frac{1}{2} \times 17' \times 0.5'\right)$$

$$= 32.25 \text{ SF}$$

$$p = 65.1$$

$$R = A/p = 32.25/65.1 = 0.4954$$

$$R^{2/3} = 0.626$$

$$Q = \frac{1.486}{n} A R^{2/3} S^{1/2}$$

$$= \frac{1.486}{0.0221} \times 32.25 \times 0.626 \times S^{1/2}$$

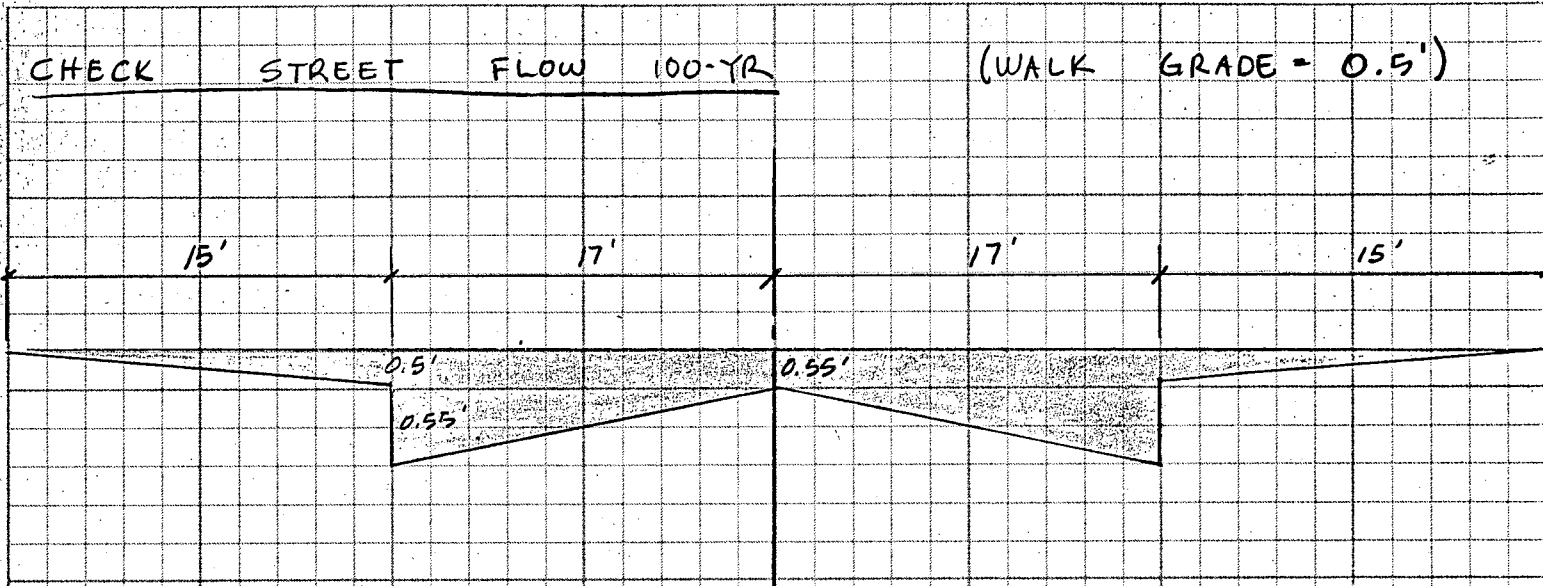
$$Q = 1357.5 S^{1/2}$$



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Project Amarado 3rd

Item Revised Drainage Plan



$$n = 0.0221 \quad (\text{see previous sheet})$$

$$A = 2 \left(\frac{1}{2} \times 15 \times 0.5 \right) + (34 \times 0.55) + 2 \left(\frac{1}{2} \times 17 \times 0.5 \right)$$

$$= 34.7 \text{ SF}$$

$$p = 65.1$$

$$R = A/p = 34.7/65.1 = 0.5330$$

$$R^{2/3} = 0.6574$$

$$Q_{\max} = \frac{1.486}{0.0221} \times 34.7 \times 0.6574 \times 5^{1/2}$$

$$Q_{\max} = 1,533.9 \text{ s}^{1/2}$$

86.5

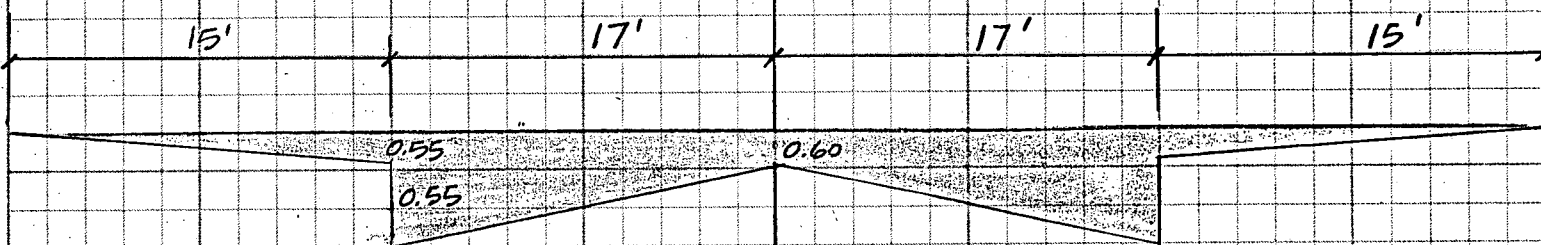


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Project Amarado 3rd

Item Revised Drainage Plan

CHECK STREET FLOW 100-YR (WALK GRADE = 0.55')



$$n = 0.0221 \text{ (see previous sheet)}$$

$$A = 2\left(\frac{1}{2} \times 15' \times 0.55'\right) + (34 \times 0.60') + 2\left(\frac{1}{2} \times 17' \times 0.5'\right)$$
$$= 37.15 \text{ SF}$$

$$p = 65.1$$

$$R = A/p = 37.15/65.1 = 0.570661$$

$$R^{2/3} = 0.687995$$

$$Q_{\max} = \frac{1.486}{0.0221} \times 37.15 \times 0.687995 \times s^{1/2}$$

$$Q_{\max} = 1,718.6 \text{ s}^{1/2}$$

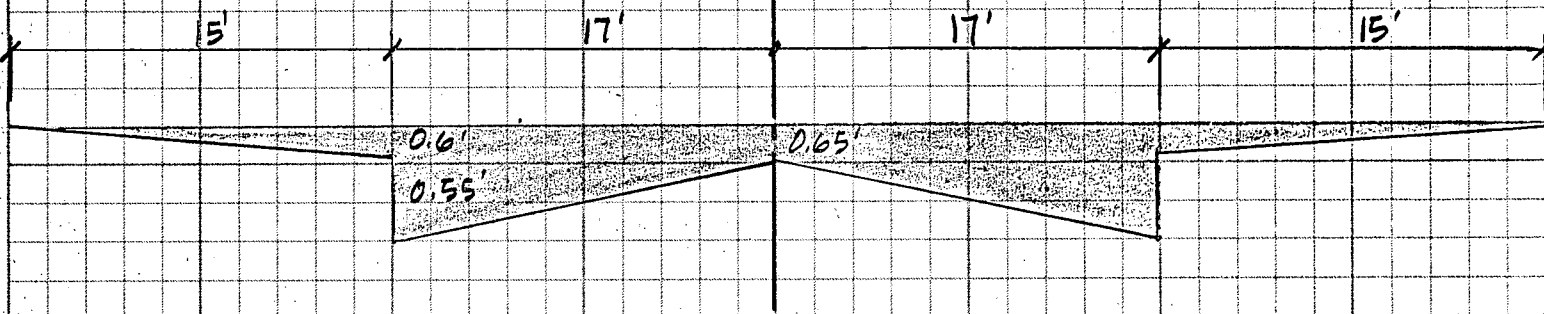


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Project Amarado 3rd

Item Revised Drainage Plan

CHECK STREET FLOW 100-YEAR (WALK GRADE = 0.6')



$n = 0.0221$ (see previous sheet)

$A = 2(\frac{1}{2} \times 15 \times 0.6) + (34 \times 0.65) + 2(\frac{1}{2} \times 17 \times 0.5)$
 $= 39.6 \text{ SF}$

$P = 65.1'$

$R = A/P = 39.6 / 65.1 = 0.6083$

$R^{2/3} = 0.71792$

$Q_{max} = \frac{1.486}{0.0221} \times 39.6 \times 0.71792 \times S^{1/2}$

$Q_{max} = 1,911.6 \text{ S}^{1/2}$



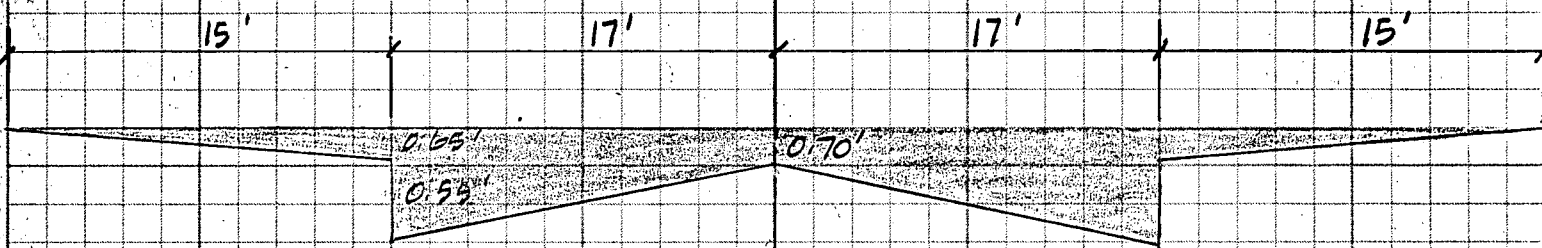
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Project Amarado 3rd

Item Revised Drainage Plan

CHECK STREET FLOW 100-YR

(WALK GRADE = 0.65')



$n = 0.0221$ (see previous sheet)

$$A = 2\left(\frac{1}{2} \times 15 \times 0.65\right) + (34 \times 0.70) + 2\left(\frac{1}{2} \times 17 \times 0.55\right)$$

$$= 42.05 \text{ SF}$$

$$p = 65.1$$

$$R = A/p = 42.05/65.1 = 0.6459$$

$$R^{2/3} = 0.747234$$

$$Q_{max} = \frac{1.486}{0.0221} \times 42.05 \times 0.747234 \times s^{1/2}$$

$$Q_{max} = 2,112.8 \text{ s}^{1/2}$$

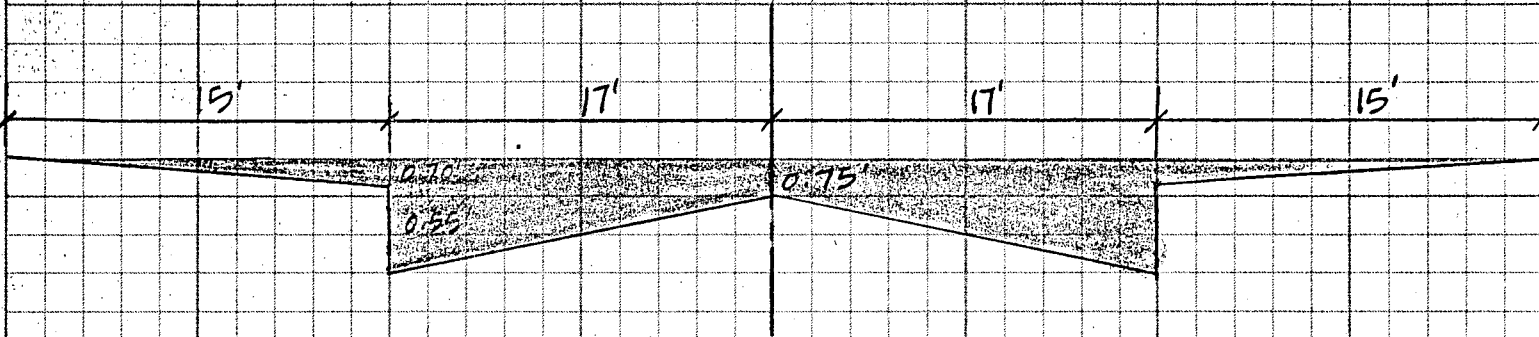


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Project Amarado 3rd

Item Revised Drainage Plan.

CHECK STREET FLOW 100 YR (WALK GRADE = 0.70')



$n = 0.0221$ (see previous sheet)

$$A = 2\left(\frac{1}{2} \times 15 \times 0.7\right) + (34 \times 0.75) + 2\left(\frac{1}{2} \times 17 \times 0.5\right)$$

$$= 44.5 \text{ SF}$$

$p = 65.1$

$$R = A/p = 44.5/65.1 = 0.683564$$

$R^{2/3} = 0.775984$

$$Q_{max} = \frac{1.486}{0.0221} \times 44.5 \times 0.775984 \times s^{1/2}$$

$Q_{max} = 2,321.9 \text{ s}^{1/2}$



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Project Amavado 3rd

Item Drainage Plan - system 100

1. Check street Flow Approaching Nodes 115-116

$Q_{100} :$

| | | |
|----------|---|-------------|
| Node 116 | = | 16.1 cfs |
| 115 | = | <u>23.7</u> |
| | | <u>39.8</u> |

$Q_2 \text{ (pipe)} = 0$

$Q_{\text{street}} = Q_{100} - Q_2 = 39.8 - 0 = 39.8$

$Q_{\text{max}} = 882^3 \times 5^{1/2}$
 $= 49.9 \text{ cfs}$

Street Flow OK
 (Use 0.3 Walk Gr.)

2. Check Street Flow Approaching Nodes 114-113

$Q_{100} :$

| | |
|----------|--------------------------|
| Node 116 | 16.1 cfs |
| 115 | 23.7 |
| 114 | $30\% \times 19.5 = 5.9$ |
| 113 | <u>8.3</u> |
| | <u>54.0 cfs</u> |

$Q_2 \text{ (pipe)} = 14.9$
 113-113

$Q_{\text{street}} = Q_{100} - Q_2 \text{ pipe} = 54.0 - 14.9 = 39.1 \text{ cfs}$

$Q_{\text{max}} = 49.9$

Street Flow OK
 (Use 0.3 Walk Gr.)



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Project Amarado 3rd.

Item Revised Drainage Plan

3. Check street Flow Approaching Nodes 109-111

| | | | | |
|-------------|-------|-----|---|--------------|
| $Q_{100} =$ | Nodes | 116 | = | 16.1 |
| | | 115 | | 23.7 |
| | | 114 | | 19.5 |
| | | 113 | | 8.3 |
| | | 112 | | 1.0 |
| | | 111 | | 13.4 |
| | | 109 | | 3.4 |
| | | 214 | | 44.4 |
| | | 213 | | 2.2 |
| | | 212 | | 10.4 |
| | | 211 | | 9.5 |
| | | | | <u>151.9</u> |

$$Q_2 = Q_{\text{pipe } 112-109} + Q_{\text{pipe } 211-210}$$
$$= 25.3 + 24.8 = 50.1$$

$$Q_{\text{street}} = 151.9 - 50.1 = 101.8 \text{ cfs}$$

$$Q_{\text{max}} = 103.1$$

street Flow OK
(Use 0.6' Walk Gr)



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Project Amarado 3rd

Item Revised Drainage Plan

4. Check Street Flow Approaching Nodes 106-107

| Q_{100} | Nodes | | |
|-----------|-------|-----|-------|
| | | 116 | 16.1 |
| | | 115 | 23.7 |
| | | 114 | 19.5 |
| | | 113 | 8.3 |
| | | 112 | 1.0 |
| | | 111 | 13.4 |
| | | 110 | 3.4 |
| | | 109 | 3.8 |
| | | 108 | 8.4 |
| | | 107 | 4.6 |
| | | 106 | 4.0 |
| | | 214 | 44.4 |
| | | 213 | 2.2 |
| | | 212 | 10.4 |
| | | 211 | 9.5 |
| | | | <hr/> |
| | | | 172.7 |

$$\begin{aligned}
 Q_c &= Q_{\text{pipe } 211-210} + Q_{\text{pipe } 109-106} + Q_{\text{pipe } 108-107} \\
 &= 24.8 + 32.5 + 2.9 \\
 &= 60.2
 \end{aligned}$$

$$\begin{aligned}
 Q_{\text{street}} &= Q_{100} - Q_{\text{pipe}} \\
 &= 172.7 - 60.2 \\
 &= 112.5 \text{ cfs}
 \end{aligned}$$

$$Q_{\text{max}} = 119.5 \text{ cfs}$$

Street Flow OK
(Use 0.65 Walk Gr)



Date Feb. 25, 1987 Page 16 of 21

Project Amarado 3rd

Item Revised Drainage Plan.

5. Check Street Flow Approaching Nodes 102-101 (W)

| Q_{100} | Node | Flow (cfs) | |
|-----------|------|--------------|-------|
| | 116 | 16.1 | |
| | 115 | 23.7 | |
| | 114 | 19.5 | |
| | 113 | 8.3 | |
| | 112 | 1.0 | |
| | 111 | 13.4 | |
| | 110 | 3.4 | |
| | 109 | 3.8 | |
| | 108 | 8.4 | |
| | 107 | 4.6 | |
| | 106 | 4.0 | |
| | 103 | 2.5 | |
| | 102 | 3.2 | (50%) |
| | 101 | 2.0 | (50%) |
| | 214 | 44.4 | |
| | 213 | 2.2 | |
| | 212 | 10.4 | |
| | 211 | 9.5 | |
| | | <u>180.4</u> | cfs |

$$Q_2 = Q_{\text{pipe } 211-210} + Q_{\text{pipe } 103-101}$$

$$= 24.8 + 38.5$$

$$= 63.3$$

$$Q_{\text{street}} = 180.4 - 63.3$$

$$= 117.1 \text{ cfs}$$

$$Q_{\text{max}} = 119.5 \text{ cfs}$$

Street Flow OK
(Use 0.65 walk Grd)



Date Feb. 12, 1987 Page 17 of 21

Project Amarado 3rd

Item Drainage Plan System 100

6. Check Street Flow Approaching Nodes 105-104

| | | | |
|-------------|------|-----|-----------------|
| Q_{100} : | Node | 105 | 21.7 cfs |
| | | 104 | 13.8 |
| | | | <u>35.5 cfs</u> |

$$Q_2 = 0$$

$$Q_{street} = Q_{100} - Q_2 = 35.5 - 0 = 35.5 \text{ cfs}$$

$$Q_{max} = 49.9 \text{ cfs}$$

Street Flow OK
(Use 0.3' Walk G)

7. Check Street Flow Approaching Nodes 102-101 (N)

| | | | |
|-------------|-------|-----|-----------------|
| Q_{100} : | Nodes | 105 | 21.7 cfs |
| | | 104 | 13.8 |
| | | 102 | 50% x 6.4 = 3.2 |
| | | 101 | 70% x 3.9 = 2.7 |
| | | | <u>41.4 cfs</u> |

$$Q_{2(\text{pipe})} = 12.6$$

$$Q_{street} = Q_{100} - Q_2 = 41.4 - 12.6 = 28.8 \text{ cfs}$$

$$Q_{max} = 49.9$$

Street Flow OK
(Use 0.3' Wlk Gr)
(Except Where 0.65 Wk Gr (W) Controls)



Date Feb. 25, 1987 Page 18 of 21

Project Amarado 3rd.

Item Revised Drainage Plan

Size Outlet Pipe For Q_{100}

$Q_{100} \sum \text{Nodes } 116-100 = 154.5$

$Q_{\text{overflow}} \text{ Nodes } 214-211 = 44.4$
 2.2
 10.4
 9.5

 66.5

$- 24.8 = 41.7$
 (Pipe # 11-210)

$Q_{100} \text{ Approaching Nodes } 101 + 102 = 154.5$
 $Q_{\text{total}} + 41.7$

 196.2 cfs

$HGL @ \text{Node } 101 = 153.9 \text{ TC}$
 0.65 Walk Grd

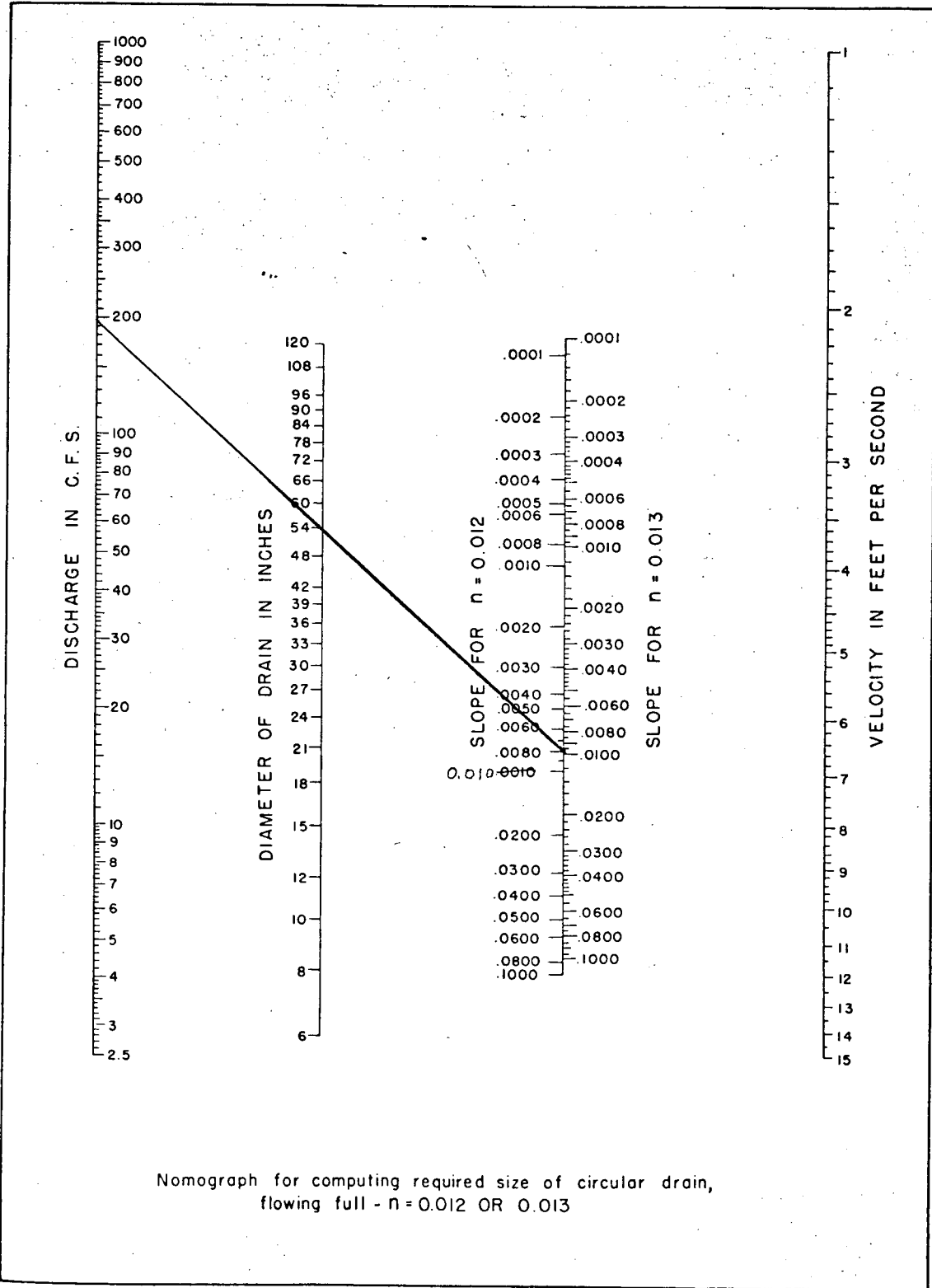
 154.55

$HGL @ \text{Channel} = 152.9$

$\text{Hyp. Slope} = \frac{154.55 - 152.9}{170} = 0.97\%$

From Page 19, USE 54" RCP

19/21





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Project Amorado 3rd

Item Revised Drainage Plan

CALC. LENGTH OF INLET NEEDED

$$Q_{100} \text{ approaching Nodes } 101-102 = 196.2 \text{ cfs}$$

$$\begin{aligned} Q_2 \text{ already in pipe} &= Q_{\text{pipe } 103-101} + Q_{\text{pipe } 104-101} + Q_{\text{pipe } 102-101} \\ &= 38.5 + 12.6 + 2.2 \\ &= 53.3 \text{ cfs} \end{aligned}$$

$$Q_{100} \text{ street} = 196.2 - 53.3 = 142.9 \text{ cfs (N+W)}$$

From Page 21, $Q/L = 3.1 \text{ cfs/ft}$ (capacity of inlet)

$$L = 142.9 \text{ cfs} / 3.1 \text{ cfs/ft} = \underline{\underline{46.1' \text{ Inlet.}}}$$

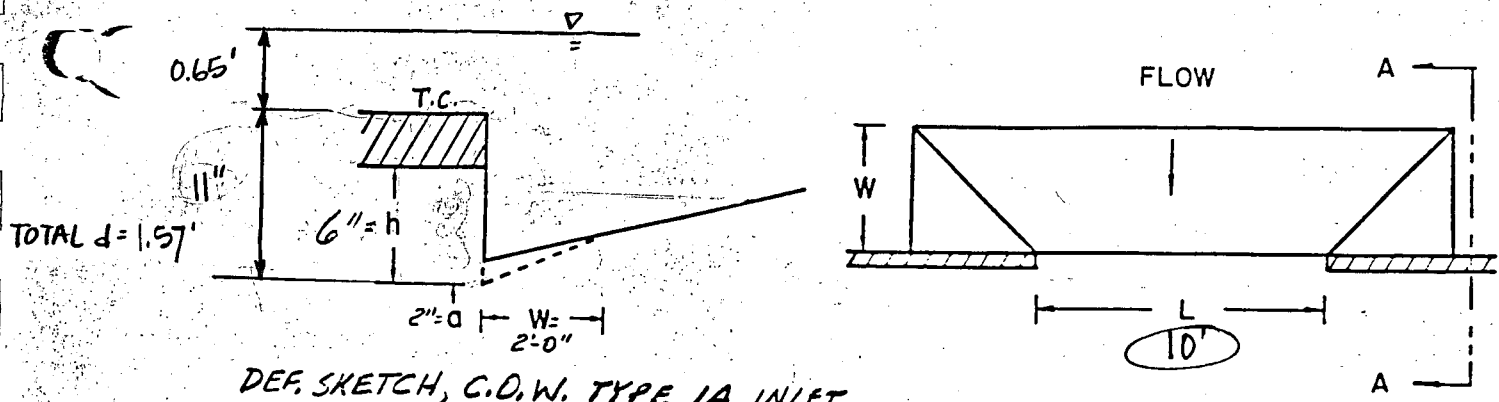
NOTE TO DESIGNER :

OPTION 1 46.1' inlet on SE side street w/ 54" outlet

OPTION 2 23'± inlet on each side street w/ 54" outlet pipe

* Approx 42" connecting Pipe

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DEF. SKETCH, C.D.W. TYPE 1A INLET

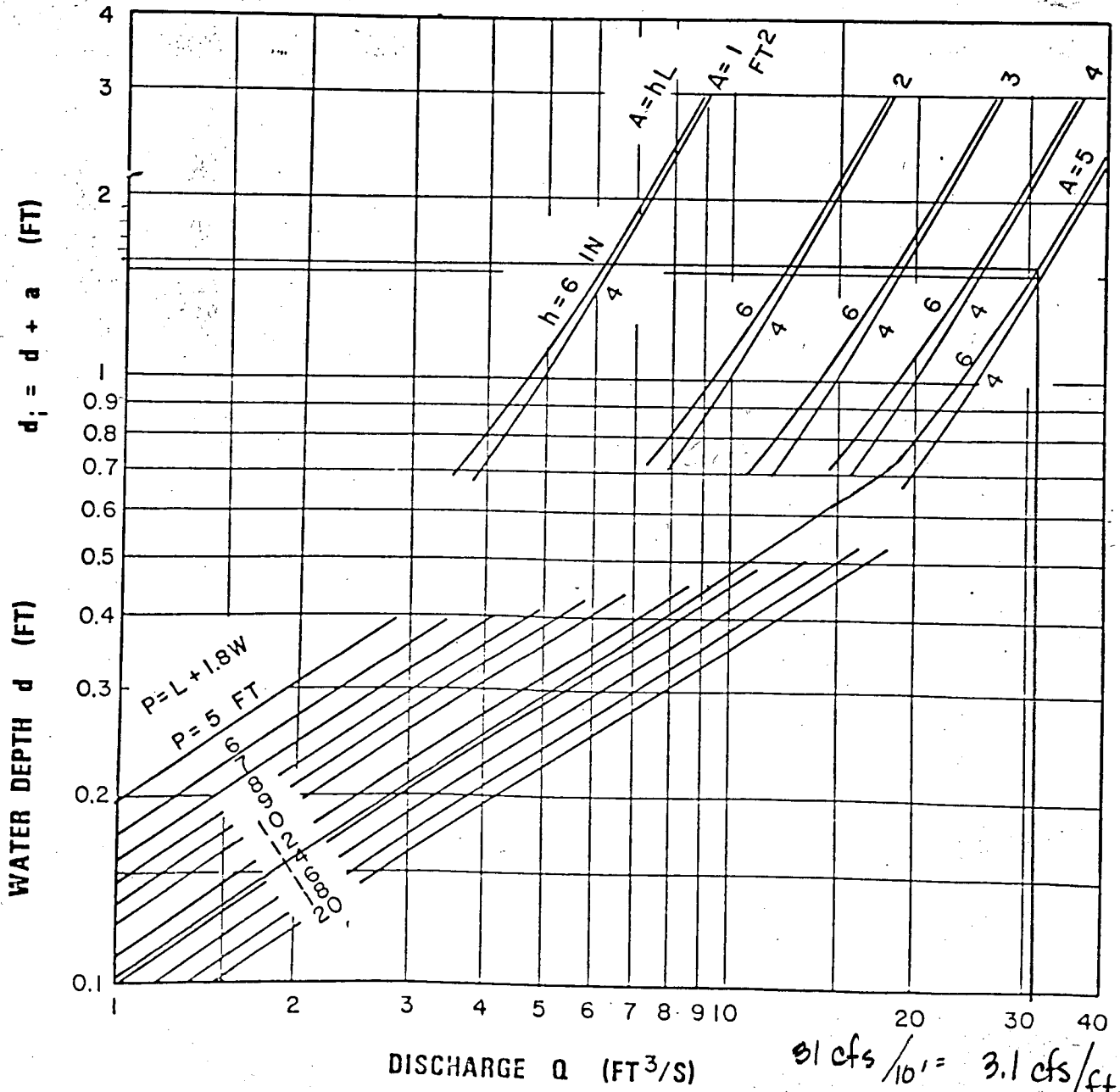


CHART 12. Depressed curb-opening inlet capacity in sump locations.

FROM: HEC-12, DRAINAGE OF HIGHWAY PAVEMENTS, FHWA, MAR, 1974

100 j, 150.0400 100 3 18 17

110 t, stonegate estates

120 t, revised drainage calcs

130 t, storm water sewer system 100 analysis

| | | | | | | | |
|----------------|--------|------|-------|--------|------|-------|--------|
| 140 i, 116 | 0.44 | 3.58 | 0.00 | 0.00 | 6.00 | 15.00 | 156.84 |
| 150 i, 115 | 0.44 | 5.28 | 0.00 | 0.00 | 8.90 | 15.00 | 156.84 |
| 160 i, 114 | 0.44 | 4.34 | 0.00 | 0.00 | 7.30 | 15.00 | 155.37 |
| 170 i, 113 | 0.44 | 1.84 | 0.00 | 0.00 | 3.10 | 15.00 | 155.37 |
| 180 i, 117 | 0.44 | 1.00 | 0.00 | 0.00 | 1.70 | 15.00 | 155.37 |
| 190 i, 112 | 0.44 | 0.23 | 0.00 | 0.00 | 0.30 | 15.00 | 155.37 |
| 200 i, 111 | 0.44 | 1.98 | 0.00 | 0.00 | 3.30 | 15.00 | 154.93 |
| 210 i, 110 | 0.44 | 0.76 | 0.00 | 0.00 | 1.30 | 15.00 | 155.08 |
| 220 i, 109 | 0.44 | 0.85 | 0.00 | 0.00 | 1.50 | 15.00 | 154.90 |
| 230 i, 108 | 0.48 | 1.57 | 0.00 | 0.00 | 2.90 | 15.00 | 154.47 |
| 240 i, 107 | 0.50 | 0.83 | 0.00 | 0.00 | 1.60 | 15.00 | 154.38 |
| 250 i, 106 | 0.44 | 0.83 | 0.00 | 0.00 | 1.40 | 15.00 | 154.32 |
| 260 i, 105 | 0.47 | 4.26 | 0.00 | 0.00 | 7.70 | 15.00 | 153.91 |
| 270 i, 104 | 0.47 | 2.71 | 0.00 | 0.00 | 4.90 | 15.00 | 153.91 |
| 280 i, 103 | 0.50 | 0.45 | 0.00 | 0.00 | 0.60 | 15.00 | 154.40 |
| 290 i, 102 | 0.50 | 1.15 | 0.00 | 0.00 | 2.20 | 15.00 | 153.90 |
| 300 i, 101 | 0.50 | 0.69 | 0.00 | 0.00 | 1.60 | 15.00 | 153.90 |
| 310 m, 100 | 150.04 | | | | | | |
| 320 p, 116 115 | 41.80 | 15 | 0.013 | 120.00 | 0.00 | | |
| 330 p, 115 113 | 280.60 | 27 | 0.013 | 20.00 | 0.00 | | |
| 340 p, 114 113 | 41.80 | 18 | 0.013 | 90.00 | 0.00 | | |
| 350 p, 117 112 | 42.30 | 15 | 0.013 | 100.00 | 0.00 | | |
| 360 p, 113 112 | 104.00 | 30 | 0.013 | 20.00 | 0.00 | | |
| 370 p, 112 109 | 303.90 | 36 | 0.013 | 10.00 | 0.00 | | |
| 380 p, 110 111 | 76.00 | 15 | 0.013 | 100.00 | 0.00 | | |
| 390 p, 111 109 | 44.60 | 18 | 0.013 | 80.00 | 0.00 | | |
| 400 p, 109 106 | 358.00 | 36 | 0.013 | 0.00 | 0.00 | | |
| 410 p, 108 107 | 76.00 | 15 | 0.013 | 110.00 | 0.00 | | |
| 420 p, 107 106 | 48.70 | 15 | 0.013 | 110.00 | 0.00 | | |
| 430 p, 106 103 | 214.80 | 36 | 0.013 | 45.00 | 0.00 | | |
| 440 p, 103 101 | 136.60 | 36 | 0.013 | 60.00 | 0.00 | | |
| 450 p, 102 101 | 44.30 | 42 | 0.013 | 0.00 | 0.00 | | |
| 460 p, 105 104 | 41.80 | 18 | 0.013 | 90.00 | 0.00 | | |
| 470 p, 104 101 | 309.80 | 24 | 0.013 | 70.00 | 0.00 | | |
| 480 p, 101 100 | 171.00 | 54 | 0.013 | 0.00 | 0.00 | | |
| 490 e | | | | | | | |

Input File: rad0100

stonegate estates
 revised drainage calcs
 storm water sewer system 100 analysis

Storm Frequency = 2-Year

* * * H Y D R O L O G Y * * *

| ***** | | | | | | | | | | | | | ***** | | | | | | | |
|----------------|-----|------|-------|--------|-------|---------|-------|-------|---------|-------|-------|-------|---------------------|--------|--------|-------|--------------|--|--|--|
| Tributary Area | | | | | | | | | | | | | Hydrology Summation | | | | Conduit Data | | | |
| ***** | | | | | | | | | | | | | ***** | | | | ***** | | | |
| Node to | C | Area | Slope | Length | TC(θ) | I(θ) | Q(θ) | TC | I | Q | Sum Q | Size | Velocity | Length | TT | TT+TC | | | | |
| Node | | (Ac) | (%) | (Ft) | (Min) | (In/Hr) | (CFS) | (Min) | (In/Hr) | (CFS) | (CFS) | | (Ft/Sec) | (Ft) | (Min) | (Min) | | | | |
| ***** | | | | | | | | | | | | | ***** | | | | ***** | | | |
| 116 | 115 | 0.44 | 3.58 | 0.00 | 0.0 | 15.00 | 4.06 | 6.00 | 15.00 | 4.06 | 6.00 | 6.00 | 15" | 4.89 | 41.80 | 0.14 | 15.14 | | | |
| 115 | 113 | 0.44 | 5.28 | 0.00 | 0.0 | 15.00 | 4.06 | 8.90 | 15.14 | 4.04 | 8.87 | 14.87 | 27" | 3.74 | 280.60 | 1.25 | 16.39 | | | |
| 114 | 113 | 0.44 | 4.34 | 0.00 | 0.0 | 15.00 | 4.06 | 7.30 | 15.00 | 4.06 | 7.30 | 7.30 | 18" | 4.13 | 41.80 | 0.17 | 15.17 | | | |
| 117 | 112 | 0.44 | 1.00 | 0.00 | 0.0 | 15.00 | 4.06 | 1.70 | 15.00 | 4.06 | 1.70 | 1.70 | 15" | 1.39 | 42.30 | 0.51 | 15.51 | | | |
| 113 | 112 | 0.44 | 1.84 | 0.00 | 0.0 | 15.00 | 4.06 | 3.10 | 16.39 | 3.92 | 2.99 | 24.94 | 30" | 5.08 | 104.00 | 0.34 | 16.73 | | | |
| 112 | 109 | 0.44 | 0.23 | 0.00 | 0.0 | 15.00 | 4.06 | 0.30 | 16.73 | 3.89 | 0.29 | 26.88 | 36" | 3.80 | 303.90 | 1.33 | 18.07 | | | |
| 110 | 111 | 0.44 | 0.76 | 0.00 | 0.0 | 15.00 | 4.06 | 1.30 | 15.00 | 4.06 | 1.30 | 1.30 | 15" | 1.06 | 76.00 | 1.20 | 16.20 | | | |
| 111 | 109 | 0.44 | 1.98 | 0.00 | 0.0 | 15.00 | 4.06 | 3.30 | 15.00 | 4.06 | 3.30 | 4.50 | 18" | 2.55 | 44.60 | 0.29 | 15.29 | | | |
| 109 | 106 | 0.44 | 0.85 | 0.00 | 0.0 | 15.00 | 4.06 | 1.50 | 18.07 | 3.77 | 1.40 | 32.50 | 36" | 4.60 | 358.00 | 1.30 | 19.36 | | | |
| 108 | 107 | 0.48 | 1.57 | 0.00 | 0.0 | 15.00 | 4.06 | 2.90 | 15.00 | 4.06 | 2.90 | 2.90 | 15" | 2.36 | 76.00 | 0.54 | 15.54 | | | |
| 107 | 106 | 0.50 | 0.83 | 0.00 | 0.0 | 15.00 | 4.06 | 1.60 | 15.54 | 4.00 | 1.58 | 4.48 | 15" | 3.65 | 48.70 | 0.22 | 15.76 | | | |
| 106 | 103 | 0.44 | 0.83 | 0.00 | 0.0 | 15.00 | 4.06 | 1.40 | 19.36 | 3.67 | 1.27 | 37.90 | 36" | 5.36 | 214.80 | 0.67 | 20.03 | | | |
| 103 | 101 | 0.50 | 0.45 | 0.00 | 0.0 | 15.00 | 4.06 | 0.60 | 20.03 | 3.63 | 0.54 | 38.43 | 36" | 5.44 | 136.60 | 0.42 | 20.45 | | | |
| 102 | 101 | 0.50 | 1.15 | 0.00 | 0.0 | 15.00 | 4.06 | 2.20 | 15.00 | 4.06 | 2.20 | 2.20 | 42" | 0.29 | 44.30 | 3.23 | 18.23 | | | |
| 105 | 104 | 0.47 | 4.26 | 0.00 | 0.0 | 15.00 | 4.06 | 7.70 | 15.00 | 4.06 | 7.70 | 7.70 | 18" | 4.36 | 41.80 | 0.16 | 15.16 | | | |
| 104 | 101 | 0.47 | 2.71 | 0.00 | 0.0 | 15.00 | 4.06 | 4.90 | 15.16 | 4.04 | 4.88 | 12.58 | 24" | 4.00 | 309.80 | 1.29 | 16.45 | | | |
| 101 | 100 | 0.50 | 0.69 | 0.00 | 0.0 | 15.00 | 4.06 | 1.60 | 20.45 | 3.60 | 1.42 | 53.51 | 54" | 3.36 | 171.00 | 0.85 | 21.30 | | | |

Input File: radoi00

stonegate estates
revised drainage calcs
storm water sewer system 100 analysis

Storm Frequency = 2-Year

* * * HYDRAULICS * * *

| Node | Hyd-Slope (Ft/Ft) | Friction (Ft) | Bend (Ft) | Transition (Ft) | Manhole (Ft) | Deflection (Ft) | Junction (Ft) | Total (Ft) | Hyd-GI Elevation | Desired Elevation | Diff. (Ft) |
|------|----------------------|------------------|--------------|--------------------|-----------------|--------------------|------------------|---------------|---------------------|----------------------|---------------|
| 116 | 0.00863 | 0.3606 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.3606 | 153.9254 | 156.8400 | 0.91 |
| 115 | 0.00230 | 0.6466 | 0.0000 | 0.0308 | 0.0000 | 0.2621 | 0.3414 | 1.2809 | 155.5648 | 156.8400 | 1.28 |
| 114 | 0.00483 | 0.2019 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.2019 | 154.4858 | 155.3700 | 0.88 |
| 113 | 0.00370 | 0.3846 | 0.0000 | 0.0184 | 0.0000 | 0.0179 | 0.5134 | 0.9343 | 154.2839 | 155.3700 | 1.09 |
| 117 | 0.00069 | 0.0293 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0293 | 153.3789 | 155.3700 | 1.99 |
| 112 | 0.00162 | 0.4936 | 0.0000 | 0.0353 | 0.0000 | 0.0330 | -0.1119 | 0.4500 | 153.3496 | 155.3700 | 2.02 |
| 111 | 0.00184 | 0.0820 | 0.0000 | 0.0083 | 0.0000 | 0.0099 | 0.2156 | 0.3158 | 153.2155 | 154.9300 | 1.71 |
| 110 | 0.00040 | 0.0308 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0308 | 153.2462 | 155.0800 | 1.83 |
| 109 | 0.00237 | 0.8499 | 0.0000 | 0.0104 | 0.0000 | 0.0080 | 0.2009 | 1.0771 | 152.8997 | 154.9000 | 2.00 |
| 108 | 0.00202 | 0.1532 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.1532 | 152.5346 | 154.4700 | 1.94 |
| 107 | 0.00481 | 0.2340 | 0.0000 | 0.0120 | 0.0000 | 0.0552 | 0.2576 | 0.5589 | 152.3814 | 154.3800 | 2.00 |
| 106 | 0.00323 | 0.6934 | 0.0000 | 0.0118 | 0.0000 | 0.0000 | 0.2753 | 0.9806 | 151.8226 | 154.3200 | 2.50 |
| 105 | 0.00537 | 0.2246 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.2246 | 151.8217 | 153.9100 | 2.09 |
| 104 | 0.00309 | 0.9580 | 0.0000 | 0.0092 | 0.0000 | 0.1474 | 0.2344 | 1.3490 | 151.5971 | 153.9100 | 2.31 |
| 103 | 0.00332 | 0.4536 | 0.0000 | 0.0013 | 0.0000 | 0.0971 | 0.0419 | 0.5938 | 150.8420 | 154.4000 | 3.56 |
| 102 | 0.00000 | 0.0002 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0002 | 150.2484 | 153.9000 | 3.65 |
| 101 | 0.00074 | 0.1266 | 0.0000 | 0.0567 | 0.0000 | 0.1411 | -0.1162 | 0.2081 | 150.2481* | 153.9000 | 3.65 |
| 100 | 0.00000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 150.0400* | 150.0400 | 0.00 |

* Starting HGL set @ 150.04 so that resulting HGL @
Node 101 = soffit of pipe = 147.42
2.83 (34" pipe)
150.25