

DRAINAGE PLAN
AND
SUPPORTING CALCULATIONS

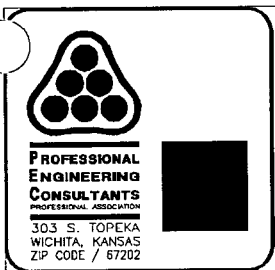
FOR

BRADLEY FAIR 2ND ADDITION
WICHITA, KANSAS

PREPARED BY
PROFESSIONAL ENGINEERING CONSULTANTS, P.A.
ENGINEERS
WICHITA, KANSAS

DECEMBER 18, 1995

MEMO



TO: M. E. Lindebak, P.E.

455 N. Main, 7th Floor

Wichita, KS 67202

PROJECT NO. 36-95785-3650

PROJECT: Bradley Fair 2nd Addition

COPIES TO:

ATTN: V. R. Huang, P.E.

DATE: 12/18/95

George Laham

FROM: M. W. Berry, P.E.

Ron Spangenberg

REFERENCE: Drainage Plan Computations

PLEASE ADVISE IMMEDIATELY OF ANY MISCONCEPTIONS OR OMISSIONS YOU BELIEVE TO BE CONTAINED HEREIN.

Attached hereto are the drainage computations for the referenced project

The publication Interim Drainage and Storm Sewer policy for Design Criteria and Documentation, City of Wichita, as revised 7/1/87 was used as the guideline for the hydrologic and hydraulic computations. This publication is hereinafter referred to as the Design Manual.

Manual #1, as referenced herein, refers to Design of Urban Highway Drainage - The State of the Art by Reitz & Jens, Inc., April 1980. Manual #2 refers to Drainage of Highway Pavements, Hydraulic Engineering Circular #12 by Tye Engineering, Inc., March 1984.

The analysis made herein is based on the available site data which includes the following:

Contour map at two foot interval and 1"=100' scale for the final plat area

Contour map at two foot interval and 1"=200' scale for the balance of the Wilson Farms tract.

City of Wichita Flood Insurance Study, May 1986

HYDROLOGIC ANALYSIS FOR STORM WATER SEWERS

For storm sewer design, the Rational Method was used for the hydrologic analysis in accordance with the Design Manual. Runoff coefficients were estimated based on tables presented in the Design Manual.

For this development, a uniform assumption of the minimum time of concentration of 15 minutes was deemed appropriate.

Travel time for flow through defined channels, pipes, etc., for these basins was estimated on the basis of Manning's Equation.

M. E. Lindebak, P.E.
Bradley Fair 2nd Addition
12/11/95
Page 2

HYDRAULIC ANALYSIS FOR STORM WATER SEWERS

For each inlet, street flooding and inlet capacity were checked for the minor storm. Conveyance in the street is based on the Modified Manning's Equation, as expressed in Manual #1, Equation (5-1), page 5-9. It has been assumed that T_c for street flow is equal for T_c for pipe flow. This is a simplifying, but conservative, assumption, since pipe flow velocities generally exceed street flow velocities.

For local streets, curb-deep flow is tolerable for the minor storm. For collector streets, a single eight-foot center lane should remain unflooded for the minor storm.

Inlet capacities were determined by the methods described in Manual #2, using Chart #12.

In this analysis, City of Wichita Type 1A inlets and 3/8 inch per foot street cross slopes have been assumed. Minimum walk grade has been assumed to be 0.3 feet above the top of curb, unless otherwise noted. Streets have been assumed to have 6-5/8 inch standard curb, unless otherwise noted.

Storm sewers are designed for the minor storm, with major storm overflows to be routed through easements and rights-of-way to an appropriate outlet.

The minor storm has a recurrence interval of five years. The major storm evaluated has a recurrence interval of one hundred years.

To simplify hydraulic analysis, the following assumptions have been made:

1. The time of concentration is identical for both the major and the minor storms.
2. The street conveyance is computed using only the pavement width. Depths above the curb up to the walk (right-of-way) elevation are used, but the conveyance of the landscaped area behind the curb was neglected. In general, this area has a very small conveyance due to the higher "n" factor.

Hydraulic computations for the pipe system were estimated using Manning's Equation to calculate friction losses for pipes flowing full. Minor losses estimated at a constant 0.5 feet per structure. All pipe area assumed to be reinforced concrete with a Manning's "n" of 0.013. It is desirable to keep the hydraulic grade line at least one foot below the top of curb for the minor storm.

HYDROLOGIC AND HYDRAULIC MODELS FOR DETENTION

Detention basins are analyzed using the US Army Corps of Engineers HEC-1 computer package. Runoff computations within that program were made using the NCRS (formerly SCS) unit hydrograph procedure utilizing the Curve Number method. Stage-discharge relationships for weirs are automatically computed by HEC-1. For culvert control structures, the FHWA HY-8 Culvert computer program is used to develop a stage-discharge curve. Reservoir routing is computed using the Modified Puls method within HEC-1.

Potential detention areas have been identified throughout the site. The effects of urbanization on the basin have been analyzed utilizing the SCS hydrologic method and the HEC-21 computer program. The results of this analysis are summarized in a table I the report.

FEMA REGULATED STREAMS

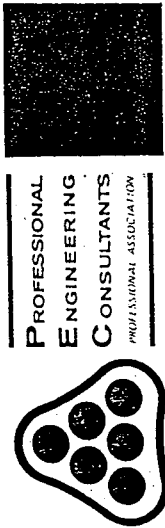
The Middle Fork of Gypsum Creek has been include in the detailed study of the City of Wichita Flood Insurance Study (FIS). Regulatory floodplain limits, regulatory floodway limits, base flood elevations, and design discharges have been identified in the FIS. For the purposes of this study, the design flows identified in the report are assumed to enter the site at 21st Street and discharge from the site at the Burlington Northern Railroad essentially unchanged. No attempt has been made to evaluate the effects of detention to be provided on this site.

DESIGN AIDS

Charts, nomographs, etc. used in these computation are reprinted in this section

DRAINAGE PLAN MAP

A map at 1"=200' scale is include in the map pocket(s) at the back of the report.



PROFESSIONAL
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1440 EAST ENGLISH
WICHITA, KANSAS 67211
(316) 262-2691

HYDROLOGY DATA SHEET

PAGE OF

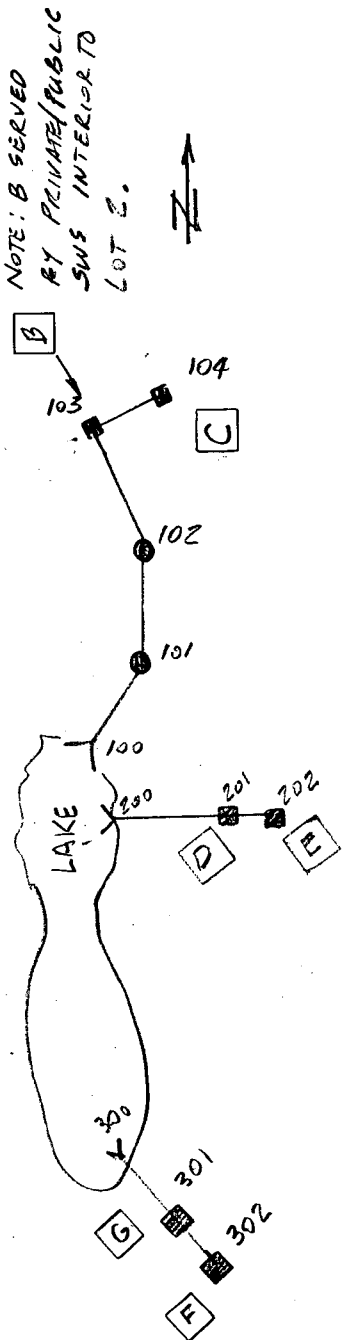
PROJECT: BRADLEY FAIR END ADD PROJECT NO. 36.95785.3653

ITEM: DATE: 12/17/95

RETURN PERIOD: 5-YR COMPUTATIONS BY: MJB REVISIONS BY:

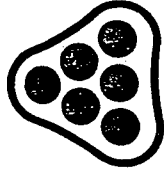
SCHEMATIC DIAGRAM:

NOTE: "G" WILL BE SERVED BY PRIVATE/PUBLIC SWS INSTALLED INTERIOR TO LOTS 1 & 2.



NOTE: B SERVED BY PRIVATE/PUBLIC SWS INTERIOR TO LOT 2.

TRIBUTARY AREA							HYDROLOGY SUMMATION					CONDUIT DATA					
SUB-BASIN (1)	C (2)	AREA (acres) (3)	SLOPE (%) (4)	LENGTH (feet) (5)	T _c (minutes) (6)	I ₀ in./hr. (7)	Q ₀ (cfs) (8)	T _c (minutes) (9)	I in./hr. (10)	Q (cfs) (11)	Σ Q (cfs) (12)	PIPE (inches) (13)	SLOPE (%) (14)	VELOCITY (ft./sec.) (15)	LENGTH (feet) (16)	T _f (minutes) (17)	T _c + T _f (minutes) (18)
C	0.09	6			15	4.56	18.9	15			18.9	30"	0.21	3.8	60	0.3	15.3
B	0.09	24			20	4.00	66.2	20	4.00	66.2	82.8	48"	0.33	6.6	525	1.3	21.3
E	0.09	2.5			15	4.56	7.9	15			7.9	24"	0.12	2.5	60	0.4	15.4
D	0.50	0.8			15	4.56	1.8	15.4	4.56	1.8	9.7	24"	0.18	3.1	75	0.4	15.8
								$\frac{15}{15.4} \times 7.9 + 1.8 = 9.5$ OR $\frac{45}{45.6} \times 7.8 + 7.9 = 9.7$									
F	0.09	10			15	4.56	31.5	15			31.5	36"	0.22	4.4	75	0.3	15.3
G	0.09	8			15	4.56	25.2	15.3	4.52	25.0	56.5	48"	0.15	4.5	75	0.3	15.6



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HYDROLOGY DATA SHEET

PAGE 1 OF 1

PROJECT: BRADLEY FAIR END ADDITION PROJECT NO. 36.95785.3650

ITEM: DATE: 12.17.95

RETURN PERIOD: 100 Yr COMPUTATIONS BY: MB REVISIONS BY: MB

SCHEMATIC DIAGRAM:

(SEE OTHER SHEET)

TRIBUTARY AREA							HYDROLOGY SUMMATION					CONDUIT DATA					
SUB-BASIN (1)	C (2)	AREA (acres) (3)	SLOPE (%) (4)	LENGTH (feet) (5)	T _c (minutes) (6)	I ₀ in./hr. (7)	Q ₀ (cfs) (8)	T _c (minutes) (9)	I in./hr. (10)	Q (cfs) (11)	Σ Q (cfs) (12)	PIPE (inches) (13)	SLOPE (%) (14)	VELOCITY (ft./sec.) (15)	LENGTH (feet) (16)	T _i (minutes) (17)	T _c + T _i (minutes) (18)
C	0.8	6			15	7.37	35.4	15			35.4	30"	0.75	7.2!	60		
B	0.8	24			20	6.53	125	20	6.53		156.7	48"	1.19	12.5!	525		
											156.7	54"	0.64	9.9!			
											156.7	60"	0.36	8.0!			
E	0.8	2.5			15	7.37	14.7				14.7	24"	0.42	4.7	60		
D	0.6	0.8			15	7.37	3.5				18.2	24"	0.65	5.8	75		
F	0.8	10			15	7.37	59	15	7.37		59	36"	0.78	8.3	75		
G	0.8	8			15	7.37	47.2	15	7.37		106	48"	0.54	8.4	75		

USE FOR Q₁₀₀



Date 12.17.95

Page of

Comp by MMS

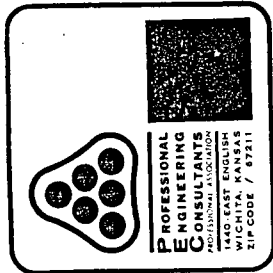
Project BRADLEY FAIR 2ND ADD 36.95785.3650

NOTE: ASSUME NO MORE THAN 1.25 AC PAUT DISCHARGES DIRECTLY ONTO STREET
 Item AT EACH ENTRANCE. BALANCE IS CARRIED TO PUBLIC SWS BY PRIVATE SWS.

INLET CAPACITY

z/n = 2000

NODE No.	HYDROLOGY		APPROACHING FLOW				INLET		ON-GRADE COMP				SUMP COMP.			
	Q ₀ cfs	Q ₀ +Q _b cfs	S ₀ o/o	S _x in/ft	d ft	T ft	TYPE	L	Lt ft	L/Lt	E ft	d _i ft	d ft	T ft	Q _i cfs	Q _b cfs
104	18.9	—	Assume 3/4 Q from NORTH				= 14.2									
NORTH	14.2		0.5	3/8	0.5	16	OK									
SOUTH	4.7		0.4	3/8	OK BY INSPECTION		1A	10'				0.6	0.43	13.8	18.9	-0-
103	66.2	Assume all except R/W (1.0 Ac)														
NORTH	10		0.5	3/8	0.46	14.7	1A	10'				0.47	0.30	9.6	10	-0-
SOUTH	Negligible															
202	7.9	—														
NORTH	4.0		0.43	3/8	0.33	10.6	1A	5'				0.4	0.23	7.4	7.9	-0-
SOUTH	3.9		0.46	3/8	0.32	10.2										
201	1.8	OK	OK BY INSPECTION (SEE 200)				1A	5'				0.17	—	—	1.8	
For 302 + 301, assume 3 drives @ 1.25 EA + R/W (1.5 Ac) = 5.25 AC																
302	16.5		0.88	3/8	0.48	15.4	1A	10'				0.62	0.45	14.4	16.5	-0-
301	16.5		0.88	3/8	0.48	15.4	1A	10'				0.62	0.45	14.4	16.5	-0-



Date 12.17.95 Page of Comp by MS

Project BRADLEY FAIR AND App 36-95785-3050 CK by

[illegible]

MAJOR STORM CHECK

[illegible]



Date _____ Page _____ of _____

Project WILSON ESTATES

Item BASIN HYDROLOGY

PRE-DEVELOPED
BASIN #

	<u>A</u>	<u>C₁₀₀</u>	<u>L₁₀₀</u>	<u>Q₁₀₀</u>
4	38.5 Ac	0.67	7.36	190 cfs
9	48.3 Ac	0.67	7.36	238 cfs

POST-DEVELOPED

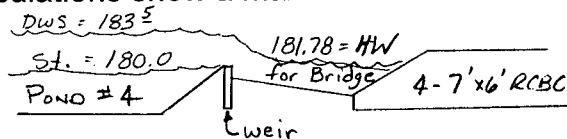
<u>BASIN #</u>	<u>A</u>	<u>C₁₀₀</u>	<u>L₁₀₀</u>	<u>Q₁₀₀</u>
4	38.5	0.76	7.36	215 cfs
9	48.3	0.76	7.36	270 cfs

NOTE:

BASINS # 1-3, 5, 6, and 8 are calculated within HEC-1
BASIN # 7 is previously calculated as shown later in this report.

Basins No. 1, 2, 3, and 9, contribute runoff to a series of proposed ponds to be built upstream of the proposed 4 - 7' X 6' RCBC at the road crossing the Middle Branch of Gypsum Creek.

All requirements for sizes and elevations of Ponds # 1 thru 3 are summarized on the drainage plan map. The outlet for Pond #1 is a 6' square drop inlet at elevation 198.0 with a 54" outlet pipe to Pond #2. Ponds #2 and #3 are each controlled by a 5' spillway and channel at elevations 195.0 and 186.0 respectively. Pond #3 drains to Pond #4, which is to be constructed by damming off the creek using a 75' concrete weir at elevation 180.0. The following weir calculations show a maximum rise of 3.5' to elevation 183.5.



$$Q = CLH^{3/2}$$

$$Q_{free} = 3.0(L)(3.5)^{3/2}$$

$$\frac{1243}{3.0 \times 3.5^{3/2}} = L_{free}$$

$$63.3' = L_{free}$$

$$\frac{D_{dn}}{D_{up}} = \frac{1.78}{3.5} = 0.5$$

$$L_{sub} = \frac{63.3}{0.84} = 75'$$

$$\frac{Q_{dn}}{Q_{up}} = 0.84 \text{ (Fig. 5-5)}$$

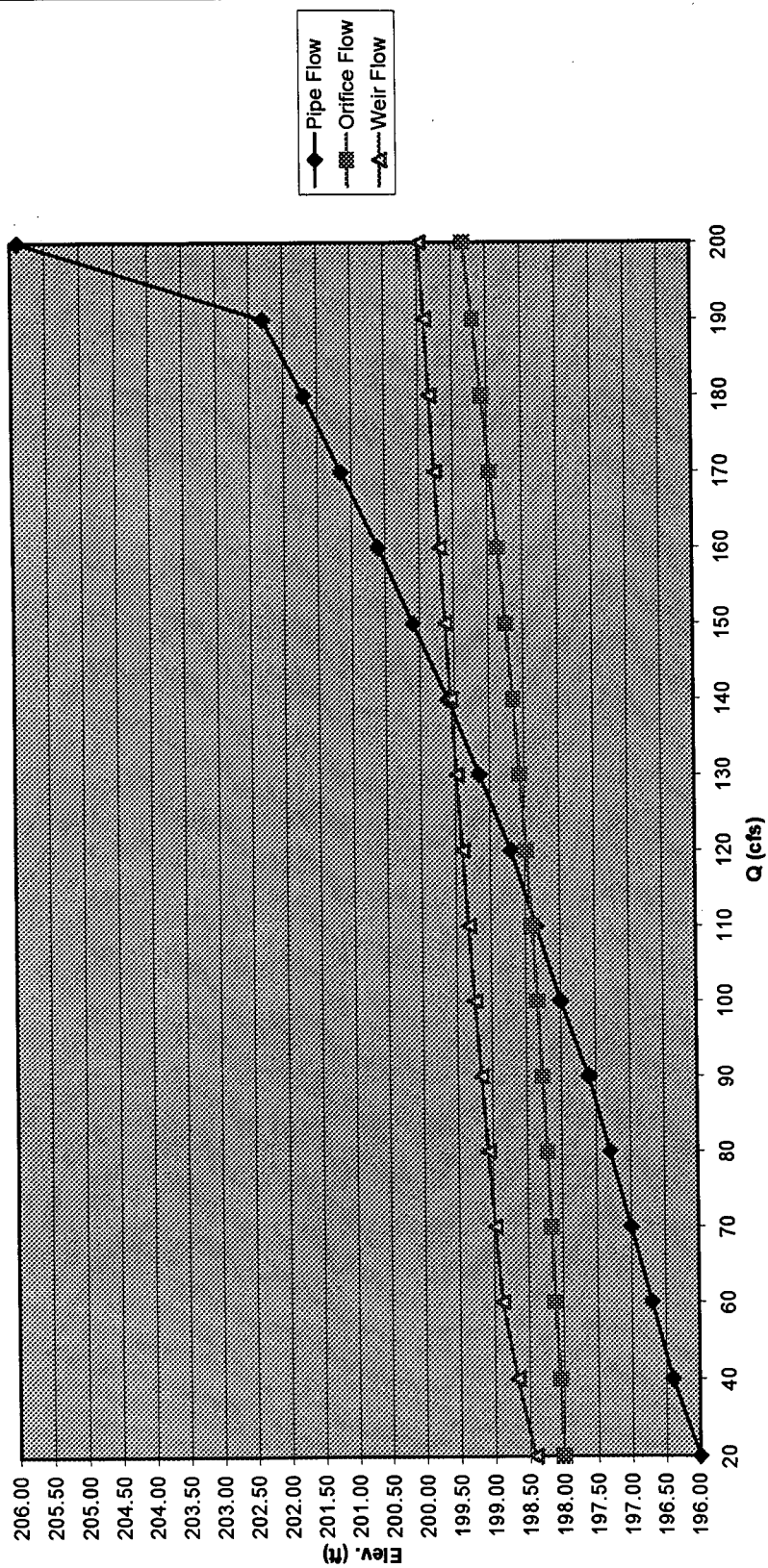
Because the pond is within the creek, Q_{100} for analysis of Pond #4, and the box culvert downstream of the weir is 1243 cfs, as defined by the Federal Emergency Management Agency (FEMA) Flood Insurance Study (F.I.S.), despite the reduction of peak on-site flows provided by the proposed detention storage.

The peak stage of Pond #4 of 183.5 is slightly higher than the published Base Flood Elevation (B.F.E.) for a short reach of the creek just upstream of the new RCBC, (up to Section Q. See FEMA B.F.E.'s within) but is lower than the B.F.E.'s for the next reach of the creek up to near the South side of 21st St. (near Sec. S)

The proposed box culvert at the road crossing was designed to handle the 100-year flow of the creek, being 1243 cfs. The culvert run shows a maximum headwater elevation of 181.78, assuming a 25' bottom width channel with 4:1 side slopes on 0.3% grade to the South as tailwater control. This will likely require some channel cleaning and/or widening south of the box.

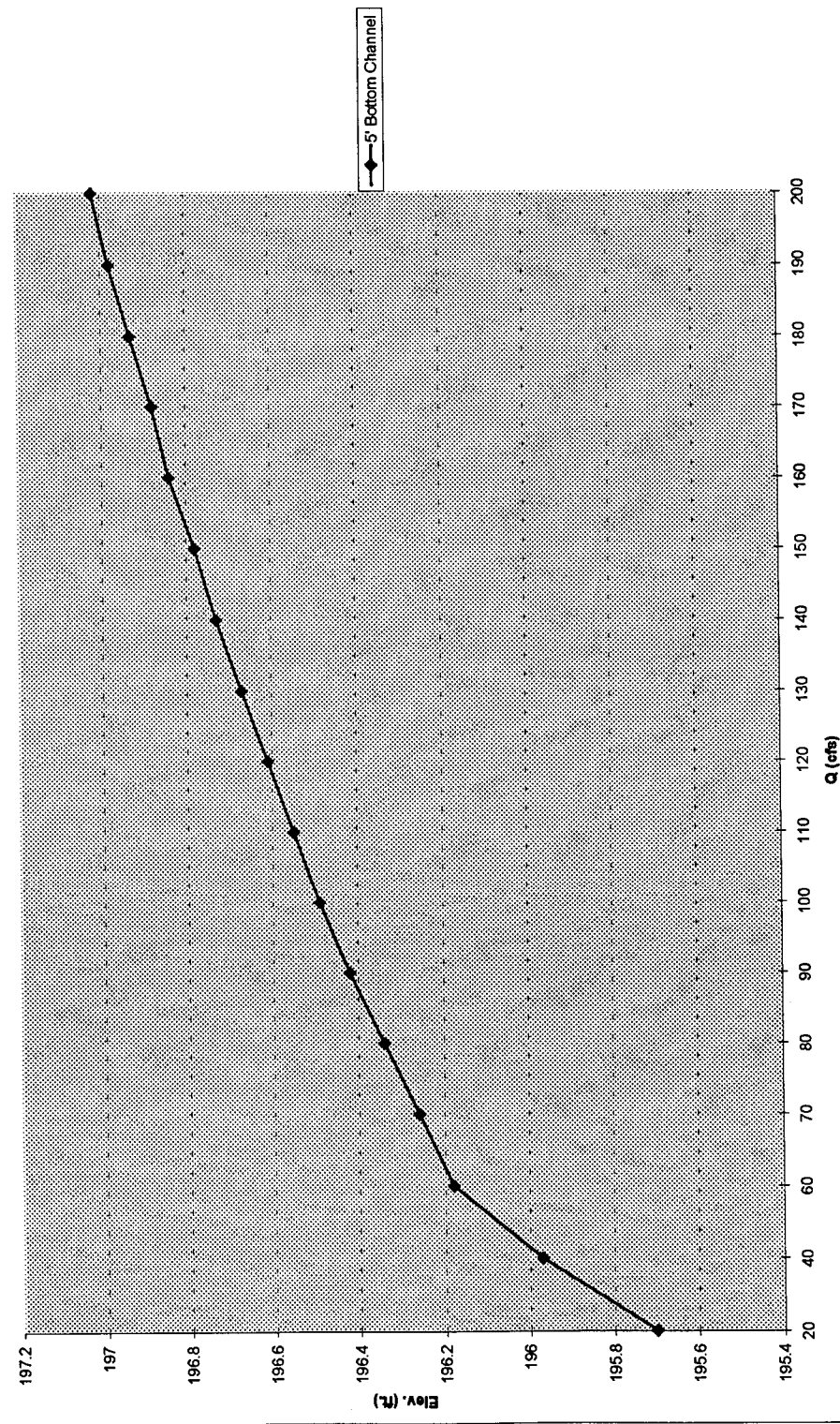
STAGE-DISCHARGE

POND #1



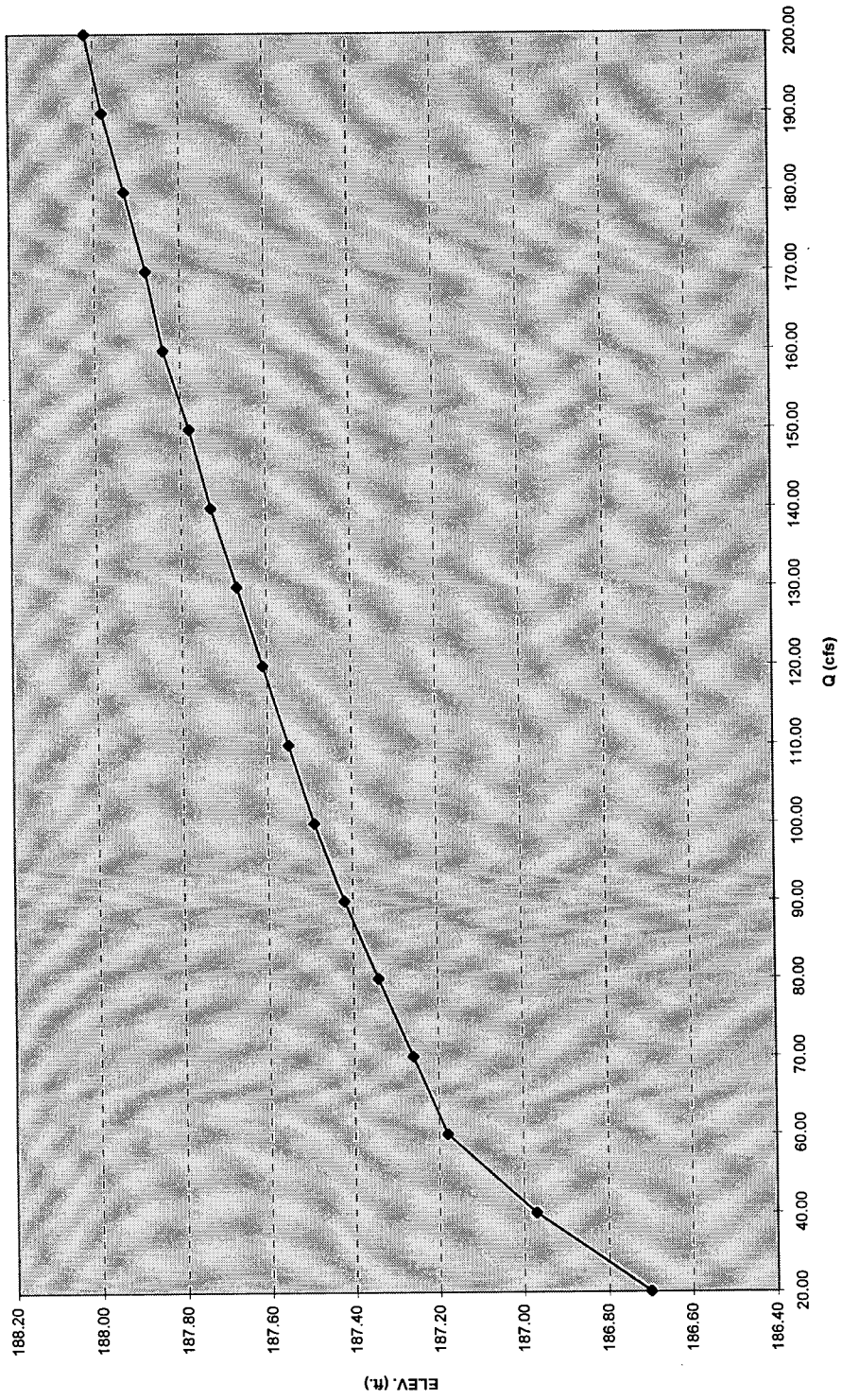
STAGE-DISCHARGE

POND #2



STAGE - DISCHARGE

POND #3



1

CURRENT DATE: 11-20-1995
CURRENT TIME: 16:44:23

FILE DATE: 11-17-1995
FILE NAME: BRADLEY

FWHA CULVERT ANALYSIS
HY-8, VERSION 3.2

SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
INLET	OUTLET	CULVERT	BARRELS	SPAN	RISE	MANNING	INLET
ELEV. (FT)	ELEV. (FT)	LENGTH (FT)	SHAPE MATERIAL	(FT)	(FT)	n	TYPE
191.00	189.00	250.01	1 RCP	4.50	4.50	.012	CONVENTIONAL

SUMMARY OF CULVERT FLOWS (CFS) FILE: BRADLEY DATE: 11-17-1995

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
197.97	100	100	0	0	0	0	0	0	1
198.33	110	110	0	0	0	0	0	0	1
198.72	120	120	0	0	0	0	0	0	1
199.14	130	130	0	0	0	0	0	0	1
199.61	140	140	0	0	0	0	0	0	1
200.08	150	150	0	0	0	0	0	0	1
200.59	160	160	0	0	0	0	0	0	1
201.13	170	170	0	0	0	0	0	0	1
201.70	180	180	0	0	0	0	0	0	1
202.29	190	190	0	0	0	0	0	0	1
205.90	200	200	0	0	0	0	0	0	1
210.00	261	261	0	0	0	0	0	0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: BRADLEY DATE: 11-17-1995

HEAD ELEV(FT)	HEAD ERROR(FT)	TOTAL FLOW(CFS)	FLOW ERROR(CFS)	% FLOW ERROR
197.97	0.00	100	0	0.00
198.33	0.00	110	0	0.00
198.72	0.00	120	0	0.00
199.14	0.00	130	0	0.00
199.61	0.00	140	0	0.00
200.08	0.00	150	0	0.00
200.59	0.00	160	0	0.00
201.13	0.00	170	0	0.00
201.70	0.00	180	0	0.00
202.29	0.00	190	0	0.00
205.90	0.00	200	0	0.00

<1> TOLERANCE (FT) = 0.010

<2> TOLERANCE (%) = 1.000

11-27-1995

```
*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* Lahey F77L-EM/32 version 5.01 *
* Dodson & Associates, Inc. *
* RUN DATE 11/27/95 TIME 10:38:23 *
*****
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```
*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *
*****
```

```

X  X  XXXXXX  XXXX  X
X  X  X      X  X  XX
X  X  X      X  X  X
XXXXXX XXXX  X  XXXX X
X  X  X      X  X  X
X  X  X      X  X  X
X  X  XXXXXX  XXXX  XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
 THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1         ID      Bradley Fair Drainage Plan
2         ID      5-, 10-, 25-, & 100-Year Storms
3         ID      Professional Engineering Consultants
4         ID      Wichita, Ks
5         ID      DRC 11/20/95
6         ID      File: T:\DAR\HEC1\BRADLEY.ih1
7         IT      6 01FEB95 0600 0 02FEB95 1154
8         IN      30 01FEB95 0600
9         IO      3 0
10        JR      PREC 0.5902 0.6875 0.8125 1.000
          *DIAGRAM
          *

11        KK      UNDEV      UNDEVELOPED CONDITIONS
12        BA      .08906
13        PB      7.8
14        PC      0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
15        PC      .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
16        PC      .880 .890 .900 .910 .916 .925 .934 .943 .952 .958
17        PC      .964 .970 .976 .982 .988 .994 1.000
18        LS      0 76 0
19        UD      0.20
          *
          *

20        KK      BASIN1      COMMERCIAL DEVELOPED CONDITIONS
21        BA      .08906
22        PB      7.8
23        PC      0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
24        PC      .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
25        PC      .880 .890 .900 .910 .916 .925 .934 .943 .952 .958
26        PC      .964 .970 .976 .982 .988 .994 1.000
27        LS      0 92 0
28        UD      0.15
          *
          *
          * 54" OUTLET PIPE FOR POND #1

29        KK      POND1
30        RS      1 ELEV 198
31        SA      2.75 3.5
32        SE      198 201
33        SQ      0 40 60 80 90 100 110 120 130 140
34        SQ      150 160 170 180 190 200
35        SE      198.0 198.65 198.9 199.05 199.15 199.25 199.3 199.4 199.5 199.6
36        SE      200.1 200.6 201.15 201.7 202.35 205.9
          *
          *

37        KK      BASIN2      COMMERCIAL DEVELOPED CONDITIONS
38        BA      0.004
39        PB      7.8
40        PC      0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
41        PC      .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
42        PC      .880 .890 .900 .910 .916 .925 .934 .943 .952 .958

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HEC-1 INPUT

PAGE 2

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
43	PC .964 .970 .976 .982 .988 .994 1.000
44	LS 0 92 0
45	UD 0.15
	*
	*
46	KK INTO2 COMBINE HYDROGRAPHS FOR BASIN 2 AND OUT OF POND #1
47	HC 2
	*
	*
	* 5' SPILLWAY FOR POND #2
48	KK POND2
49	RS 1 ELEV 195
50	SA 0.5 0.8
51	SE 195 197
52	SQ 0 40 60 80 90 100 110 120 130 140
53	SQ 150 160 170 180 190 200
54	SE 195 195.95 196.18 196.35 196.42 196.5 196.56 196.61 196.67 196.72
55	SE 196.78 196.84 196.89 196.93 196.98 197.02
	*
	*
56	KK BASIN3 COMMERCIAL DEVELOPED CONDITIONS
57	BA .00456
58	PB 7.8
59	PC 0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
60	PC .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
61	PC .880 .890 .900 .910 .916 .925 .934 .943 .952 .958
62	PC .964 .970 .976 .982 .988 .994 1.000
63	LS 0 92 0
64	UD 0.15
	*
	*
65	KK INTO3 COMBINE HYDROGRAPHS FOR BASIN 3 AND OUT OF POND #2
66	HC 2
	*
	*
	* 5' SPILLWAY FOR POND #3
67	KK POND3
68	RS 1 ELEV 186
69	SA 0.5 0.8
70	SE 186 189
71	SQ 0 40 60 80 90 100 110 120 130 140
72	SQ 150 160 170 180 190 200
73	SE 186 186.95 187.18 187.35 187.42 187.5 187.56 187.61 187.67 187.72
74	SE 187.78 187.84 187.89 187.93 187.98 188.02
	*
75	ZZ

11-27-1995

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
11	UNDEV	
	.	
20	.	BASIN1
	.	V
	.	V
29	.	POND1
	.	.
37	.	.
	.	BASIN2
	.	.
46	.	INTO2.....
	.	V
	.	V
48	.	POND2
	.	.
56	.	.
	.	BASIN3
	.	.
65	.	INTO3.....
	.	V
	.	V
67	.	POND3

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```
*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* Lahey F77L-EM/32 version 5.01 *
* Dodson & Associates, Inc. *
* RUN DATE 11/27/95 TIME 10:38:23 *
*****
```

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *
*****
```

Bradley Fair Drainage Plan
5-, 10-, 25-, & 100-Year Storms
Professional Engineering Consultants
Wichita, Ks
DRC 11/20/95
File: T:\DAR\HEC1\BRADLEY.ih1

```
9 IO      OUTPUT CONTROL VARIABLES
          IPRNT      3 PRINT CONTROL
          IPLOT      0 PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA
          NMIN      6 MINUTES IN COMPUTATION INTERVAL
          IDATE     1FEB95 STARTING DATE
          ITIME     0600 STARTING TIME
          NQ        300 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE    2FEB95 ENDING DATE
          NDTIME    1154 ENDING TIME
          ICENT     19 CENTURY MARK

          COMPUTATION INTERVAL 0.10 HOURS
          TOTAL TIME BASE 29.90 HOURS

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME     ACRE-FEET
SURFACE AREA       ACRES
TEMPERATURE        DEGREES FAHRENHEIT

JP        MULTI-PLAN OPTION
          NPLAN      1 NUMBER OF PLANS

JR        MULTI-RATIO OPTION
          RATIOS OF PRECIPITATION
          0.59      0.69      0.81      1.00
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*** **

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*****
* UNDEV *
* UNDEVELOPED CONDITIONS *
*****

8 IN      TIME DATA FOR INPUT TIME SERIES
          JXMIN      30 TIME INTERVAL IN MINUTES
          JXDATE     1FEB95 STARTING DATE
          JXTIME     600 STARTING TIME

SUBBASIN RUNOFF DATA

12 BA     SUBBASIN CHARACTERISTICS
          TAREA      0.09 SUBBASIN AREA

PRECIPITATION DATA

13 PB     STORM      7.80 BASIN TOTAL PRECIPITATION

14 PI     INCREMENTAL PRECIPITATION PATTERN
```

11-27-1995

[illegible]

18 LS	SCS LOSS RATE		
	STRTL	0.63	INITIAL ABSTRACTION
	CRVNR	76.00	CURVE NUMBER
	RTIMP	0.00	PERCENT IMPERVIOUS AREA

19 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 0.20 LAG

UNIT HYDROGRAPH
12 END-OF-PERIOD ORDINATES

54.	161.	161.	97.	12	END OF PERIOD CLOSURES	7.	4.	2.
1.	0.			49.	25.	13.		

TOTAL RAINFALL = 7.80, TOTAL LOSS = 2.82, TOTAL EXCESS = 4.98

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)				
+ 242.	6.10	39.	12.	10.	10.
	(INCHES)	4.093	4.976	4.976	4.976
	(AC-FT)	19.	24.	24.	24.

CUMULATIVE AREA = 0.09 SQ MI

☆☆☆ ☆☆☆ ☆☆☆ ☆☆☆ ☆☆☆

HYDROGRAPH AT STATION UNDEV
FOR PLAN 1, RATIO = 0.59

TOTAL RAINFALL = 4.60, TOTAL LOSS = 2.39, TOTAL EXCESS = 2.21

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)				
+ 106.	6.10				
	(CFS)				
	(INCHES)	17.	5.	4.	4.
	(AC-FT)	1.815	2.213	2.213	2.213
		9.	11.	11.	11.

CUMULATIVE AREA = 0.09 SQ MI

HYDROGRAPH AT STATION UNDEV
FOR PLAN 1, RATIO = 0.69

TOTAL RAINFALL = 5.36, TOTAL LOSS = 2.53, TOTAL EXCESS = 2.84

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)				
+ 138.	6.10	22.	7.	5.	5.
	(INCHES)	2.331	2.837	2.837	2.837
	(AC-FT)	11.	13.	13.	13.

BRADLEY FAIR PONDS #1, #2, AND #3

11-27-1995

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

27 LS SCS LOSS RATE
 STRIL 0.17 INITIAL ABSTRACTION
 CRVNER 92.00 CURVE NUMBER
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

28 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 0.15 LAG

UNIT HYDROGRAPH
 10 END-OF-PERIOD ORDINATES

102.	217.	147.	61.	28.	12.	5.	2.	1.	0.
------	------	------	-----	-----	-----	----	----	----	----

TOTAL RAINFALL = 7.80, TOTAL LOSS = 0.95, TOTAL EXCESS = 6.85

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+	(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	343.	6.00	(CFS)			
			53.	16.	13.	13.
		(INCHES)	5.534	6.846	6.846	6.846
		(AC-FT)	26.	33.	33.	33.

CUMULATIVE AREA = 0.09 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN1
 FOR PLAN 1, RATIO = 0.59

TOTAL RAINFALL = 4.60, TOTAL LOSS = 0.90, TOTAL EXCESS = 3.70

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+	(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	191.	6.00	(CFS)			
			29.	9.	7.	7.
		(INCHES)	3.026	3.703	3.703	3.703
		(AC-FT)	14.	18.	18.	18.

CUMULATIVE AREA = 0.09 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN1
 FOR PLAN 1, RATIO = 0.69

TOTAL RAINFALL = 5.36, TOTAL LOSS = 0.92, TOTAL EXCESS = 4.44

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+	(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	227.	6.00	(CFS)			
			35.	11.	9.	9.
		(INCHES)	3.622	4.444	4.444	4.444
		(AC-FT)	17.	21.	21.	21.

CUMULATIVE AREA = 0.09 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN1
 FOR PLAN 1, RATIO = 0.81

TOTAL RAINFALL = 6.34, TOTAL LOSS = 0.94, TOTAL EXCESS = 5.40

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+	(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	274.	6.00	(CFS)			
			42.	13.	10.	10.
		(INCHES)	4.388	5.402	5.402	5.402

(AC-FT) 21. 26. 26. 26.

CUMULATIVE AREA = 0.09 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN1
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 0.95, TOTAL EXCESS = 6.85

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+	(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	343.	6.00	(CFS)			
			53.	16.	13.	13.
		(INCHES)	5.534	6.846	6.846	6.846
		(AC-FT)	26.	33.	33.	33.

CUMULATIVE AREA = 0.09 SQ MI

*** **

*
29 KK * POND1 *
*

HYDROGRAPH ROUTING DATA

30 RS STORAGE ROUTING
NSTPS 1 NUMBER OF SUBREACHES
ITYP ELEV TYPE OF INITIAL CONDITION
RSVRIC 198.00 INITIAL CONDITION
X 0.00 WORKING R AND D COEFFICIENT

31 SA	AREA	2.8	3.5								
32 SE	ELEVATION	198.00	201.00								
33 SQ	DISCHARGE	0.	40.	60.	80.	90.	100.	110.	120.	130.	140.
		150.	160.	170.	180.	190.	200.				
35 SE	ELEVATION	198.00	198.65	198.90	199.05	199.15	199.25	199.30	199.40	199.50	199.60
		200.10	200.60	201.15	201.70	202.35	205.90				

COMPUTED STORAGE-ELEVATION DATA

STORAGE	0.00	9.35
ELEVATION	198.00	201.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	0.00	1.84	2.57	3.02	3.32	3.62	3.78	4.08	4.39	4.71
OUTFLOW	0.00	40.00	60.00	80.00	90.00	100.00	110.00	120.00	130.00	140.00
ELEVATION	198.00	198.65	198.90	199.05	199.15	199.25	199.30	199.40	199.50	199.60
STORAGE	6.31	7.97	9.35	9.88	11.87	14.32	29.88			
OUTFLOW	150.00	160.00	167.27	170.00	180.00	190.00	200.00			
ELEVATION	200.10	200.60	201.00	201.15	201.70	202.35	205.90			

*** *** *** *** ***

HYDROGRAPH AT STATION POND1
FOR PLAN 1, RATIO = 0.59

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+	(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	128.	6.20	(CFS)			
			29.	9.	7.	7.
		(INCHES)	3.006	3.703	3.703	3.703

BRADLEY FAIR PONDS #1, #2, AND #3

11-27-1995

		(AC-FT)	14.	18.	18.	18.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)					
4.	6.20		1.	0.	0.	0.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)					
199.48	6.20		198.41	198.13	198.10	198.10
CUMULATIVE AREA =			0.09 SQ MI			

*** *** *** *** ***

HYDROGRAPH AT STATION POND1
FOR PLAN 1, RATIO = 0.69

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)					
143.	6.20	(CFS)				
		(INCHES)	34.	11.	9.	9.
		(AC-FT)	3.599	4.444	4.444	4.444
			17.	21.	21.	21.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)					
5.	6.20		1.	0.	0.	0.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)					
199.75	6.20		198.48	198.15	198.12	198.12
CUMULATIVE AREA =			0.09 SQ MI			

*** *** *** *** ***

HYDROGRAPH AT STATION POND1
FOR PLAN 1, RATIO = 0.81

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)					
151.	6.20	(CFS)				
		(INCHES)	42.	13.	10.	10.
		(AC-FT)	4.361	5.402	5.402	5.402
			21.	26.	26.	26.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)					
7.	6.20		2.	1.	0.	0.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)					
200.17	6.20		198.59	198.19	198.15	198.15
CUMULATIVE AREA =			0.09 SQ MI			

*** *** *** *** ***

HYDROGRAPH AT STATION POND1
FOR PLAN 1, RATIO = 1.00

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)					
165.	6.20	(CFS)				
		(INCHES)	53.	16.	13.	13.
		(AC-FT)	5.503	6.846	6.846	6.846
			26.	33.	33.	33.

BRADLEY FAIR PONDS #1, #2, AND #3

11-27-1995

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)	6-HR	24-HR	72-HR	29.90-HR
9.	6.20	2.	1.	1.	1.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
(FEET)	(HR)	6-HR	24-HR	72-HR	29.90-HR
200.85	6.20	198.79	198.25	198.20	198.20

CUMULATIVE AREA = 0.09 SQ MI

*** **

 * *
 37 KK * BASIN2 * COMMERCIAL DEVELOPED CONDITIONS
 * *

8 IN TIME DATA FOR INPUT TIME SERIES
 JXMIN 30 TIME INTERVAL IN MINUTES
 JXDATE 1FEB95 STARTING DATE
 JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

38 BA SUBBASIN CHARACTERISTICS
 TAREA 0.00 SUBBASIN AREA

PRECIPITATION DATA

39 PB STORM 7.80 BASIN TOTAL PRECIPITATION

40 PI INCREMENTAL PRECIPITATION PATTERN

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.08	0.08	0.08	0.08
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

44 LS SCS LOSS RATE
 STRTL 0.17 INITIAL ABSTRACTION
 CRVNER 92.00 CURVE NUMBER
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

45 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 0.15 LAG

UNIT HYDROGRAPH
10 END-OF-PERIOD ORDINATES

5.	10.	7.	3.	1.	1.	0.	0.	0.	0.
----	-----	----	----	----	----	----	----	----	----

TOTAL RAINFALL = 7.80, TOTAL LOSS = 0.95, TOTAL EXCESS = 6.85

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
15.	6.00	2.	1.	1.	1.
(INCHES)		5.534	6.846	6.846	6.846

(AC-FT) 1. 1. 1. 1.

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN2
FOR PLAN 1, RATIO = 0.59

TOTAL RAINFALL = 4.60, TOTAL LOSS = 0.90, TOTAL EXCESS = 3.70

PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW		
+	(CFS)	(HR)	24-HR	72-HR	29.90-HR
+	9.	6.00	(CFS)		
			1.	0.	0.
			(INCHES)	3.026	3.703
			(AC-FT)	1.	1.

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN2
FOR PLAN 1, RATIO = 0.69

TOTAL RAINFALL = 5.36, TOTAL LOSS = 0.92, TOTAL EXCESS = 4.44

PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW		
+	(CFS)	(HR)	24-HR	72-HR	29.90-HR
+	10.	6.00	(CFS)		
			2.	0.	0.
			(INCHES)	3.622	4.444
			(AC-FT)	1.	1.

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN2
FOR PLAN 1, RATIO = 0.81

TOTAL RAINFALL = 6.34, TOTAL LOSS = 0.94, TOTAL EXCESS = 5.40

PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW		
+	(CFS)	(HR)	24-HR	72-HR	29.90-HR
+	12.	6.00	(CFS)		
			2.	1.	0.
			(INCHES)	4.388	5.402
			(AC-FT)	1.	1.

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN2
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 0.95, TOTAL EXCESS = 6.85

PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW		
+	(CFS)	(HR)	24-HR	72-HR	29.90-HR
+	15.	6.00	(CFS)		
			2.	1.	1.
			(INCHES)	5.534	6.846
			(AC-FT)	1.	1.

CUMULATIVE AREA = 0.00 SQ MI

*** **

 * INT02 * COMBINE HYDROGRAPHS FOR BASIN 2 AND OUT OF POND #1
 *

47 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION INTO2
 FOR PLAN 1, RATIO = 0.59

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+	(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	133.	6.20	(CFS)			
			30.	9.	7.	7.
		(INCHES)	3.006	3.703	3.703	3.703
		(AC-FT)	15.	18.	18.	18.

CUMULATIVE AREA = 0.09 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION INTO2
 FOR PLAN 1, RATIO = 0.69

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+	(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	151.	6.10	(CFS)			
			36.	11.	9.	9.
		(INCHES)	3.599	4.444	4.444	4.444
		(AC-FT)	18.	22.	22.	22.

CUMULATIVE AREA = 0.09 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION INTO2
 FOR PLAN 1, RATIO = 0.81

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+	(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	160.	6.10	(CFS)			
			44.	14.	11.	11.
		(INCHES)	4.361	5.402	5.402	5.402
		(AC-FT)	22.	27.	27.	27.

CUMULATIVE AREA = 0.09 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION INTO2
 FOR PLAN 1, RATIO = 1.00

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+	(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	174.	6.10	(CFS)			
			55.	17.	14.	14.
		(INCHES)	5.503	6.846	6.846	6.846
		(AC-FT)	27.	34.	34.	34.

CUMULATIVE AREA = 0.09 SQ MI

*** **

 * *
 48 KK * POND2 *
 * *

HYDROGRAPH ROUTING DATA

49 RS STORAGE ROUTING
 NSTPS 1 NUMBER OF SUBREACHES
 ITYP ELEV TYPE OF INITIAL CONDITION
 RSVRIC 195.00 INITIAL CONDITION
 X 0.00 WORKING R AND D COEFFICIENT

50 SA AREA 0.5 0.8

51 SE ELEVATION 195.00 197.00

52 SQ DISCHARGE 0. 40. 60. 80. 90. 100. 110. 120. 130. 140.
 150. 160. 170. 180. 190. 200.

54 SE ELEVATION 195.00 195.95 196.18 196.35 196.42 196.50 196.56 196.61 196.67 196.72
 196.78 196.84 196.89 196.93 196.98 197.02

COMPUTED STORAGE-ELEVATION DATA

STORAGE 0.00 1.29
 ELEVATION 195.00 197.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE 0.00 0.54 0.69 0.80 0.85 0.91 0.95 0.99 1.03 1.07
 OUTFLOW 0.00 40.00 60.00 80.00 90.00 100.00 110.00 120.00 130.00 140.00
 ELEVATION 195.00 195.95 196.18 196.35 196.42 196.50 196.56 196.61 196.67 196.72

STORAGE 1.12 1.16 1.20 1.23 1.27 1.29 1.30
 OUTFLOW 150.00 160.00 170.00 180.00 190.00 195.00 200.00
 ELEVATION 196.78 196.84 196.89 196.93 196.98 197.00 197.02

*** WARNING *** MODIFIED PULS ROUTING MAY BE NUMERICALLY UNSTABLE FOR OUTFLOWS BETWEEN 110. TO 200.
 THE ROUTED HYDROGRAPH SHOULD BE EXAMINED FOR OSCILLATIONS OR OUTFLOWS GREATER THAN PEAK INFLOWS.
 THIS CAN BE CORRECTED BY DECREASING THE TIME INTERVAL OR INCREASING STORAGE (USE A LONGER REACH.)

*** *** *** *** ***

HYDROGRAPH AT STATION POND2
 FOR PLAN 1, RATIO = 0.59

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)				
	(CFS)				
+ 132.	6.20	30.	9.	7.	7.
	(INCHES)	3.005	3.703	3.703	3.703
	(AC-FT)	15.	18.	18.	18.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)				
1.	6.20	0.	0.	0.	0.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)				
196.68	6.20	195.57	195.18	195.15	195.15

CUMULATIVE AREA = 0.09 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION POND2
 FOR PLAN 1, RATIO = 0.69

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR

BRADLEY FAIR PONDS #1, #2, AND #3

11-27-1995

+	(CFS)	(HR)				
+	150.	6.20	(CFS)	36.	11.	9.
			(INCHES)	3.597	4.444	4.444
			(AC-FT)	18.	22.	22.
PEAK STORAGE	TIME			MAXIMUM AVERAGE STORAGE		
			6-HR	24-HR	72-HR	29.90-HR
+	(AC-FT)	(HR)				
	1.	6.20		0.	0.	0.
PEAK STAGE	TIME			MAXIMUM AVERAGE STAGE		
			6-HR	24-HR	72-HR	29.90-HR
+	(FEET)	(HR)				
	196.78	6.20		195.65	195.21	195.17
						195.17

CUMULATIVE AREA = 0.09 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION POND2
FOR PLAN 1, RATIO = 0.81

PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	159.	6.20	(CFS)	44.	14.	11.
			(INCHES)	4.359	5.402	5.402
			(AC-FT)	22.	27.	27.
PEAK STORAGE	TIME			MAXIMUM AVERAGE STORAGE		
			6-HR	24-HR	72-HR	29.90-HR
+	(AC-FT)	(HR)				
	1.	6.20		0.	0.	0.
PEAK STAGE	TIME			MAXIMUM AVERAGE STAGE		
			6-HR	24-HR	72-HR	29.90-HR
+	(FEET)	(HR)				
	196.83	6.20		195.74	195.25	195.20
						195.20

CUMULATIVE AREA = 0.09 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION POND2
FOR PLAN 1, RATIO = 1.00

PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	174.	6.20	(CFS)	55.	17.	14.
			(INCHES)	5.500	6.846	6.846
			(AC-FT)	27.	34.	34.
PEAK STORAGE	TIME			MAXIMUM AVERAGE STORAGE		
			6-HR	24-HR	72-HR	29.90-HR
+	(AC-FT)	(HR)				
	1.	6.20		1.	0.	0.
PEAK STAGE	TIME			MAXIMUM AVERAGE STAGE		
			6-HR	24-HR	72-HR	29.90-HR
+	(FEET)	(HR)				
	196.91	6.20		195.87	195.30	195.24
						195.24

CUMULATIVE AREA = 0.09 SQ MI

*** **

* *
56 KK BASIN3 * COMMERCIAL DEVELOPED CONDITIONS
* *

P.E.C.

```

8 IN      TIME DATA FOR INPUT TIME SERIES
          JXMIN      30    TIME INTERVAL IN MINUTES
          JXDATE     1FEB95 STARTING DATE
          JXTIME      600   STARTING TIME

```

57 BA SUBBASIN CHARACTERISTICS
TAREA 0.00 SUBBASIN AREA

58 PB STORM 7.80 BASIN TOTAL PRECIPITATION

[illegible]

```

63 LS      SCS LOSS RATE
           STRL      0.17  INITIAL ABSTRACTION
           CRVNR      92.00 CURVE NUMBER
           RTIMP      0.00 PERCENT IMPERVIOUS AREA

```

64 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 0.15 LAG

UNIT HYDROGRAPH
10 END-OF-PERIOD ORDINATES

5.	11.	8.	3.	1.	1.	0.	0.	0.	0.
----	-----	----	----	----	----	----	----	----	----

TOTAL RAINFALL = 7.80, TOTAL LOSS = 0.95, TOTAL EXCESS = 6.85

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)				
+ 18.	6.00	3.	1.	1.	1.
	(INCHES)	5.534	6.846	6.846	6.846
	(AC-FT)	1.	2.	2.	2.

CUMULATIVE AREA = 0.00 SQ MI







HYDROGRAPH AT STATION BASIN3
FOR PLAN 1, RATIO = 0.59

TOTAL RAINFALL = 4.60, TOTAL LOSS = 0.90, TOTAL EXCESS = 3.70

PEAK FLOW		TIME	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	10.	6.00				
		(CFS)	1.	0.	0.	0.
		(INCHES)	3.026	3.703	3.703	3.703
		(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN3
FOR PLAN 1, RATIO = 0.69

TOTAL RAINFALL = 5.36, TOTAL LOSS = 0.92, TOTAL EXCESS = 4.44

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
(CFS)	(HR)		6-HR	24-HR	72-HR	29.90-HR	
+	12.	6.00	(CFS)	2.	1.	0.	0.
			(INCHES)	3.622	4.444	4.444	4.444
			(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN3
FOR PLAN 1, RATIO = 0.81

TOTAL RAINFALL = 6.34, TOTAL LOSS = 0.94, TOTAL EXCESS = 5.40

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
(CFS)	(HR)		6-HR	24-HR	72-HR	29.90-HR	
+	14.	6.00	(CFS)	2.	1.	1.	1.
			(INCHES)	4.388	5.402	5.402	5.402
			(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN3
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 0.95, TOTAL EXCESS = 6.85

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
(CFS)	(HR)		6-HR	24-HR	72-HR	29.90-HR	
+	18.	6.00	(CFS)	3.	1.	1.	1.
			(INCHES)	5.534	6.846	6.846	6.846
			(AC-FT)	1.	2.	2.	2.

CUMULATIVE AREA = 0.00 SQ MI

*** ***

* *
65 KK * INTO3 * COMBINE HYDROGRAPHS FOR BASIN 3 AND OUT OF POND #2
* *

66 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION INTO3
FOR PLAN 1, RATIO = 0.59

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+			(CFS)			

+	137.	6.20	32.	10.	8.	8.
		(INCHES)	3.004	3.703	3.703	3.703
		(AC-FT)	16.	19.	19.	19.

CUMULATIVE AREA = 0.10 SQ MI

***	***	***	***	***
-----	-----	-----	-----	-----

HYDROGRAPH AT STATION INTO3
FOR PLAN 1, RATIO = 0.69

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
		(CFS)				
+	156.	6.20	38.	12.	9.	9.
		(INCHES)	3.596	4.444	4.444	4.444
		(AC-FT)	19.	23.	23.	23.

CUMULATIVE AREA = 0.10 SQ MI

***	***	***	***	***
-----	-----	-----	-----	-----

HYDROGRAPH AT STATION INTO3
FOR PLAN 1, RATIO = 0.81

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
		(CFS)				
+	169.	6.10	46.	14.	11.	11.
		(INCHES)	4.358	5.402	5.402	5.402
		(AC-FT)	23.	28.	28.	28.

CUMULATIVE AREA = 0.10 SQ MI

***	***	***	***	***
-----	-----	-----	-----	-----

HYDROGRAPH AT STATION INTO3
FOR PLAN 1, RATIO = 1.00

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
		(CFS)				
+	187.	6.10	58.	18.	14.	14.
		(INCHES)	5.500	6.846	6.846	6.846
		(AC-FT)	29.	36.	36.	36.

CUMULATIVE AREA = 0.10 SQ MI

*** **

* *
67 KK * POND3 *
* *

HYDROGRAPH ROUTING DATA

68 RS	STORAGE ROUTING		
	NSIPS	1	NUMBER OF SUBREACHES
	ITYP	ELEV	TYPE OF INITIAL CONDITION
	RSVRIC	186.00	INITIAL CONDITION
	X	0.00	WORKING R AND D COEFFICIENT

69 SA	AREA	0.5	0.8
-------	------	-----	-----

70 SE	ELEVATION	186.00	189.00
-------	-----------	--------	--------

71 SQ	DISCHARGE	0.	40.	60.	80.	90.	100.	110.	120.	130.	140.
		150.	160.	170.	180.	190.	200.				

BRADLEY FAIR PONDS #1, #2, AND #3

11-27-1995

73 SE	ELEVATION	186.00	186.95	187.18	187.35	187.42	187.50	187.56	187.61	187.67	187.72
		187.78	187.84	187.89	187.93	187.98	188.02				

COMPUTED STORAGE-ELEVATION DATA

STORAGE	0.00	1.93
ELEVATION	186.00	189.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	0.00	0.52	0.65	0.76	0.80	0.85	0.89	0.92	0.96	1.00
OUTFLOW	0.00	40.00	60.00	80.00	90.00	100.00	110.00	120.00	130.00	140.00
ELEVATION	186.00	186.95	187.18	187.35	187.42	187.50	187.56	187.61	187.67	187.72

STORAGE	1.04	1.08	1.11	1.14	1.17	1.20	1.93
OUTFLOW	150.00	160.00	170.00	180.00	190.00	200.00	444.95
ELEVATION	187.78	187.84	187.89	187.93	187.98	188.02	189.00

*** WARNING *** MODIFIED PULS ROUTING MAY BE NUMERICALLY UNSTABLE FOR OUTFLOWS BETWEEN 100. TO 445.
 THE ROUTED HYDROGRAPH SHOULD BE EXAMINED FOR OSCILLATIONS OR OUTFLOWS GREATER THAN PEAK INFLOWS.
 THIS CAN BE CORRECTED BY DECREASING THE TIME INTERVAL OR INCREASING STORAGE (USE A LONGER REACH.)

HYDROGRAPH AT STATION POND3
 FOR PLAN 1, RATIO = 0.59

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW
		6-HR 24-HR 72-HR 29.90-HR
+ (CFS)	(HR)	
+ 134.	6.20	32. 10. 8. 8.
		(INCHES) 3.003 3.703 3.703 3.703
		(AC-FT) 16. 19. 19. 19.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE
		6-HR 24-HR 72-HR 29.90-HR
+ (AC-FT)	(HR)	
+ 1.	6.20	0. 0. 0. 0.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE
		6-HR 24-HR 72-HR 29.90-HR
+ (FEET)	(HR)	
+ 187.69	6.20	186.60 186.19 186.16 186.16

CUMULATIVE AREA = 0.10 SQ MI

HYDROGRAPH AT STATION POND3
 FOR PLAN 1, RATIO = 0.69

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW
		6-HR 24-HR 72-HR 29.90-HR
+ (CFS)	(HR)	
+ 156.	6.20	38. 12. 9. 9.
		(INCHES) 3.595 4.444 4.444 4.444
		(AC-FT) 19. 23. 23. 23.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE
		6-HR 24-HR 72-HR 29.90-HR
+ (AC-FT)	(HR)	
+ 1.	6.20	0. 0. 0. 0.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE
		6-HR 24-HR 72-HR 29.90-HR
+ (FEET)	(HR)	
+ 187.81	6.20	186.67 186.22 186.18 186.18

CUMULATIVE AREA = 0.10 SQ MI

HYDROGRAPH AT STATION POND3

FOR PLAN 1, RATIO = 0.81

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW 24-HR	72-HR	29.90-HR
+ (CFS)	(HR)					
+ 168.	6.20	(CFS)	46.	14.	11.	11.
		(INCHES)	4.356	5.402	5.402	5.402
		(AC-FT)	23.	28.	28.	28.
PEAK STORAGE	TIME			MAXIMUM AVERAGE STORAGE		
+ (AC-FT)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+ 1.	6.20		0.	0.	0.	0.
PEAK STAGE	TIME			MAXIMUM AVERAGE STAGE		
+ (FEET)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+ 187.88	6.20		186.77	186.26	186.21	186.21

CUMULATIVE AREA = 0.10 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION POND3
FOR PLAN 1, RATIO = 1.00

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW 24-HR	72-HR	29.90-HR
+ (CFS)	(HR)					
+ 186.	6.10	(CFS)	58.	18.	14.	14.
		(INCHES)	5.497	6.846	6.846	6.846
		(AC-FT)	29.	36.	36.	36.
PEAK STORAGE	TIME			MAXIMUM AVERAGE STORAGE		
+ (AC-FT)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+ 1.	6.10		1.	0.	0.	0.
PEAK STAGE	TIME			MAXIMUM AVERAGE STAGE		
+ (FEET)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+ 187.96	6.10		186.90	186.31	186.25	186.25

CUMULATIVE AREA = 0.10 SQ MI

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION				
				RATIO 1 0.59	RATIO 2 0.69	RATIO 3 0.81	RATIO 4 1.00	
HYDROGRAPH AT +	UNDEV	0.09	1	FLOW TIME	106. 6.10	138. 6.10	179. 6.10	242. 6.10
HYDROGRAPH AT +	BASIN1	0.09	1	FLOW TIME	191. 6.00	227. 6.00	274. 6.00	343. 6.00
ROUTED TO +	POND1	0.09	1	FLOW TIME	128. 6.20	143. 6.20	151. 6.20	165. 6.20
** PEAK STAGES IN FEET **								
			1	STAGE TIME	199.48 6.20	199.75 6.20	200.17 6.20	200.85 6.20
HYDROGRAPH AT +	BASIN2	0.00	1	FLOW TIME	9. 6.00	10. 6.00	12. 6.00	15. 6.00
2 COMBINED AT +	INTO2	0.09	1	FLOW TIME	133. 6.20	151. 6.10	160. 6.10	174. 6.10
ROUTED TO +	POND2	0.09	1	FLOW TIME	132. 6.20	150. 6.20	159. 6.20	174. 6.20
** PEAK STAGES IN FEET **								
			1	STAGE TIME	196.68 6.20	196.78 6.20	196.83 6.20	196.91 6.20
HYDROGRAPH AT +	BASIN3	0.00	1	FLOW TIME	10. 6.00	12. 6.00	14. 6.00	18. 6.00
2 COMBINED AT +	INTO3	0.10	1	FLOW TIME	137. 6.20	156. 6.20	169. 6.10	187. 6.10
ROUTED TO +	POND3	0.10	1	FLOW TIME	134. 6.20	156. 6.20	168. 6.20	186. 6.10
** PEAK STAGES IN FEET **								
			1	STAGE TIME	187.69 6.20	187.81 6.20	187.88 6.20	187.96 6.10

*** NORMAL END OF HEC-1 ***

CURRENT DATE: 11-22-1995
CURRENT TIME: 08:45:46

FILE DATE: 11-21-1995
FILE NAME: BRADLY#4

FHWA CULVERT ANALYSIS
HY-8, VERSION 3.2

SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
INLET	OUTLET	CULVERT	BARRELS	SPAN	RISE	MANNING	INLET
ELEV.	ELEV.	LENGTH	SHAPE	(FT)	(FT)	n	TYPE
(FT)	(FT)	(FT)	MATERIAL				
175.50	175.00	90.00	4 RCB	7.00	6.00	.012	CONVENTIONAL

SUMMARY OF CULVERT FLOWS (CFS) FILE: BRADLY#4 DATE: 11-21-1995

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
180.77	1000	1000	0	0	0	0	0	0	1
180.85	1024	1024	0	0	0	0	0	0	1
180.94	1049	1049	0	0	0	0	0	0	1
181.03	1073	1073	0	0	0	0	0	0	1
181.12	1097	1097	0	0	0	0	0	0	1
181.21	1122	1122	0	0	0	0	0	0	1
181.30	1146	1146	0	0	0	0	0	0	1
181.39	1170	1170	0	0	0	0	0	0	1
181.48	1194	1194	0	0	0	0	0	0	1
181.62	1219	1219	0	0	0	0	0	0	1
181.78	1243	1243	0	0	0	0	0	0	1
186.00	2189	2189	0	0	0	0	0	0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: BRADLY#4 DATE: 11-21-1995

HEAD ELEV(FT)	HEAD ERROR(FT)	TOTAL FLOW(CFS)	FLOW ERROR(CFS)	% FLOW ERROR
180.77	0.00	1000	0	0.00
180.85	0.00	1024	0	0.00
180.94	0.00	1049	0	0.00
181.03	0.00	1073	0	0.00
181.12	0.00	1097	0	0.00
181.21	0.00	1122	0	0.00
181.30	0.00	1146	0	0.00
181.39	0.00	1170	0	0.00
181.48	0.00	1194	0	0.00
181.62	0.00	1219	0	0.00
181.78	0.00	1243	0	0.00

<1> TOLERANCE (FT) = 0.010

<2> TOLERANCE (%) = 1.000

CURRENT DATE: 11-22-1995
CURRENT TIME: 08:45:46

FILE DATE: 11-21-1995
FILE NAME: BRADLY#4

CULVERT # 1

PERFORMANCE CURVE FOR 4 BARREL(S)

Q (cfs)	HWE (ft)	TWE (ft)	ICH (ft)	OCH (ft)	FLOW TYPE	CCE (ft)	FCE (ft)	TCE (ft)	VO (fps)
1000	180.77	179.91	5.27	4.67	5-S2	0.00	0.00	0.00	11.93
1024	180.85	179.98	5.35	4.84	5-S2	0.00	0.00	0.00	12.01
1049	180.94	180.03	5.44	5.01	5-S2	0.00	0.00	0.00	12.09
1073	181.03	180.09	5.53	5.18	5-S2	0.00	0.00	0.00	12.16
1097	181.12	180.15	5.62	5.35	5-S2	0.00	0.00	0.00	12.24
1122	181.21	180.21	5.71	5.51	5-S2	0.00	0.00	0.00	12.31
1146	181.30	180.26	5.80	5.62	5-S2	0.00	0.00	0.00	12.38
1170	181.39	180.32	5.89	5.79	5-S2	0.00	0.00	0.00	12.45
1194	181.48	180.37	5.98	5.95	5-S2	0.00	0.00	0.00	12.52
1219	181.62	180.43	6.07	6.12	5-S2	0.00	0.00	0.00	8.02
1243	181.78	180.48	6.16	6.28	5-S2	0.00	0.00	0.00	8.10

El. inlet face invert 175.50 ft El. outlet invert 175.00 ft
El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

***** SITE DATA ***** CULVERT INVERT *****

INLET STATION (FT) 0.00
INLET ELEVATION (FT) 175.50
OUTLET STATION (FT) 90.00
OUTLET ELEVATION (FT) 175.00
NUMBER OF BARRELS 4.00
SLOPE (V-FT/H-FT) 0.0056
CULVERT LENGTH ALONG SLOPE (FT) 90.00

***** CULVERT DATA SUMMARY *****

BARREL SHAPE BOX
BARREL SPAN 7.00 FT
BARREL RISE 6.00 FT
BARREL MATERIAL CONCRETE
BARREL MANNING'S N 0.012
INLET TYPE CONVENTIONAL
INLET EDGE AND WALL SQUARE EDGE (30-75 DEG. FLARE)
INLET DEPRESSION NONE

CURRENT DATE: 11-22-1995
CURRENT TIME: 08:45:46

FILE DATE: 11-21-1995
FILE NAME: BRADLY#4

TAILWATER

***** REGULAR CHANNEL CROSS SECTION *****
BOTTOM WIDTH (FT) 25.00
SIDE SLOPE H/V (X:1) 4.0
CHANNEL SLOPE V/H (FT/FT) 0.003
MANNING'S N (.01-0.1) 0.040
CHANNEL INVERT ELEVATION (FT) 175.00
CULVERT NO.1 OUTLET INVERT ELEVATION 175.00 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

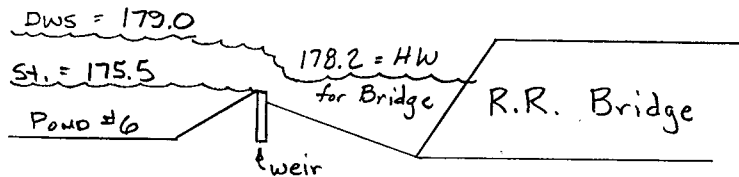
FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
1000.00	179.91	0.362	4.55	0.92
1024.30	179.98	0.362	4.59	0.93
1048.60	180.03	0.362	4.61	0.94
1072.90	180.09	0.363	4.64	0.95
1097.20	180.15	0.363	4.67	0.96
1121.50	180.21	0.363	4.70	0.98
1145.80	180.26	0.363	4.73	0.99
1170.10	180.32	0.363	4.76	1.00
1194.40	180.37	0.364	4.78	1.01
1218.70	180.43	0.364	4.81	1.02
1243.00	180.48	0.364	4.83	1.03

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH (FT)	35.00
CREST LENGTH (FT)	50.00
OVERTOPPING CREST ELEVATION (FT)	186.00

Basin #5 drains to an existing pond, No. 5. However, the pond will have to be modified to meet the size and elevation requirements shown on the drainage plan map. The outlet for the pond is a 54" RCP with a 6' square drop inlet structure at elevation 181.5. Pond #5 discharges into Pond #6, which is to be constructed by damming the creek at elevation 175.5 using a 97' weir. Maximum stage for Pond #6 is 197.0, using FEMA defined $Q_{100} = 1243$ cfs. Pond No. 6 also collects runoff from Basin #4.

The tailwater elevation used in analysis of Pond #5 was assumed to be 2.0' above the static pool elevation of Pond #6, or 177.5. FEMA's BFE just upstream of the railroad bridge of 178.2 was used the tailwater elevation for analysis of flow over the weir control structure for Pond #6. The following are the weir length calculations for Pond #6.

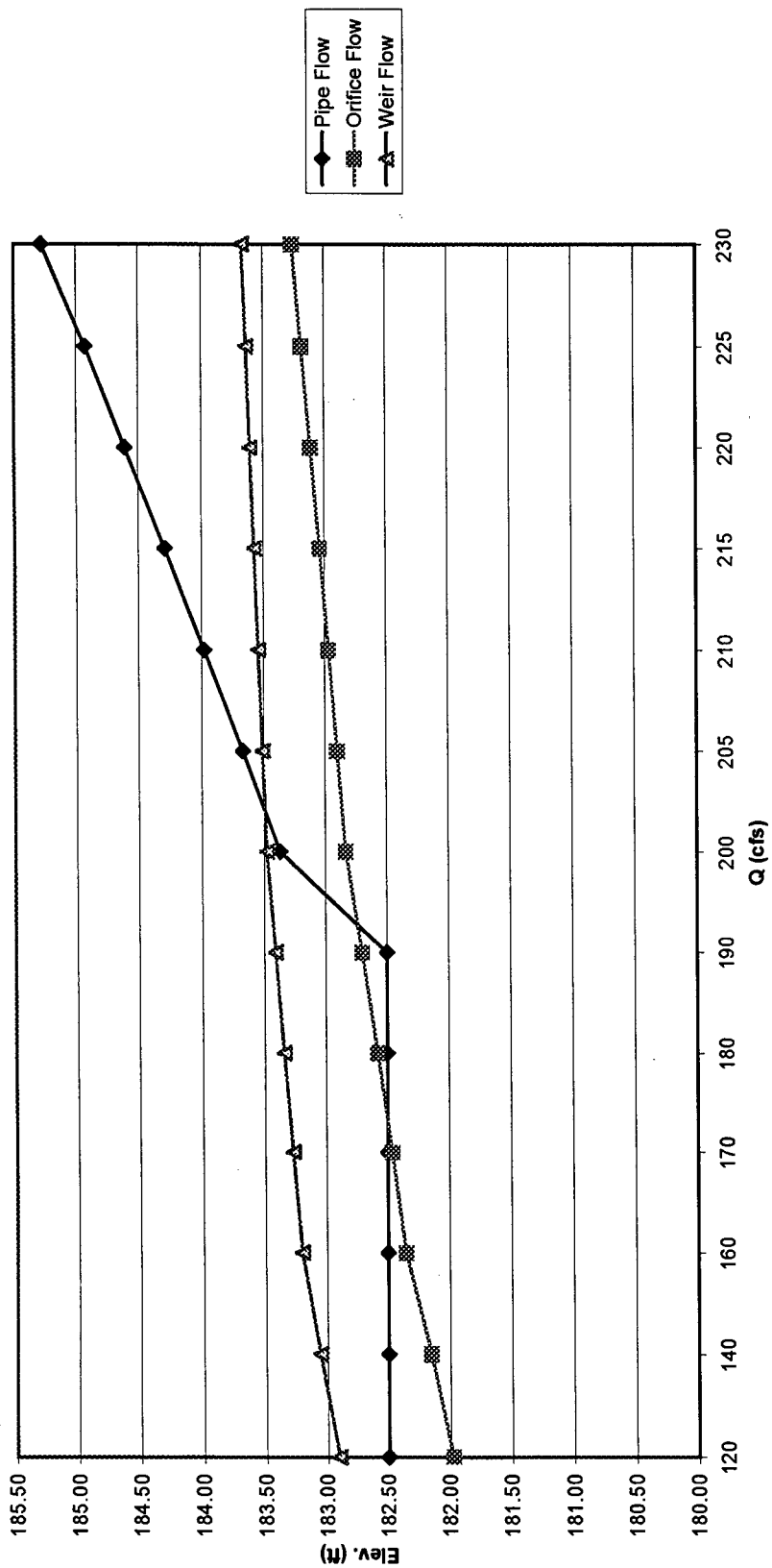


$$\begin{aligned}
 Q &= CLH^{1.5} \\
 Q_{free} &= 3.0(L)(3.5)^{1.5} \\
 \frac{1243}{3.0 \times 3.5^{1.5}} &= L_{free} \\
 63.3 &= L_{free}
 \end{aligned}
 \qquad
 \begin{aligned}
 \frac{D_{dn}}{D_{up}} &= \frac{2.7}{3.5} = 0.77 \\
 \frac{Q_{dn}}{Q_{up}} &= 0.65 \\
 L_{sub} &= \frac{63.3}{0.65} = \underline{97'}
 \end{aligned}$$

A short reach of the creek (from Pond #6 to approximately Section O) will have a maximum stage higher than the published B.F.E.'s. However, the rise occurs only this property and will not affect any neighboring property, upstream or downstream.

STAGE-DISCHARGE

POND #5



1

CURRENT DATE: 11-22-1995
CURRENT TIME: 16:08:43

FILE DATE: 11-22-1995
FILE NAME: BRADLY#5

FHWA CULVERT ANALYSIS
HY-8, VERSION 3.2

SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
INLET	OUTLET	CULVERT	BARRELS	SPAN	RISE	MANNING	INLET
ELEV.	ELEV.	LENGTH	SHAPE	(FT)	(FT)	n	TYPE
(FT)	(FT)	(FT)	MATERIAL				
174.00	171.50	250.01	1 RCP	4.50	4.50	.012	CONVENTIONAL

SUMMARY OF CULVERT FLOWS (CFS) FILE: BRADLY#5 DATE: 11-22-1995

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
183.37	200	200	0	0	0	0	0	0	1
183.67	205	205	0	0	0	0	0	0	1
183.98	210	210	0	0	0	0	0	0	1
184.29	215	215	0	0	0	0	0	0	1
184.61	220	220	0	0	0	0	0	0	1
184.93	225	225	0	0	0	0	0	0	1
185.28	230	230	0	0	0	0	0	0	1
185.65	235	235	0	0	0	0	0	0	1
186.01	240	240	0	0	0	0	0	0	7
186.21	245	242	0	0	0	0	0	3	3
186.34	250	244	0	0	0	0	0	6	3
186.00	240	240	0	0	0	0	0	0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: BRADLY#5 DATE: 11-22-1995

HEAD ELEV(FT)	HEAD ERROR(FT)	TOTAL FLOW(CFS)	FLOW ERROR(CFS)	% FLOW ERROR
183.37	0.00	200	0	0.00
183.67	0.00	205	0	0.00
183.98	0.00	210	0	0.00
184.29	0.00	215	0	0.00
184.61	0.00	220	0	0.00
184.93	0.00	225	0	0.00
185.28	0.00	230	0	0.00
185.65	0.00	235	0	0.00
186.01	-0.01	240	0	0.09
186.21	0.00	245	-0	-0.01
186.34	-0.00	250	0	0.00

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

11-27-1995

```
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   MAY 1991
*   VERSION 4.0.1E
*   Lahey F77L-EM/32 version 5.01
*   Dodson & Associates, Inc.
*   RUN DATE 11/27/95 TIME 10:03:23
*****
```

```
*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*****
```

```

X  X XXXXXX XXXX      X
X  X X      X  X      XX
X  X X      X          X
XXXXXX XXXX  X      XXXX X
X  X X      X          X
X  X X      X  X      X
X  X XXXXXX XXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
 THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1 ID Bradley Fair Drainage Plan
 2 ID Pond #5
 3 ID 5-, 10-, 25-, & 100-Year Storms
 4 ID Professional Engineering Consultants
 5 ID Wichita, Ks
 6 ID DRC 11/20/95
 7 ID File: T:\DAR\HEC1\BRADLEY2.ih1
 8 IT 6 01FEB95 0600 0 02FEB95 1154
 9 IN 30 01FEB95 0600
 10 IO 3 0
 11 JR PREC 0.5902 0.6875 0.8125 1.000

*
 *DIAGRAM
 *

12 KK UNDEV UNDEVELOPED BASIN
 13 BA .11992
 14 PB 7.8
 15 PC 0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
 16 PC .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
 17 PC .880 .890 .900 .910 .916 .925 .934 .943 .952 .958
 18 PC .964 .970 .976 .982 .988 .994 1.000
 19 LS 0 80 0
 20 UD 0.15

*
 *

21 KK BASIN1 RESIDENTIAL DEVELOPED CONDITIONS
 22 BA .11992
 23 PB 7.8
 24 PC 0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
 25 PC .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
 26 PC .880 .890 .900 .910 .916 .925 .934 .943 .952 .958
 27 PC .964 .970 .976 .982 .988 .994 1.000
 28 LS 0 87 0
 29 UD 0.15

*
 *

54" OUTLET FROM POND #5

30 KK POND5
 31 RS 1 ELEV 181.5
 32 SA 2.75 3.5
 33 SE 181.5 186
 34 SQ 0 140 160 170 180 190 200 205 210 215
 35 SQ 220 225 230
 36 SE 181.5 183.05 183.2 183.27 183.4 183.45 183.49 183.65 184.0 184.3
 37 SE 184.6 184.9 185.3
 38 ZZ

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT		
LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
12	UNDEV	
	.	
21	.	BASIN1
	.	V
	.	V
30	.	POND5

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   MAY 1991
*   VERSION 4.0.1E
*   Lahey F77L-EM/32 version 5.01
*   Dodson & Associates, Inc.
*   RUN DATE 11/27/95 TIME 10:03:23
*****
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* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*****
```

```
Bradley Fair Drainage Plan
Pond #5
5-, 10-, 25-, & 100-Year Storms
Professional Engineering Consultants
Wichita, Ks
DRC 11/20/95
File: T:\DAR\HEC1\BRADLEY2.ih1
```

```
10 IO      OUTPUT CONTROL VARIABLES
           IPRNT      3 PRINT CONTROL
           IPLOT      0 PLOT CONTROL
           QSCAL      0. HYDROGRAPH PLOT SCALE

IT         HYDROGRAPH TIME DATA
           NMIN      6 MINUTES IN COMPUTATION INTERVAL
           IDATE     1FEB95 STARTING DATE
           ITIME     0600 STARTING TIME
           NQ       300 NUMBER OF HYDROGRAPH ORDINATES
           NDDATE    2FEB95 ENDING DATE
           NDTIME    1154 ENDING TIME
           ICENT     19 CENTURY MARK

           COMPUTATION INTERVAL 0.10 HOURS
           TOTAL TIME BASE 29.90 HOURS

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW              CUBIC FEET PER SECOND
STORAGE VOLUME    ACRE-FEET
SURFACE AREA      ACRES
TEMPERATURE       DEGREES FAHRENHEIT

JP         MULTI-PLAN OPTION
           NPLAN      1 NUMBER OF PLANS

JR         MULTI-RATIO OPTION
           RATIOS OF PRECIPITATION
           0.59      0.69      0.81      1.00
```

*** **

```
*****
*
* UNDEV *      UNDEVELOPED BASIN
*
*****
```

```
9 IN      TIME DATA FOR INPUT TIME SERIES
           JXMIN     30 TIME INTERVAL IN MINUTES
           JXDATE    1FEB95 STARTING DATE
           JXTIME    600 STARTING TIME
```

SUBBASIN RUNOFF DATA

```
13 BA     SUBBASIN CHARACTERISTICS
           TAREA     0.12 SUBBASIN AREA
```

PRECIPITATION DATA

```
14 PB     STORM      7.80 BASIN TOTAL PRECIPITATION
```


CUMULATIVE AREA = 0.12 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION UNDEV
FOR PLAN 1, RATIO = 0.81

TOTAL RAINFALL = 6.34, TOTAL LOSS = 2.25, TOTAL EXCESS = 4.09

PEAK FLOW	TIME		6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	289.	6.00	(CFS)			
			43.	13.	11.	11.
		(INCHES)	3.362	4.087	4.087	4.087
		(AC-FT)	22.	26.	26.	26.

CUMULATIVE AREA = 0.12 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION UNDEV
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 2.36, TOTAL EXCESS = 5.44

PEAK FLOW	TIME		6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	384.	6.00	(CFS)			
			58.	18.	14.	14.
		(INCHES)	4.469	5.438	5.438	5.438
		(AC-FT)	29.	35.	35.	35.

CUMULATIVE AREA = 0.12 SQ MI

*** ***

 * *
 21 KK * BASIN1 * RESIDENTIAL DEVELOPED CONDITIONS
 * *

9 IN TIME DATA FOR INPUT TIME SERIES
 JXMIN 30 TIME INTERVAL IN MINUTES
 JXDATE 1FEB95 STARTING DATE
 JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

22 BA SUBBASIN CHARACTERISTICS
 TAREA 0.12 SUBBASIN AREA

PRECIPITATION DATA

23 PB STORM 7.80 BASIN TOTAL PRECIPITATION

24 PI INCREMENTAL PRECIPITATION PATTERN

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.08	0.08	0.08	0.08
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

28 LS SCS LOSS RATE
 STRTL 0.30 INITIAL ABSTRACTION
 CRVNER 87.00 CURVE NUMBER
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

29 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 0.15 LAG

UNIT HYDROGRAPH
 10 END-OF-PERIOD ORDINATES

137.	292.	198.	82.	37.	16.	7.	3.	1.	0.
------	------	------	-----	-----	-----	----	----	----	----

TOTAL RAINFALL = 7.80, TOTAL LOSS = 1.54, TOTAL EXCESS = 6.26

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	434.	6.00	(CFS)			
			66.	20.	16.	16.
		(INCHES)	5.112	6.255	6.255	6.255
		(AC-FT)	33.	40.	40.	40.

CUMULATIVE AREA = 0.12 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN1
 FOR PLAN 1, RATIO = 0.59

TOTAL RAINFALL = 4.60, TOTAL LOSS = 1.41, TOTAL EXCESS = 3.20

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	226.	6.00	(CFS)			
			34.	10.	8.	8.
		(INCHES)	2.627	3.195	3.195	3.195
		(AC-FT)	17.	20.	20.	20.

CUMULATIVE AREA = 0.12 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN1
 FOR PLAN 1, RATIO = 0.69

TOTAL RAINFALL = 5.36, TOTAL LOSS = 1.45, TOTAL EXCESS = 3.91

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	275.	6.00	(CFS)			
			41.	13.	10.	10.
		(INCHES)	3.210	3.910	3.910	3.910
		(AC-FT)	21.	25.	25.	25.

CUMULATIVE AREA = 0.12 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN1
 FOR PLAN 1, RATIO = 0.81

TOTAL RAINFALL = 6.34, TOTAL LOSS = 1.50, TOTAL EXCESS = 4.84

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	339.	6.00	(CFS)			
			51.	16.	13.	13.
		(INCHES)	3.967	4.841	4.841	4.841

(AC-FT) 25. 31. 31. 31.

CUMULATIVE AREA = 0.12 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN1
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 1.54, TOTAL EXCESS = 6.26

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	434.	66.	20.	16.	16.
	6.00	5.112	6.255	6.255	6.255
		(INCHES)	33.	40.	40.
		(AC-FT)	33.	40.	40.

CUMULATIVE AREA = 0.12 SQ MI

*** **

* *
30 KK * POND5 *
* *

HYDROGRAPH ROUTING DATA

31 RS	STORAGE ROUTING										
	NSTPS	1	NUMBER OF SUBREACHES								
	ITYP	ELEV	TYPE OF INITIAL CONDITION								
	RSVRIC	181.50	INITIAL CONDITION								
	X	0.00	WORKING R AND D COEFFICIENT								
32 SA	AREA	2.8	3.5								
33 SE	ELEVATION	181.50	186.00								
34 SQ	DISCHARGE	0.	140.	160.	170.	180.	190.	200.	205.	210.	215.
		220.	225.	230.							
36 SE	ELEVATION	181.50	183.05	183.20	183.27	183.40	183.45	183.49	183.65	184.00	184.30
		184.60	184.90	185.30							

COMPUTED STORAGE-ELEVATION DATA

STORAGE	0.00	14.03
ELEVATION	181.50	186.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	0.00	4.45	4.90	5.12	5.51	5.67	5.79	6.28	7.38	8.33
OUTFLOW	0.00	140.00	160.00	170.00	180.00	190.00	200.00	205.00	210.00	215.00
ELEVATION	181.50	183.05	183.20	183.27	183.40	183.45	183.49	183.65	184.00	184.30
STORAGE	9.30	10.28	11.62	14.03						
OUTFLOW	220.00	225.00	230.00	238.75						
ELEVATION	184.60	184.90	185.30	186.00						

*** *** *** *** ***

HYDROGRAPH AT STATION POND5
FOR PLAN 1, RATIO = 0.59

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	148.	34.	10.	8.	8.
	6.20	2.618	3.195	3.195	3.195
		(INCHES)	3.195	3.195	3.195

		(AC-FT)	17.	20.	20.	20.
PEAK STORAGE	TIME			MAXIMUM AVERAGE STORAGE		
			6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)					
5.	6.20		1.	0.	0.	0.
PEAK STAGE	TIME			MAXIMUM AVERAGE STAGE		
			6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)					
183.11	6.20		181.87	181.61	181.59	181.59
CUMULATIVE AREA =			0.12 SQ MI			

*** *** *** *** ***

HYDROGRAPH AT STATION POND5
FOR PLAN 1, RATIO = 0.69

PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
			6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)					
		(CFS)				
+ 185.	6.20		41.	13.	10.	10.
		(INCHES)	3.200	3.910	3.910	3.910
		(AC-FT)	20.	25.	25.	25.
PEAK STORAGE	TIME			MAXIMUM AVERAGE STORAGE		
			6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)					
6.	6.20		1.	0.	0.	0.
PEAK STAGE	TIME			MAXIMUM AVERAGE STAGE		
			6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)					
183.43	6.20		181.95	181.64	181.61	181.61
CUMULATIVE AREA =			0.12 SQ MI			

*** *** *** *** ***

HYDROGRAPH AT STATION POND5
FOR PLAN 1, RATIO = 0.81

PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
			6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)					
		(CFS)				
+ 208.	6.20		51.	16.	13.	13.
		(INCHES)	3.954	4.841	4.841	4.841
		(AC-FT)	25.	31.	31.	31.
PEAK STORAGE	TIME			MAXIMUM AVERAGE STORAGE		
			6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)					
7.	6.20		2.	0.	0.	0.
PEAK STAGE	TIME			MAXIMUM AVERAGE STAGE		
			6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)					
183.89	6.20		182.06	181.67	181.64	181.64
CUMULATIVE AREA =			0.12 SQ MI			

*** *** *** *** ***

HYDROGRAPH AT STATION POND5
FOR PLAN 1, RATIO = 1.00

PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
			6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)					
		(CFS)				
+ 223.	6.20		66.	20.	16.	16.
		(INCHES)	5.095	6.255	6.255	6.255
		(AC-FT)	33.	40.	40.	40.

PEAK STORAGE	TIME	6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)				
10.	6.20	2.	1.	1.	1.

PEAK STAGE	TIME	6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)				
184.78	6.20	182.28	181.74	181.69	181.69

CUMULATIVE AREA = 0.12 SQ MI

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION				
				RATIO 1 0.59	RATIO 2 0.69	RATIO 3 0.81	RATIO 4 1.00	
HYDROGRAPH AT +	UNDEV	0.12	1	FLOW TIME	179. 6.00	227. 6.00	289. 6.00	384. 6.00
HYDROGRAPH AT +	BASIN1	0.12	1	FLOW TIME	226. 6.00	275. 6.00	339. 6.00	434. 6.00
ROUTED TO +	POND5	0.12	1	FLOW TIME	148. 6.20	185. 6.20	208. 6.20	223. 6.20
** PEAK STAGES IN FEET **								
			1	STAGE TIME	183.11 6.20	183.43 6.20	183.89 6.20	184.78 6.20

*** NORMAL END OF HEC-1 ***



Date _____ Page _____ of _____

Project BRADLEY FAIR II / WILSON ESTATES

Item BASIN #6

$$A_{dev} = 23.15 \text{ Ac.}$$

$$A_{undevel.} = 28.85 \text{ Ac.}$$

Q DEVELOPED

$$C_{100} = 0.76$$

$$L_{100} = 7.36$$

$$A = 23.15$$

$$Q_{100} = 0.76 (7.36) (23.15)$$

$$Q_{100} = 129.5 \text{ cfs}$$

Q UNDEVELOPED

$$C_{100} = 0.67$$

$$L_{100} = 7.36$$

$$A = 28.85$$

$$Q_{100} = 0.67 (7.36) (28.85)$$

$$Q_{100} = 142.3 \text{ cfs}$$

$$Q_{100} (\text{DEV.}) < Q_{100} (\text{UNDEV.})$$

DETENTION STORAGE NOT REQUIRED

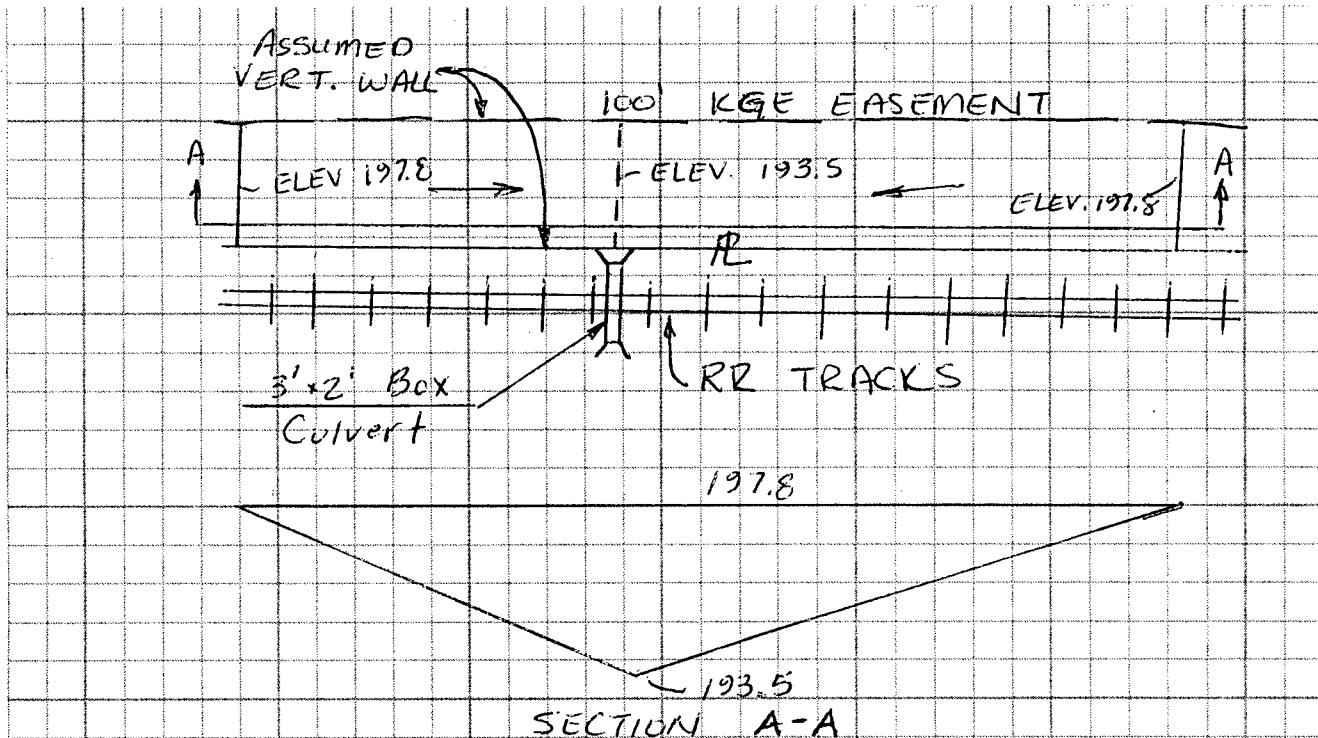
4.5' HEAD REQ'D FOR 129.5 cfs in 5'x4' RCBC. (Proposed, Part of Webb Rd. Project)
 $1.0' + 4.5' + 186.5 \text{ ft} = \underline{192.0} \Rightarrow \text{min. pad for Lots adjacent to Box.}$

NOTE: 100-YEAR FLOW DOES NOT TOP WEBB RD.

THEREFORE, SET MIN PAD LOTS ADJACENT TO WEBB RD.
AT ELEV. $192.12 + 1.0' = \underline{193.12 \text{ or higher}}$

@ Low Pt. WEBB + 1.0' $\nearrow$

Basin No. 8 drains to the existing 3' X 2' stone and concrete box culvert under the railroad tracks near the southwest corner of the site. Runoff will be directed to the culvert via storm sewer and /or ditches. No detention ponds will be constructed within this basin. However, storage will occur naturally within the 100' KG&E easement. For use in the HEC-1 model, a pond with vee-shaped bottom and vertical sides at the property line and easement line was assumed, as shown:



Per the HEC-1 output, the peak Pre-Developed Q_{100} is 66 cfs, the peak Developed Q_{100} , with detention, is 30 cfs, and the maximum ponding elevation is 196.02.

1

CURRENT DATE: 12-13-1995
CURRENT TIME: 10:28:45FILE DATE: 12-13-1995
FILE NAME: RR_3x2FHWA CULVERT ANALYSIS
HY-8, VERSION 3.2

SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
193.50	193.49	50.00	1 RCB	3.00	2.00	.012	CONVENTIONAL

SUMMARY OF CULVERT FLOWS (CFS) FILE: RR_3x2 DATE: 12-13-1995

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
196.43	35	35	0	0	0	0	0	0	1
196.76	39	39	0	0	0	0	0	0	1
197.13	43	43	0	0	0	0	0	0	1
197.53	47	47	0	0	0	0	0	0	1
197.82	51	50	0	0	0	0	0	1	30
197.86	55	50	0	0	0	0	0	5	7
197.89	59	50	0	0	0	0	0	8	6
197.92	63	50	0	0	0	0	0	12	5
197.94	67	51	0	0	0	0	0	16	4
197.96	71	51	0	0	0	0	0	20	4
197.98	75	51	0	0	0	0	0	23	4
197.80	49	49	0	0	0	0	0	0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: RR_3x2 DATE: 12-13-1995

HEAD ELEV(FT)	HEAD ERROR(FT)	TOTAL FLOW(CFS)	FLOW ERROR(CFS)	% FLOW ERROR
196.43	0.00	35	0	0.00
196.76	0.00	39	0	0.00
197.13	0.00	43	0	0.00
197.53	0.00	47	0	0.00
197.82	-0.00	51	1	1.37
197.86	-0.00	55	0	0.87
197.89	-0.00	59	0	0.59
197.92	-0.00	63	0	0.66
197.94	-0.00	67	1	0.98
197.96	-0.00	71	1	0.87
197.98	-0.00	75	1	0.72

<1> TOLERANCE (FT) = 0.010

<2> TOLERANCE (%) = 1.000

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   MAY 1991
*   VERSION 4.0.1E
*   Lahey F77L-EM/32 version 5.01
*   Dodson & Associates, Inc.
*   RUN DATE 12/13/95 TIME 10:34:13
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*
*****

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X  X XXXXXX XXXX  X
X  X X  X  X  XX
X  X X  X  X  X
XXXXXX XXXX  X  XXXX  X
X  X X  X  X  X
X  X X  X  X  X
X  X XXXXXX XXXX  XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1          ID      Bradley Fair Drainage Plan
2          ID      Pond #5
3          ID      5-, 10-, 25-, & 100-Year Storms
4          ID      Professional Engineering Consultants
5          ID      Wichita, Ks
6          ID      DRC 11/20/95
7          ID      File: T:\DAR\HEC1\BRADLEY-1.H
8          IT      6 01FEB95 0600 0 02FEB95 1154
9          IN      30 01FEB95 0600
10         IO      3 0
11         JR      PREC 0.5902 0.6875 0.8125 1.000
*
*DIAGRAM
*
12         KK      UNDEV      UNDEVELOPED BASIN
13         BA      .0206
14         PB      7.8
15         PC      0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
16         PC      .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
17         PC      .880 .890 .900 .910 .916 .925 .934 .943 .952 .958
18         PC      .964 .970 .976 .982 .988 .994 1.000
19         LS      0 80 0
20         UD      0.15
*
*
21         KK      BASIN1      RESIDENTIAL DEVELOPED CONDITIONS
22         BA      .0206
23         PB      7.8
24         PC      0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
25         PC      .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
26         PC      .880 .890 .900 .910 .916 .925 .934 .943 .952 .958
27         PC      .964 .970 .976 .982 .988 .994 1.000
28         LS      0 87 0
29         UD      0.15
*
*
30         KK      RRROW
31         RS      1 ELEV 193.5
32         SA      0 0.69 1.37 2.41

```

33	SE	193.5	194	196	197.8							
34	SQ	0	35	39	43	47	51	55	59	63	67	
35	SQ	71	75									
36	SE	193.5	196.43	196.76	197.13	197.53	197.82	197.86	197.89	197.92	197.94	
37	SE	197.96	197.98									
	*											
38	ZZ											

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT
 LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

12 UNDEV

21 . BASIN1
 . V
 . V

30 . RRROW

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

 *
 * FLOOD HYDROGRAPH PACKAGE (HEC-1) *
 * MAY 1991 *
 * VERSION 4.0.1E *
 * Lahey F77L-EM/32 version 5.01 *
 * Dodson & Associates, Inc. *
 * RUN DATE 12/13/95 TIME 10:34:13 *

 *
 * U.S. ARMY CORPS OF ENGINEERS *
 * HYDROLOGIC ENGINEERING CENTER *
 * 609 SECOND STREET *
 * DAVIS, CALIFORNIA 95616 *
 * (916) 551-1748 *

Bradley Fair Drainage Plan
 Pond #5
 5-, 10-, 25-, & 100-Year Storms
 Professional Engineering Consultants
 Wichita, Ks
 DRC 11/20/95
 File: T:\DAR\HEC1\BRADLEY2.ih1

10 IO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

NMIN	6	MINUTES IN COMPUTATION INTERVAL
IDATE	1FEB95	STARTING DATE
ITIME	0600	STARTING TIME
NQ	300	NUMBER OF HYDROGRAPH ORDINATES
NDDATE	2FEB95	ENDING DATE
NDTIME	1154	ENDING TIME
ICENT	19	CENTURY MARK

COMPUTATION INTERVAL 0.10 HOURS
 TOTAL TIME BASE 29.90 HOURS

ENGLISH UNITS

DRAINAGE AREA	SQUARE MILES
PRECIPITATION DEPTH	INCHES
LENGTH, ELEVATION	FEET
FLOW	CUBIC FEET PER SECOND
STORAGE VOLUME	ACRE-Feet
SURFACE AREA	ACRES
TEMPERATURE	DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 0.59 0.69 0.81 1.00

+	31.	6.00	(CFS)	5.	1.	1.	1.
			(INCHES)	2.097	2.550	2.550	2.550
			(AC-FT)	2.	3.	3.	3.

CUMULATIVE AREA = 0.02 SQ MI

***	***	***	***	***
-----	-----	-----	-----	-----

HYDROGRAPH AT STATION UNDEV
FOR PLAN 1, RATIO = 0.69

TOTAL RAINFALL = 5.36, TOTAL LOSS = 2.15, TOTAL EXCESS = 3.21

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)	(CFS)			
+	39.	6.00	6.	2.	1.	1.
			(INCHES)	2.643	3.211	3.211
			(AC-FT)	3.	4.	4.

CUMULATIVE AREA = 0.02 SQ MI

***	***	***	***	***
-----	-----	-----	-----	-----

HYDROGRAPH AT STATION UNDEV
FOR PLAN 1, RATIO = 0.81

TOTAL RAINFALL = 6.34, TOTAL LOSS = 2.25, TOTAL EXCESS = 4.09

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)	(CFS)			
+	50.	6.00	7.	2.	2.	2.
			(INCHES)	3.362	4.087	4.087
			(AC-FT)	4.	4.	4.

CUMULATIVE AREA = 0.02 SQ MI

***	***	***	***	***
-----	-----	-----	-----	-----

HYDROGRAPH AT STATION UNDEV
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 2.36, TOTAL EXCESS = 5.44

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)	(CFS)			
+	66.	6.00	10.	3.	2.	2.
			(INCHES)	4.469	5.438	5.438
			(AC-FT)	5.	6.	6.

CUMULATIVE AREA = 0.02 SQ MI

*** **

* *
21 KK * BASIN1 * RESIDENTIAL DEVELOPED CONDITIONS
* *

9 IN TIME DATA FOR INPUT TIME SERIES
JXMIN 30 TIME INTERVAL IN MINUTES
JXDATE 1FEB95 STARTING DATE
JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

+	(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	47.	6.00	(CFS) 7.	2.	2.	2.
			(INCHES) 3.210	3.910	3.910	3.910
			(AC-FT) 4.	4.	4.	4.

CUMULATIVE AREA = 0.02 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN1
FOR PLAN 1, RATIO = 0.81

TOTAL RAINFALL = 6.34, TOTAL LOSS = 1.50, TOTAL EXCESS = 4.84

PEAK FLOW	TIME	6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(CFS)			
+	58.	6.00	9.	3.	2.
			(INCHES) 3.967	4.841	4.841
			(AC-FT) 4.	5.	5.

CUMULATIVE AREA = 0.02 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BASIN1
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 1.54, TOTAL EXCESS = 6.26

PEAK FLOW	TIME	6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(CFS)			
+	74.	6.00	11.	3.	3.
			(INCHES) 5.112	6.255	6.255
			(AC-FT) 6.	7.	7.

CUMULATIVE AREA = 0.02 SQ MI

*** ***

* *
* *
30 KK * RRROW *
* *
* *

HYDROGRAPH ROUTING DATA

31 RS	STORAGE ROUTING										
	NSTPS	1	NUMBER OF SUBREACHES								
	ITYP	ELEV	TYPE OF INITIAL CONDITION								
	RSVRIC	193.50	INITIAL CONDITION								
	X	0.00	WORKING R AND D COEFFICIENT								
32 SA	AREA	0.0	0.7	1.4	2.4						
33 SE	ELEVATION	193.50	194.00	196.00	197.80						
34 SQ	DISCHARGE	0.	35.	39.	43.	47.	51.	55.	59.	63.	67.
		71.	75.								
36 SE	ELEVATION	193.50	196.43	196.76	197.13	197.53	197.82	197.86	197.89	197.92	197.94
		197.96	197.98								

COMPUTED STORAGE-ELEVATION DATA

STORAGE	0.00	0.12	2.14	5.49
---------	------	------	------	------

ELEVATION 193.50 194.00 196.00 197.80

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	0.00	0.12	2.14	2.77	3.33	4.02	4.87	5.49	5.54	5.64
OUTFLOW	0.00	5.97	29.86	35.00	39.00	43.00	47.00	50.72	51.00	55.00
ELEVATION	193.50	194.00	196.00	196.43	196.76	197.13	197.53	197.80	197.82	197.86
STORAGE	5.71	5.79	5.84	5.89	5.94					
OUTFLOW	59.00	63.00	67.00	71.00	75.00					
ELEVATION	197.89	197.92	197.94	197.96	197.98					

*** *** *** *** ***

HYDROGRAPH AT STATION RRROW
FOR PLAN 1, RATIO = 0.59

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)	(CFS)				
+ 16.	6.30	(INCHES)	6.	2.	1.	1.
		(AC-FT)	2.623	3.195	3.195	3.195
			3.	4.	4.	4.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)					
1.	6.30		0.	0.	0.	0.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)					
194.88	6.30		193.99	193.65	193.62	193.62

CUMULATIVE AREA = 0.02 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION RRROW
FOR PLAN 1, RATIO = 0.69

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)	(CFS)				
+ 20.	6.30	(INCHES)	7.	2.	2.	2.
		(AC-FT)	3.206	3.910	3.910	3.910
			4.	4.	4.	4.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)					
1.	6.30		0.	0.	0.	0.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)					
195.15	6.30		194.09	193.68	193.65	193.65

CUMULATIVE AREA = 0.02 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION RRROW
FOR PLAN 1, RATIO = 0.81

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)	(CFS)				
+ 24.	6.30	(INCHES)	9.	3.	2.	2.
		(AC-FT)	3.963	4.841	4.841	4.841
			4.	5.	5.	5.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)					

2.	6.30	0.	0.	0.	0.
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)				
195.49	6.30	194.23	193.72	193.68	193.68

CUMULATIVE AREA = 0.02 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION RRROW
FOR PLAN 1, RATIO = 1.00

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	29.90-HR	
+ (CFS)	(HR)					
30.	6.30	11.	3.	3.	3.	
		(INCHES)	5.105	6.255	6.255	6.255
		(AC-FT)	6.	7.	7.	7.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)				
2.	6.30	1.	0.	0.	0.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)				
196.02	6.30	194.45	193.79	193.73	193.73

CUMULATIVE AREA = 0.02 SQ MI

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION			
				RATIO 1	RATIO 2	RATIO 3	RATIO 4
				0.59	0.69	0.81	1.00
HYDROGRAPH AT							
+ UNDEV	0.02	1	FLOW	31.	39.	50.	66.
			TIME	6.00	6.00	6.00	6.00
HYDROGRAPH AT							
+ BASIN1	0.02	1	FLOW	39.	47.	58.	74.
			TIME	6.00	6.00	6.00	6.00
ROUTED TO							
+ RRROW	0.02	1	FLOW	16.	20.	24.	30.
			TIME	6.30	6.30	6.30	6.30
** PEAK STAGES IN FEET **							
		1	STAGE	194.88	195.15	195.49	196.02
			TIME	6.30	6.30	6.30	6.30

*** NORMAL END OF HEC-1 ***

The second portion of this drainage plan was devoted to Pond design and detention storage analysis for the entire site. The purpose of this analysis is to ensure that development of this property does not adversely affect any neighboring properties. To show this, there are four points of concentration where on-site runoff will exit the Willson Property, these being: 1. 3' X 2' box culvert under RR in SW corner, @. RR biidge at approximately center of section, 3. Proposed 5' X 4' RCBC at SE corner to be built with Webb Rd. Project byt County, and 4. 2 - 5' X 4' RCBC just north of 19th St.

Following are the peak Pre-Developed and Developed on-site generated Q_{100} 's for each point.

Point #	Contributing Basin	Q_{100} pre.	Q_{100} dev.
1	8	66	30
2	1-5,9	1083	894
3	6	142	130
4	RCBC and drainage system previously designed for Q_{100}		

In each case the peak developed flow is less than the peak pre-developed flow. This is accomplished through detention storage to be provided by construction of new ponds.

ATTACHMENT D

DRAINAGE CRITERIA

CITY OF WICHITA, KANSAS

RECOMMENDED RUNOFF COEFFICIENTS FOR RATIONAL METHOD
AND PERCENT IMPERVIOUS FOR UNIT HYDROGRAPH METHOD

Land Use or Surface Characteristics	Percent Impervious	Frequency			
		2	5	10	100
1. Business:					
Downtown Areas	95	0.84	0.85	0.87	0.91
Neighborhood Areas	70	0.68	0.69	0.73	0.80
2. Residential:					
Single Family (Soil Group D)					
1/8 Acre	50	0.57	0.61	0.66	0.79
1/4 Acre	38	0.50	0.54	0.62	0.76
1/3 Acre	30	0.46	0.50	0.59	0.73
1/2 Acre	25	0.42	0.48	0.56	0.72
3/4 Acre	22	0.42	0.46	0.55	0.71
1 Acre	20	0.41	0.45	0.54	0.71
Multi-Family (Soil Group D)					
Multi-Unit (detached)	60	0.62	0.66	0.72	0.82
Multi-Unit (attached)	65	0.64	0.68	0.73	0.83
Apartments	75	0.70	0.73	0.79	0.86
Single Family (Soil Group C)					
1/8 Acre	50	0.55	0.58	0.64	0.73
1/4 Acre	38	0.48	0.51	0.57	0.68
1/3 Acre	30	0.43	0.46	0.53	0.65
1/2 Acre	25	0.40	0.43	0.50	0.63
3/4 Acre	22	0.39	0.42	0.49	0.62
1 Acre	20	0.37	0.40	0.48	0.61
Multi-Family (Soil Group C)					
Multi-Unit (detached)	60	0.60	0.63	0.69	0.77
Multi-Unit (attached)	65	0.63	0.66	0.71	0.79
Apartments	75	0.68	0.72	0.77	0.83
Single-Family (Soil Group B)					
1/8 Acre	50	0.52	0.54	0.59	0.67
1/4 Acre	38	0.44	0.46	0.52	0.61
1/3 Acre	30	0.39	0.41	0.47	0.57
1/2 Acre	25	0.36	0.38	0.44	0.54
3/4 Acre	22	0.34	0.36	0.42	0.52
1 Acre	20	0.33	0.35	0.40	0.51
Multi-Family (Soil Group B)					
Multi-Unit (detached)	60	0.58	0.60	0.65	0.72
Multi-Unit (attached)	65	0.61	0.64	0.68	0.75
Apartments	75	0.67	0.70	0.74	0.80

Land Use or Face Characteristics	Percent Impervious	Frequency			
		<u>2</u>	<u>5</u>	<u>10</u>	<u>100</u>
<u>Single Family (Soil Group A)</u>					
1/8 Acre	50	0.47	0.50	0.54	0.60
1/4 Acre	38	0.39	0.41	0.45	0.52
1/3 Acre	30	0.33	0.35	0.39	0.47
1/2 Acre	25	0.30	0.31	0.35	0.44
3/4 Acre	22	0.28	0.29	0.33	0.42
1 Acre	20	0.26	0.28	0.32	0.40
<u>Multi-Family (Soil Group A)</u>					
Multi-Unit (detached)	60	0.55	0.57	0.61	0.67
Multi-Unit (attached)	65	0.58	0.60	0.64	0.70
Apartments	75	0.65	0.68	0.72	0.77
3. Industrial:					
Light Areas	70	0.68	0.69	0.73	0.80
Heavy Areas	80	0.74	0.76	0.79	0.84
4. Playgrounds:					
	15	0.33	0.35	0.42	0.55
5. Schools:					
	40	0.49	0.51	0.56	0.66
6. Railroad Yard Areas:					
	30	0.43	0.45	0.50	0.62
Undeveloped Urban Areas:					
Offsite Flow Analysis (when land use not defined)	45	0.52	0.54	0.59	0.68
8. Streets:					
Paved	99	0.87	0.88	0.90	0.93
Gravel	00	0.24	0.26	0.33	0.48
9. Drive, Parking Lots and Walks:					
	96	0.87	0.87	0.88	0.89
10. Roofs:					
	90	0.80	0.85	0.90	0.93
11. Urban Lawn Areas (See Note No. 1 below):					
<u>Soil Group A</u>					
Slope less than 1%	00	0.08	0.09	0.13	0.23
Slope 1% to 4%	00	0.12	0.13	0.17	0.27
Slope more than 4%	00	0.16	0.17	0.21	0.31
<u>Soil Group B</u>					
Slope less than 1%	00	0.16	0.18	0.24	0.37
Slope 1% to 4%	00	0.20	0.22	0.28	0.41
Slope more than 4%	00	0.24	0.26	0.32	0.45
<u>Soil Group C</u>					
Slope less than 1%	00	0.24	0.27	0.35	0.51
Slope 1% to 4%	00	0.26	0.29	0.37	0.53
Slope more than 4%	00	0.28	0.31	0.39	0.55

Land Use or Surface Characteristics	Percent Impervious	Frequency			
		<u>2</u>	<u>5</u>	<u>10</u>	<u>100</u>
<u>Soil Group D</u>					
Slope less than 1%	00	0.28	0.33	0.43	0.63
Slope 1% to 4%	00	0.30	0.35	0.45	0.65
Slope more than 4%	00	0.32	0.37	0.47	0.67

Note No. 1: Coefficients shown in the above table are for pervious open space areas with thick turf which includes pervious areas in parks and cemeteries. Coefficients shown above must be increased 0.02 for use with agricultural pasture areas. Coefficients shown above must be reduced by 0.04 for use with agricultural cultivated areas. Group A soils are well-drained, coarse textured sands with high infiltration rates. Group B soils are moderately well-drained, moderately coarse textured soils with moderate infiltration rates. Group C soils are moderately poor-drained, moderately fine textured soils with slow infiltration rates. Group D soils are poor-drained, fine textured soils with very slow infiltration rates.

GENERAL NOTE: These Rational Formula Coefficients may not be valid for basins 320 acres or larger.

April 15, 1986

ATTACHMENT A
DRAINAGE CRITERIA MANUAL

CITY OF WICHITA, KANSAS

RAINFALL INTENSITY TABLE FOR SEDGWICK COUNTY, KANSAS

The following tabulation contains rainfall intensity in inches
per hour as derived from ESSA Weather Bureau Technical Paper
40 Modified to NWS Hydro-35, 1977 During First Hour

TDF

DURATION IN MINUTES	RETURN PERIODS OF						
	1-YR	2-YR	5-YR	10-YR	25-YR	50-YR	100-YR
5	4.18	5.57	6.53	7.41	8.52	9.48	10.32
6	3.99	5.32	6.25	7.09	8.16	9.09	9.89
7	3.81	5.09	5.99	6.81	7.84	8.74	9.50
8	3.66	4.89	5.75	6.55	7.55	8.42	9.15
9	3.52	4.70	5.54	6.31	7.28	8.13	8.83
10	3.39	4.52	5.34	6.09	7.04	7.86	8.54
11	3.27	4.36	5.16	5.89	6.81	7.61	8.27
12	3.18	4.21	4.99	5.71	6.60	7.38	8.02
13	3.05	4.08	4.84	5.53	6.41	7.17	7.79
14	2.96	3.95	4.69	5.37	6.23	6.97	7.57
15	2.87	3.83	4.56	5.22	6.06	6.78	7.37
16	2.78	3.72	4.43	5.08	5.90	6.60	7.18
17	2.71	3.61	4.31	4.95	5.75	6.44	7.00
18	2.63	3.51	4.20	4.83	5.61	6.29	6.84
19	2.56	3.42	4.10	4.71	5.47	6.14	6.68
20	2.50	3.33	4.00	4.60	5.35	6.00	6.53
21	2.44	3.25	3.90	4.50	5.23	5.87	6.39
22	2.38	3.17	3.81	4.40	5.12	5.75	6.26
23	2.32	3.10	3.73	4.31	5.01	5.63	6.13
24	2.27	3.03	3.65	4.22	4.91	5.52	6.01
25	2.22	2.96	3.57	4.13	4.81	5.41	5.90
26	2.20	2.90	3.50	4.05	4.72	5.31	5.79
27	2.16	2.84	3.43	3.98	4.63	5.21	5.69
28	2.14	2.78	3.37	3.90	4.55	5.12	5.59
29	2.11	2.72	3.30	3.83	4.47	5.03	5.49
30	2.08	2.67	3.24	3.76	4.39	4.94	5.40
31	2.05	2.62	3.19	3.70	4.32	4.86	5.32
32	2.02	2.57	3.10	3.63	4.25	4.79	5.22
33	1.99	2.52	3.05	3.57	4.18	4.71	5.14
34	1.96	2.48	3.01	3.51	4.11	4.63	5.07
35	1.93	2.44	2.98	3.46	4.05	4.56	5.00
36	1.91	2.39	2.93	3.41	3.99	4.50	4.93
37	1.89	2.35	2.88	3.36	3.93	4.43	4.86
38	1.87	2.32	2.84	3.31	3.87	4.37	4.79
39	1.85	2.28	2.80	3.26	3.82	4.31	4.73
40	1.83	2.24	2.76	3.22	3.76	4.25	4.66
41	1.81	2.21	2.72	3.17	3.71	4.19	4.60
42	1.79	2.18	2.68	3.13	3.66	4.13	4.54
43	1.77	2.14	2.64	3.09	3.61	4.08	4.49
44	1.75	2.11	2.61	3.05	3.57	4.03	4.43
45	1.73	2.08	2.57	3.01	3.52	3.98	4.38

TABLE 3

cf
FULL FLOW COEFFICIENT VALUES
CIRCULAR CONCRETE PIPE

$S = Q^2/K^2$
 $Q = K\sqrt{S}$
 $K = Q/\sqrt{S}$

D Pipe Diameter (inches)	A Area (Square Feet)	R Hydraulic Radius (Feet)	Value of $C_1 = \frac{1.486}{n} \times A \times R^{3/2} = K$			
			n=0.010	n=0.011	n=0.012	n=0.013
8	0.349	0.167	15.8	14.3	13.1	12.1
10	0.545	0.208	28.4	25.8	23.6	21.8
12	0.785	0.250	46.4	42.1	38.6	35.7
15	1.227	0.312	84.1	76.5	70.1	64.7
18	1.767	0.375	137	124	114	105
21	2.405	0.437	206	187	172	158
24	3.142	0.500	294	267	245	226
27	3.976	0.562	402	366	335	310
30	4.909	0.625	533	485	444	410
33	5.940	0.688	686	624	574	530
36	7.069	0.750	867	788	722	666
42	9.621	0.875	1308	1189	1090	1006
48	12.566	1.000	1867	1698	1556	1436
54	15.904	1.125	2557	2325	2131	1967
60	19.635	1.250	3385	3077	2821	2604
66	23.758	1.375	4364	3967	3636	3357
72	28.274	1.500	5504	5004	4587	4234
78	33.183	1.625	6815	6195	5679	5242
84	38.485	1.750	8304	7549	6920	6388
90	44.170	1.875	9985	9078	8321	7681
96	50.266	2.000	11850	10780	9878	9119
102	56.745	2.125	13940	12670	11620	10720
108	63.617	2.250	16230	14760	13530	12490
114	70.882	2.375	18750	17040	15620	14420
120	78.540	2.500	21500	19540	17920	16540
126	86.590	2.625	24480	22260	20400	18830
132	95.033	2.750	27720	25200	23100	21330
138	103.870	2.875	31210	28370	26010	24010
144	113.100	3.000	34960	31780	29130	26890

TABLE 4
FULL FLOW COEFFICIENT VALUES
ELLIPTICAL CONCRETE PIPE

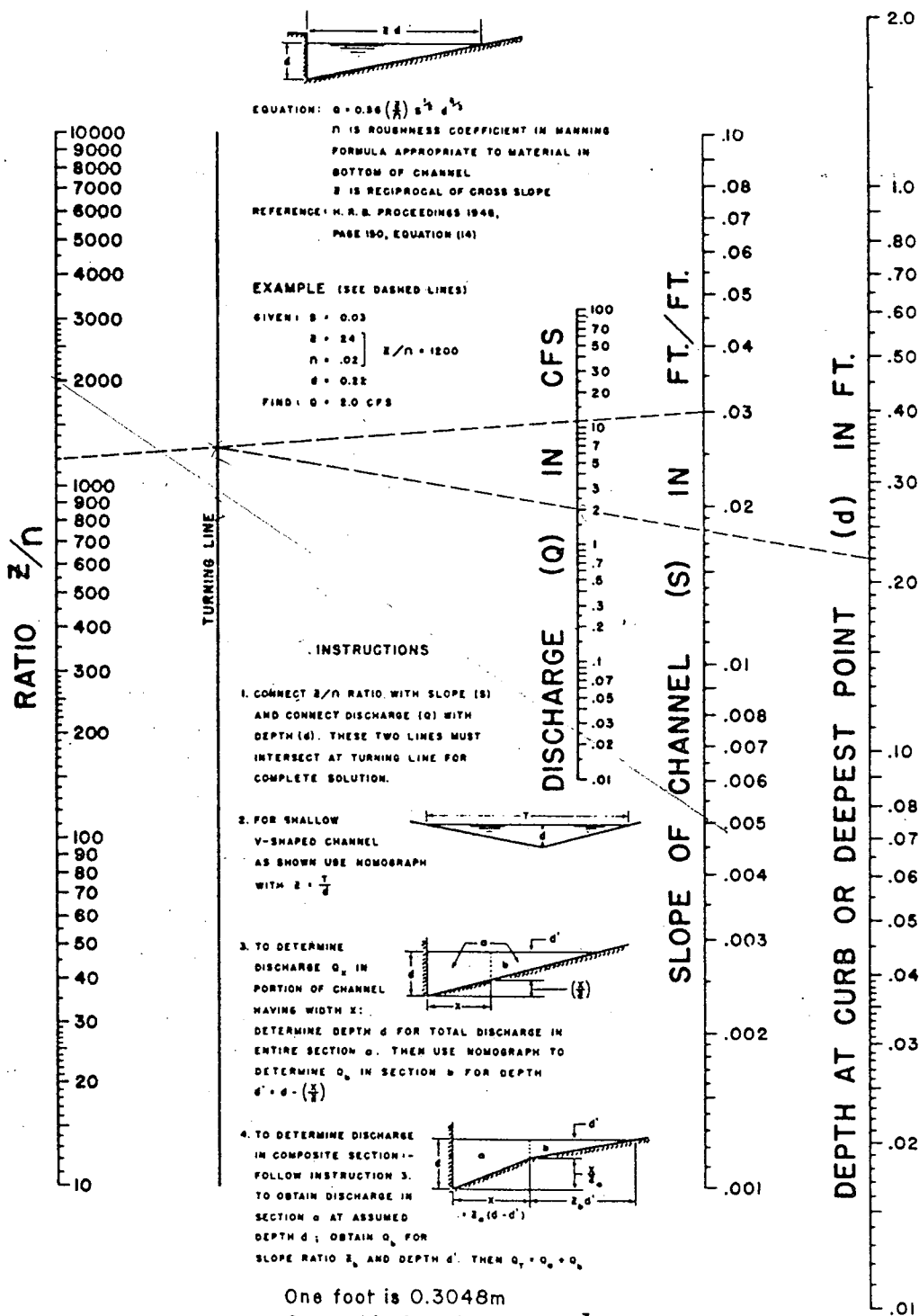
Pipe Size R x S (HE) S x R (VE) (Inches)	Approximate Equivalent Circular Diameter (Inches)	A Area (Square Feet)	R Hydraulic Radius (Feet)	Value of $C_1 = \frac{1.486}{n} \times A \times R^{3/2} = K$			
				n=0.010	n=0.011	n=0.012	n=0.013
14 x 23	18	1.8	0.367	138	125	116	108
19 x 30	24	3.3	0.490	301	274	252	232
22 x 34	27	4.1	0.546	405	368	339	313
24 x 38	30	5.1	0.613	547	497	456	421
27 x 42	33	6.3	0.686	728	662	607	560
29 x 45	36	7.4	0.736	891	810	746	686
32 x 49	39	8.8	0.812	1140	1036	948	875
34 x 53	42	10.2	0.875	1386	1260	1156	1067
38 x 60	48	12.9	0.969	1878	1707	1565	1445
43 x 68	54	16.6	1.106	2835	2395	2196	2027
48 x 76	60	20.5	1.229	3491	3174	2910	2686
53 x 83	66	24.8	1.352	4503	4094	3753	3464
58 x 91	72	29.5	1.475	5680	5164	4734	4370
63 x 98	78	34.6	1.598	7027	6388	5856	5406
68 x 106	84	40.1	1.721	8560	7790	7140	6590
72 x 113	90	46.1	1.845	10300	9365	8584	7925
77 x 121	96	52.4	1.967	12220	11110	10190	9403
82 x 128	102	59.2	2.091	14380	13070	11980	11060
87 x 136	108	66.4	2.215	16770	15240	13970	12900
92 x 143	114	74.0	2.340	19380	17620	16150	14910
97 x 151	120	82.0	2.461	22190	20180	18490	17070
106 x 166	132	99.2	2.707	28630	26020	23860	22020
116 x 180	144	118.6	2.968	36400	33100	30340	28000

TABLE 5

FULL FLOW COEFFICIENT VALUES
CONCRETE ARCH PIPE

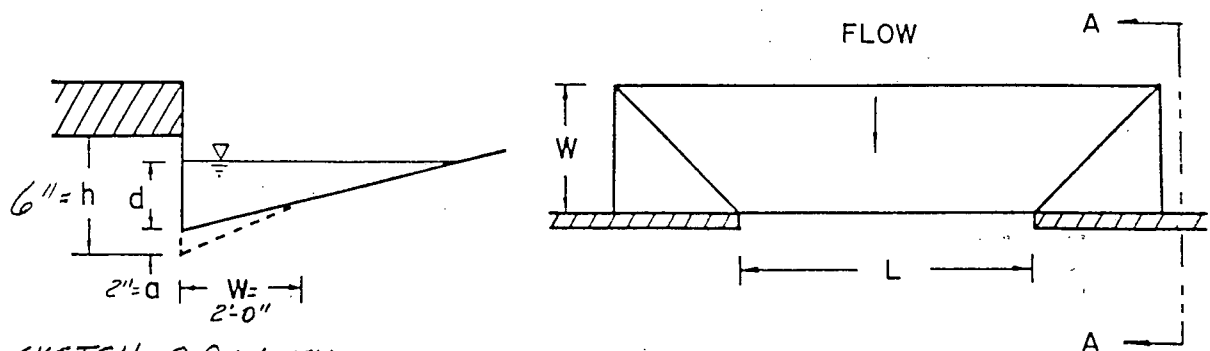
Pipe Size R x S (Inches)	Approximate Equivalent Circular Diameter (Inches)	A Area (Square Feet)	R Hydraulic Radius (Feet)	Value of $C_1 = \frac{1.486}{n} \times A \times R^{3/2} = K$			
				n=0.010	n=0.011	n=0.012	n=0.013
11 x 18	15	1.1	0.25	65	59	54	50
13 1/2 x 22	18	1.6	0.30	110	100	91	84
15 1/2 x 26	21	2.2	0.36	165	150	137	127
18 x 28 1/2	24	2.8	0.45	243	221	203	187
22 1/2 x 36 1/4	30	4.4	0.56	441	401	368	339
26 5/8 x 43 3/4	36	6.4	0.68	736	669	613	566
31 1/8 x 51 1/8	42	8.8	0.80	1125	1023	938	866
36 x 58 1/2	48	11.4	0.90	1579	1435	1315	1214
40 x 65	54	14.3	1.01	2140	1945	1783	1646
45 x 73	60	17.7	1.13	2851	2592	2376	2193
54 x 88	72	25.6	1.35	4641	4219	3867	3559
62 x 102	84	34.6	1.57	6941	6310	5784	5339
72 x 115	90	44.5	1.77	9668	8789	8056	7436
77 1/4 x 122	96	51.7	1.92	11850	10770	9872	9112
87 1/8 x 138	108	66.0	2.17	16430	14940	13690	12640
96 3/4 x 154	120	81.8	2.42	21975	19977	18312	16904
106 1/2 x 168 1/4	132	99.1	2.65	28292	25720	23577	21763

NOMOGRAPH FOR FLOW IN TRIANGULAR CHANNELS



$$\frac{1}{z} = \frac{3/8}{12} \quad z = 32$$

$$\frac{z}{n} = \frac{32}{0.016} = 2000$$



DEF. SKETCH, C.D.W. TYPE 1A INLET

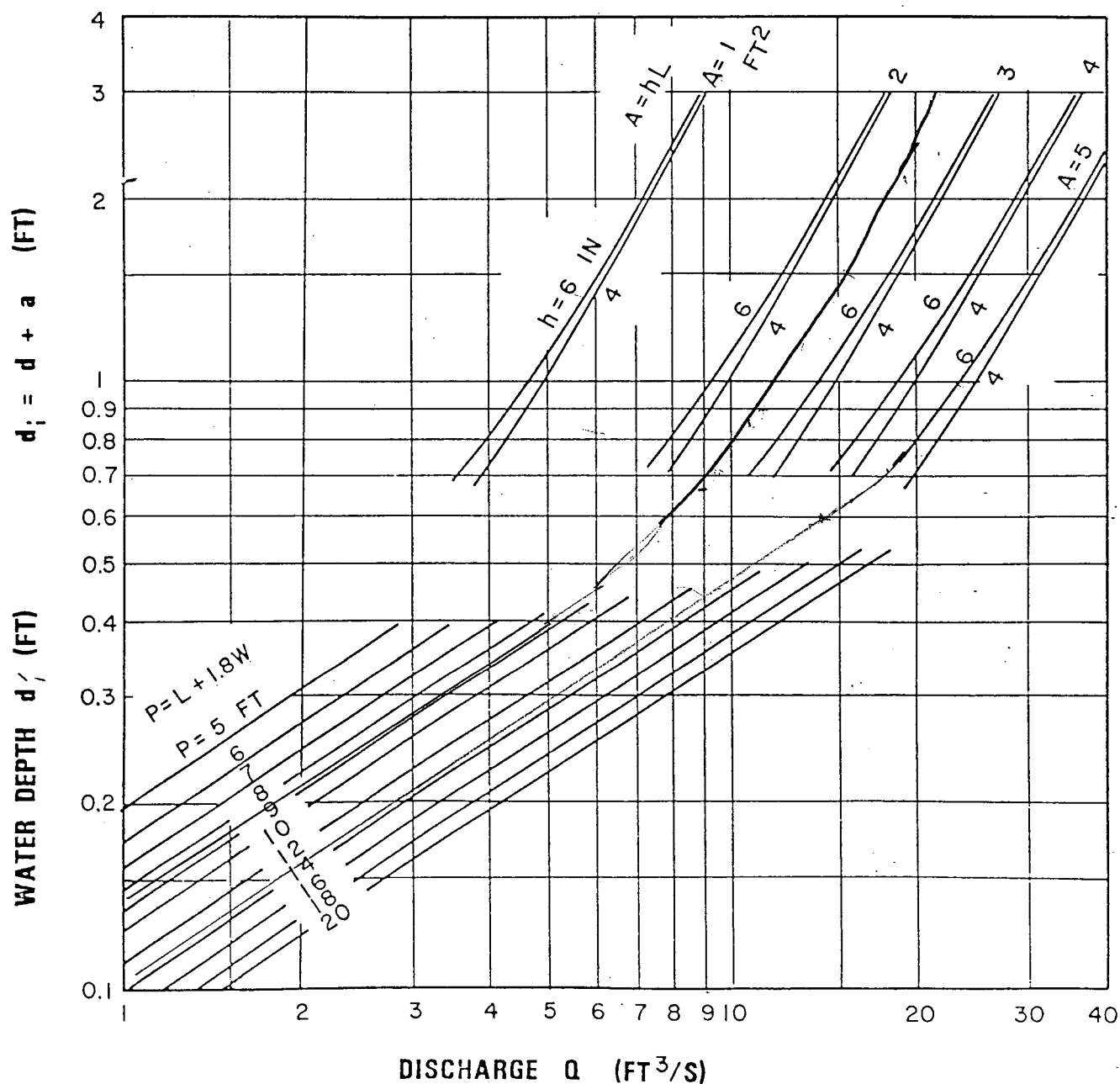


CHART 12. Depressed curb-opening inlet capacity in sump locations.

FROM: HEC-12, DRAINAGE OF HIGHWAY PAVEMENTS, F.H.W.A., MAR., 1984

SOIL LEGEND

SYMBOL	HYDROLOGIC Group	NAME
Aa	B	Albion-Shellabarger sandy loams, 1 to 4 percent slopes
Ab	B	Albion and Shellabarger sandy loams, 7 to 15 percent slopes
Ba	C	Blanket silt loam, 0 to 1 percent slopes
Bb	C	Blanket silt loam, 1 to 3 percent slopes
Ca	B	Canadian fine sandy loam
Cb	B	Canadian-Waldeck fine sandy loams
Cc	D	Carwile fine sandy loam
Cd	B	Clark-Ost clay loams, 1 to 4 percent slopes
Ce	C	Ciime silty clay, 3 to 6 percent slopes
Ea	B	Elandco silt loam
Eb	B	Elandco silt loam, occasionally flooded
Ec	B	Elandco silt loam, frequently flooded
Fa	B	Farnum loam, 0 to 1 percent slopes
Fb	B	Farnum loam, 1 to 3 percent slopes
Fc	B	Farnum loam, sandy substratum, 0 to 1 percent slopes
Ga	D	Goessel silty clay, 0 to 1 percent slopes
Gb	D	Goessel silty clay, 1 to 2 percent slopes
Ia	D	Irwin silty clay loam, 1 to 3 percent slopes
Ib	D	Irwin silty clay loam, 3 to 6 percent slopes
Ic	D	Irwin silty clay loam, 2 to 6 percent slopes, eroded
La	C	Lesho loam
Lb	A	Lincoln soils
Ma	B	Milan loam, 1 to 3 percent slopes
Mb	B	Milan loam, 3 to 6 percent slopes
Mc	B	Milan clay loam, 2 to 6 percent slopes, eroded
Na	B	Naron fine sandy loam
Oc	D	Owens clay loam, 1 to 3 percent slopes
Od	D	Owens-Rock outcrop complex, 3 to 10 percent slopes
Pa		Pits
Pb	D	Plevna fine sandy loam
Pc	A	Pratt loamy fine sand, undulating
Pd	A	Pratt-Tivoli complex, rolling
Ra	D	Renfrow silty clay loam, 1 to 3 percent slopes
Rb	D	Renfrow silty clay loam, 3 to 6 percent slopes
Rc	D	Renfrow-Owens clay loams, 1 to 4 percent slopes
Rd	D	Rosehill silty clay, 1 to 3 percent slopes
Sa	B	Shellabarger sandy loam, 1 to 3 percent slopes
Sb	B	Shellabarger sandy loam, 3 to 6 percent slopes
Sc	B	Shellabarger sandy loam, 3 to 6 percent slopes, eroded
Ta	D	Tabler silty clay loam
Tb	D	Tabler-Drummond complex
Ua	B	Urban land-Canadian complex
Ub	B	Urban land-Elandco complex
Uc	B	Urban land-Farnum complex, 0 to 3 percent slopes
Ud	D	Urban land-Irwin complex, 1 to 3 percent slopes
Ue	D	Urban land-Tabler complex
Va	B	Vanoss silt loam, 0 to 1 percent slopes
Vb	B	Vanoss silt loam, 1 to 3 percent slopes
Vc	B	Vanoss silt loam, 3 to 6 percent slopes
Vd	B	Vanoss silt loam, 3 to 6 percent slopes, eroded
Ve	D	Vernon sandy loam, 1 to 3 percent slopes
Vf	D	Vernon sandy loam, 3 to 6 percent slopes
Wa	C	Waldeck sandy loam
Wb	D	Waurika silt loam

(Joins sheet 27)

N



Mile

5,000 Feet

(Joins sheet 36)

Scale: 1:20000

380 000 FEET

(Joins sheet 43)

2365 000 FEET

FLOODING SOURCE		FLOODWAY			BASE FLOOD WATER SURFACE ELEVATION			
CROSS SECTION	DISTANCE ¹	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NGVD)	WITHOUT FLOODWAY (FEET NGVD)	WITH FLOODWAY (FEET NGVD)	INCREASE (FEET)
MIDDLE BRANCH GYPSUM CREEK								
A	1000	109	690	2.7	1339.7	1339.7	1340.3	0.6
B	1269	109	646	2.9	1339.8	1339.8	1340.4	0.6
C	1391	32	270	7.0	1340.6	1340.6	1340.6	0.0
D	1891	45	405	4.7	1341.2	1341.2	1341.9	0.7
E	3760	70	202	9.3	1346.8	1346.8	1346.8	0.0
F	3860	70	376	5.0	1348.0	1348.0	1348.5	0.5
G	5010	119	626	3.0	1349.4	1349.4	1350.3	0.9
H	5460	110	474	4.0	1350.1	1350.1	1350.8	0.7
M	12,627	60 ²	216	5.8	1363.1	1363.1	1364.0	0.9
N	12,821	80	478	2.6	1365.6	1365.6	1365.8	0.2
O	13,611	150	530	2.3	1366.2	1366.2	1366.9	0.7
P	15,301	75	399	3.1	1369.3	1369.3	1369.4	0.1
Q	15,457	75	276	4.5	1370.8	1370.8	1370.8	0.0
R	16,037	100	327	3.8	1372.6	1372.6	1373.4	0.8
S	16,882	100	479	2.6	1376.1	1376.1	1376.3	0.2

¹FEET ABOVE CONFLUENCE WITH GYPSUM CREEK

²THIS WIDTH IS BEYOND CORPORATE LIMITS

TABLE 4

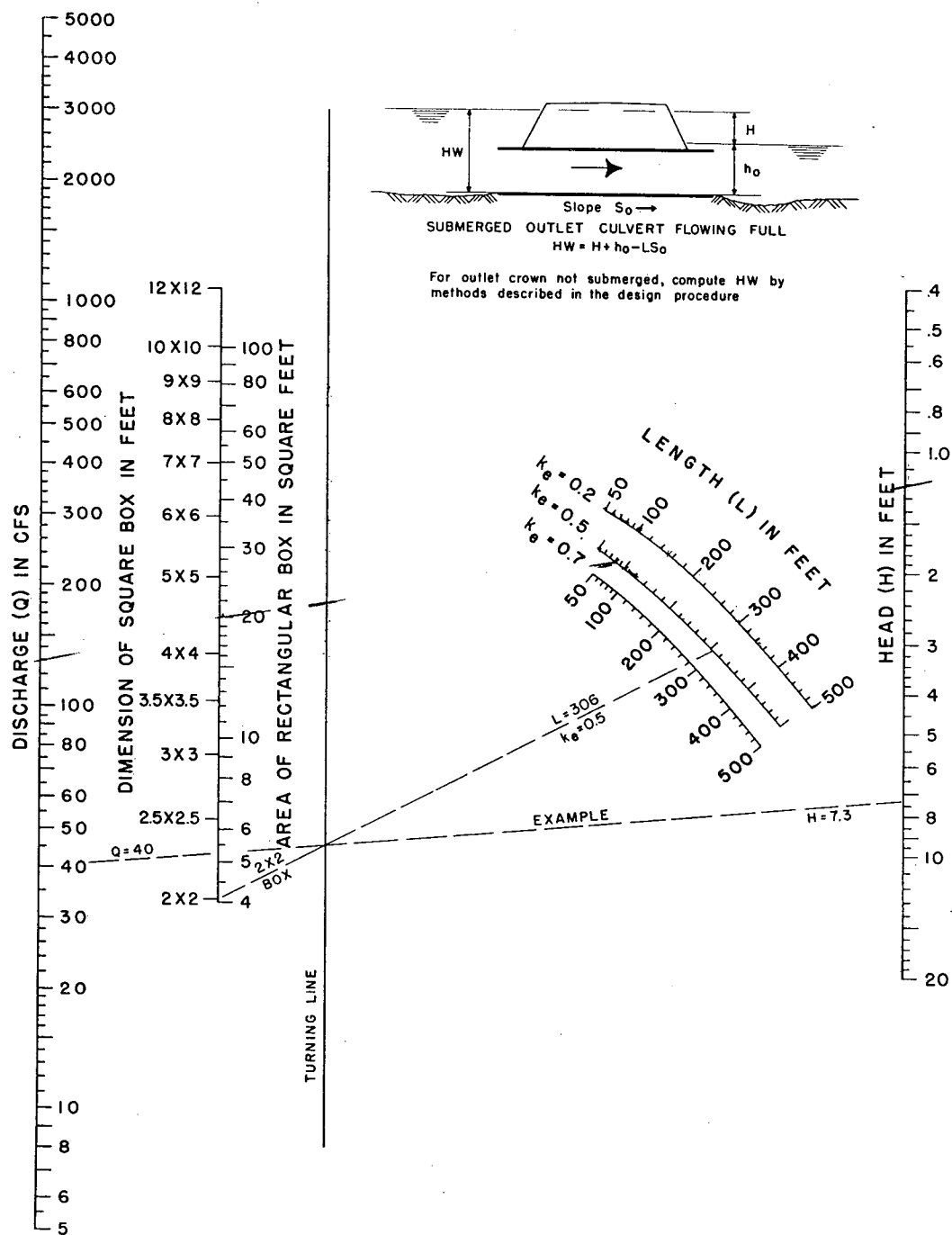
FEDERAL EMERGENCY MANAGEMENT AGENCY

CITY OF WICHITA, KS
(SEDGWICK CO.)

FLOODWAY DATA

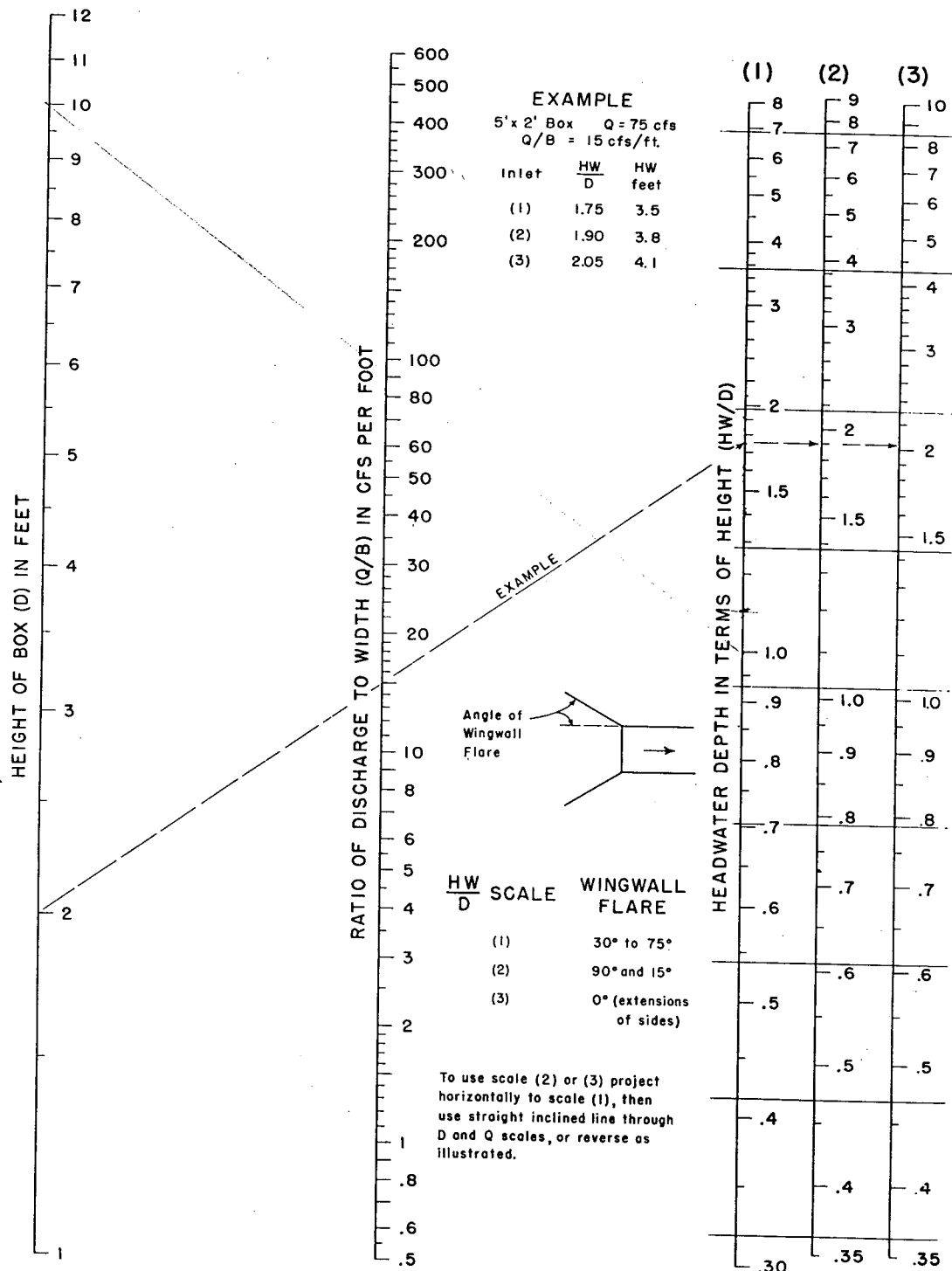
MIDDLE BRANCH GYPSUM CREEK

CHART 8

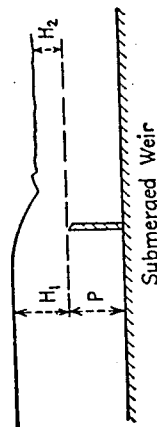


HEAD FOR
CONCRETE BOX CULVERTS
FLOWING FULL
 $n = 0.012$

CHART I



HEADWATER DEPTH
FOR BOX CULVERTS
WITH INLET CONTROL



WEIRS

5-19

the upstream side of the weir, H_1 , but also to the head on the downstream side, H_2 , and to a lesser extent, to the height of the weir crest above the floor of the channel, P . Early experiments by Francis (1848, 1883), Fteley and Stearns (1882), Bazin (1894), Cone (1916), and Cox (1928) have been summarized by Vennard and Weston.¹ They showed that the various test data could be presented in an orderly manner by selecting as variables Q/Q_1 and H_2/H_1 , where Q_1 is the discharge at the head H_1 , computed from the equation for free discharge (unsubmerged), which is expressed in general terms as follows:

$$Q_1 = CH_1^n \quad (5-49)$$

By plotting Q/Q_1 against H_2/H_1 , they found that the various data tended to fall on a single curve, except for small values of P/H_1 .

In 1947, Villemonte² presented the results of a series of tests on submerged sharp-crested weirs. He conducted tests on rectangular, triangular, parabolic, cusped, and proportional weirs. He showed that the results for all types could be represented by the single equation

$$\frac{Q}{Q_1} = \left[1 - \left(\frac{H_2}{H_1} \right)^n \right]^{0.385} \quad (5-50)$$

where n is the exponent in the free-discharge equation [Eq. (5-49)], and the other terms are as previously defined. This equation was found to satisfy all test results, with a maximum deviation of 5 per cent for some of the individual test results.

In 1949, Mavis³ presented results of tests on rectangular, triangular, parabolic, circular, sutor, and cusped weirs. He found that a single equation could be used to express the results for all the tests. His equation with subscripts changed to conform with usage in this book is

$$\frac{Q}{Q_1} = 1 - \left(0.45S + \frac{0.40}{2(10-10S)} \right) \quad (5-51)$$

¹ John K. Vennard and Ray F. Weston, Submergence Effect on Sharp-crested Weirs, *Eng. News-Record*, June 3, 1943, p. 818.

² James R. Villemonte, Submerged-weir Discharge Studies, *Eng. News-Record*, Dec. 25, 1947, p. 866.

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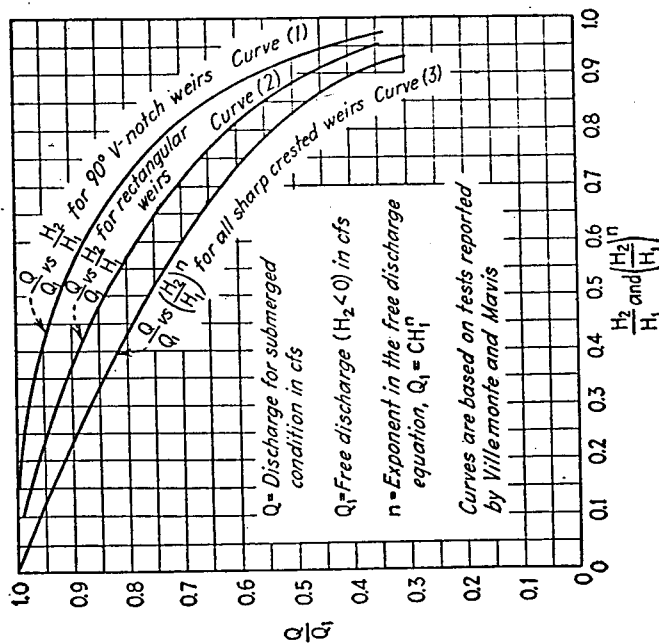


FIG. 5-5