

THE CITY OF WICHITA



DEPARTMENT OF PUBLIC WORKS
ENGINEERING DIVISION
CITY HALL — SEVENTH FLOOR
455 NORTH MAIN STREET
WICHITA, KANSAS 67202
(316) 268-4501

November 19, 1979

Professional Engineering Consultants
1440 East English
Wichita, KS 67211

ATTENTION CHRIS BRENNENSTUHL

Gentlemen:

Re: Drainage Plan: David's East 2nd Addition

This letter varifies the various points discussed in the telephone conversation last October about the drainage plan of the subject plat. In order to satisfactorily drain the plat, please submit the following additional information:

1. The plan shows 50 feet and 40 feet additional Drainage Easements north and west of the plat to be acquired by separate instrument. These easements shall be obtained prior to recording of this plat.
2. The plan shows a "temporary channel" that spreads out into the wide low area in the tract immediately to the south of the plat. The only access to the David's store off Kellogg Avenue is a road through the unplatted tract. The subdivision regulations do not permit drainage of public water across private property, therefore, in order to use the "temporary channel" as shown, a temporary drainage easement sufficiently wide to contain the runoff, shall be provided along the "temporary channel" alignment shown and then south along west line of the access road. The structure under access road shall be redesigned if necessary and complete design of this structure should be submitted. The potential flood water elevation in the area upstream from the structure under Kellogg is 1350.0 ft. Hence the access road shall be filled to elevation 1351.0. The minimum pad elevation for the south 100 feet of the plat shall be 1353.0 feet. The west bank of the proposed ditch west of the access road shall be at elevation 1351.0 feet or higher.
3. The ditch along north line of Kellogg Drive shall be constructed to contain the 100 year runoff in the "temporary ditch", and a sufficiently wide drainage easement to construct the ditch shall be obtained at the time of recording this plat.

THE CITY OF WICHITA

Chris Brenenstuhl
Page 2
November 19, 1979

4. The proposed building floor elevation shall be 1355.5 feet.
5. The developer shall guarantee the construction of the proposed channel and the installation of new structure under the access road if required.
6. Permanent drainage easement of sufficient width shall be provided and construction of such ditch guaranteed by the developer for draining the west roadside ditch along west line of Webb Road.

The above information should be submitted to the Engineering Department and Flood Control Office before final drainage plan can be approved. It is also strongly recommended to provide on site detention. By constructing a detention storage pond in the unplatted tract south of the plat. The existing structure under Kellogg flowing south is a 3-6 x 3 box having capacity of approximately 175 cfs for 1.0 ft. head above the box. It has also been established that the capacity of the existing channel south of Kellogg Avenue is very limited and flood damage to property is frequent in the area. The 100 year flow to box is estimated at 525 cfs.

Please feel free to call me at (316)268-4235, if you need additional information.

Very truly yours,

Yash D. Desai, P.E.
Drainage Chief Engineer

YDD/dla

cc: Jack Galbraith, Chief Planner - City of Wichita
Max Greene, Flood Control & Landfill Director - City of Wichita
Don Anderson, Director of Economic Development - City of Wichita

David's East 2nd Addition

1 Building floor Elevation should be 1355.50

2 Total drainage area at Box = 250 Ac

$$Q_{100} = 525 \text{ cfs}$$

$$\text{Existy RCB size} - 3 - 6' \times 3' \text{ FE} = 1343.8$$

$$\text{HW/Rise} = 1.85$$

$$\text{HW} = 5.55$$

$$\text{Flood water elev} = 1349.35'$$

Shaded area will be flooded.

3 East portion of lot and parking area drain south across property line to the unplatted area with no drainage easement. It will surface drain toward channel. Although the unplatted area is owned by the same owner.



MEMO

TO: Max Greene, P. E.
Director of Land Fill
and Flood Control
City Hall - 455 N. Main
Wichita, Kansas 67202

PROJECT NO. 30-78000-254

PROJECT: David's Replat

COPIES TO:

ATTN: Paul Johnston, P. E.

DATE: October 4, 1979

Yash Desai, P. E. ✓

FROM: John E. Scott

Louise Olivarez

REFERENCE: David's Replat

Revised Drainage Plan

PLEASE ADVISE IMMEDIATELY OF ANY MISCONCEPTIONS OR OMISSIONS YOU BELIEVE TO BE CONTAINED HEREIN.

Transmitted herewith is the Revised Drainage Plan for David's Replat. The added channel and Section 'BB' is as per plans previously approved by the City of Wichita Engineering Department. The design data for the channel has been already transmitted to Paul Johnston by Ron Pletcher of this office. The Final Plat will be filed October 22 and will be heard by the Subcommittee November 1, 1979.

If any additional information is required, please contact me as soon as possible.



MEMO

TO: Mr. Michael E. Lindebak, P.E.
City Engineer
7th Floor - City Hall
455 North Main
Wichita, Kansas 67202

PROJECT NO. 36-84019-2-177

PROJECT: Chelsea Brooke

Addition S/D 84116

DATE: December 21, 1984

COPIES TO:

ATTN:

Mr. Jeff Greenberg

FROM: Dick Linn

Mr. Jim Beckett

REFERENCE: Drainage problem at US-54 box culvert

PLEASE ADVISE IMMEDIATELY OF ANY MISCONCEPTIONS OR OMISSIONS YOU BELIEVE TO BE CONTAINED HEREIN.

The preliminary plat of Chelsea Brooke Addition was approved by the Subdivision Committee on December 6, 1984, subject to several conditions. One of the requirements is to submit a drainage plan to the City Engineer for review and approval. It was suggested by the Subdivision Committee that the City Engineer meet with representatives of Beech Aircraft Corporation to discuss the possibility of a detention system to minimize the downstream drainage problems.

The box culvert under Kellogg (US-54) has a limited capacity as well as the downstream drainage channel.

The drainage concept submitted with the preliminary plat provided for an open channel system along the north, west, and south perimeter of the Chelsea Brooke Addition. The channel would be sized to carry the 100-year storm runoff (without detention) from the 138-acre drainage basin on the Beech property, as well as the 19.2-acre Addition.

The 100-year storm runoff from the total drainage basin (247 acres) upstream from the box culvert is a total of 537 cfs (without detention). This runoff volume exceeds the capacity of the existing box culvert. If a 5-acre detention pond were constructed at the outlet to the 138-acre Beech drainage basin, the total runoff at the US-54 box culvert could be reduced to 450 cfs. The box culvert can pass this volume at HW elevation of 1348.5.

? (Area?)
Storage Vol
in Ac-ft

Attached is a summary of the drainage study data.

Please contact me if additional information is desired.

1. Need calculation to show a 5-acre detention pond has the storage capacity to reduce the peak run-off of the 138-Acre Beech drainage basin from 286 cfs to 40 cfs.
2. Is Beech agreeable to have the detention pond on their property?



Date 12/20/1984 Page _____ of _____

Project Chelsea Brooke Addn.

Item Summary of drainage study

I. Drainage to U.S.-54 Box Culvert

1. Drainage Area #1 (Beech)

D.A. = 138 acres (assumed 20% developed)

$Q_{100} = 286$ cfs

2. Drainage Area #2A (Beech)

D.A. = 27 Acres

$Q_{100} = 61$ cfs

3. Drainage Area #2B (Chelsea Brooke Addn.)

D.A. = 19.2 Acres

$Q_{100} = 121$ cfs

4. Drainage Area #3W (part of David's Site)

D.A. = 6 Acres

$Q_{100} = 51$ cfs

5. Drainage Area #3 (easterly portion of area)

D.A. = 68 acres

$Q_{100} = 250$ cfs

Total runoff at culvert (undetained) = 537 cfs

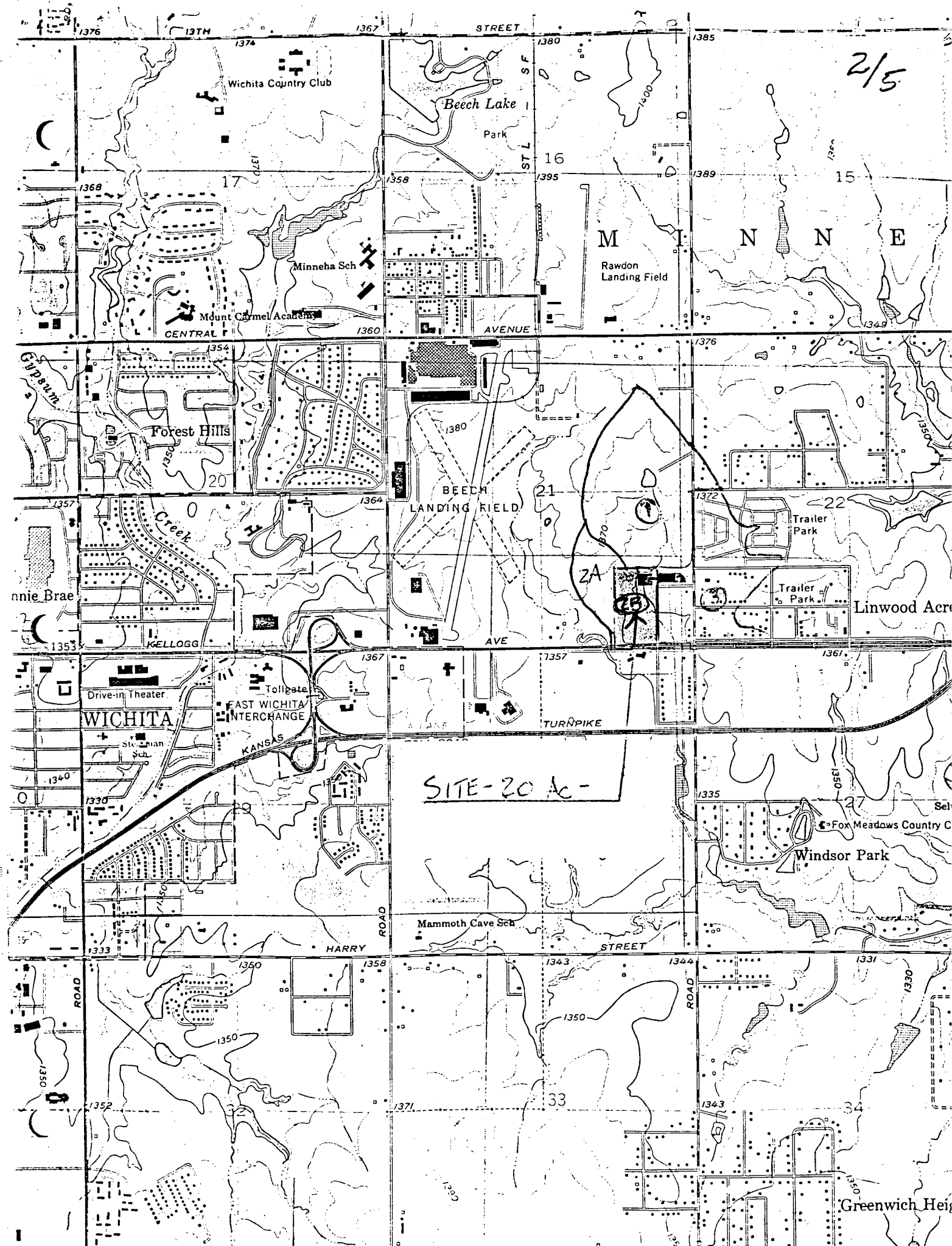
HW = 5.7' = elevation 1349.5

II. Drainage to Culvert with 5 acre detention pond

Beech outflow (D.A. #1) = 40 cfs

Q_{100} @ box culvert = 450 cfs

HW = 4.65' = elevation 1348.45



2/5

SITE-20 Ac

ZA

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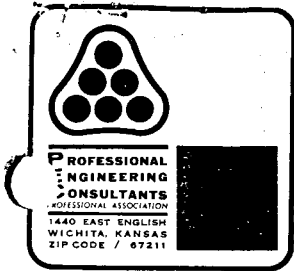
1371

1350

1343

1330

Greenwich Heig



Date 12/11/84 MMB Page 1 of

Project CHELSEA BROOKS ADD'N 36-84019-2

Item DESIGN FLOW FOR EXISTING 6x3 RCB

Assumptions

1) Inlet control governs, Outlet channel is assumed to have sufficient capacity to preclude a high tailwater condition.

2)

DA # 1

Ref: Notes 11/16/84, Sh 3 of 3

DA = 138 Ac
 20% Imp. (Present condition)
 D Soil
 CN = 84
 $\lambda = 4600'$
 Slope $Y = 2\%$
 25% H.L.M.
 $T_c = 53$ min.
 $C = 0.47$ (Ross Miller)
 $Q_{100} = 286$ cfs

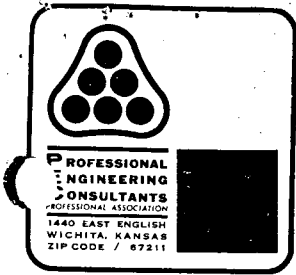
From Rating Curve attached

$V \approx 3.7$ ft/s
 $\lambda = 2000'$
 $T_t = 9$ min

$T_c + T_t = 62$ min
 $Q_{100} = 286$ cfs

DA # 2A

DA = 27 Ac
 0% Imp
 D Soil
 CN = 80
 $\lambda = 2000'$
 $Y = 2\%$ H.L.M. = 0%
 Lag = 0.39 hr
 $T_c = 39$ min
 $\lambda_{100} = 5.53$ in/hr
 $C = 0.41$ (Ross Miller)
 $Q_{100} = 61$ cfs
 $T_t = \frac{1000'}{3.5 \text{ ft/s}} = 5 \text{ min}$ $T_c + T_t = 44$ min.



Date 12-11-84 MWB Page 2 of

Project Chelsea Brooks Add 36-84019-2

Item Design Flow for Exist 3-6'x3' RCB

DA #2B

From notes of 11-16-84, as revised.

DA = 19.2 Ac

CN = 90

D Soil

$L = 1380'$

$Y = 1\%$

Assume 100% HLM

50% Imp (Composite)

$S = 1.11$

Log = 0.27 hr

$T_c = 12 \text{ min} \rightarrow \text{USE } 15 \text{ min}$

$C = 0.70$ (Rossmiller)

$Q_{100} = 121 \text{ cfs}$ ($T_t = 0$)

DA #3

$Q_{100} = 250 \text{ cfs}$ } From notes
 $T_c + T_t = 24 \text{ min}$ } 12/7/84 Sh 1.

DA #3W

$Q_{100} = 51 \text{ cfs}$ @ $T_c = 15 \text{ min}$

(From notes 12/7/84, Sh 1)

Combine Q_{100} 's

$286 + 3.85 \left(\frac{61}{5.03} + \frac{121}{8.98} + \frac{250}{7.48} + \frac{51}{8.98} \right) = 535$

$61 + 39 \left(\frac{286}{62} \right) + 5.03 \left(\frac{121}{8.98} + \frac{250}{7.48} + \frac{51}{8.98} \right) = 505$

$121 + 15 \left(\frac{286}{62} + \frac{61}{44} + \frac{250}{24} \right) + 51 = 418$

$250 + 24 \left(\frac{286}{62} + \frac{61}{44} \right) + \frac{7.48}{8.98} (121 + 51) = 537$

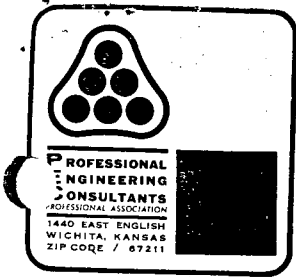
$\Sigma Q_{100} = 537 \text{ cfs}$ @ 6x3 RCB

W/ NO DETENTION

$G/B = 30$

$H/W = 5.7' = \text{elev } 1349.5$

only 0.2' below
Shoulder elev.



Date 12-11-84 MMB Page 3 of

Project Chelsea Brooke Add 36-84019-2

Item Design Flow at 3-6'x3' RCB

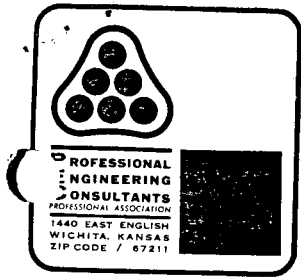
If detention by Beech is constructed, with 36" RCP outfall @ approx 40 cfs, find Q_{100}

Substitute 40 cfs @ $T_c = 24$ min 7
for 286 cfs @ 62 min

$$Q_{100} = 250 + 24 + \frac{24}{44} (61) + \frac{7.48}{8.98} (121 + 51)$$
$$= 450 \text{ cfs } 466 \text{ cfs}$$

$$HW = 4.65' = \text{elev} = 1348.45$$

Would flood grassed area south of exist parking lot, but would not flood parking lot itself
Shld El @ RCB = 49.7



Date 12-7-84 MWB Page 1 of 2

Project Chelsea Brooke Addition

Item _____

From DA #3

From Sh No 7 of calc's dated 6/28/83, which referenced US 54 - Greenwich calc's.

$$\left. \begin{array}{l} Q_{100} = 250 \text{ cfs} \\ Q_{10} = 169 \text{ cfs} \\ Q_5 = 145 \text{ cfs} \end{array} \right\} T_c = 20 \text{ min} \quad T_t = 4 \text{ min} \quad T_c + T_t = 24 \text{ min @ } 6 \times 3 \text{ RCB}$$

From DA #31W

From Sh No B dated 6/28/83

$$\left. \begin{array}{l} Q_{100} = 51 \text{ cfs @ } T_c = 15 \text{ min (By Rossmiller)} \\ Q_{10} = 35 \text{ cfs} \\ Q_5 = 30 \text{ cfs} \end{array} \right\}$$

From DA #2B

From Sh No 3 dated 11/16/84 (Revised)

$$\left. \begin{array}{l} Q_{100} = 121 \text{ cfs @ } T_c = 15 \text{ min} \\ Q_{10} = 81 \text{ cfs} \\ Q_5 = 69 \text{ cfs} \end{array} \right\}$$

Estimate 36" RCP from Beech @ 0.30%

$$K = 666 \quad (n = 0.013)$$

$$Q = K\sqrt{S} = 666 \sqrt{0.003} = 36 \text{ cfs} \Rightarrow \text{USE } 40$$

COMBINE Q at 6' x 3' RCB entrance

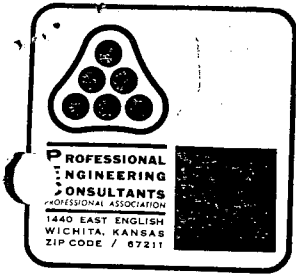
$$\begin{array}{lll} 15 \text{ min} & i_5 = 5.21 \text{ in/hr} & i_{10} = 6.08 \text{ in/hr} & i_{100} = 8.98 \text{ in/hr} \\ 24 \text{ min} & i_5 = 4.34 \text{ in/hr} & i_{10} = 5.07 \text{ in/hr} & i_{100} = 7.48 \text{ in/hr} \end{array}$$

$$\sum Q_5 = 145 + 40 + \frac{4.34}{5.21} (30 + 69) = 267 \text{ cfs} \quad \begin{array}{l} * \text{ HW for } 6 \times 3 \text{ RCB (Inlet control)} \\ \text{HW/D} = 0.98' \quad \text{HW} = 2.94' \end{array}$$

$$\sum Q_{10} = 169 + 40 + \frac{5.07}{6.08} (35 + 81) = 306 \text{ cfs} \quad \begin{array}{l} \text{HW/D} = 1.1' \quad \text{HW} = 3.3' \end{array}$$

$$\sum Q_{100} = 250 + 40 + \frac{7.48}{8.98} (51 + 121) = 433 \text{ cfs} \quad \begin{array}{l} \text{HW/D} = 1.5' \quad \text{HW} = 4.5' \end{array}$$

* The HW elev assumes Inlet Control, i.e., the downstream channel & structures do not cause sufficient tailwater to force outlet control operation.



Date 12-7-84 MNB Page 2 of 2

Project Chelsea Brook Addition

Item _____

Estimate H.G.L. slope

$$L = 1600'$$

$$\begin{array}{r} \text{E@ Box} = 1343.6 \\ + \quad 4.5 \\ \hline 1348.1 \end{array}$$

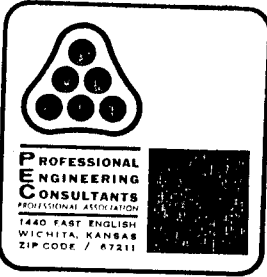
Est 3 structures w/ 0.25' head loss each

$$\begin{array}{l} \text{E@ outlet of pond} = 1349 \\ \text{HW@ pond} = \text{elev } 1353.5 \end{array}$$

$$\frac{1353.5 - 3 @ 0.25' - 1348.1}{1600} = 0.0029 \text{ ft/ft}$$

$K = 666 \text{ (} n = 0.013, 36" \phi \text{ RCP)}$

$$Q = KVS = 666 \sqrt{0.003} = 36.5 \text{ cfs}$$



Date _____ Page 2 of _____
 Project _____
 Item _____

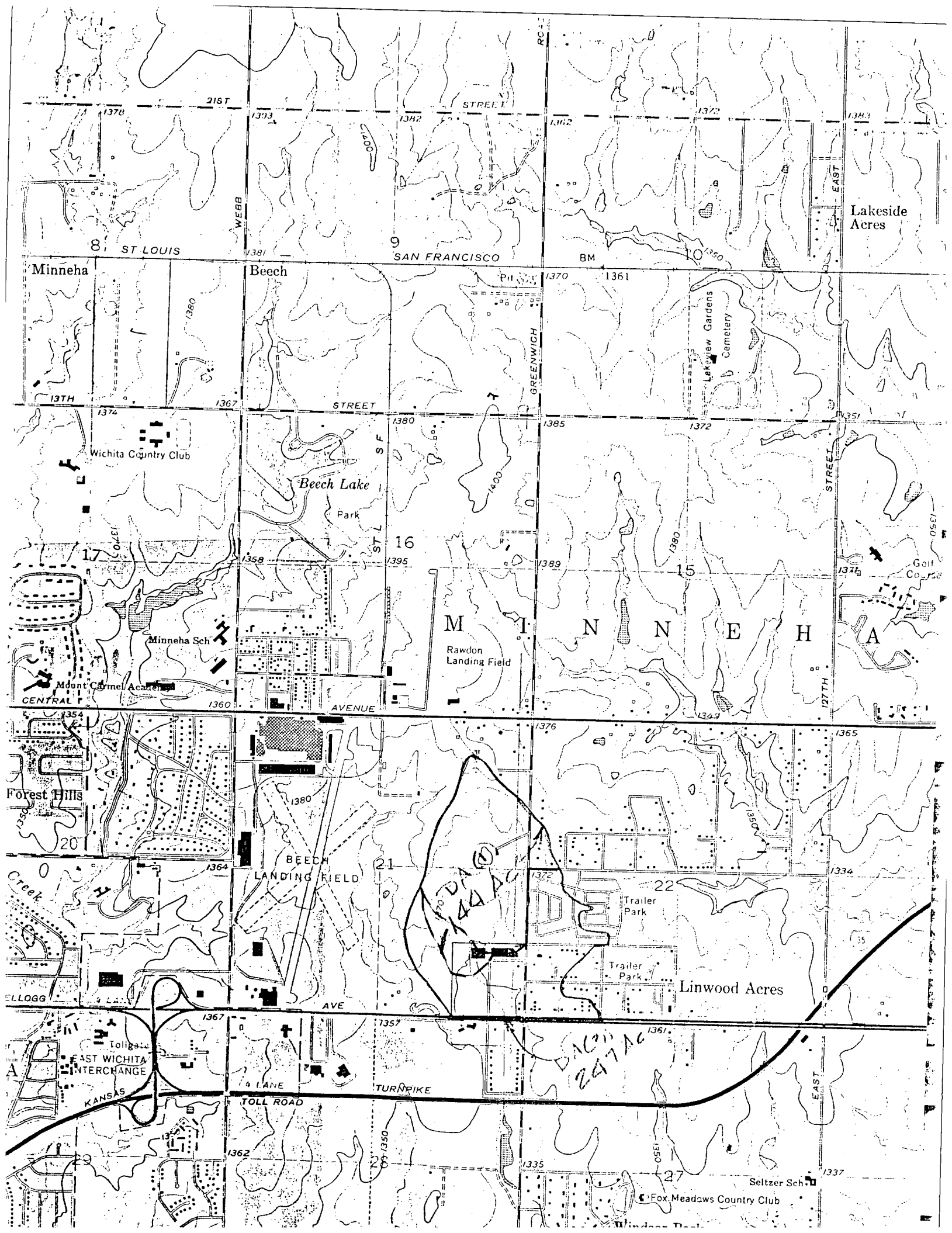
ALTERNATE II: CHANNEL DESIGN FOR SIMILAR DEVELOPMENT

DRAINAGE AREA	DA (Ac.)	C	L (MI)	H (FT)	L _c (MIN)	Q ₁₀₀ (IN/HR)	Q ₁₀₀ (CFS)
→ 1	138	0.42	0.87	40	32.1	6.44	<u>368</u>
2	185	0.40	0.98	42	36.3	5.85	<u>432</u>
→ 3	250	0.40	1.14	45	41.7	5.25	<u>525</u>
4	255	0.37	1.42	47	53.0	4.35	412

CHANNEL DESIGN

B = 50.00'
 n = 0.030
 z = 4

S =	0.10%	0.15%	0.20%	0.25%	0.30%	0.35%	0.4%
Q _{DES} = 368	2.42' 2.54 FPS 366 CFS (-0.44%)	<u>2.15'</u> 2.90 FPS 365 CFS (-0.76%)	1.99' 3.20 FPS 368 CFS (-0.09%)	1.83' 3.43 FPS 364 CFS (-0.25%)	1.75' 3.63 FPS 363 CFS (-1.32%)	1.68' 3.82 FPS 363 CFS (-1.32%)	1.61' 3.99 FPS 364 CFS (-1.11%)
Q _{DES} = 432	2.65' 2.68 FPS 429 CFS (-0.65%)	<u>2.36'</u> 3.06 FPS 429 CFS (-0.66%)	2.17' 3.37 FPS 429 CFS (-0.80%)	2.04' 3.63 FPS 431 CFS (-0.27%)	1.93' 3.85 FPS 430 CFS (-0.50%)	1.84' 4.04 FPS 428 CFS (-1.03%)	1.77' 4.22 FPS 426 CFS (-1.22%)



Lakeside Acres

Minneha

Beech

ST LOUIS

SAN FRANCISCO

Wichita Country Club

Beech Lake

Park

Minneha Sch

MINNEHA

Rawdon Landing Field

Forest Hills

BEECH LANDING FIELD

Trailer Park

Linwood Acres

EAST WICHITA INTERCHANGE

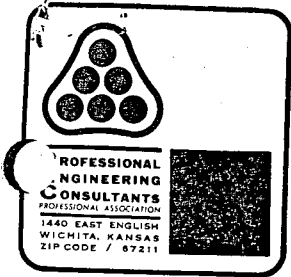
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Seltzer Sch

Fox Meadows Country Club

DAN 26776



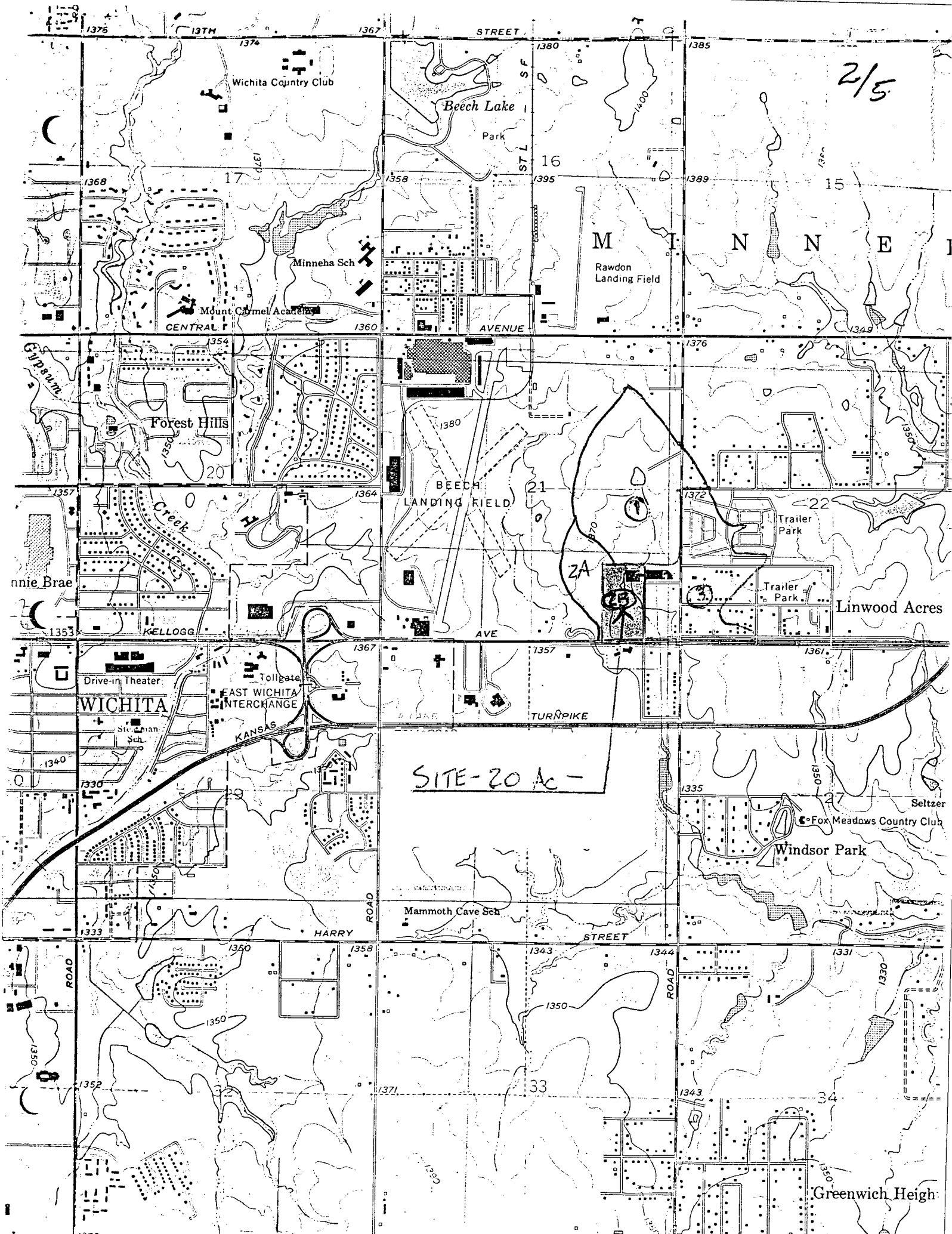
Date 11-16-84 MAB Page 1 of 5

Project CHELSEA BROOKE 36-84019-2

Item DRAINAGE PLAN CALC'S

ASSUMPTIONS & METHODOLOGY

- ① Undeveloped runoff (Q_{UD}) from Beech DA #1 will be carried along the north & west sides of the plat (DA=138 Ac.) Assume 20% Impervious (Present cond.)
- ② Developed runoff (Q_{D}) from plat will be added in ditch along south side of plat. (DA #2B) (Assume industrial development, 72% Imp.)
- ③ Hydrology will be by Rossmiller Modified Rational Method, with T_c by Modified Curve No. Method (Eq. 3-2, TR-55 by SCS)
- ④ West berm of ditch along west side of property is assumed to direct Beech drainage from west. (DA #2A)
- ⑤ Adequate outfall capacity at Kellogg is assumed. (Existing 6x3 RCP & outfall channel are presently undersized)



2/5

SITE-20 Ac

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21

15

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27

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34

17

20

30

32

31

Greenwich Heigh

Wichita Country Club

Beech Lake Park

Minneha Sch

Mount Carmel Academy

Forest Hills

Beech Landing Field

Linwood Acres

WICHITA

EAST WICHITA INTERCHANGE

Windsor Park

Seltzer

Fox Meadows Country Club

Mammoth Cave Sch

nnie Brae

Drive-in Theater

Tollgate

St. Julian Sch

ROAD

HARRY ROAD

STREET

ROAD

CENTRAL

AVENUE

AVE

TURPIKE

KELLOGG

WICHITA

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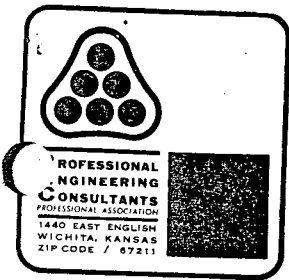
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CENTRAL

AVENUE



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Project CHELSEA BROOKE

Item DRAINAGE PLAN

DA #1

DA = 138 Ac

20% Imp

D Soil

$CN = 0.2 \times 98 + 0.8 \times 80 = 84$

$L = 4600'$

slope (Y) = 2%

Assume 25% H.L.M.

$S = \frac{1000}{CN} - 10 = 1.96$

$L = \frac{L^{0.8}(S+1)^{0.7}}{1900 \sqrt{Y}} = 0.68 \text{ hr}$

$F_{imp} = 0.57 \quad F_{full} = 0.87$

$T_c = \frac{60}{0.6} F_{imp} F_{full} L = 53 \text{ min}$

$\mu_{100} = 4.35 \text{ in/hr}$

$C = 0.47$ (By Rosiniller Nemograph)

$Q_{100} = 286 \text{ cfs}$

DESIGN Q_{100} FOR REACH 1 = 286 cfs

DA #2B

DA = ¹⁵20 Ac

72% Imp

D Soil

D.A. = 4.2 Ac. Fldwy
0% Imp.

$CN = 0.72 \times 98 + 0.28 \times 80 = 93$

$[0.72 \times 98 + 0.28 \times 80] / 15 + 80(4.2) / 19.2 = 90$

$L = 1300'$

slope = 1% = Y

Assume 100% H.L.M.

56% overall imp.

$S = \frac{1000}{CN} - 10 = 0.76$

$L = \frac{L^{0.8}(S+1)^{0.7}}{1900 \sqrt{Y}} = 0.24 \text{ hr}$

$F_{imp} = 0.78 \quad F_{full} = 0.58$

$T_c = \frac{60}{0.6} F_{imp} F_{full} L = 12.2 \text{ min}$

USE $T_c = 15 \text{ min}$ ✓

(APPARENTLY METHOD NOT TOO ACCURATE FOR HIGHLY IMPERVIOUS AREAS)

$\mu_{100} = 6.98 \text{ in/hr}$

$C = 0.79 \quad 0.70$

$Q_{100} = 142 \text{ cfs} \quad 121$

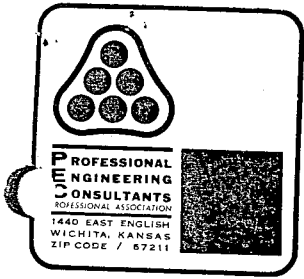
Combine for Q_{100}

$Q_{100} = 142 + \frac{15}{53} (286) = 223 \text{ cfs}$

OR

$286 + \frac{4.35}{6.98} (121) = 344 \text{ cfs}$

DESIGN Q_{100} FOR REACH 2 IS 344 cfs



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Project CHELSEA BROOK

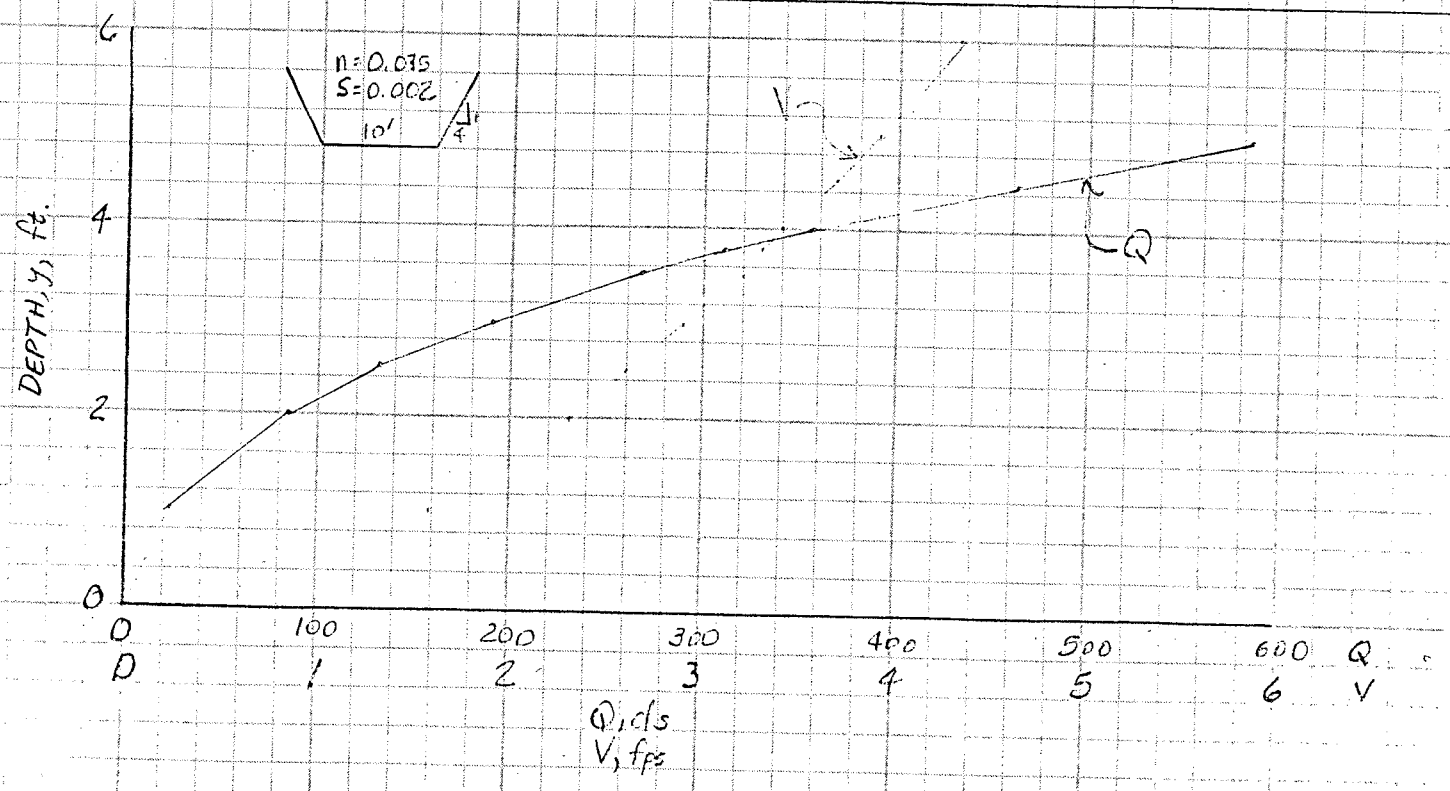
Item Ditch size

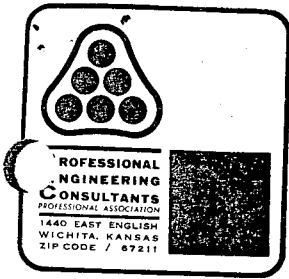
y, ft	A, ft^2	$Q, ft^3/sec$	$V, ft/sec$
1	14	22	1.6
2	36	84	2.3
2.5	50	132	2.6
3	66	192	2.9
3.5	84	267	3.2
3.75	94	310	3.3
4	104	357	3.4
4.5	126	462	3.7
5	150	584	3.9
6	204	883	4.3

Choose 10' bottom w/ 4:1 side slopes
 $n=0.035$ $S=0.002$ ft/ft

For Reach 1:
 $Q_{100} = 286 cfs, y = 3.7$ ft $V = 3.2$ ft/sec

For Reach 2:
 $Q_{100} = 344 cfs, y = 4.0$ ft, $V = 3.4$ ft/sec





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Project CHELSEA BROCKLE

Item SELECT R.C. BOX SIZE

Ref: HEC-5 Hydraulic Charts for the Selection of Highway Culverts

Inlet control Chart 1

Let HW depth: = 5'
 Assume $K_c = 0.2$ (45° wings, rounded top)
 $Q = 354 \text{ cfs}$
 344

D	HW/D	Q/B	B req'd
3	1.67	26	13.6 14x3
4	1.25	30	11.8 12x4
5	1.00	33	10.7 11x5

Outlet control

Assume Total available head
 would be 1' surcharge +
 $(300' @ 0.50\% = 0.6) = 1.6'$

$L = 300'$ Chart 8
 $K_c = 0.2$

$A = 48 \text{ ft}^2$

Use 2-6x4x300' R.C.B

Cost estimate

Rebar 8.3 CY
 Barrel 5000 0.51 243 CY

$\approx 250 \text{ CY}$
 @ \$310/CY for steel + conc
 = \$77,500

USE \$50 K.