

PROFESSIONAL
ENGINEERING
CONSULTANTS
PROFESSIONAL ASSOCIATION

GOLDEN HILLS ADDITION

DRAINAGE PLAN
AND
SUPPORTING CALCULATIONS

JUNE 7, 1985

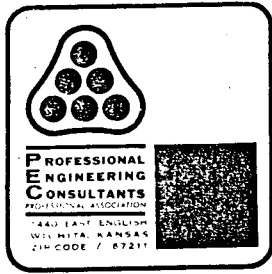
OWNER: SUNRISE ENTERPRISES, LTD.
P.O. BOX 131
GODDARD, KANSAS 67052

ENGINEER: PROFESSIONAL ENGINEERING CONSULTANTS, P.A.
1440 EAST ENGLISH
WICHITA, KANSAS 67211

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WICHITA, KANSAS 67211



MEMO

TO: File

PROJECT NO. 36-85032-

PROJECT: Golden Hills

Drainage Plan

DATE: 6/4/85

COPIES TO:

ATTN:

M.E. Lindebak, P.E.,

FROM: Michael W. Berry, P.E.

Attn: C. Breitenstein, P.E.

REFERENCE: Drainage Plan Computations

PLEASE ADVISE IMMEDIATELY OF ANY MISCONCEPTIONS OR OMISSIONS YOU BELIEVE TO BE CONTAINED HEREIN.

Attached hereto are the computations for the referenced drainage plan.

The publication "Interim Drainage and Storm Sewer Policy for Design Criteria and Documentation, City of Wichita," noted ~~"Tentative" and dated 5/2/85,~~ ^{revised 7/1/87} as provided by D.E. Schneider of the MAPD, Division of Design, was used as a guide for the hydrologic and hydraulic computations. This publication is hereinafter referred to as the "Policy Manual." This ~~"Policy Manual" was used for this project as a test of the procedures given therein.~~

Manual #1, as referenced ^{therein} herein, refers to "Design of Urban Highway Drainage - The State of the Art," by Reitz & Jens, Inc., April, 1980. Manual #2 refers to "Drainage of Highway Pavements, Hydraulic Engineering Circular #12," by Tye Engineering, Inc., March, 1984.

HYDROLOGY METHODS

The rational method was used for hydrologic analysis. Runoff coefficients were based on the table provided in Attachment D, of the "Policy Manual." ~~The average lot in this development is 1/6 Ac; thus, the average of the 1/8 and 1/4 Ac values was used for C.~~

The time of concentration for overland flow was determined by either the velocities given in Attachment E, of the "Policy Manual" or by the Kinematic Wave Theory, as presented in Section 4.1.3, of Manual #2. Time of travel in street gutters was determined by the method used in Section 4.1.3, of Manual #2. ¹⁵ The minimum time of concentration for design purposes was taken to be ten minutes, ~~for single-family areas and five minutes for commercial and/or multi-family areas.~~

The two-year ^{return period} design storm was used ^{as the basis of design, per Table 1 of the "Policy Manual"} for basins which do not discharge onto arterial streets. The five-year design storm was used for basins discharging onto arterial streets. ~~In all cases,~~ a check was made that the 100-year runoff was confined to the right-of-way.

Also,

HYDRAULIC DESIGN

For each inlet, street flooding and inlet capacity was checked for the minor storm. Conveyance in the street was based on the modified Manning Eq:

$$Q = 0.56/n(S_x)^{5/3}(T)^{8/3}\sqrt{S} \quad (\text{Eq. 4, Manual \#2})$$

It was assumed that t_c , for street flow, was equal to t_c , for pipe flow. This should be a conservative assumption.

For local streets, curb-deep flow is tolerable for the minor storm. For collectors, a single eight-foot center lane should remain unflooded for the minor storm. ~~For arterials, one eight-foot lane in each direction should remain unflooded for the five-year storm.~~

Inlet capacities were determined by the methods presented in Manual #2, using charts 9, 10, and 12. Carryover flows were added to the next inlet downstream.

In this analysis, City of Wichita Type 1A Inlets, 3/8 in/ft street cross-slope, and 6-5/8 Std. curb and gutter were assumed to be utilized.

Pipe systems were designed using the calculated capacity of each inlet, ^{on the basis of a} ~~System 450 and System 300 were designed for a five-year minor storm because they~~ ^{Sys- two year storm} ~~adjoin arterial streets. All other systems were designed on the basis of a~~ two-year minor storm.

Preliminary pipe sizes were estimated and tabulated ^{under "conduit Data",} ~~on the "Hydrology Data Sheets."~~ Fine-tuning of the pipe design was performed using PEC's Storm Program. ^{was used} This program uses Manning's Equation to calculate friction losses in pipes flowing full. Minor losses are accounted for using conservation of momentum principles. It is desirable to keep the hydraulic grade line approximately one-foot ^{6 inches} below the ~~top of curb~~ ^{flow line} elevations. Several trials were made; only the ~~computations for the best system are printed herein.~~

MAJOR STORM OVERFLOW

For each subarea, a check was made for conveyance capacity of the major storm. To simplify analysis, the following assumptions were made:

1. The time of concentration is identical for both the major and minor storm. Thus, a ratio of rainfall intensities is used to determine Q_{100} @ each point.
2. The pipe system capacity during the major storm is assumed to be the same as during the minor storm. This is a conservative assumption, because increased ponding depths during the major storm event will increase the available head on the inlet/pipe system, thus increasing the capacity.

Page 3 The conveyance capacity of the street RLW's was calculated for several gradients, and used as a check against tabulated discharges for the 100yr event

3. ~~Street conveyance was analyzed using only the street width. Depths above the curb up to the walk grade were used, but the conveyance of the parking was neglected. In general, the parking area conveyance is quite small, due to the relatively higher n-factor. Again, Eq. 4, of Manual #2, was used.~~

In general, ^{if} the minimum grade at the right-of-way line is 0.3' above the top of the curb. ~~Where~~ ^{such} walk grades higher than minimum are required to confine the major storm overflow, ^{such} walk elevations are shown on the drainage plan. ^{will be noted and identified.}

END

GENERAL SUMMARY OF SYSTEMS

For systems 100, 700 and 800, the minor storm is conveyed through pipe systems and the major storm is conveyed through the streets to Reserves B or C. Rear lot drainage around the perimeter of the plat is assumed to drain out across the plat boundary.

For systems 300 and 450, the minor storm (five-year) discharge is conveyed through pipes and the major storm (100-year) discharge is conveyed through street rights-of-way to either Central Ave. or 119th Street West. It is presumed that the 100-foot arterial street rights-of-way will convey the major storm overflow.

For system 500, the minor storm (two-year) is conveyed in a pipe system with an outfall on the east side of 119th Street West. No accounting of 119th Street drainage or any areas west of 119th Street West was made for the design of this outfall. Separate analysis and design will be required for this area. It might be advantageous for the City/County officials to fund this analysis and design, and to upsize the proposed 42" conduit to handle the area lying outside of the Golden Hills plat. The outfall will daylight in the east ditch of 119th Street West and will be conveyed to Cowskin Creek.

The major storm overflow is routed at Hickory and at Bekemeyer (through a flume) to 119th Street West right-of-way. The right-of-way is presumed to have capacity to convey this flow.

FEMA FLOODPLAIN REQUIREMENTS

Portions of Blks 10 and 12 lie within the regulatory floodplain of Cowskin Creek. The minimum pad elevation for these lots shall be one-foot above the 100-year design water surface and are as follows:

Blk. 10, Lots 20 thru 52	1332.30 M.S.L.	144.8
Blk. 10, Lots 53 thru 61	1331.60 M.S.L.	144.2
Blk. 12, Lots 16 thru 24	1331.60 M.S.L.	144.2

MWB/mkm



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Project Golden Hills Drainage Plan

Item System 100 - Shefford

RECURRENT INTERVAL, YEARS (2) 5 10 25 50 100

RE	OVERLAND FLOW				GUTTER FLOW							HYDROLOGY				
	L ft	S _o Ext ft/ft	V ^N ft/sec	t _o min	T _a /T _z	L ft	S _x in/ft	S _o %	V ft/s	t _g min	t _o = t _g + t _z min	T ft	C	i in/hr	A Ac	Q cfs
0	125	0.01	0.7	3	0	780	3/8	1.19	2.5	5.3	8.3	11	0.48	7.25	2.8	9.74
0	125	0.01	0.7	3	0	300	3/8	0.43	2.3	2.2	10.5	13	0.48	4.66	2.8	6.3
0	125	0.01	0.7	3	0	230	3/8	0.86	1.63	2.4	5.4	4	0.48	7.25	5.8	20.2
0	125	0.01	0.7	3	0.3	780	3/8	1.19	2.7	4.8	10.2	12	0.48	4.35	5.8	12.1
0	125	0.01	0.7	3	0.9	300	3/8	0.43	2.3	2.2	12.4	13	0.48	4.35	5.8	12.1
30	125	0.01	0.7	3	0	110	3/8	0.32	0.5	3.4	6.4	3	0.52	3.78	5.5	10.8
30	125	0.01	0.7	3	0.5	330	3/8	0.32	1.0	5.5	11.9	6	0.52	3.78	5.5	10.8
30	125	0.01	0.7	3	0.4	670	3/8	1.83	3.1	3.6	15.5	6	0.52	3.78	5.5	10.8
30	125	0.01	0.7	3	0.4	250	3/8	0.43	2.0	2.1	17.6	14	0.52	3.78	5.5	10.8
30	125	0.01	0.7	3	1.0	20	3/8	3.00	5.2	0.4	18.0	9	0.52	3.78	5.5	10.8
40	125	0.01	0.7	3	0	150	3/8	0.60	2.1	1.2	4.2	6	0.52	3.78	5.5	10.8
40	125	0.01	0.7	3	0.6/6	350	3/8	3.37	4.2	1.4	5.6	6	0.52	3.78	5.5	10.8
40	125	0.01	0.7	3	0.6/6	240	3/8	2.83	4.7	0.9	6.5	8	0.52	3.78	5.5	10.8
40	125	0.01	0.7	3	0.8/14	320	3/8	0.32	1.9	2.9	10	14	0.52	3.78	5.5	10.8
50	100	0.01	0.7	2.4	0	250	3/8	0.43	1.1	3.8	6.2	7	0.48	4.75	1.74	4.0
50	100	0.01	0.7	2.4	0	175	3/8	3.00	4.2	0.7	6.9	6.5	0.48	4.75	1.74	4.0
50	100	0.01	0.7	2.4	0.6	280	3/8	0.32	1.6	2.9	10	11	0.48	4.75	1.74	4.0
160	100	USE	10 min	T _c	0								0.48	4.75	0.5	1.1
190	100	USE	10 min	T _c	0								0.48	4.75	0.6	1.4

Component is 1/16" diameter

3/8"

T_c

T_c

Soil

Soil



Date 5/28/85 Page 2 of 2

Project GOLDEN HILLS DRAINAGE PLAN

Item SYSTEM 100 CON'T.

RECURRENCE INTERVAL, YEARS (2) 5 10 25 50 100

REB	OVERLAND FLOW			GUTTER FLOW							HYDROLOGY						
	L ft	S _o ft/ft	V ft/sec	t _o min	T ₁ /T ₂	T _a /T _z	L ft	S _x	S _o	V ft/s	t _g min	t _c =t _o +t _g min	T ft	C	i in/hr	A Ac	Q cfs
70	125	0.01	0.7	3	0	0.65	500	3/8	4.0	3.6	2.3	5.3	8	0.48	4.75	3.2	7.3
100	125	0.01	0.7	3	0.6	0.82	350	3/8	0.32	1.9	3.1	10	14	0.48	4.75	2.4	5.5



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Project GOLDEN HILLS DRAINAGE PLAN

Item SYSTEM 300 CENTRAL AVE

RECURRENCE INTERVAL, YEARS 2 (5) 10 25 50 100

res	OVERLAND FLOW				GUTTER FLOW							HYDROLOGY					
	L ft	S _o ft/ft	V ft/sec	t _o min	T ₁ /T ₂	T _a /T _e	L ft	S _x	S _o	V ft/s	t _g min	t _g +t _o min	T ft	C	i in/hr	A Ac	Q cfs
10	140	0.01	0.7	3.3	0	0.65	575	3/8"	1.10	1.9	5.0	10	8	0.57	6.11	1.4	4.9
20	140	0.01	0.7	3.3	0	0.65	600	"	0.86	1.95	5.1	8.4	11	0.57	6.11	2.9	10.1
25	800	0.01	2.0	6.7	0	0.65	350	"	1.10	3.7	1.6	10	13	0.57	6.11	2.9	10.1
1 K.W.	800	"	"	9.0	0	0.65	850	"	0.4	1.9	7.4	9.0	17	0.73	6.36	4.7	21.8
30	75	0.01	0.7	1.8	0	0.65	850	"	0.4	1.5	9.3	11.1	12	0.54	5.87	2.4	7.6
50	90	0.01	0.7	2.2	0	0.65	500	"	0.32	2.1	6.2	10	12	0.57	6.11	1.6	5.6
60	USE	T _e = 12 min															
80	USE	T _e = 10 min															
100	USE	T _e = 10 min															
100	150	0.01	0.7	3.6	0	0.65	900	3/8"	0.32	1.5	10	13.6	14	0.57	5.41	3.6	11.1
100	75	0.01	0.7	1.8	0	0.65	900	"	0.32	1.5	10	11.8	14	0.57	5.73	2.9	9.5



Date _____ Page _____ of _____

Project _____

Item _____

RECURRENCE INTERVAL, YEARS (2) 5 10 25 50 100

res	OVERLAND FLOW				GUTTER FLOW						HYDROLOGY						
	L ft	S _o ft/ft	V ft/sec	t _o min	T ₁ /T ₂	T _a /T ₂	L ft	S _x in/ft	S _o	V ft/s	t _g min	t _c = t _o + t _g min	T _D ft	C	i in/hr	A Ac.	Q cfs
05 ROLL	125'	0.01	0.7	3	0	0.65	1320	3/8	0.32	1.26	17.5	20.5	11	0.52	3.60	6.1	11.4
					11/4	0.90	325	"	0.36	2.1	1.8	32.3	14	0.52	3.49	13.0	23.6
20	125	0.01	0.7	3	0	0.65	550	"	0.50	0.9	10.2	13.2	5	0.52	4.29	1.2	2.7
					0	0.65	750	"	0.36	1.4	9.1	12.1	6	0.52	4.17	9.1	19.7
30 C	125	0.01	0.7	3	6/12	0.77	300	"	0.50	2.6	1.9	14	12	0.48	4.75	2.8	6.4
					0	0.65	550	"	0.32	1.5	7.1	10.1	6	0.48	4.75	0.7	1.6
60 B	125	0.01	0.7	3	0	0.65	250	"	0.32	1.0	4.2	10	4	0.48	4.75	1.6	3.6
					0	0.65	550	"	0.32	1.3	7.1	10.1	6	0.48	4.75	2.5	5.6
80 B	125	0.01	0.7	3	0	0.65	550	"	0.32	1.3	7.1	10.1	6	0.48	4.75	2.5	5.6
					0	0.65	550	"	0.32	1.3	7.1	10.1	6	0.48	4.75	2.5	5.6
100 B	125	0.01	0.7	3	0	0.65	1330	3/8	0.32	1.26	17.5	20.5	11	0.52	3.60	6.9	12.9
					0	0.65	1330	3/8	0.32	1.26	17.5	20.5	11	0.52	3.60	6.9	12.9

Estimated



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Project GOLDEN HILLS DRAINAGE PLAN

Item SYSTEM 700

RECURRENCE INTERVAL, YEARS (2) 5 10 25 50 100

res	OVERLAND FLOW				GUTTER FLOW							HYDROLOGY					
	L ft	S ₀ ft/ft	V ft/sec	t ₀ min	T ₁ /T ₂	T _a /T _z	L ft	S _x	S ₀	V ft/s	t _g min	t _g min	t _g min	T ft	C	i in/hr	A Ac.
00 Soil	125	0.01	0.7	3	0	0.65	520	3/8"	0.32%	1.5	5.8	10	14	0.52	4.75	3.8	9.4
105 Soil	125	0.01	0.7	3	0	0.65	350	"	1.26%	1.7	3.4	6.4	6	0.52	4.75	4.9	12.1
					4/4	0.74	530	"	0.80%	2.7	3.3	10	14	0.52	4.75	2.3	5.7
110 Soil	120	0.01	0.7	3.8	0	0.65	330	"	0.86%	1.7	3.3	10	8	0.52	4.75	2.3	5.7
120 Soil	125	0.01	0.7	3	0	0.65	500	"	0.36%	1.4	6.0	9	11	0.48	4.75	4.9	11.2
					0.78	0.90	150	"	1.75%	4.8	0.5	10	14	0.48	4.75	4.9	11.2
130 Soil	125	0.01	0.7	3	0	0.65	300	"	0.86%	1.4	3.7	6.7	6	0.48	4.40	3.4	7.2
					0.42	0.74	410	"	0.43%	1.6	4.4	11.1	10	0.48	4.40	3.4	7.2
					1.00	1.0	200	"	1.75%	4.3	0.8	11.9	10	0.48	4.40	3.4	7.2
740 Soil	80	0.01	0.7	1.9	0	0.65	500	"	0.36%	1.4	3.7	5.6	6	0.48	4.75	2.5	5.7
					0.67	0.85	350	"	1.75%	3.4	1.7	10	9	0.48	4.75	2.5	5.7



Date 5/29/85 MMB Page _____ of _____

Project GOLDEN HILLS DRAINAGE PLAN

Item MISC AREAS

RECURRENCE INTERVAL, YEARS 2 5 10 25 50 100

DES	OVERLAND FLOW			GUTTER FLOW							HYDROLOGY						
	L ft	S _o ft/ft	V ft/sec	t _o min	T ₁ /T ₂	T _a /T ₂	L ft	S _x 1"/1	S _o %	V ft/s	t _g min	t _c = t _o + t _g min	T ft	C	i in/hr	A Ac.	Q cfs
30	130	0.01	0.7	3.1	0	0.65	880	3/8	0.4	1.7	8.8	11.9	14	0.55	5.71	2.5	7.9
60	140	0.01	0.7	4.5	0	0.65	1500	3/8	0.4	1.7	14.7	19.2	14	0.55	4.74	6.0	15.6
90	300	0.01		2.5	6	0.74	600	3/8	0.7	2.7	3.7	10	15	0.69	6.11	3.3	13.9
10	160	0.01	2.0	1.3	0	0.65	200	3/8	0.32	1.3	3.9	10	6	0.69	6.11	0.5	2.1
120	140	0.01	2.0	1.2	0	0.65	775	3/8	0.32	1.5	8.6	10	14	0.52	6.11	2.0	6.4
100	150	0.01	0.7	3.6	0	0.65	275	3/8	2.88	3.1	1.5	10	6	0.48	4.75	1.1	2.5
210	150	0.01	0.7	3.6	0	0.65	275	3/8	2.88	3.1	1.5	10	8	0.48	4.75	1.8	4.1

2-YR DESIGN

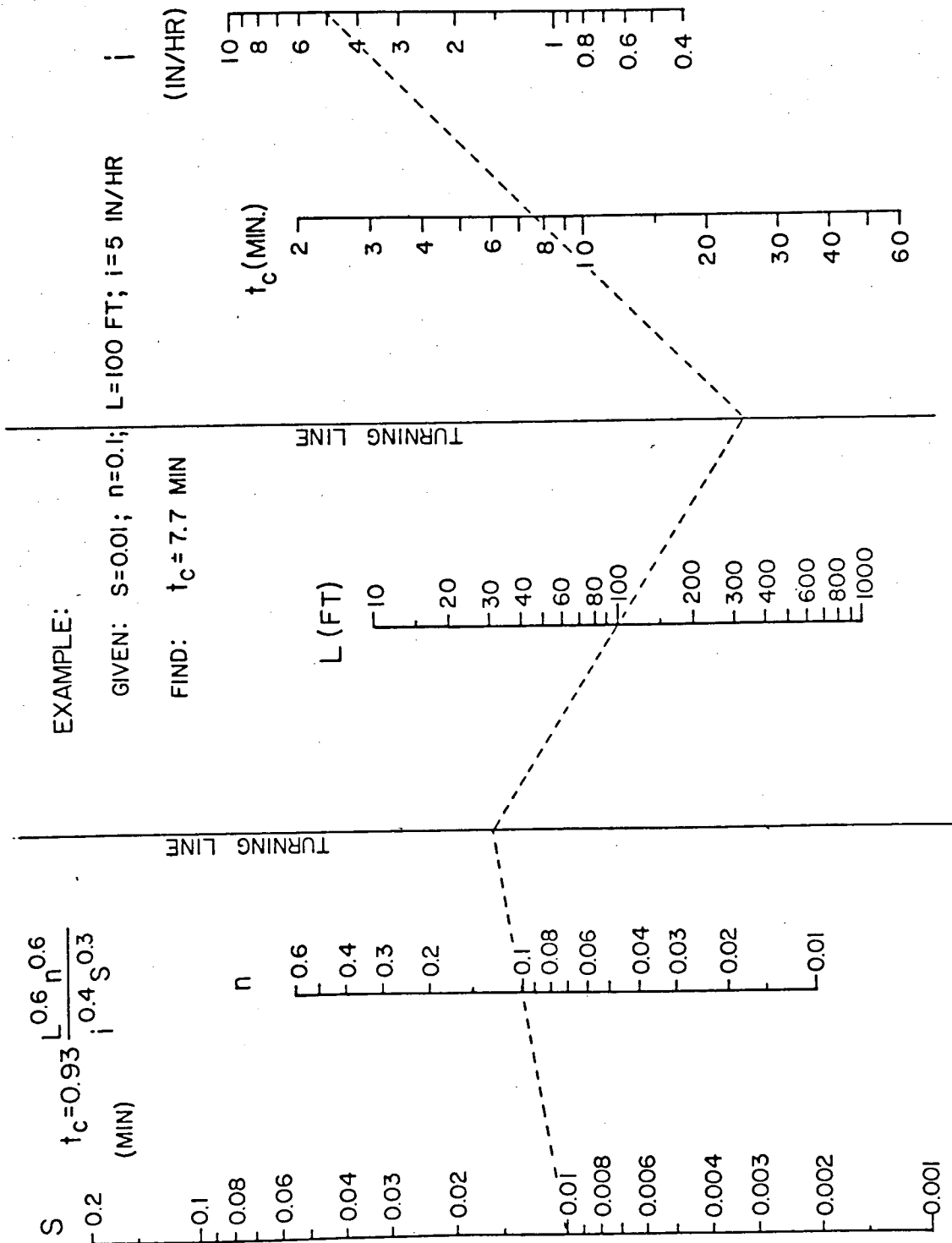


CHART 1. Kinematic wave formulation for determining time of concentration.

From: HEC-12, DRAINAGE OF HIGHWAY PAVEMENTS, FHWA, MAR. 1984

Table 3. Spread at average velocity in a reach of triangular gutter.

T_1/T_2	\emptyset	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8
T_a/T_2	0.65	0.66	0.68	0.70	0.74	0.77	0.82	0.86	0.90

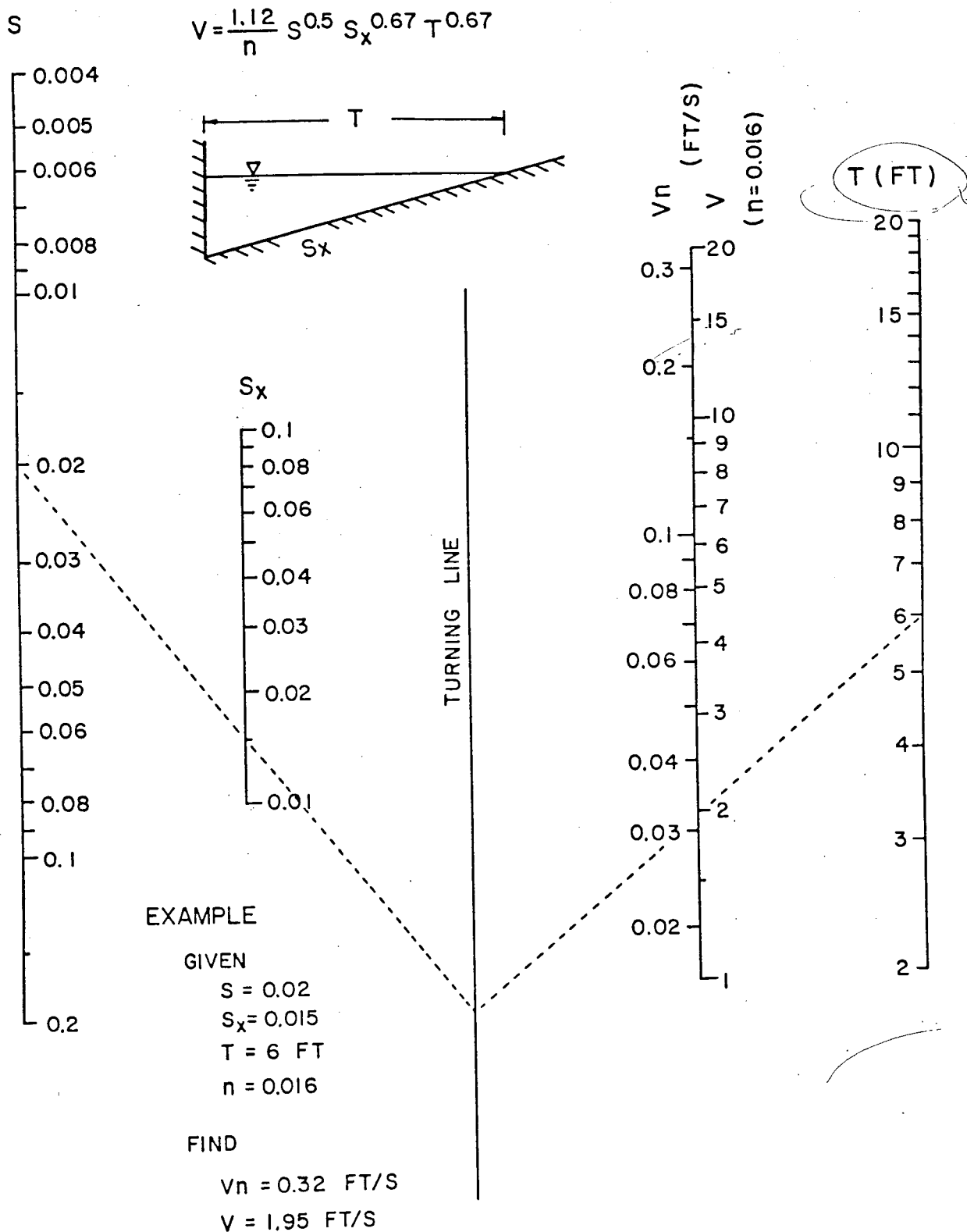


CHART 2. Velocity in triangular gutter sections.

From HEC-12: DRAINAGE OF HIGHWAY PAVEMENTS, F.H.W.A., Mar. 1984

April, 1985

ATTACHMENT A
DRAINAGE CRITERIA MANUAL

CITY OF WICHITA, KANSAS

RAINFALL INTENSITY TABLE FOR SEDGWICK COUNTY, KANSAS

The following tabulation contains rainfall intensity in inches per hour as derived from ESSA Weather Bureau Technical Paper 40.

DURATION IN MINUTES	RETURN PERIODS OF						
	1-YR	2-YR	5-YR	10-YR	25-YR	50-YR	100-YR
5	4.67	6.23	8.00	9.34	10.67	12.23	13.79
6	4.35	5.80 ⁻⁴³	7.45	8.70	9.94	11.39	12.84
7	4.09	5.46 ⁻³⁴	7.02	8.19	9.36	10.72	12.09
8	3.88	5.18 ⁻²⁸	6.66	7.77	8.89	10.18	11.48
9	3.71	4.95 ⁻²³	6.36	7.43	8.49	9.72	10.96
10	3.56	4.75 ⁻²⁰	6.11	7.13	8.15	9.33	10.52
11	3.43	4.58 ⁻¹⁷	5.89	6.87	7.85	8.99	10.14
12	3.32	4.40	5.69	6.64	7.59	8.69	9.80
13	3.21	4.29	5.51	6.43	7.35	8.42	9.50
14	3.12	4.17	5.36	6.25	7.14	8.18	9.23
15	3.04	4.06	5.21	6.08	6.95	7.97	8.98
16	2.96	3.96	5.09	5.93	6.78	7.77	8.76
17	2.90	3.86	4.97	5.79	6.62	7.59	8.55
18	2.83	3.78	4.86	5.67	6.48	7.42	8.37
19	2.77	3.70	4.76	5.55	6.34	7.27	8.19
20	2.72	3.63	4.66	5.44	6.22	7.12	8.03
21	2.67	3.56	4.57	5.34	6.10	6.99	7.88
22	2.62	3.49	4.49	5.24	5.99	6.86	7.74
23	2.57	3.43	4.41	5.15	5.89	6.74	7.60
24	2.53	3.38	4.34	5.07	5.79	6.63	7.48
25	2.49	3.32	4.27	4.99	5.70	6.53	7.36
26	2.45	3.23	4.21	4.91	5.61	6.43	7.25
27	2.42	3.18	4.15	4.84	5.53	6.33	7.14
28	2.38	3.05	4.09	4.77	5.45	6.25	7.04
29	2.35	2.97	4.02	4.68	5.38	6.16	6.95
30	2.32	2.89	3.92	4.56	5.31	6.08	6.79
31	2.29	2.82	3.82	4.44	5.19	6.00	6.62
32	2.26	2.75	3.73	4.33	5.07	5.87	6.45
33	2.24	2.68	3.64	4.23	4.95	5.73	6.30
34	2.19	2.62	3.55	4.13	4.83	5.60	6.16
35	2.14	2.57	3.47	4.04	4.73	5.47	6.02
36	2.09	2.51	3.40	3.95	4.62	5.35	5.89
37	2.05	2.46	3.33	3.87	4.52	5.23	5.76
38	2.00	2.41	3.26	3.79	4.43	5.13	5.64
39	1.96	2.36	3.19	3.71	4.34	5.02	5.53
40	1.92	2.32	3.13	3.64	4.26	4.92	5.42
41	1.89	2.27	3.07	3.57	4.18	4.83	5.32
42	1.85	2.23	3.01	3.51	4.10	4.74	5.22
43	1.82	2.19	2.96	3.44	4.02	4.65	5.13
44	1.78	2.15	2.91	3.38	3.95	4.56	5.03
45	1.75	2.11	2.86	3.32	3.88	4.48	4.95

ATTACHMENT D

DRAINAGE CRITERIA

CITY OF WICHITA, KANSAS

RECOMMENDED RUNOFF COEFFICIENTS FOR RATIONAL METHOD
AND PERCENT IMPERVIOUS FOR UNIT HYDROGRAPH METHOD

Land Use or Surface Characteristics	Percent Impervious	Frequency			
		<u>2</u>	<u>5</u>	<u>10</u>	<u>100</u>
1. Business:					
Downtown Areas	95	0.84	0.85	0.87	0.91
Neighborhood Areas	70	0.68	0.69	0.73	0.80
2. Residential:					
<u>Single Family (Soil Group D)</u>					
1/8 Acre	50	0.57	0.61	0.66	0.79
1/4 Acre	38	0.50	0.54	0.62	0.76
1/3 Acre	30	0.46	0.50	0.59	0.73
1/2 Acre	25	0.42	0.48	0.56	0.72
3/4 Acre	22	0.42	0.46	0.55	0.71
1 Acre	20	0.41	0.45	0.54	0.71
<u>Multi-Family (Soil Group D)</u>					
Multi-Unit (detached)	60	0.62	0.66	0.72	0.82
Multi-Unit (attached)	65	0.64	0.68	0.73	0.83
Apartments	75	0.70	0.73	0.79	0.86
<u>Single Family (Soil Group C)</u>					
1/8 Acre	50	0.55	0.58	0.64	0.73
1/4 Acre	38	0.48	0.51	0.57	0.68
1/3 Acre	30	0.43	0.46	0.53	0.65
1/2 Acre	25	0.40	0.43	0.50	0.63
3/4 Acre	22	0.39	0.42	0.49	0.62
1 Acre	20	0.37	0.40	0.48	0.61
<u>Multi-Family (Soil Group C)</u>					
Multi-Unit (detached)	60	0.60	0.63	0.69	0.77
Multi-Unit (attached)	65	0.63	0.66	0.71	0.79
Apartments	75	0.68	0.72	0.77	0.83
<u>Single-Family (Soil Group B)</u>					
1/8 Acre	50	0.52	0.54	0.59	0.67
1/4 Acre	38	0.44	0.46	0.52	0.61
1/3 Acre	30	0.39	0.41	0.47	0.57
1/2 Acre	25	0.36	0.38	0.44	0.54
3/4 Acre	22	0.34	0.36	0.42	0.52
1 Acre	20	0.33	0.35	0.40	0.51
<u>Multi-Family (Soil Group B)</u>					
Multi-Unit (detached)	60	0.58	0.60	0.65	0.72
Multi-Unit (attached)	65	0.61	0.64	0.68	0.75
Apartments	75	0.67	0.70	0.74	0.80

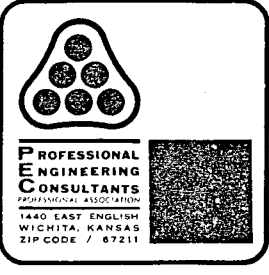
ATTACHMENT E

DRAINAGE CRITERIA

CITY OF WICHITA, KANSAS

AVERAGE OVERLAND FLOW VELOCITY FOR USE WITH URBANIZED AREAS

Surface Type	VELOCITY IN FEET/SECOND FOR SLOPES IN PERCENT SHOWN																			
	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0	20.0
Forrest with Heavy Ground Litter or Meadow	0.08	0.11	0.14	0.16	0.18	0.19	0.20	0.22	0.23	0.25	0.35	0.42	0.50	0.55	0.60	0.66	0.70	0.75	0.80	1.10
Fallow or Minimum Tillage Cultivation	0.15	0.21	0.26	0.29	0.33	0.35	0.39	0.41	0.44	0.46	0.65	0.80	0.92	1.10	1.20	1.30	1.40	1.50	1.60	2.10
Short Grass Pasture or Lawns	0.23	0.32	0.38	0.44	0.50	0.53	0.58	0.62	0.66	0.70	1.00	1.20	1.40	1.60	1.80	1.90	2.00	2.10	2.20	3.20
Almost Bare Ground	0.32	0.44	0.53	0.62	0.69	0.75	0.82	0.87	0.92	0.98	1.40	1.70	1.90	2.10	2.30	2.50	2.70	2.90	3.10	4.40
Grassed Waterway	0.50	0.68	0.83	0.95	1.10	1.20	1.30	1.40	1.50	1.60	2.20	2.60	3.00	3.40	3.70	4.00	4.30	4.60	4.80	7.00
Paved Areas (Sheet Flow) or Shallow Gutter Flow	0.63	0.89	1.10	1.30	1.50	1.60	1.70	1.80	1.90	2.00	2.80	3.40	4.00	4.50	4.90	5.30	5.70	6.00	6.20	9.00



Date _____ Page _____ of _____
 Project _____
 Item _____

$z/m = 2000$
 5 10 25 50 100-YR will be higher than actual.
 Assume T_t in gutter = T_t in pipe. This will be conservative, for pipe velocities are in 5 ft/s range, whereas gutter velocities are in 1.5 - 4 ft/sec. Thus calculated Q will be higher than actual.

SYSTEM 100 SHEFFORD

NODE NO	HYDROLOGY		APPROACHING FLOW				INLET		ON-GRADE COMP			SUMP COMP.			Q_b cfs	
	Q_0 cfs	Q_{0+G} cfs	S_0 %	S_x in/ft	d ft	T ft	Type	L	LT ft	L/LT	E	d_i ft	d ft	T ft		Q_i cfs
10	5.8	5.8	0.43	3/8	0.39	12.5	1A	5	24	0.21	0.33	0.58	0.41	13.1	1.9	3.9
50	3.9	7.8	0.32	3/8	0.46	14	1A	5							7.8	-0-
20	11.9	11.9														
W	5.9		1.83	3/8	0.30	9.6										
S	6.0		0.43	3/8	0.42	13.4	1A	10							11.9	-0-
30	10.8	10.8														
W	5.4		2.83	3/8	0.28	9										
S	5.4		3.00	3/8	0.25	8	1A	10							10.8	-0-
140	6.7	6.7	0.32	3/8	0.43	14	1A	5							6.7	-0-
170	7.3	7.3	0.32	3/8	0.45	14	1A	5							7.3	-0-
180	5.5	5.5	0.32	3/8	0.40	12.8	1A	5							5.5	-0-
160	0.9	0.9	0.32	3/8	0.21	6.7	1A	5							0.9	-0-
190	1.4	1.4	0.32	3/8	0.24	7.7	1A	5							1.4	-0-

Spill Over Crown

SPILL PIPE OVER CROWN



Date _____ Page _____ of _____
 Project _____
 Item _____

Assume T_e in gutter = T_e in pipe. This will be conservative, for pipe velocities are in 5 ft/s range, which is greater velocities are in 1.5 - 4 ft/sec. Thus calculated Q will be higher than actual.

$z/n = 2000$
 5-YR

NODE NO	HYDROLOGY		APPROACHING FLOW			INLET		ON-GRADE COUP			SUMP COMP.			Q_1 cfs	Q_2 cfs	
	Q_0 cfs	Q_{0+NB} cfs	S_0 %	S_x in./ft	d ft	T ft	Type	L	LT ft	L/LT	E	d_i ft	d ft			T ft
310	4.9	4.9	1.10	3/8	0.31	9.9	1A	10	33	0.30	0.48	0.61	0.44	14.1	2.4	2.5
350	5.4	8.1	0.45	3/8	0.28	9.0	-OK-									
N-W	5.6	5.6	0.32	3/8	0.40	12.8	1A	5							8.1	-0-
360	3.8	3.8	0.32	3/8	0.34	10.9	1A	5	18	0.28	0.45				1.7	2.1
380	2.1	4.2	0.45	3/8	0.34	10.9	1A	5	22	0.22	0.35				1.5	2.7
400	11.1	2.7	0.32	3/8	0.52	14	←	from Nelson Cavington								
			0.45	3/8	0.29	9.3	←	from Nelson Central								
410	3.9	3.9	0.32	3/8	0.47	14	1A	10	28	0.36	0.55	0.58	0.41	13.1	3.1	-0-
320	10	10	0.32	3/8	0.50	14	1A	10							4.9	4.0
325	31	21	0.41	3/8	0.63	20	1A	10							15.5	-0-
330	7.1	7.1	0.41	3/8	0.42	13.4	1A	10	22	0.45	0.7	0.62	0.45	14.4	15.5	-0-
370	4.9	7.0	0.45	3/8	0.42	13.4	1A	10	22	0.45	0.7	0.62	0.45	14.4	15.5	-0-

* As shown on B.F.A. plans



z/n = 2000
 2-YR
 Assume T_t in gutter = T_t in pipe. This will be conservative, for pipe velocities are in 5 ft/s range, whereas gutter velocities are in 1.5 - 4 ft/sec. Thus calculated Q will be higher than actual.

NODE NO	HYDROLOGY		APPROACHING FLOW			INLET		ON-GRADE COMP		SUMP COMP.			Q_1 cfs	Q_b cfs			
	Q_0 cfs	Q_{0TB} cfs	S_o %	S_x in/ft	d ft	T ft	Type	L	L_T ft	L/L_T	E	d_i ft			d ft	T ft	
105	11.4	11.4	0.32	3/8	0.49	14	1A	10	0.4			0.47	0.3	9.6	11.4	-0-	0.06 OVER CROWN
110	12.7	12.7	0.32	3/8	0.42	13.4	1A	10				0.57	0.4	12.8	12.7	-0-	CURB DEEP
130	19.7	19.7	0.40	3/8	0.42	13.4						0.75	0.58	14	19.7	-0-	SPILL OVER CROWN
120	2.2	2.2	0.50	3/8	0.50	14	1A	10				0.22	0.05	0.7	2.2	-0-	0.07 OVER CROWN
160	6.4	6.4	0.40	3/8	0.43	14	1A	5				0.51	0.34	10.9	6.4	-0-	
170	1.6	1.6	OK BY INSPECTION (EXCESS CAPACITY FROM E. SIDE)	3/8	0.42	13.4	1A	5				0.17	0	0	1.6	-0-	
180	5.7	5.7	0.32	3/8	0.25	8.0	1A	5				0.44	0.27	8.6	5.7	-0-	
190	3.6	3.6	0.32	3/8	0.41	13.1	1A	5				0.32	0.15	4.8	3.6	-0-	



Date _____

Page _____

of _____

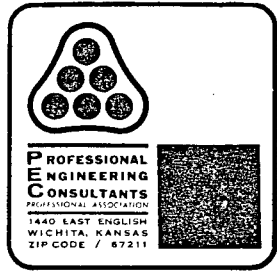
Assume T_t in gutter = T_t in pipe. This will be conservative, for pipe velocities are in 5 ft/s range, whereas gutter velocities are in 1.5 - 4 ft/sec. Thus calculated Q will be higher than actual.

$n = 2000$
2-YR

NODE NO	HYDROLOGY		APPROACHING FLOW				INLET		ON-GRADE COMP		SUMP COMP.			Q_1 cfs	Q_b cfs	
	Q_0 cfs	Q_{p100} cfs	S_0 %	S_x in/ft	d ft	T ft	Type	L	LT ft	L/LT	E	d_i ft	d ft			T ft
100	9.4	9.4	0.32	3/8	0.44	14.1	1A	10				0.45	0.28	9.0	9.4	-0-
North	7.0	7.0	0.80	3/8	0.26	8.3										
South	2.4	2.4														
705	12.0	12.0	0.80	3/8	0.45	14.4	1A	10	39	0.26	0.45				5.4	6.6
710	5.5	12.1					1A	10							12.1	-0-
W.	8.4		0.52	3/8	0.47	14										
E.	3.7		0.86	3/8	0.28	9										
720	10.3	10.3	1.75	3/8	0.26	8.3	1A	10							10.3	-0-
W.	3.3		0.43	3/8	0.41	13.1										
So.	7.0															
730	7.1	7.1	1.75	OK BY INSPECTION		INSPECTION	1A	5							7.1	-0-
740	5.2	5.2	1.75	OK BY INSPECTION		INSPECTION	1A	5							5.2	-0-

0.10' OVER CROWN

0.04 OVER CROWN



$z/n = 2000$
 -YR 800 & 810
 -YR 450 & 900 & S
 Assume T_e in gutter = T_e in pipe. This will be conservative, for pipe velocities are in 5 ft/s range, which is gutter velocities are in 1.5 - 4 ft/sec. Thus calculated Q will be higher than actual.

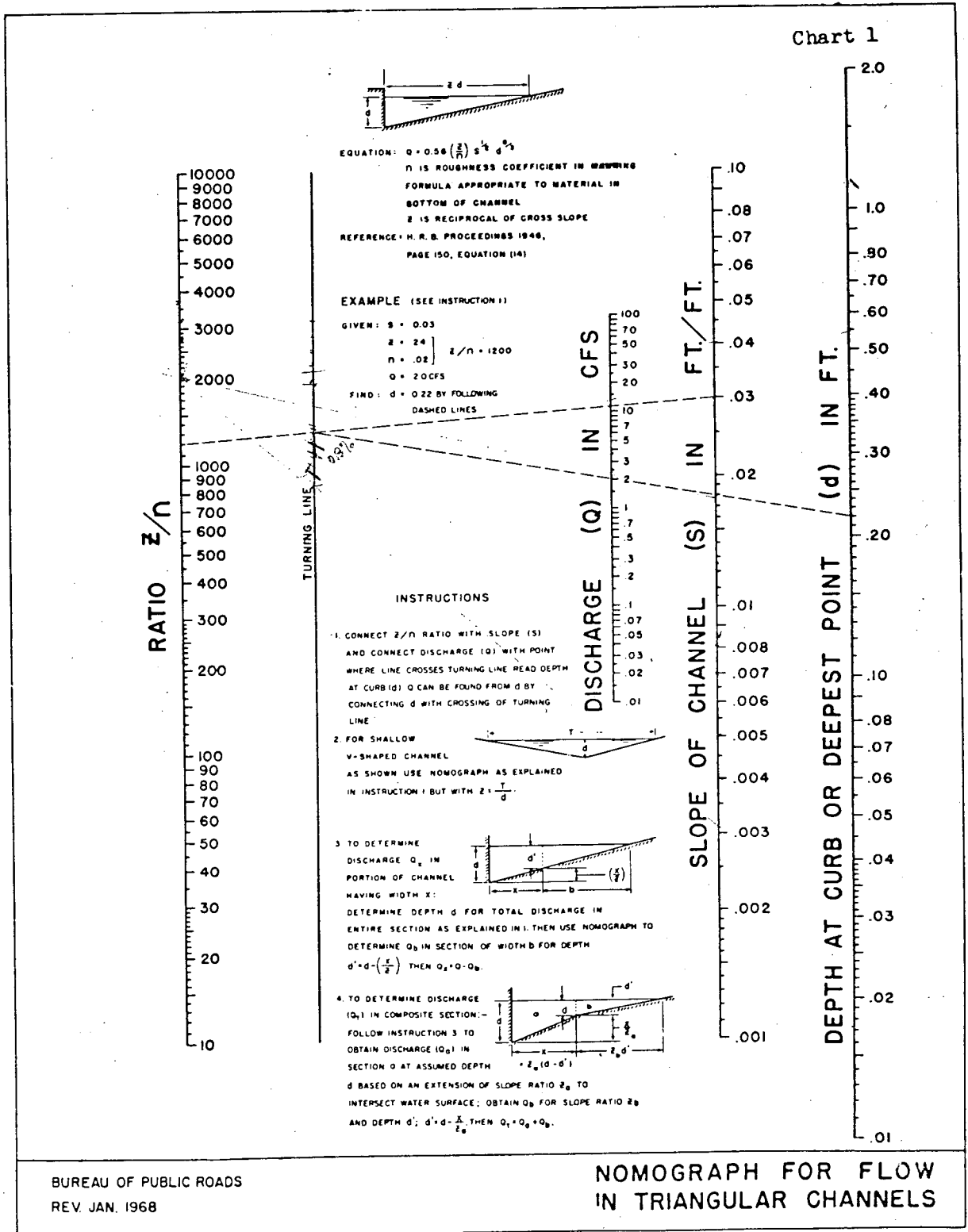
NODE NO	HYDROLOGY		APPROACHING FLOW				INLET		ON-GRADE COMP		SUMP COMP.			Q_b cfs		
	Q_0 cfs	Q_{0+L} cfs	S_0 %	S_x in/ft	d ft	T ft	Type	L	LT ft	L/LT	E	d_i ft	d ft		T ft	Q_i cfs
150	7.9	7.9	0.40	3/8	0.42	13.4	1A	5				0.59	0.42	13.4	7.9	-0-
160	15.6	15.6	0.40	3/8	0.55	14	1A	10				0.62	0.45	14.4	15.6	-0-
120	6.4	6.4	0.32	3/8	0.42	13.7	V.G.	→								
110	2.1	8.5	0.70	3/8	0.41	13.4	To be designed									
200	13.9	22.4	0.70	3/8	0.57	18.2	Exceeds Use									
310	4.1	4.1	0.32	OK BY INSPECTION			1A	5				0.35	0.18	5.0	4.1	-0-
300	2.5	2.5	0.32	OK BY INSPECTION			1A	5				0.25	0.08	2.60	2.5	-0-

0.01' over crown
 1.5-YR
 CURB DEEP

w/ Central Ave
 No not let Area cap drain out into street, to back of inlet and/or pvt. system.

2-5-YR DESIGN ↑
 2-YR DESIGN ↓

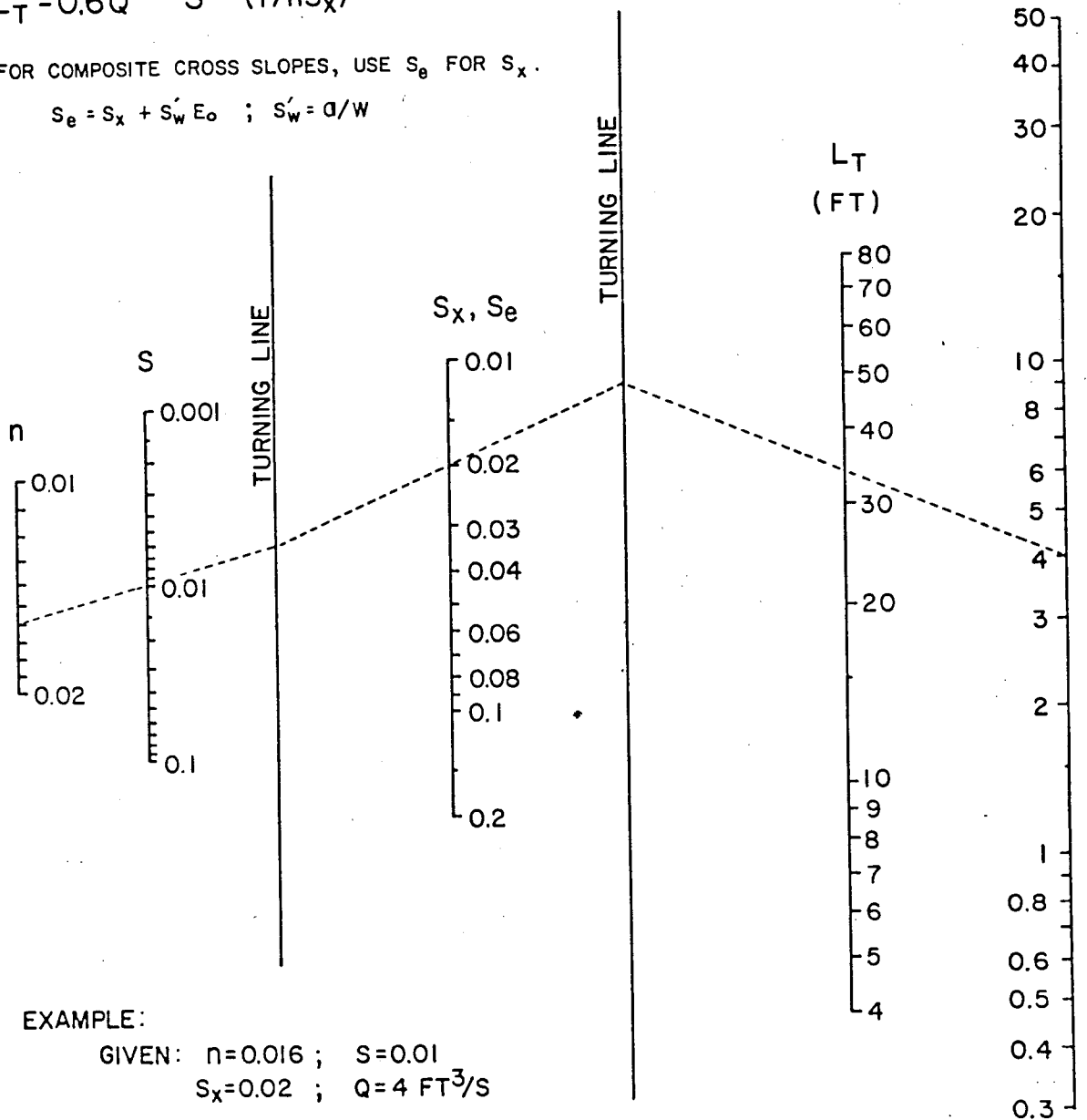
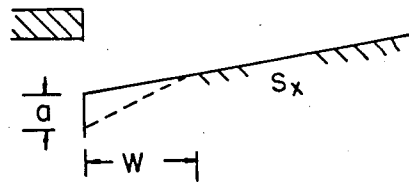
Appendix C - CAPACITY OF GUTTERS AND GRATE INLET



$$L_T = 0.6Q^{0.42} S^{0.3} (1/nS_x)^{0.6}$$

FOR COMPOSITE CROSS SLOPES, USE S_e FOR S_x .

$$S_e = S_x + S'_w E_o \quad ; \quad S'_w = a/W$$



EXAMPLE:

GIVEN: $n=0.016$; $S=0.01$
 $S_x=0.02$; $Q=4 \text{ FT}^3/\text{S}$

FIND: $L_T = 34 \text{ FT}$

CHART 9. Curb-opening and slotted drain inlet length for total interception.

FROM: HEC-12, DRAINAGE OF HIGHWAY PAVEMENTS, F.H.W.A., MAR. 1984.

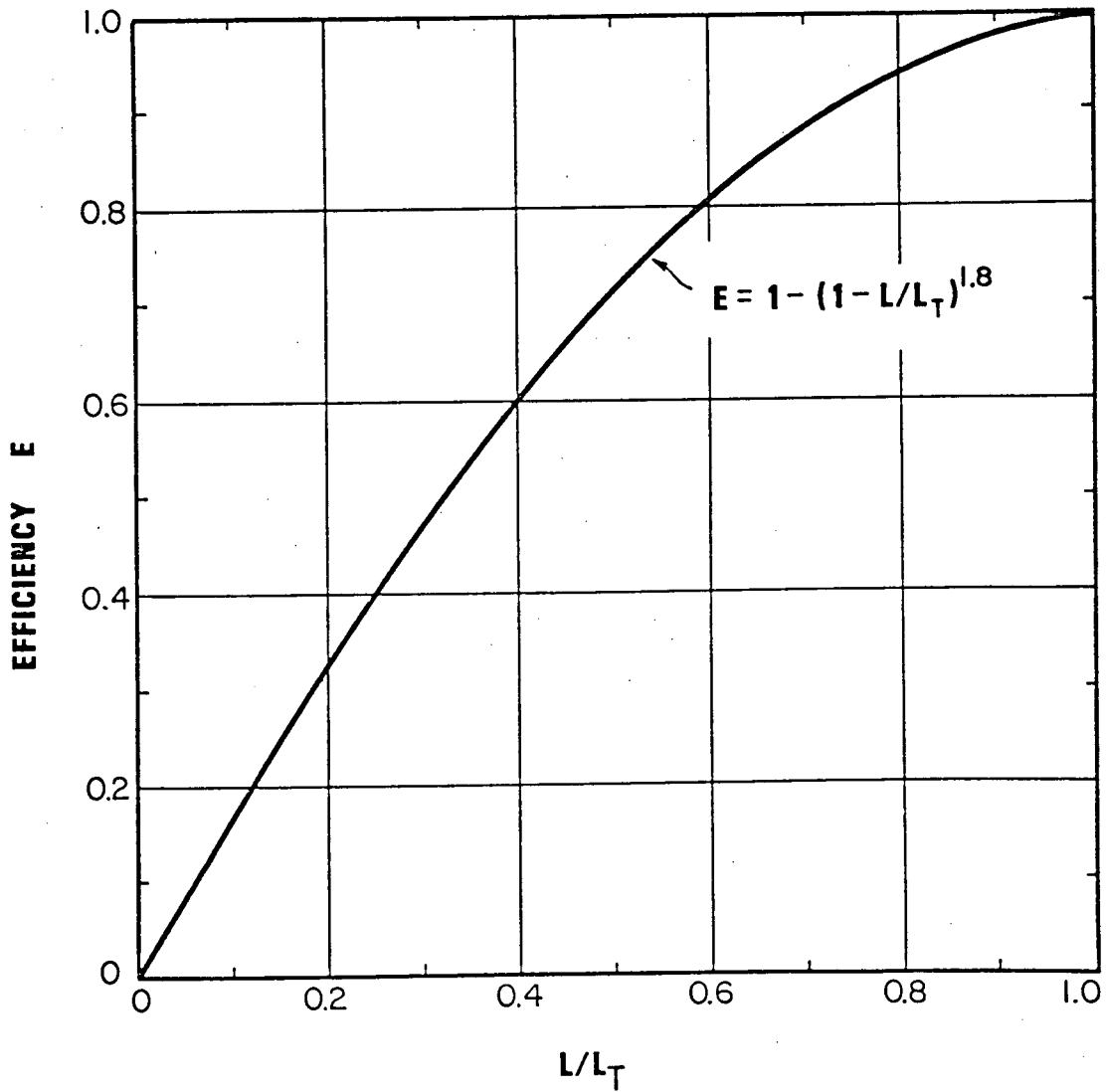
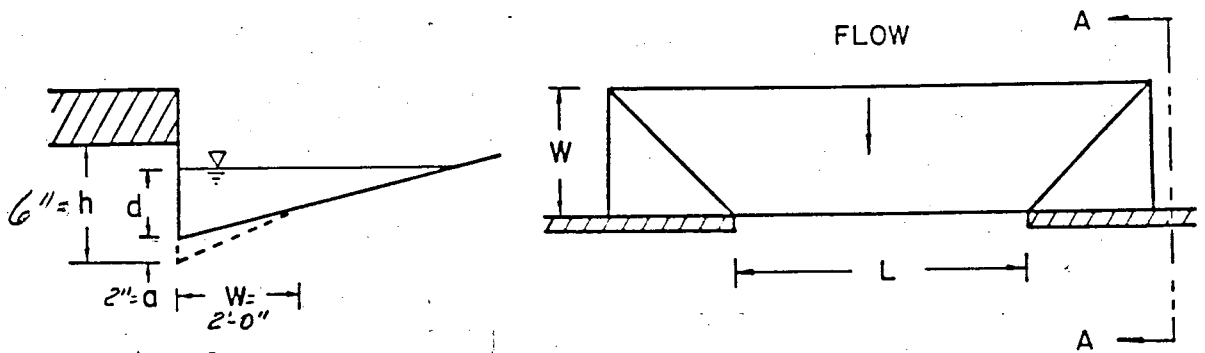


CHART 10. Curb-opening and slotted drain inlet interception efficiency.

FROM: HEC-12, DRAINAGE OF HIGHWAY PAVEMENTS, F.H.W.A., Mar. 1984



DEF. SKETCH, C.O.W. TYPE 1A INLET

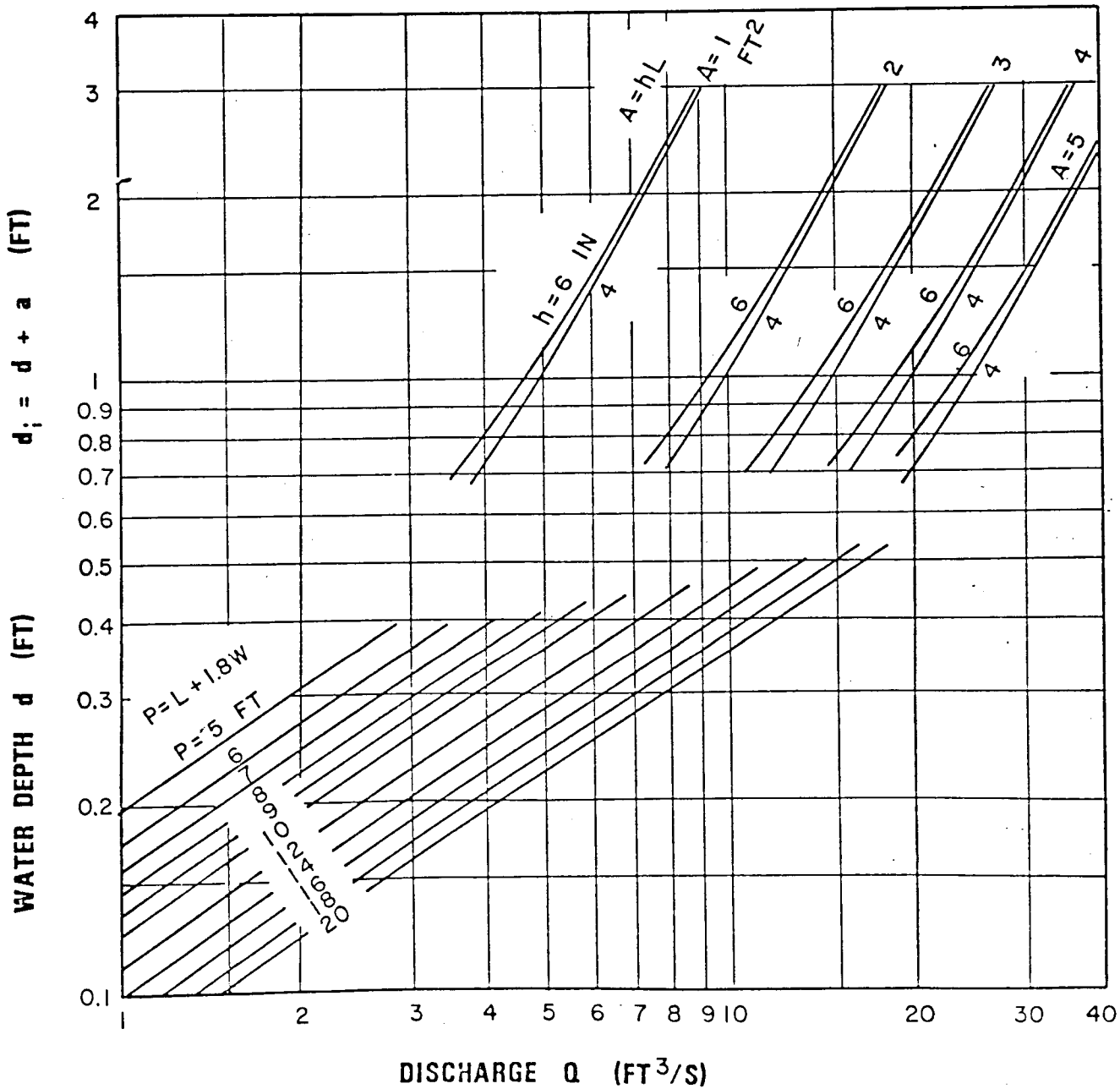


CHART 12. Depressed curb-opening inlet capacity in sump locations.

FROM: HEC-12, DRAINAGE OF HIGHWAY PAVEMENTS, F.H.W.A., MAR., 1984

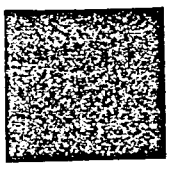
HYDROLOGY DATA SHEET

PAGE 1 OF 2

PROJECT: GOLDEN HILLS DRAINAGE PAU PROJECT NO. _____

ITEM: SYSTEM NO / SHEPHERD DATE: 5/28/85

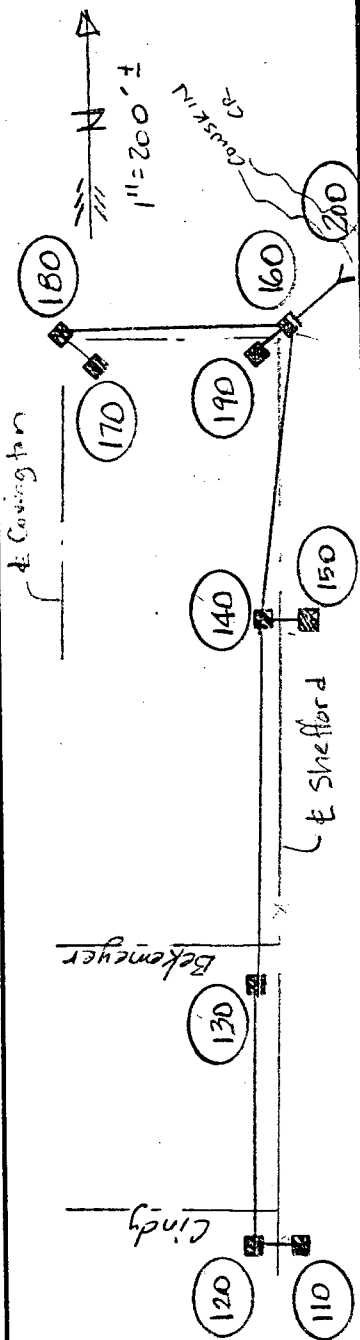
RETURN PERIOD: 2-YR COMPUTATIONS BY: MWS REVISIONS BY: _____



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1440 EAST ENGLISH
WICHITA, KANSAS 67211
(316) 262-2691

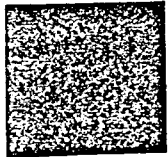
SCHMATIC DIAGRAM:



HYDROLOGY DATA										CONDUIT DATA										
SUB-BASIN					HYDROLOGY SUMMATION					HYDROLOGY DATA					CONDUIT DATA					
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	
AREA (acres)	SLOPE (%)	LENGTH (feet)	T _c (minutes)	I ₀ (in./hr.)	C ₀ (cfs)	T _c (minutes)	I (in./hr.)	Q (cfs)	Σ Q (cfs)	PIPE (inches)	SLOPE (%)	VELOCITY (ft./sec.)	LENGTH (feet)	T ₁ (minutes)	T _c + T ₁ (minutes)	AREA (acres)	SLOPE (%)	LENGTH (feet)	T _c (minutes)	
110	0.48	2.8	13	4.66	6.3	13	4.66	6.3	6.3	15	0.95	5.1	30	0.1	15.1					
120	0.48	5.8	12.4	4.35	12.1	13	4.29	11.9	18.2	18	1.05	10.3	270	0.4	13.4					
130	0.52	5.5	18.0	3.78	10.8	18	3.78	16.0	26.8	30	0.43	5.5	380	1.2	19.2					
150	0.48	1.7	10	4.75	4.0	10	4.75	4.0	4.0	15	0.38	3.3	30	0.2	10.2					
140	0.52	3.5	10	4.75	8.6	19.2	3.69	6.7	36.6	36	0.30	5.2	300	1.0	20.2					
170	0.48	3.2	10	4.75	7.3	10	4.75	7.3	7.3	18	0.48	4.1	30	0.1	10.1					
180	0.48	2.4	10	4.75	5.5	20.2	3.62	9.8	12.8	24	0.32	4.1	260	1.1	11.2					

HYDROLOGY DATA SHEET

PAGE 2 OF 2



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PROFESSIONAL ASSOCIATION

1440 EAST ENGLISH
WICHITA, KANSAS 67211
(316) 262 2691

PROJECT: GOLDEN HILLS DATA SHEET PROJECT NO. _____

ITEM: SYSTEM 300 CENTRAL AVE DATE: 5/27/85

RETURN PERIOD: 5-YR COMPUTATIONS BY: MAB REVISIONS BY: _____

Schematic Diagram:

See sh 1 of 2 for sketch

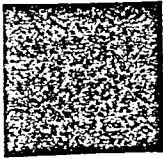
76

TRIBUTARY AREA										HYDROLOGY SUMMATION					CONDUIT DATA				
SUB-BASIN (1)	C (2)	AREA (acres) (3)	SLOPE (%) (4)	LENGTH (feet) (5)	T _{c0} (minutes) (6)	I ₀ in./hr. (7)	Q ₀ (cfs) (8)	T _c (minutes) (9)	I in./hr. (10)	Q (cfs) (11)	Σ Q (cfs) (12)	PIPE (inches) (13)	SLOPE (%) (14)	VELOCITY (ft./sec.) (15)	LENGTH (feet) (16)	T ₁ (minutes) (17)	T _c + T ₁ (minutes) (18)		
380	0.57	3.6			10	6.11	2.1	10	6.11	2.1	2.1	15	0.11	1.7	50	0.5	10.5		
370	0.54	1.6			10	6.11	5.6					42	0.32	5.95	200	0.6	12.8		
400	0.57	3.6			13.6	5.41	11.1	13.6	5.41	11.1	11.1	21	0.49	4.6	30	0.1	13.7		
410	0.57	2.9			11.8	5.73	9.5	13.7	5.39	8.9	20	30	0.24	4.1	75	0.3	14.0		
								12.8	5.54 (13.7)										
390												42	0.57	7.9	520				
430																			

HYDROLOGY DATA SHEET

PAGE _____ OF _____

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PROFESSIONAL ASSOCIATION

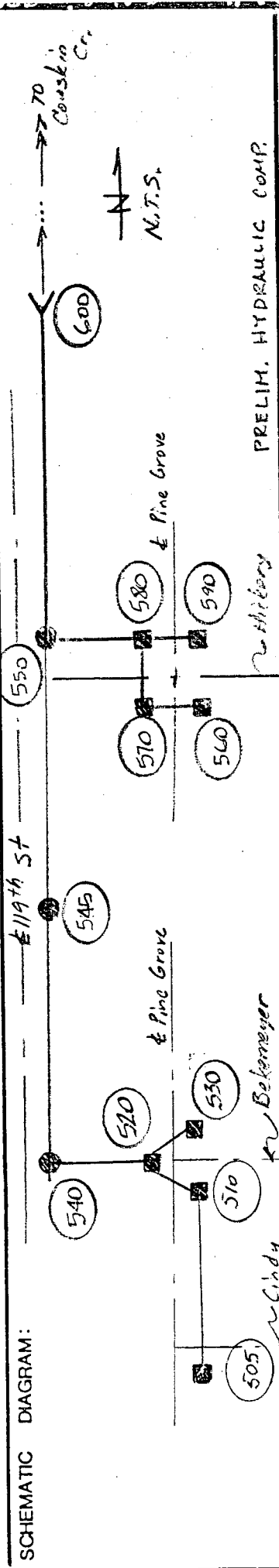


1440 EAST ENGLISH
WICHITA, KANSAS 67211
(316) 262-2691

PROJECT: GOLDEN HILLS DRAINAGE PLAN

ITEM: _____ DATE: 5-24-85

RETURN PERIOD: 2 COMPUTATIONS BY: MWS REVISIONS BY: _____



HYDROLOGY SUMMATION										CONDUIT DATA						
TRIBUTARY AREA																
Sub-basin (1)	Area (acres) (3)	Slope (%) (4)	Length (feet) (5)	T _c (minutes) (6)	I ₀ in./hr. (7)	Q ₀ (cfs) (8)	T _c (minutes) (9)	I in./hr. (10)	Q (cfs) (11)	Σ Q (cfs) (12)	Pipe (inches) (13)	Slope (%) (14)	Velocity (ft./sec.) (15)	Length (feet) (16)	T ₁ (minutes) (17)	T _c + T ₁ (minutes) (18)
505	6.1	0.52		20.5	3.60	11.4	20.5	3.60	11.4	11.40	24"	0.25	3.6	260	1.1	21.6
510	6.9	0.52		20.5	3.60	12.9	20.5	3.52	12.6	24.01	30"	0.34	4.9	50	-	21.6
530	9.1	0.52		14	4.17	19.7	14	4.17	19.7	19.7	24"	0.76	6.3	50	-	14
520	1.2	0.52		13.2	4.29	2.7	21.6	3.52	2.2	42.8	36"	0.41	6.1	160	0.4	22
540	-	-		-	-	-	22	-	-	42.8	36"	"	"	440	1.2	23.2
545	-	-		-	-	-	23.2	-	-	42.8	36"	"	"	440	1.2	25.4

HYDROLOGY DATA SHEET

PAGE 36 OF

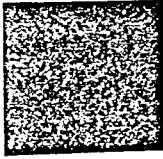
PROJECT: GOLDEN HILLS DRAINAGE PLAN

PROJECT NO. 36

ITEM:

DATE: 5-24-85

RETURN PERIOD: 2 COMPUTATIONS BY: M/B REVISIONS BY:



PROFESSIONAL ENGINEERING CONSULTANTS
PROFESSIONAL ASSOCIATION

1440 EAST ENGLISH
WICHITA, KANSAS 67211
(316) 262-2691

SCHEMATIC DIAGRAM:

See Previous Sheet for Sketch

PRELIM HYDR. COMP.

HYDROLOGY DATA																	
TRIBUTARY AREA					HYDROLOGY SUMMATION					CONDUIT DATA							
SUB-BASIN (1)	C (2)	AREA (acres) (3)	SLOPE (%) (4)	LENGTH (feet) (5)	T _c (minutes) (6)	I ₀ in./hr. (7)	Q ₀ (cfs) (8)	T _c (minutes) (9)	I in./hr. (10)	Q (cfs) (11)	Σ Q (cfs) (12)	PIPE (inches) (13)	SLOPE (%) (14)	VELOCITY (ft./sec.) (15)	LENGTH (feet) (16)	T _f (minutes) (17)	T _c + T _f (minutes) (18)
560	0.48	2.8			10.1	4.75	6.4	10.1	4.75	6.4	6.4	18"	0.37	3.6	80	0.4	10.5
570	0.48	0.7			10	4.75	1.6	10.5	4.67	1.6	8.0	21"	0.26	3.3	75	0.1	10.6
590	0.48	2.5			10.1	4.75	5.6	10.1	4.75	5.6	5.6	18"	0.28	3.2	80	0.4	10.5
580	0.48	1.6			10.1	4.75	3.6	10.5	4.67	3.5	17.1	30"	0.20	3.5	160	0.8	11.3
	1				Route to 550 @ 25.4 min.			25.4	3.28	12.0							
550	-							25.4	3.28		54.8	42"	0.30	5.7	400	1.2	26.6



PROFESSIONAL
ENGINEERING
CONSULTANTS
PROFESSIONAL ASSOCIATION

1440 EAST ENGLISH
WICHITA, KANSAS 67211
(316) 262 2691

HYDROLOGY DATA SHEET

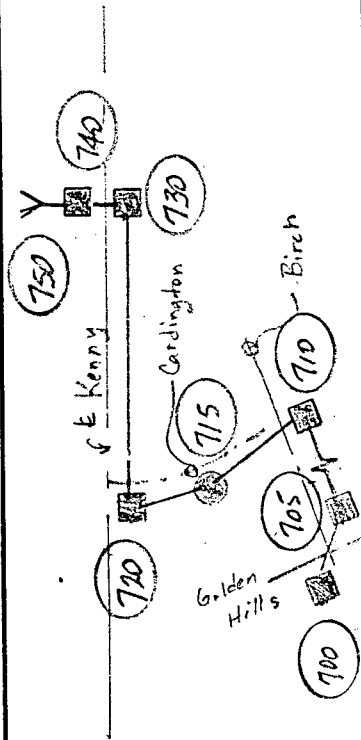
PAGE ____ OF ____

PROJECT: GOLDEN HILLS DRAINAGE PLAN PROJECT NO. _____

ITEM: SYSTEM 700 DATE: 5-28-85

RETURN PERIOD: 2-YR COMPUTATIONS BY: MWS REVISIONS BY: _____

SCHEMATIC DIAGRAM:



TRIBUTARY AREA

HYDROLOGY SUMMATION

CONDUIT DATA

SUB-BASIN (1)	C (2)	TRIBUTARY AREA				HYDROLOGY SUMMATION				CONDUIT DATA							
		AREA (acres) (3)	SLOPE (%) (4)	LENGTH (feet) (5)	T _c (minutes) (6)	I ₀ in./hr. (7)	Q ₀ (cfs) (8)	T _c (minutes) (9)	I in./hr. (10)	Q (cfs) (11)	Σ Q (cfs) (12)	PIPE (inches) (13)	SLOPE (%) (14)	VELOCITY (ft./sec.) (15)	LENGTH (feet) (16)	T ₁ (minutes) (17)	T _c + T ₁ (minutes) (18)
700	0.52	3.8	-	-	10	4.75	9.4	10	4.75	9.4	9.4	18	0.8	5.3	65	0.2	10.2
705	0.52	4.9	-	-	10	4.75	12.1	10.2	4.71	12.0	21.4	24	0.9	6.8	230	0.6	10.8
710	0.52	2.3	-	-	10	4.75	5.7	10.8	4.61	5.5	26.9	30	0.43	5.5	300	0.9	11.7
715	-	-	-	-	-	-	-	11.7	-	-	26.9	30	0.43	5.5	180	0.5	12.2
720	0.48	4.9	-	-	10	4.75	11.2	12.2	4.38	10.3	37.2	30	0.82	7.6	225	0.5	12.7
730	0.48	3.4	-	-	11.9	4.40	7.2	12.7	4.31	7.1	44.3	30	1.16	9.1	30	0.1	12.8
740	0.48	2.5	-	-	10	4.75	5.7	12.8	4.30	5.2	49.5	30	1.46	10.1	20	-	12.8

Node	Flow	Area	Velocity	Depth	Velocity	Depth	Area	Velocity	Depth	Area
130 t: MMB 5/29/85										
140 i	110	0.48	2.80	0.00	0.00	1.90	13.00	152.10		
150 i	120	0.48	5.80	0.00	0.00	0.00	12.40	152.10		
160 i	130	0.52	5.50	0.00	0.00	0.00	18.00	147.00		
170 i	150	0.48	1.70	0.00	0.00	7.80	10.00	144.60		
180 i	140	0.52	3.50	0.00	0.00	0.00	10.00	144.60		
185 i	170	0.48	3.20	0.00	0.00	0.00	10.00	145.00		
190 i	180	0.48	2.40	0.00	0.00	0.00	10.00	145.00		
200 i	190	0.48	0.60	0.00	0.00	0.00	10.00	144.50		
210 i	160	0.48	0.50	0.00	0.00	0.00	10.00	144.50		
220 m	200	142.00								
230 p	110	30.00	15	0.013	90.00	0.00				
240 p	120	270.00	21	0.013	0.00	0.00				
250 p	130	380.00	30	0.013	5.00	0.00				
260 p	150	30.00	18	0.013	90.00	0.00				
270 p	140	300.00	36	0.013	40.00	0.00				
280 p	170	30.00	18	0.013	135.00	0.00				
290 p	180	240.00	24	0.013	45.00	0.00				
300 p	160	50.00	36	0.013	0.00	0.00				
310 p	190	30.00	15	0.013	0.00	0.00				
320 e										

GOLDEN HILLS DRAINAGE PLAN
 SYSTEM 100 SHEFFORD
 MMB 5/29/85

Input File: sys100

Date: 05-30-1985
 Time: 16:12:52

F/M/L

Storm Frequency = 2-Year

* * * H Y D R O L O G Y * * *

Node to Node	Area (Ac)	Slope (%)	Length (Ft)	TC (0) (Min)	I (0) (In/Hr)	Q (0) (CFS)	Hydrology			Conduit Data							
							TC (Min)	I (In/Hr)	Q (CFS)	Sum Q (CFS)	Sum Q (CFS)	Size	Velocity (Ft/Sec)	Length (Ft)	TT (Min)	TT+TC (Min)	
110	120	0.48	2.80	0.00	0.0	13.00	4.29	1.90	13.00	4.29	1.90	1.90	15"	1.55	30.00	0.32	13.32
120	130	0.48	5.80	0.00	0.0	12.40	4.37	12.17	12.40	4.37	12.17	13.94	21"	5.80	270.00	0.78	13.18
130	140	0.52	5.50	0.00	0.0	18.00	3.78	10.81	18.00	3.78	10.81	23.15	30"	4.72	380.00	1.34	19.34
150	140	0.48	1.70	0.00	0.0	10.00	4.75	7.80	10.00	4.75	7.80	7.80	18"	4.41	30.00	0.11	10.11
140	160	0.52	3.50	0.00	0.0	10.00	4.75	8.65	19.34	3.68	6.69	35.90	36"	5.08	300.00	0.98	20.33
170	180	0.48	3.20	0.00	0.0	10.00	4.75	7.30	10.00	4.75	7.30	7.30	18"	4.13	30.00	0.12	10.12
180	160	0.48	2.40	0.00	0.0	10.00	4.75	5.48	10.12	4.73	5.45	12.75	24"	4.06	260.00	1.07	11.19
160	200	0.48	0.50	0.00	0.0	10.00	4.75	1.14	20.33	3.61	0.87	47.93	36"	6.78	50.00	0.12	20.45
190	160	0.48	0.60	0.00	0.0	10.00	4.75	1.37	10.00	4.75	1.37	1.37	15"	1.12	30.00	0.45	10.45

GOLDEN HILLS DRAINAGE PLAN
 SYSTEM 100 SHEFFORD
 MMB 5/29/85

Input File: sys100

Date: 05-30-1985
 Time: 16:12:52

* * * H Y D R A U L I C S * * *

Storm Frequency = 2-Year

```

*****
Node      Hyd-Slope      Friction      Bend      Transition      Manhole      Deflection      Junction      Total      Hyd-GI      Desired      Diff.
      (Ft/Ft)      (Ft)      (Ft)      (Ft)      (Ft)      (Ft)      (Ft)      (Ft)      Elevation      Elevation      (Ft)
*****
110      0.00087      0.0260      0.0000      0.0000      0.0000      0.0000      0.0000      0.0260      148.1728      152.1000      3.93
120      0.00774      2.0894      0.0000      0.0484      0.0000      0.0186      1.3548      3.5113      148.1469      152.1000      3.95
130      0.00319      1.2108      0.0000      0.0352      0.0000      0.0000      0.2693      1.5153      144.6356      147.0000      2.36
150      0.00551      0.1654      0.0000      0.0000      0.0000      0.0000      0.0000      0.1654      143.2857      144.6000      1.31
140      0.00290      0.8691      0.0000      0.0055      0.0000      0.0054      0.3951      1.2751      143.1203      144.6000      1.48
170      0.00483      0.1450      0.0000      0.0000      0.0000      0.0000      0.0000      0.1450      143.3278      145.0000      1.67
180      0.00318      0.8263      0.0000      0.0019      0.0000      0.2157      0.2938      1.3377      143.1828      145.0000      1.82
190      0.00045      0.0135      0.0000      0.0000      0.0000      0.0000      0.0000      0.0135      141.8586      144.5000      2.64
160      0.00516      0.2582      0.0000      0.0313      0.0000      0.0757      0.4800      0.8452      141.8452      144.5000      2.65
200      0.00000      0.0000      0.0000      0.0000      0.0000      0.0000      0.0000      0.0000      141.0000      142.0000      1.00
*****

```

100 J, 146.6000 430 3 13 12
 110 t, GOLDEN HILLS DRAINAGE PLAN
 120 t, SYSTEM 300 CENTRAL AVE 5-YR PIPE DESIGN
 130 t, NMB 5/29/85

140 I,	310	0.57	1.40	0.00	0.00	0.00	2.40	10.00	158.60
150 I,	320	0.57	2.90	0.00	0.00	0.00	0.00	10.00	158.60
160 I,	325	0.73	4.70	0.00	0.00	0.00	0.00	9.00	156.70
170 I,	330	0.54	2.40	0.00	0.00	0.00	5.00	11.10	156.70
180 I,	350	0.57	1.60	0.00	0.00	0.00	8.10	10.00	156.10
190 I,	340	0.57	1.10	0.00	0.00	0.00	1.70	10.00	156.10
200 m,	340	154.90							
210 I,	380	0.57	0.60	0.00	0.00	0.00	1.50	10.00	153.80
220 I,	370	0.54	1.60	0.00	0.00	0.00	4.90	10.00	153.80
230 I,	400	0.57	3.60	0.00	0.00	0.00	13.10	13.60	153.80
240 I,	410	0.57	2.90	0.00	0.00	0.00	4.90	11.80	153.80
250 m,	390	152.90							
260 m,	430	150.40							
270 P,	310	30.00	15 0.013	45.00	0.00	0.00			
280 P,	320	30.00	21 0.013	45.00	0.00	0.00			
290 P,	325	50.00	36 0.013	90.00	0.00	0.00			
300 P,	330	340.00	36 0.013	0.00	0.00	0.00			
310 F,	350	30.00	15 0.013	90.00	0.00	0.00			
320 P,	340	75.00	18 0.013	90.00	0.00	0.00			
330 P,	340	250.00	36 0.013	0.00	0.00	0.00			
340 P,	380	50.00	15 0.013	90.00	0.00	0.00			
350 P,	370	200.00	36 0.013	0.00	0.00	0.00			
360 P,	400	30.00	18 0.013	90.00	0.00	0.00			
370 P,	410	75.00	21 0.013	90.00	0.00	0.00			
380 P,	390	520.00	42 0.013	0.00	0.00	0.00			
390 e									

GOLDEN HILLS DRAINAGE PLAN
 SYSTEM 300 CENTRAL AVE 5-YR PIPE DESIGN
 MMB 5/29/85

Storm Frequency = 5-Year

Input File: sves300

Date: 06-03-1985
 Time: 12:58:38
 F/M/L

* * * H Y D R O L O G Y * * *

Tributary Area		Hydrology		Summation		Conduit Data										
Node	Area (Ac)	TC (Min)	I (In/Hr)	TC (Min)	I (In/Hr)	Size	Velocity (Ft/Sec)	Length (Ft)	TI (Min)	TI+TC (Min)						
310	320 0.57	1.40	0.00	0.0	10.00	6.11	2.40	10.00	6.11	2.40	15"	1.96	30.00	0.26	10.26	
320	325 0.57	2.90	0.00	0.0	10.00	6.11	10.10	10.00	6.11	10.10	21"	5.17	30.00	0.10	10.10	
325	330 0.73	4.70	0.00	0.0	9.00	6.37	21.85	10.10	6.09	20.89	36"	4.72	50.00	0.18	10.27	
330	340 0.54	2.40	0.00	0.0	11.10	5.87	5.00	10.27	6.05	4.63	36"	5.37	340.00	1.06	11.33	
350	360 0.57	1.60	0.00	0.0	10.00	6.11	8.10	10.00	6.11	8.10	18"	5.54	75.00	0.23	10.30	
360	340 0.57	1.10	0.00	0.0	10.00	6.11	1.70	10.08	6.09	1.70	36"	6.70	250.00	0.62	11.95	
340	370 0.00	0.00	0.00	0.0	0.00	0.00	0.00	11.33	5.82	0.00	47.39	15"	1.22	50.00	0.68	10.68
350	370 0.57	0.60	0.00	0.0	10.00	6.11	1.50	10.00	6.11	1.50	15"	7.55	200.00	0.44	12.39	
370	390 0.54	1.60	0.00	0.0	10.00	6.11	4.90	11.95	5.70	4.57	36"	7.55	200.00	0.44	12.39	
400	410 0.57	3.60	0.00	0.0	13.60	5.42	13.10	13.60	5.42	13.10	18"	7.41	30.00	0.07	13.67	
410	390 0.57	2.90	0.00	0.0	11.80	5.73	4.90	13.67	5.41	4.63	21"	7.37	75.00	0.17	13.84	
390	430 0.00	0.00	0.00	0.0	0.00	0.00	0.00	12.39	5.62	0.00	69.28	42"	7.20	520.00	1.20	13.59

GOLDEN HILLS DRAINAGE PLAN
 SYSTEM 300 CENTRAL AVE 5-YR PIPE DESIGN
 MMB 5/29/85

Input File: sys300

Storm Frequency = 5-Year

* * * H Y D R A U L I C S * * *

Node	Hyd-Slope (Ft/Ft)	Friction (Ft)	Bend (Ft)	Transition (Ft)	Manhole (Ft)	Deflection (Ft)	Junction (Ft)	Total (Ft)	Hyd-GI Elevation	Desired Elevation	Diff. (Ft)
310	0.00138	0.0414	0.0000	0.0000	0.0000	0.0000	0.0000	0.0414	156.6614	158.6000	1.94
320	0.00617	0.1850	0.0000	0.0356	0.0000	0.0129	1.0408	1.2743	156.6199	158.6000	1.98
325	0.00250	0.1248	0.0000	0.0140	0.0000	0.0704	0.6311	0.8604	155.3457	156.7000	1.35
330	0.00324	1.1011	0.0000	0.0103	0.0000	0.1726	0.2198	1.5037	154.4852	156.7000	2.21
350	0.01572	0.4717	0.0000	0.0000	0.0000	0.0000	0.0000	0.4717	154.5618	156.1000	1.54
360	0.00870	0.6521	0.0000	0.0399	0.0000	0.3382	0.0784	1.1086	154.0901	156.1000	2.01
340	0.00505	1.2623	0.0000	0.0250	0.0000	0.0000	0.5224	1.8097	152.9815	154.9000	1.92
380	0.00054	0.0270	0.0000	0.0000	0.0000	0.0000	0.0000	0.0270	151.1988	153.8000	2.60
370	0.00641	1.2821	0.0000	0.0188	0.0000	0.0000	0.4057	1.7066	151.1718	153.8000	2.63
400	0.01555	0.4666	0.0000	0.0000	0.0000	0.0000	0.0000	0.4666	151.8697	153.8000	1.93
410	0.01252	0.9388	0.0000	0.0020	0.0000	0.4267	0.5705	1.9378	151.4031	153.8000	2.40
390	0.00474	2.4654	0.0000	0.0162	0.0000	0.0000	0.3835	2.8652	149.4652	152.9000	3.43
430	0.00000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	146.6000	150.4000	3.80

100 J	151.0000	600	2	12	11															
110 t	GOLDEN HILLS DRAINAGE PLAN																			
120 t	SYSTEM 500-PINE GROVE																			
130 i	505	0.52	6.10	0.00	0.00	5/24/85	0.00	0.00	20.50	158.50										
140 i	510	0.52	6.90	0.00	0.00		0.00	0.00	20.50	157.40										
150 i	530	0.52	9.10	0.00	0.00		0.00	0.00	14.00	157.40										
160 i	520	0.52	1.20	0.00	0.00		0.00	0.00	13.20	157.40										
170 m	540	157.10																		
180 m	545	158.50																		
190 i	560	0.48	2.30	0.00	0.00		0.00	0.00	10.10	159.10										
200 i	570	0.48	0.70	0.00	0.00		0.00	0.00	10.00	159.10										
210 i	590	0.48	2.50	0.00	0.00		0.00	0.00	10.10	159.10										
220 i	580	0.48	1.60	0.00	0.00		0.00	0.00	10.10	159.10										
230 m	550	158.30																		
240 m	600	153.00																		
250 p	505	510	260.00	21	0.013	45.00	0.00	0.00												
260 p	510	520	50.00	30	0.013	45.00	0.00	0.00												
270 p	530	520	50.00	24	0.013	45.00	0.00	0.00												
280 p	520	540	160.00	42	0.013	90.00	0.00	0.00												
290 p	540	545	440.00	42	0.013	0.00	0.00	0.00												
300 p	545	550	440.00	42	0.013	0.00	0.00	0.00												
310 p	570	570	80.00	15	0.013	90.00	0.00	0.00												
320 p	580	580	35.00	18	0.013	90.00	0.00	0.00												
330 p	590	580	80.00	15	0.013	0.00	0.00	0.00												
340 p	580	550	160.00	21	0.013	90.00	0.00	0.00												
350 p	550	600	400.00	42	0.013	0.00	0.00	0.00												
360 e																				

Trial # 5
SYSTEM 500
(LISE)

GOLDEN HILLS DRAINAGE PLAN
SYSTEM 500-PINE GROVE

MMB

5/24/85

Input File: sv5500

Storm Frequency = 2-Year

Date: 05-24-1985
Time: 15:55:28

* * * H Y D R O L O G Y * * *

***** Tributary Area *****		***** Hydrology *****		***** Summation *****		***** Conduit Data *****											
Node to	Area (Ac)	Slope (%)	Length (Ft)	TC (Min)	I (In/Hr)	Q (CFS)	Sum Q (CFS)	Size	Velocity (Ft/Sec)	Length (Ft)	TT (Min)	TT+TC (Min)					
505	510	0.52	6.10	0.00	0.0	20.50	3.59	11.40	20.50	3.59	11.40	11.40	21"	4.74	260.00	0.94	21.41
510	520	0.52	6.90	0.00	0.0	20.50	3.59	12.89	21.41	3.53	12.67	24.07	30"	4.90	50.00	0.17	21.58
530	520	0.52	9.10	0.00	0.0	14.00	4.17	19.73	14.00	4.17	19.73	19.73	24"	6.28	50.00	0.13	14.13
520	540	0.52	1.20	0.00	0.0	13.20	4.27	2.66	21.58	3.52	2.20	43.00	42"	4.47	160.00	0.60	22.18
540	545	0.00	0.00	0.00	0.0	0.00	0.00	0.00	22.18	3.48	0.00	43.00	42"	4.47	440.00	1.64	23.82
545	550	0.00	0.00	0.00	0.0	0.00	0.00	0.00	23.82	3.39	0.00	43.00	42"	4.47	440.00	1.64	25.46
560	570	0.48	2.80	0.00	0.0	10.10	4.74	6.36	10.10	4.74	6.36	6.36	15"	5.19	80.00	0.26	10.36
570	580	0.48	0.70	0.00	0.0	10.00	4.75	1.60	10.36	4.69	1.58	7.94	18"	4.49	35.00	0.13	10.49
590	580	0.48	2.50	0.00	0.0	10.10	4.74	5.68	10.10	4.74	5.68	5.68	15"	4.63	80.00	0.29	10.39
580	550	0.48	1.60	0.00	0.0	10.10	4.74	3.64	10.49	4.67	3.58	17.19	21"	7.15	160.00	0.37	10.86
550	600	0.00	0.00	0.00	0.0	0.00	0.00	0.00	25.46	3.30	0.00	55.32	42"	5.75	400.00	1.16	26.62

GOLDEN HILLS DRAINAGE PLAN
SYSTEM 500-PINE GROVE

MMB 5/24/85

Input File: sys500

Storm Frequency = 2-Year

* * * H Y D R A U L I C S * * *

Node	Hyd-Slope (Ft/Ft)	Friction (Ft)	Bend (Ft)	Transition (Ft)	Manhole (Ft)	Deflection (Ft)	Junction (Ft)	Total (Ft)	Hyd-GI Elevation (Ft)	Desired Elevation (Ft)	Diff. (Ft)
505	0.00517	1.3453	0.0000	0.0000	0.0000	0.0000	0.0000	1.3453	156.2647	158.5000	1.54
510	0.00344	0.1722	0.0000	0.0025	0.0000	0.0759	0.5664	0.8170	155.6194	157.4000	1.78
530	0.00761	0.3803	0.0000	0.0000	0.0000	0.0000	0.0000	0.3803	155.1827	157.4000	2.22
520	0.00183	0.2922	0.0000	0.0127	0.0000	0.0813	-0.0447	0.3415	154.8024	157.4000	2.60
540	0.00183	0.8036	0.0000	0.0000	0.0155	0.1551	0.0091	0.9833	154.4609	157.1000	2.64
545	0.00183	0.8036	0.0000	0.0000	0.0155	0.0000	0.0091	0.8283	153.4776	158.5000	5.02
560	0.00971	0.7766	0.0000	0.0000	0.0000	0.0000	0.0000	0.7766	156.9873	159.1000	2.11
570	0.00571	0.2000	0.0000	0.0208	0.0000	0.2088	0.0741	0.5238	156.2107	159.1000	2.89
590	0.00774	0.6191	0.0000	0.0000	0.0000	0.0000	0.0000	0.6191	156.3061	159.1000	2.79
580	0.01176	1.8824	0.0000	0.0479	0.0000	0.1568	0.9506	3.0376	155.6869	159.1000	3.41
550	0.00302	1.2095	0.0000	0.0203	0.0000	0.0000	0.4195	1.6493	152.6493	158.8000	6.15
600	0.00000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	151.0000	153.0000	2.00

GOLDEN HILLS DRAINAGE PLAN
 SYSTEM 700 MMB 6-02-85
 GOLDEN HILLS/BIRCH/CARDINGTON/KENNY

Input File: sys700

Storm Frequency = 2-Year

Date: 06-03-1985
 Time: 13:22:40

* * * H Y D R O L O G Y * * *

Tributary Area		Hydrology Summation										Conduit Data					
Node to	Area (Ac)	Slope (%)	Length (Ft)	TC (Min)	I (In/Hr)	Q (CFS)	TC (Min)	I (In/Hr)	Q (CFS)	Sum Q (CFS)	Size	Velocity (Ft/Sec)	Length (Ft)	TT (Min)	TT+TC (Min)		
700	705	0.52	3.80	0.00	0.0	10.00	4.75	9.39	10.00	4.75	9.39	9.39	18"	5.32	65.00	0.20	10.20
705	710	0.52	4.50	0.00	0.0	10.00	4.75	5.40	10.20	4.72	5.36	14.75	24"	4.70	230.00	0.82	11.02
710	715	0.52	2.30	0.00	0.0	10.00	4.75	12.10	11.02	4.58	11.65	26.40	30"	5.38	300.00	0.93	11.95
715	720	0.00	0.00	0.00	0.0	0.00	0.00	0.00	11.95	4.44	0.00	26.40	30"	5.38	180.00	0.56	12.51
720	730	0.48	4.90	0.00	0.0	10.00	4.75	11.18	12.51	4.36	10.25	36.65	30"	7.47	225.00	0.50	13.01
730	740	0.48	3.40	0.00	0.0	11.90	4.44	7.25	13.01	4.29	7.00	43.65	36"	6.18	30.00	0.08	13.09
740	750	0.48	2.50	0.00	0.0	10.00	4.75	5.70	13.09	4.28	5.14	48.79	36"	6.90	20.00	0.05	13.14

GOLDEN HILLS DRAINAGE PLAN
 SYSTEM 700 MMB 6-02-85
 GOLDEN HILLS/BIRCH/CARDINGTON/KENNY

Input File: sys700

Storm Frequency = 2-Year

* * * H Y D R A U L I C S * * *

Node	Hyd-Slope (Ft/Ft)	Friction (Ft)	Bend (Ft)	Transition (Ft)	Manhole (Ft)	Deflection (Ft)	Junction (Ft)	Total (Ft)	Hyd-Gl Elevation	Desired Elevation	Diff. (Ft)
700	0.00800	0.5199	0.0000	0.0000	0.0000	0.0000	0.0000	0.5199	156.1841	159.5000	3.32
705	0.00425	0.9780	0.0000	0.0193	0.0000	0.0587	0.2757	1.3317	155.6642	159.0000	3.34
710	0.00414	1.2430	0.0000	0.0107	0.0000	0.1712	0.5832	2.0081	154.3325	158.2000	3.87
715	0.00414	0.7458	0.0000	0.0000	0.0000	0.0262	0.0208	0.8152	152.3245	156.8000	4.48
720	0.00798	1.7963	0.0000	0.0416	0.0000	0.2397	0.3646	2.9422	151.5093	155.8000	4.29
730	0.00428	0.1285	0.0000	0.0547	0.0000	0.4328	0.0096	0.6256	148.5671	152.0000	3.43
740	0.00535	0.1070	0.0000	0.0148	0.0000	0.0000	0.3198	0.4415	147.9415	152.0000	4.06
750	0.00000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	147.5000	147.5000	0.00

Q = CLH^{1.48}



Date 5/30/85 MWB Page _____ of _____

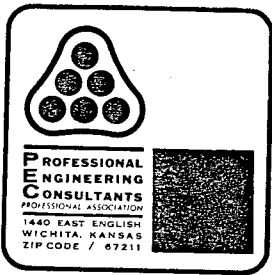
Project GOLDEN HILLS DRAINAGE PLAN

Item SYSTEM 100/300

Q100 CHECK

‡ Approx. for mini-sump

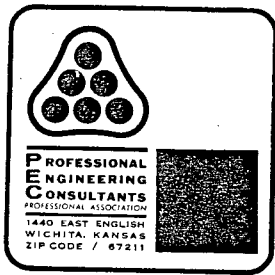
NODE	Tc Min	i100/12	Q2 cfs	Q100 cfs	ΣQ cfs	Qpipe cfs	Q100-Qp cfs	So %	Bk-Bk Street Width	MAX DISCHARGE (cfs) @ d =				
										T.C. +0.3'	T.C. +0.4'	T.C. +0.52'	T.C. +0.63'	T.C. +0.63'
110	13	2.21	5.8	12.8	10.9	1.9	10.9	0.43	29'	14.6				
120	13	2.21	11.9	26.3	14.4	11.9	14.4	0.43	"	14.6				
130	18	2.21	10.8	23.9	27.5	10.8	13.1	3.00	"	38.6				
140	19	2.21	6.7	14.8	35.6	6.7	8.1	0.32	"		34.8	SPILL	O.B TO	E SIDE
150	10	2.21	3.9	8.6	12.5	7.8	0.8	0.32	"	12.6				
		0.8 + 0.8 + 10.9 =		4										
190	10	2.21	1.37	3.0	37.2	1.4	1.6	0.27‡	"		32	Spill 5.2 cfs to E. side		
		Ignore Q100 overflow from 170/80. Will overtop curb & enter creek												
		System 300: Check side streets only. Assume conveyance in Central Ave 100' R.O.W. is adequate.												
310	10	2.21	4.9	10.8				1.1	35'	23.8				OK
320	10	2.21	6.1	13.5				1.1	"	23.8				OK
350	10	2.21	5.6	12.4				0.32	29'	12.6				OK
360	10	2.21	3.8	8.4				0.32	"	12.6				OK
400	13.6	2.21	11.1	24.6				0.32	"	12.6	34.8			
410	13.7	2.21	8.9	19.7				0.32	"	12.6	34.8			



Date 5/30/85 MNB Page of
 Project GOLDEN HILLS DRAINAGE PLAN
 Item SYSTEM 500

Q100 CHECK

NODE	Tc Min	i100/12	Q2 cfs	Q100 cfs	ΣQ cfs	Qpipe cfs	Q100-Qp cfs	So %	Bk-Bk Street Width	MAX DISCHARGE (cfs) @ d =					
										T.C. +0.3'	T.C. +0.41'	T.C. +0.52'	T.C. +0.63'	T.C. +0.63'	
505	20.5	2.21	11.4	25.2	13.8	11.4	13.8	0.32	29'	12.6	34.8				
510	21.4	2.21	12.7 from	28.1 So.	21.5		12.7	15.4		"	12.6	34.8			
530	14	2.21	19.7 from	43.6 No.	29		19.7	23.9			15.8	43.5			
520	22	2.21	2.2	4.8	2.8	2.2	2.2	OK BY INSPECTION							
ΣQ ₁₀₀ arriving @ Beckmeyer & Pine Grove = 13.8 + 28.1 + 43.6 = 85.5 cfs ΣQ ₁₀₀ @ 520, 530, 510 = 12.7 + 19.7 + 2.2 = 34.6 Design Flume for 85.5 - 34.6 = 50.9 cfs (NO)															
For b = 18', Q = 51 cfs, n = 0.016, d = 0.5' = S _{min} = 0.008 ff/ft															
560	10.1	2.21	6.4	14.2		6.4	7.8	0.32	35	12.6	34.8				
570	10.4	2.21	1.6	3.5		1.6	1.9	0.32	35	12.6					
580	10.1	2.21	5.7	12.6		5.7	6.9	0.32	35	12.6					
590	10.5	2.21	3.6	8.0		3.6	4.4	0.32	35	12.6					
@ Pine Grove & Hickory: ΣQ ₁₀₀ = 38.3 cfs Qp = 17.3 cfs Overflow = 21 cfs S _o = $\frac{0.4}{17.5} = 0.23\%$ = 0.23% = 21.0 for full width															



Date 5/30/85 MWB Page _____ of _____

Project GOLDEN HILLS DRAINAGE PLAN

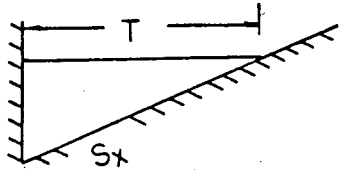
Item SYSTEM 700 / 800 / MISC.

Q100 CHECK

NODE	Tc Min	i100/12	Q2 cfs	Q100 cfs	ΣQ cfs	Qpipe cfs	Q100-Qp cfs	So %	Bk-Bk Street Width	MAX DISCHARGE (cfs) @ d =				
										T.C. +0.3'	T.C. +0.4'	T.C. +0.52	T.C. +0.63'	T.C. +0.63'
700	10	2.21	9.4	20.8	11.4	9.4	11.4	0.32	35	12.9	37.9			
705	10.2	2.21	12.0	26.5	32.5	5.4	21.1	0.80	35	20.3	60			
710	10.8	2.21	5.5	12.2	32.6	12.1	0.1	0.32	29	12.6	34.8			
720	12.2	2.21	10.3	22.8	45.1	10.3	12.5	0.43	29	14.9	44	SPILL	OVER CROWN	1.1 cfs
730								1.75						
740								1.75						
800	10	2.21	2.5	5.5		2.5	3.0	2.88	29	DK BY INSPECTION				
810	10	2.21	4.1	9.1		4.1	5.0	2.88	29	DK BY INSPECTION				
450	11.9	2.21	7.9	17.5		7.9	9.6	0.40	29	14.1	38.9			
460	19.2	2.21	15.6	34.5		15.6	18.9	0.40	29	14.1	38.9			
910	10	2.21	2.1	4.6		2.1	2.5	0.32	29	12.6	34.8			
920	10	2.21	6.4	14.2		6.4	7.8	0.32	29	12.6	34.8			

OVERFLOW AT 740 TOPS CURB & INTO RESERVE C

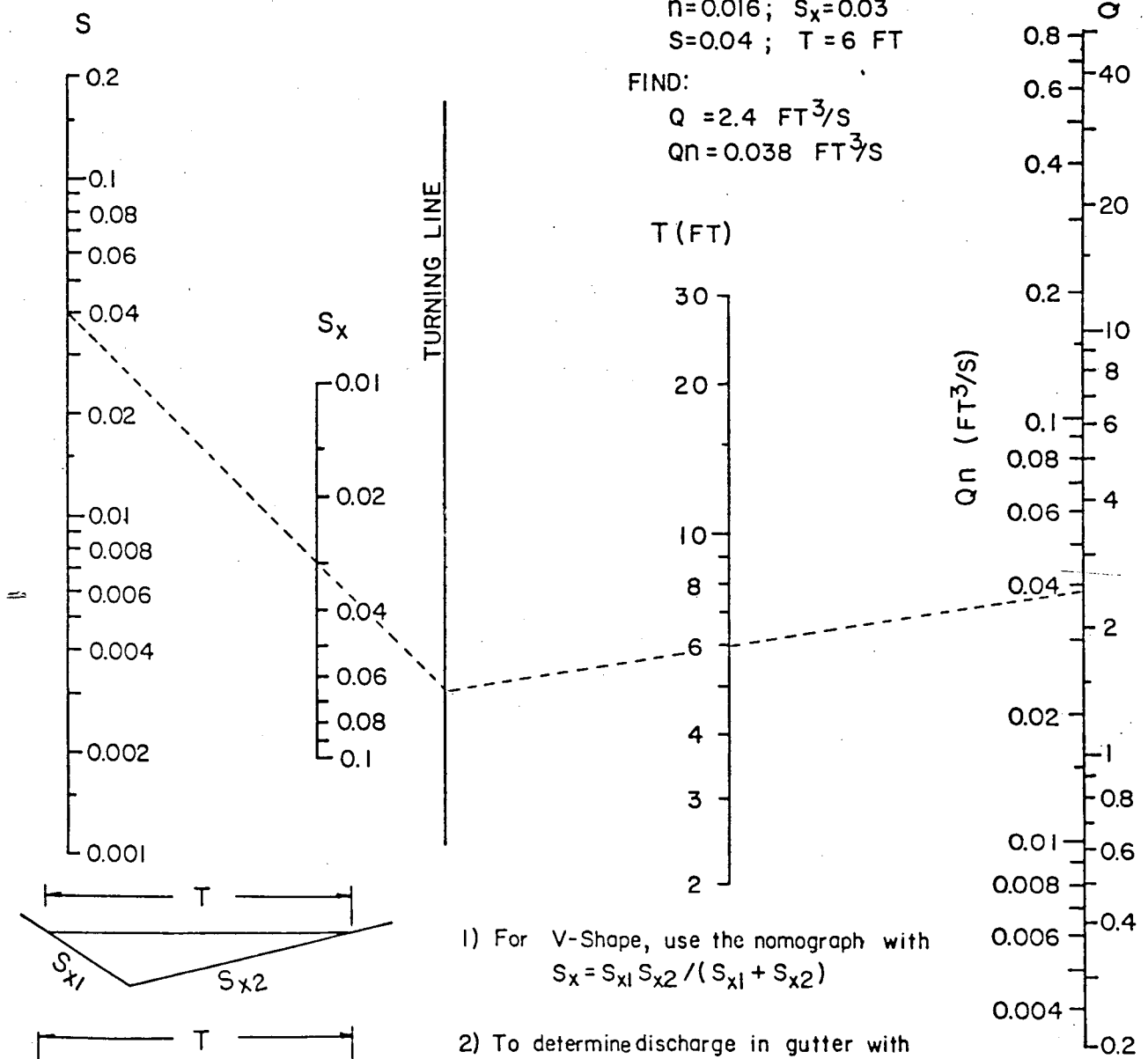
OVERFLOW TOP CURB & FLOWS DIRECTLY TO COWSKIN CR



$$Q = \frac{0.56}{n} S_x^{1.67} S^{0.5} T^{2.67}$$

EXAMPLE: GIVEN:
 $n=0.016$; $S_x=0.03$
 $S=0.04$; $T=6$ FT

FIND:
 $Q = 2.4$ FT³/S
 $Qn = 0.038$ FT³/S



- 1) For V-Shape, use the nomograph with $S_x = S_{x1} S_{x2} / (S_{x1} + S_{x2})$
- 2) To determine discharge in gutter with composite cross slopes, find Q_s using T_s and S_x . Then, use CHART 4 to find E_o . The total discharge is $Q = Q_s / (1 - E_o)$, and $Q_w = Q - Q_s$.

CHART 3. Flow in triangular gutter sections.

FROM: HEC-12 DRAINAGE OF HIGHWAY SUBURBS F.H.W. A., Mar. 1984



Date 6-5-85 MMB Page _____ of _____

Project GOLDEN HILLS DRAINAGE PLAN

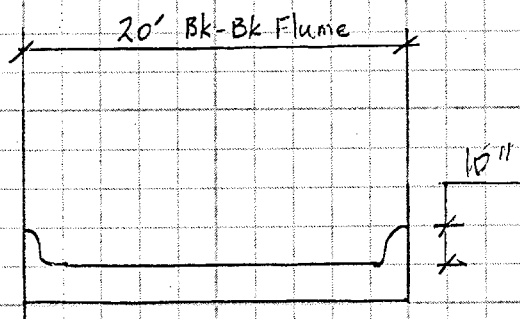
Item BEKEMEYER FLUME

$$\Sigma Q_{100} = 13.8 + 28.1 + 43.6 = 85.5 \text{ cfs} \quad (\text{Added peak on peak})$$

$$\Sigma Q_{\text{PIPE}} = 12.7 + 19.7 + 2.2 = 34.6 \text{ cfs} \quad (\text{Assume capacity} = 2\text{-yr discharge})$$

Design flume for $85.5 - 34.6 = 50.9 \text{ cfs}$

Proposed section



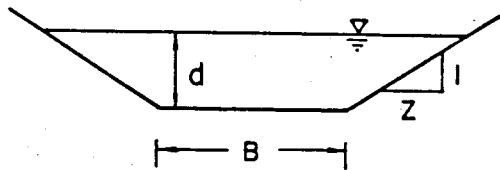
$$\begin{aligned} S &= 0.002 \text{ ft/ft} \\ n &= 0.016 \\ B &= 19' \\ d_{\text{max}} &= 0.83' \\ Q &= 51 \text{ cfs} \\ Q_n &= 0.82 \\ z &= 0 \end{aligned}$$

Using Chart 16, p. 94, HEC-12

$$\frac{d}{B} = 0.041$$

$$d = 0.041(19) = 0.78' \text{ OK}$$

$$V = \frac{Q}{A} = \frac{51}{(0.78)(19)} = 3.4 \text{ ft/sec}$$



NOTE: Project horizontally from Z=0 scale to obtain values for Z=1 to 6

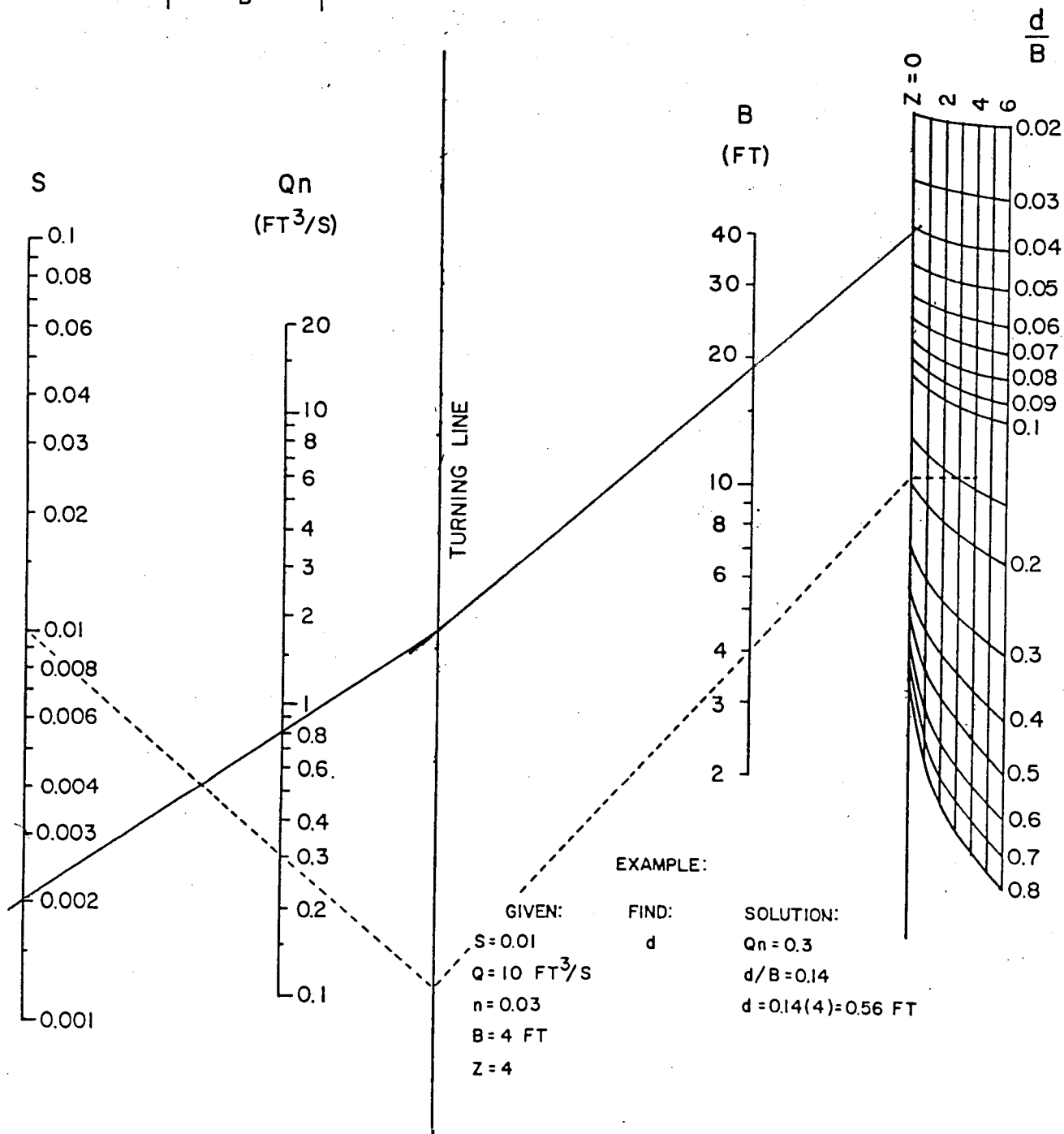


CHART 13. Solution of Manning's equation for channels of various side slopes.



1" = 1000'

119th St. W

CORPORATE LIMITS

CENTRAL

AVENUE

LUCILLE

CORPORATE LIMITS

CORPORATE

County of Sedgwick

PROPOSED GOLDEN HILLS PLAT

Cowskin Creek

Cowskin Creek

1330'
43.3

1329' MSL
142.2

Middle Fork Calfskin Creek

North Fork Calfskin Creek

MAPLE CEDAR CREST STREET

CORPORATE LIMITS

County of Sedgwick

CORPORATE LIMITS

KENT MILLSTEAD PARTRIDGE TAFT CAR GTON COVINGTON

SHEFFORD

CIRCLE LAKE

WEST SHORE

HIDDEN VALLEY

VALLEY HI

MILLSTEAD PARTRIDGE TAFT CAR GTON COVINGTON

KENT

MILLSTEAD

PARTRIDGE

TAFT

CAR

GTON

COVINGTON

SHEFFORD

CIRCLE LAKE

WEST SHORE

HIDDEN VALLEY

VALLEY HI

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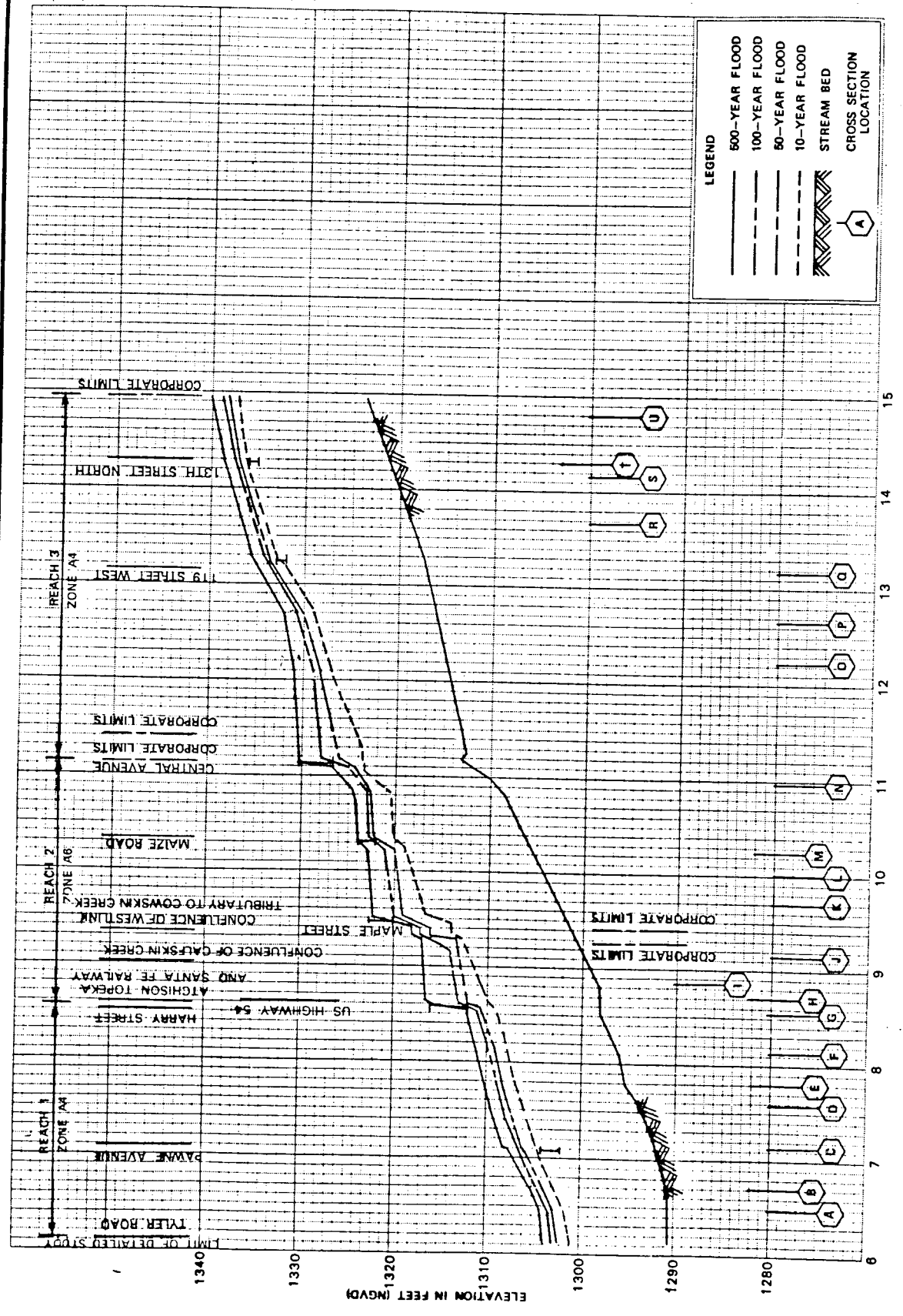
CIRCLE LAKE

WEST SHORE

HIDDEN VALLEY

VALLEY HI

FLOOD PROFILES
COMSKIN CREEK



STREAM DISTANCE IN MILES ABOVE CONFLUENCE WITH WICHITA-VALLEY CENTER FLOODWAY