

**Creekside at Pembrook**  
**Wichita, Sedgwick County, Kansas**

04/29/04

Creekside at Pembrook is an 18.6 acre, single family, residential development within the city limits of Wichita in Sedgwick County, Kansas. The 47 lot development consists of streets, storm sewer and a detention pond. This report contains a drawing of the drainage plan, supporting calculations and data for the Creekside at Pembrook Drainage Plan.

**Hydrology**

The proposed plat lies in the NE 1/4, Section 2, T27S, R1E. The soil on-site is comprised of Elandco silt loam, Farnum loam, Irwin silty clay loam, which are classified in hydrologic groups B, B and D, respectively. The land is currently used for agricultural purposes and has short grass and bare ground throughout except for along the drainage channel on the west property line which is heavily wooded. The site is bordered to the north by an agricultural field, to the east by Oliver, and to the south and west by Greenbriar Manor. A natural drainage channel runs along the west property line from the north to the south property lines and has approximately 303 acres of contributing area including this site. Existing Basin A drains off the site to Oliver on the east and Existing Basin B drains into the natural drainage channel on the west. Proposed Basin 1 flows to a proposed pond and eventually to the natural drainage channel on the west where it combines with Basin 2. Basin 3 drains to the same outfall as Existing Basin A.

The Rational Method was used to calculate runoff quantities. Runoff coefficients were estimated based on tables presented in the Design Aids section of this report using fully developed conditions. Time of concentration was based on slope, flow velocity and length of flow through each basin and was not allowed to be less than 15 minutes. The HEC-1 computer program was used to route the runoff through the ponds and determine the post-development conditions leaving the site.

The analysis was made based on the available site data which includes the following: 1" = 60' topographic map with 1' contours of the site, a Sedgwick County Soil Survey Map and noted references.

### **Storm Sewer Design**

For the storm sewer hydrologic analysis, the Rational Method was again used. Runoff coefficients were estimated using the charts in the design aids section of this report. For this development, a uniform assumption of the minimum time of concentration of 15 minutes was deemed appropriate. Travel time for flow through defined channels, pipes, etc, for these basins was estimated on the basis of Manning's Equation.

In the hydraulic analysis, the storm sewers are designed for the minor storm, with major storm overflows to be routed through easements and rights-of-way to an appropriate outlet. The minor storm has a recurrence interval of two years. The major storm evaluated has a recurrence interval of one hundred years. To simplify this analysis, the time of concentration is identical for both the major and minor storms.

For each inlet, street flooding and inlet capacity were checked for the minor storm. Conveyance in the street is based on the Modified Manning's Equation, as expressed in the Design of Urban Highway Drainage – The State of the Art, Equation (5-1), pages 5-9. It has been assumed that  $T_c$  for street flow is equal to  $T_c$  for pipe flow. This is a simplifying, but conservative, assumption since pipe flow velocities generally exceed street flow velocities. For local streets, curb-deep flow is tolerable for the minor storm. For collector streets, a single eight-foot lane should remain unflooded for the minor storm.

Inlet capacities were determined by the methods described in Drainage of Highway Pavements, Hydraulic Engineering Circular #12, using Chart #12 as found in the Design Aids section. City of Wichita Type 1A inlets and 3/8 inch per foot cross slopes have been assumed. Minimum walk grade has been assumed to be 0.3 feet above the top of

curb, unless otherwise noted. Streets have been assumed to have 6-5/8 inch standard curb, unless otherwise noted.

Hydraulic computation for the storm sewer pipe system was performed using PEC's STORM computer program. This program uses Manning's Equation to calculate friction losses for pipes flowing full. Minor losses are computed by momentum principles at each structure. All pipe area is assumed to be reinforced concrete with a Manning's "n" of 0.013. It is desirable to keep the hydraulic grade line at least one foot below the top of curb for the minor storm. The calculations and the STORM analyses for the storm sewers are included in this report.

### Design Aids

This section includes material used to assist in designing the drainage system. A 1" = 60' scale Drainage Plan map (Attachment A) and a 1" = 60' scale Four-Corner Plan map (Attachment B) are enclosed in the pockets.

### References

Design of Urban Highway Drainage – The State of the Art, by Reitz & Jens, Inc., April 1980.

Drainage of Highway Pavements, Hydraulic Engineering Circular #12, by Tye Engineering, Inc., March 1984.

Interim Drainage and Storm Sewer Policy for Design Criteria and Documentation, City of Wichita, Kansas, 1985.

Soil Survey of Sedgwick County, Kansas, US Department of Agriculture, Soil Conservation Service, 1979.

Project: Creekside at Pembrook  
 Date: 4/28/2004  
 Prep. By: BLB

Manual Input

**OFFSITE**

Total Area 3.68 Acres

Soil Group	A	B	C	D	Total
	(% of Total Area)	(% of Total Area)	(% of Total Area)	(% of Total Area)	
	0%	50%	0%	50%	100%
Acres	0.00	1.84	0.00	1.84	3.68

Land Use	Commercial	Industrial	Multi-Family	Public	Single Family	Vacant/Agriculture	Total
	(% of Total Area)	(% of Total Area)	(% of Total Area)	(% of Total Area)	(% of Total Area)	(% of Total Area)	
Future	0%	0%	0%	0%	0%	100%	100%
Acres	0.00	0.00	0.00	0.00	0.00	3.68	3.68

**Existing**

Length of Flow 700 ft  
 Slope 1.69 %  
 Waterflow Desc bare / short grass  
 Avg Velocity 0.55 ft/sec  
 Tc 0.35 hours

15 min <= Tc <= 24 hrs

Runoff Coefficients \* Used Soil Group D To Be Conservative

Return Period (Years)	Commercial	Industrial	Multi-Family	Public	Single Family	Vacant/Agriculture
2	0.68	0.68	0.70	0.49	0.50	0.54
5	0.69	0.69	0.73	0.51	0.54	0.56
10	0.73	0.73	0.79	0.56	0.62	0.61
25	0.75	0.75	0.81	0.59	0.66	0.64
50	0.77	0.77	0.83	0.62	0.70	0.67
100	0.80	0.80	0.86	0.66	0.76	0.70

Future Conditions

Return Period (Years)	Runoff Coefficient *	Rainfall Intensity (in/hr)	Area (Acres)	Runoff (cfs)
2	0.54	3.25	3.68	6.46
5	0.56	3.90	3.68	8.04
10	0.61	4.50	3.68	10.10
25	0.64	5.23	3.68	12.32
50	0.67	5.87	3.68	14.47
100	0.70	6.39	3.68	16.46

Project: Creekside at Pembroke  
 Date: 4/28/2004  
 Prep. By: BLB

Manual Input

**Basin A**

Total Area 1.10 Acres

Soil Group	A (% of Total Area)	B (% of Total Area)	C (% of Total Area)	D (% of Total Area)	Total
	0%	50%	0%	50%	100%
Acres	0.00	0.55	0.00	0.55	1.10

Land Use	Commercial (% of Total Area)	Industrial (% of Total Area)	Multi-Family (% of Total Area)	Public (% of Total Area)	Single Family (% of Total Area)	Vacant/Agriculture (% of Total Area)
Existing	0%	0%	0%	0%	0%	100%
Acres	0.00	0.00	0.00	0.00	0.00	1.10

**Existing**

Length of Flow 575 ft  
 Slope 0.59 %  
 Waterflow Desc bare / short grass  
 Avg Velocity 0.55 ft/sec  
 Tc 0.29 hours

15 min <= Tc <= 24 hrs

Runoff Coefficients \* Used Soil Group D To Be Conservative

Return Period (Years)	Commercial	Industrial	Multi-Family	Public	Single Family	Vacant/Agriculture
2	0.68	0.68	0.70	0.49	0.50	0.54
5	0.69	0.69	0.73	0.51	0.54	0.56
10	0.73	0.73	0.79	0.56	0.62	0.61
25	0.75	0.75	0.81	0.59	0.66	0.64
50	0.77	0.77	0.83	0.62	0.70	0.67
100	0.80	0.80	0.86	0.66	0.76	0.70

Existing Conditions

Return Period (Years)	Runoff Coefficient *	Rainfall Intensity (in/hr)	Area (Acres)	Runoff (cfs)
2	0.54	3.61	1.10	2.14
5	0.56	4.31	1.10	2.65
10	0.61	4.95	1.10	3.32
25	0.64	5.75	1.10	4.05
50	0.67	6.44	1.10	4.75
100	0.70	7.00	1.10	5.39

Project: Creekside at Pembrook  
 Date: 4/28/2004  
 Prep. By: BLB

Manual Input

**Basin B**

Total Area 21.36 Acres

Soil Group	A (% of Total Area)	B (% of Total Area)	C (% of Total Area)	D (% of Total Area)	Total
	0.00	21.36	0.00	0.00	21.36
	0%	100%	0%	0%	100%

Land Use	Commercial (% of Total Area)	Industrial (% of Total Area)	Multi-Family (% of Total Area)	Public (% of Total Area)	Single Family (% of Total Area)	Vacant/Agriculture (% of Total Area)
Existing	0.00	0.00	0.00	0.00	0.00	21.36
	0%	0%	0%	0%	0%	100%

Length of Flow: Existing 1375 ft  
 Slope: 1.45 %  
 Waterflow Desc: bare / short grass  
 Avg Velocity: 0.30 ft/sec  
 Tc: 1.27 hours

15 min <= Tc <= 24 hrs

Runoff Coefficients \* Used Soil Group D To Be Conservative

Return Period (Years)	Commercial	Industrial	Multi-Family	Public	Single Family	Vacant/Agriculture
2	0.68	0.68	0.70	0.49	0.50	0.54
5	0.69	0.69	0.73	0.51	0.54	0.56
10	0.73	0.73	0.79	0.56	0.62	0.61
25	0.75	0.75	0.81	0.59	0.66	0.64
50	0.77	0.77	0.83	0.62	0.70	0.67
100	0.80	0.80	0.86	0.66	0.76	0.70

Existing Conditions

Return Period (Years)	Runoff Coefficient *	Rainfall Intensity (in/hr)	Area (Acres)	Runoff (cfs)
2	0.54	1.41	21.36	16.26
5	0.56	1.85	21.36	22.13
10	0.61	2.19	21.36	28.53
25	0.64	2.58	21.36	35.27
50	0.67	2.93	21.36	41.93
100	0.70	3.26	21.36	48.74

# CREEKSIDE AT PEMBROOK



BASIN A = 1.10 AC.  
BASIN B = 21.36 AC.

EXISTING BASIN MAP

Project: Creekside at Pembrook  
 Date: 4/28/2004  
 Prep. By: BLB

Manual Input

**Basin 1**

Total Area 4.48 Acres

Soil Group	A (% of Total Area)	B (% of Total Area)	C (% of Total Area)	D (% of Total Area)	Total
	0%	60%	0%	40%	100%
Acres	0.00	2.69	0.00	1.79	4.48

Land Use	Commercial (% of Total Area)	Industrial (% of Total Area)	Multi-Family (% of Total Area)	Public (% of Total Area)	Single Family (% of Total Area)	Vacant/Agriculture (% of Total Area)
Future	0%	0%	0%	0%	100%	0%
Acres	0.00	0.00	0.00	0.00	4.48	0.00

Length of Flow 925 ft  
 Slope 1.51 %  
 Waterflow Desc lawns / short grass  
 Avg Velocity 0.24 ft/sec  
 Tc 1.07 hours

15 min <= Tc <= 24 hrs

Runoff Coefficients \* Used Soil Group D To Be Conservative

Return Period (Years)	Commercial	Industrial	Multi-Family	Public	Single Family	Vacant/Agriculture
2	0.68	0.68	0.70	0.49	0.50	0.54
5	0.69	0.69	0.73	0.51	0.54	0.56
10	0.73	0.73	0.79	0.56	0.62	0.61
25	0.75	0.75	0.81	0.59	0.66	0.64
50	0.77	0.77	0.83	0.62	0.70	0.67
100	0.80	0.80	0.86	0.66	0.76	0.70

Future Conditions

Return Period (Years)	Runoff Coefficient *	Rainfall Intensity (in/hr)	Area (Acres)	Runoff (cfs)
2	0.50	1.61	4.48	3.61
5	0.54	2.07	4.48	5.01
10	0.62	2.44	4.48	6.78
25	0.66	2.86	4.48	8.46
50	0.70	3.25	4.48	10.19
100	0.76	3.60	4.48	12.26

Project: Creekside at Pembrook  
 Date: 4/28/2004  
 Prep. By: BLB

Manual Input

**Basin 2**

Total Area 12.51 Acres

Soil Group	A	B	C	D	Total
	(% of Total Area)	(% of Total Area)	(% of Total Area)	(% of Total Area)	(% of Total Area)
	0%	100%	0%	0%	100%
Acres	0.00	12.51	0.00	0.00	12.51

Land Use	Commercial	Industrial	Multi-Family	Public	Single Family	Vacant/Agriculture
	(% of Total Area)	(% of Total Area)	(% of Total Area)	(% of Total Area)	(% of Total Area)	(% of Total Area)
Future	0%	0%	0%	0%	80%	20%
Acres	0.00	0.00	0.00	0.00	10.01	2.50

Future  
 Length of Flow 1175 ft  
 Slope 1.16 %  
 Waterflow Desc lawns / short grass  
 Avg Velocity 0.24 ft/sec  
 Tc 1.36 hours

15 min <= Tc <= 24 hrs

Runoff Coefficients \* Used Soil Group D To Be Conservative

Return Period (Years)	Commercial	Industrial	Multi-Family	Public	Single Family	Vacant/Agriculture
2	0.68	0.68	0.70	0.49	0.50	0.54
5	0.69	0.69	0.73	0.51	0.54	0.56
10	0.73	0.73	0.79	0.56	0.62	0.61
25	0.75	0.75	0.81	0.59	0.66	0.64
50	0.77	0.77	0.83	0.62	0.70	0.67
100	0.80	0.80	0.86	0.66	0.76	0.70

Future Conditions

Return Period (Years)	Runoff Coefficient *	Rainfall Intensity (in/hr)	Area (Acres)	Runoff (cfs)
2	0.51	1.33	12.51	8.45
5	0.54	1.76	12.51	11.98
10	0.62	2.08	12.51	16.08
25	0.66	2.43	12.51	19.94
50	0.69	2.79	12.51	24.22
100	0.75	3.10	12.51	29.01

Project: Creekside at Pembrook  
 Date: 4/28/2004  
 Prep. By: BLB

Manual Input

**Basin 3**

Total Area 1.49 Acres

Soil Group	A (% of Total Area)	B (% of Total Area)	C (% of Total Area)	D (% of Total Area)	Total
	0%	60%	0%	40%	100%
Acres	0.00	0.89	0.00	0.60	1.49

Land Use	Commercial (% of Total Area)	Industrial (% of Total Area)	Multi-Family (% of Total Area)	Public (% of Total Area)	Single Family (% of Total Area)	Vacant/Agriculture (% of Total Area)
Future	0%	0%	0%	0%	100%	0%
Acres	0.00	0.00	0.00	0.00	1.49	0.00

Length of Flow 600 ft  
 Slope 0.67 %  
 Waterflow Desc lawns / short grass  
 Avg Velocity 0.24 ft/sec  
 Tc 0.69 hours

15 min <= Tc <= 24 hrs

Runoff Coefficients \* Used Soil Group D To Be Conservative

Return Period (Years)	Commercial	Industrial	Multi-Family	Public	Single Family	Vacant/Agriculture
2	0.68	0.68	0.70	0.49	0.50	0.54
5	0.69	0.69	0.73	0.51	0.54	0.56
10	0.73	0.73	0.79	0.56	0.62	0.61
25	0.75	0.75	0.81	0.59	0.66	0.64
50	0.77	0.77	0.83	0.62	0.70	0.67
100	0.80	0.80	0.86	0.66	0.76	0.70

Future Conditions

Return Period (Years)	Runoff Coefficient *	Rainfall Intensity (in/hr)	Area (Acres)	Runoff (cfs)
2	0.50	2.21	1.49	1.65
5	0.54	2.72	1.49	2.19
10	0.62	3.17	1.49	2.93
25	0.66	3.71	1.49	3.65
50	0.70	4.19	1.49	4.37
100	0.76	4.60	1.49	5.21

**32.0** Maximum Q (cfs)  
**5.000** Weir Width (feet)  
**154.00** Weir Elevation

<u>Q</u> (cfs)	<u>Weir</u> <u>Width</u> (feet)	<u>Weir</u> <u>Elevation</u>	<u>q</u>	<u>Critical</u> <u>Depth</u> (feet)	<u>Energy</u> <u>Head</u> (feet)	<u>Water</u> <u>Surface</u> <u>Elevation</u>
0.0	5.000	154.00	0.0	0.00	0.00	<b>154.00</b>
3.2	5.000	154.00	0.6	0.23	0.35	<b>154.35</b>
6.4	5.000	154.00	1.3	0.37	0.56	<b>154.56</b>
9.6	5.000	154.00	1.9	0.49	0.73	<b>154.73</b>
12.8	5.000	154.00	2.6	0.59	0.88	<b>154.88</b>
16.0	5.000	154.00	3.2	0.68	1.02	<b>155.02</b>
19.2	5.000	154.00	3.8	0.77	1.16	<b>155.16</b>
22.4	5.000	154.00	4.5	0.85	1.28	<b>155.28</b>
25.6	5.000	154.00	5.1	0.93	1.40	<b>155.40</b>
28.8	5.000	154.00	5.8	1.01	1.52	<b>155.52</b>
32.0	5.000	154.00	6.4	1.08	1.63	<b>155.63</b>

Circular Pond Sizing with Elevations

Floor Area (Acres) 1.04  
 Floor Elevation (ft) 142.00  
 Static Pool Elevation (ft) 152.00  
 Side Slopes to Static ( \_ :1) 2  
 Side Slopes beyond Static ( \_ :1) 4

	Elevation (ft)	Radius (ft)	Area (ft^2)	Area (Acres)	Storage (ft^3)	Storage (C.Y.)
	142.00	120.08	45302.40	1.04	0.00	0.00
	143.00	122.08	46823.99	1.07	46063.19	1706.04
	144.00	124.08	48370.71	1.11	93673.11	3469.37
	145.00	126.08	49942.56	1.15	142867.44	5291.39
	146.00	128.08	51539.55	1.18	193683.90	7173.48
	147.00	130.08	53161.67	1.22	246160.17	9117.04
	148.00	132.08	54808.92	1.26	300333.96	11123.48
	149.00	134.08	56481.31	1.30	356242.97	13194.18
	150.00	136.08	58178.82	1.34	413924.89	15330.55
	151.00	138.08	59901.47	1.38	473417.43	17533.98
Static Pool	152.00	140.08	61649.26	1.42	534758.28	19805.86
	153.00	144.08	65220.22	1.50	607874.41	22513.87
	154.00	148.08	68891.71	1.58	685164.69	25376.47
	155.00	152.08	72663.74	1.67	766779.91	28399.26
	156.00	156.08	76536.30	1.76	852870.88	31587.81
	157.00	160.08	80509.39	1.85	943588.39	34947.72
	158.00	164.08	84583.00	1.94	1039083.24	38484.56
	159.00	168.08	88757.15	2.04	1139506.21	42203.93
	160.00	172.08	93031.84	2.14	1245008.12	46111.41

## SUB-BASIN CALCULATIONS

### Runoff Coefficients

C2        0.44  
C100      0.61

### Intensity

Tc        15 min  
i2        3.5 in/hr  
i100      7.8 in/hr

Basin	Node	Area	Q2	Q100
2A	N/A	4.08	6.28	29.90
2B	110	0.82	1.26	6.01
2C	120	1.20	1.85	8.79
2D	130	0.66	1.02	4.84
2E	122	0.65	1.00	4.76
2F	140	1.08	1.66	7.91
2G	123	1.10	1.69	8.06
2H	124	0.45	0.69	3.30
2I	125	0.54	0.83	3.96
2J	150	0.88	1.36	6.45
2K	160	1.04	1.60	7.62

## INLET SIZING

### Curb Inlets

Node	Q <sub>in</sub>	Q <sub>max</sub> (L=5')	Q <sub>max</sub> (L=10')	Use L=
110	0.82	11	22	5
120	1.20	11	22	5
124	0.45	11	22	5
125	0.54	11	22	5
150	0.88	11	22	5
160	1.04	11	22	5

### Area Inlets

Node	Q <sub>100</sub>	Size	Perimeter	Ponding Depth
122	4.76	2' x 2'	8	0.34
123	8.06	2' x 2'	8	0.48
130	4.84	2' x 2'	8	0.34
140	7.91	2' x 2'	8	0.48

### Neenah R4826 2' x 2' Area Inlet

1.3 SF of open area

8 F Perimeter

## STREET FLOW CHECKS

Basin	Node	Q2	Q100
2B	110	1.26	6.01
2C	120	1.85	8.79
2H	124	0.69	3.30
2I	125	0.83	3.96
2J	150	1.36	6.45
2K	160	1.60	7.62

### 2 Year

Node	Q2	Street Slope	d	dmax	Comment
120	1.85	0.96	0.22	0.55	OK

\* By inspection, all nodes are OK

### 100 Year

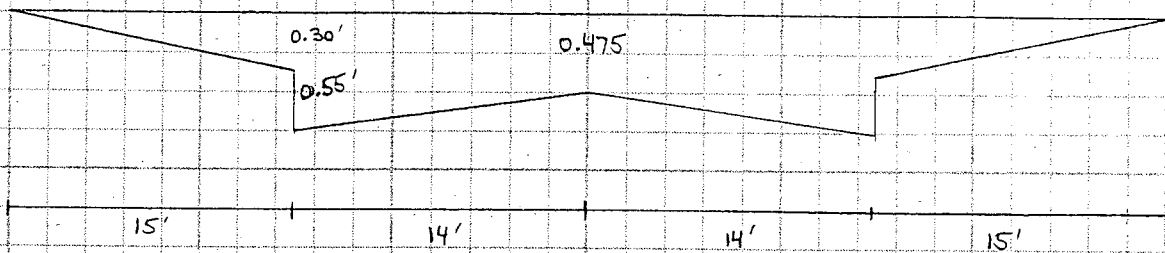
Location	Q100	Qpipe	Qstreet	S	Qmax	Comment
Approaching node 120	8.79	1.85	6.94	0.96	79.41	OK

\* By inspection, all nodes are OK



S. TOPEKA - WICHITA, KANSAS 67202 Project \_\_\_\_\_ Date \_\_\_\_\_  
 316-262-2691 - FAX 316-262-3003  
 www.pecl.com - designers@pecl.com Item \_\_\_\_\_ By \_\_\_\_\_

DETERMINE CAPACITIES OF STANDARD CURB STREETS w/ 0.3' WALK  
 GRADE FOR 100-YR STORM ANALYSIS (58' ROW, 29' BK-BK)



$$\frac{(2 \times 14.5 \times 0.030) + (2 \times 3.05 \times 0.013) + (2 \times 12 \times 0.016)}{59.1} = 0.02256 = n$$

$$(2 \times \frac{1}{2} \times 15 \times 0.30) + (28 \times 0.85) - (2 \times \frac{1}{2} \times 14 \times 0.375) = 23.05 \text{ SF} = A$$

$$59.1 \text{ ft} = P$$

$$23.05 / 59.1 = 0.390 = R$$

$$(0.390)^{2/3} = 0.534 = R^{2/3}$$

$$\frac{1.486}{n} AR^{2/3} S^{1/2} = Q$$

$$\frac{1.486}{0.02256} (23.05)(0.534) S^{1/2} = \underline{\underline{810.47 S^{1/2} = Q}}$$

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* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   JUN 1998
*   VERSION 4.1
*
* RUN DATE 28APR04 TIME 15:06:58
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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

1 ID Creekside at Pembroke 36-04165-3104
2 ID Proposed Drainage at Northwest corner of site
3 ID By BLB DATE 04-28-04

```

\*\*\* LIST \*\*\*  
\*\*\* FREE \*\*\*

\*DIAGRAM

```

4 IT 15 27SEP99 1200 0 28SEP99 2000
5 IN 15 27SEP99 1200
6 IO 0 5
7 JR PREC 7.8

```

\*  
\*

\* OFFSITE

```

8 KK OFF
9 KO 5
10 BA 0.0058
11 PB 1.00
12 PC 0.000 0.003 0.006 0.008 0.011 0.014 0.017 0.019 0.022 0.025
13 PC 0.029 0.032 0.035 0.038 0.042 0.045 0.048 0.052 0.056 0.060
14 PC 0.064 0.068 0.072 0.076 0.080 0.085 0.090 0.095 0.100 0.105
15 PC 0.110 0.115 0.120 0.127 0.134 0.140 0.147 0.155 0.163 0.172

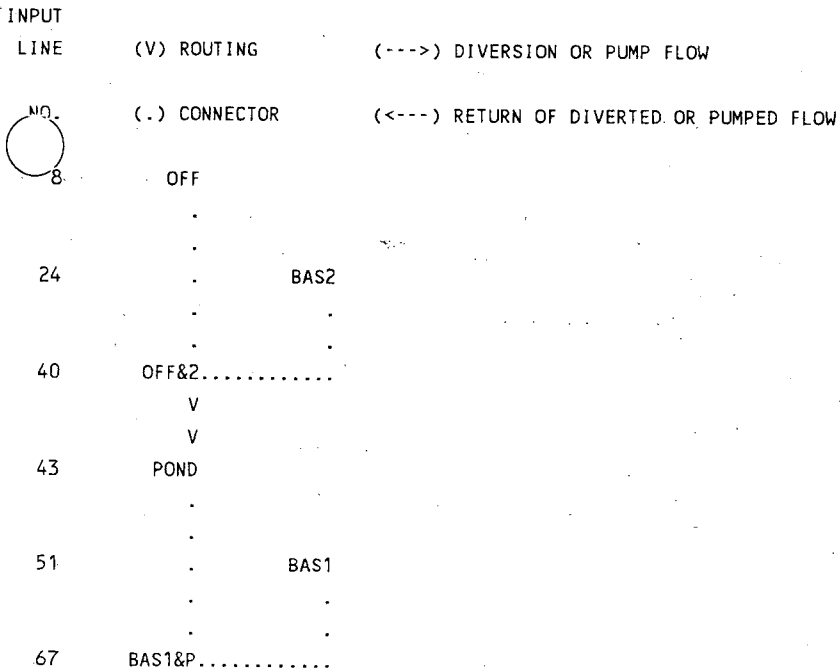
```



55	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
56	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
57	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
58	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
59	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
60	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
61	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
62	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
63	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
64	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
65	LS	0	85	25							
66	UD	0.750									

67 KK BAS1&P  
68 KO 5  
69 HC 2 0  
70 ZZ

SCHEMATIC DIAGRAM OF STREAM NETWORK



(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
\* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
\* JUN 1998 \*  
\* VERSION 4.1 \*  
\* IN DATE 28APR04 TIME 15:06:58 \*  
\*\*\*\*\*

\*\*\*\*\*  
\* U.S. ARMY CORPS OF ENGINEERS \*  
\* HYDROLOGIC ENGINEERING CENTER \*  
\* 609 SECOND STREET \*  
\* DAVIS, CALIFORNIA 95616 \*  
\* (916) 756-1104 \*  
\*\*\*\*\*

Creekside at Pembroke 36-04165-3104  
Proposed Drainage at Northwest corner of site  
By BLB      DATE 04-28-04

6 IO      OUTPUT CONTROL VARIABLES  
          IPRNT            0    PRINT CONTROL  
          IPLOT            5    PLOT CONTROL  
          QSCAL            0.    HYDROGRAPH PLOT SCALE

IT      HYDROGRAPH TIME DATA  
          NMIN            15    MINUTES IN COMPUTATION INTERVAL  
          IDATE          27SEP99    STARTING DATE  
          ITIME          1200    STARTING TIME  
          NQ             129    NUMBER OF HYDROGRAPH ORDINATES  
          NDDATE        28SEP99    ENDING DATE  
          NDTIME        2000    ENDING TIME  
          ICENT          19    CENTURY MARK

          COMPUTATION INTERVAL    .25 HOURS  
          TOTAL TIME BASE        32.00 HOURS

ENGLISH UNITS

DRAINAGE AREA            SQUARE MILES  
PRECIPITATION DEPTH      INCHES  
LENGTH, ELEVATION        FEET  
FLOW                     CUBIC FEET PER SECOND  
STORAGE VOLUME          ACRE-FEET  
SURFACE AREA             ACRES  
TEMPERATURE              DEGREES FAHRENHEIT

JP      MULTI-PLAN OPTION  
          NPLAN            1    NUMBER OF PLANS

JR      MULTI-RATIO OPTION  
          RATIOS OF PRECIPITATION  
          7.80

\*\*\* \*\*

\*\*\*\*\*

\*            \*

8 KK    \*        OFF    \*

\*            \*

\*\*\*\*\*

9 KO      OUTPUT CONTROL VARIABLES  
          IPRNT            5    PRINT CONTROL  
          IPLOT            5    PLOT CONTROL  
          QSCAL            0.    HYDROGRAPH PLOT SCALE

\*\*\* \*\*

\*\*\*\*\*  
 \* \*  
 \* BAS2 \*  
 \* \*  
 \*\*\*\*\*

24 KK

OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
 IPLOT 5 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

25 KO

\*\*\* \*\*

\*\*\*\*\*  
 \* \*  
 \* OFF&2 \*  
 \* \*  
 \*\*\*\*\*

40 KK

OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
 IPLOT 5 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

41 KO

\*\* \*\*

\*\*\*\*\*  
 \* \*  
 \* POND \*  
 \* \*  
 \*\*\*\*\*

43 KK

HYDROGRAPH ROUTING DATA

44 RS

STORAGE ROUTING

NSTPS 1 NUMBER OF SUBREACHES  
 ITYP ELEV TYPE OF INITIAL CONDITION  
 RSVRIC 142.00 INITIAL CONDITION  
 X .00 WORKING R AND D COEFFICIENT

45 SA

AREA 1.6 1.7 1.8 1.9

46 SE

ELEVATION 154.00 155.00 156.00 157.00

47 SQ

DISCHARGE 0. 3. 6. 10. 13. 16. 19. 22. 26. 29.  
 32.

49 SE

ELEVATION 154.00 154.35 154.56 154.73 154.88 155.02 155.16 155.28 155.40 155.52  
 155.60

\*\*\*

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	1.62	3.34	5.14
ELEVATION	154.00	155.00	156.00	157.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	.56	.90	1.18	1.43	1.62	1.66	1.89	2.10	2.30
OUTFLOW	.00	3.20	6.40	9.60	12.80	15.54	16.00	19.20	22.40	25.60
ELEVATION	154.00	154.35	154.56	154.73	154.88	155.00	155.02	155.16	155.28	155.40

STORAGE	2.51	2.64	3.34	5.14
OUTFLOW	28.80	32.00	48.00	88.00
ELEVATION	155.52	155.60	156.00	157.00

\*\*\*\*\*

HYDROGRAPH AT STATION POND  
PLAN 1, RATIO = 7.80

\*\*\*\*\*

				*			*													
DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE
				*			*													
27	SEP	1200	1	0.	.0	154.0	* 27	SEP	2245	44	2.	.3	154.2	* 28	SEP	0930	87	2.	.4	154.3
27	SEP	1215	2	0.	.0	154.0	* 27	SEP	2300	45	2.	.3	154.2	* 28	SEP	0945	88	2.	.4	154.2
27	SEP	1230	3	0.	.0	154.0	* 27	SEP	2315	46	2.	.4	154.2	* 28	SEP	1000	89	2.	.4	154.2
27	SEP	1245	4	0.	.0	154.0	* 27	SEP	2330	47	3.	.4	154.3	* 28	SEP	1015	90	2.	.4	154.2
27	SEP	1300	5	0.	.0	154.0	* 27	SEP	2345	48	3.	.5	154.3	* 28	SEP	1030	91	2.	.4	154.2
27	SEP	1315	6	0.	.0	154.0	* 28	SEP	0000	49	6.	.8	154.5	* 28	SEP	1045	92	2.	.3	154.2
27	SEP	1330	7	0.	.0	154.0	* 28	SEP	0015	50	10.	1.2	154.8	* 28	SEP	1100	93	2.	.3	154.2
27	SEP	1345	8	0.	.0	154.0	* 28	SEP	0030	51	15.	1.6	155.0	* 28	SEP	1115	94	2.	.3	154.2
27	SEP	1400	9	0.	.0	154.0	* 28	SEP	0045	52	19.	1.9	155.2	* 28	SEP	1130	95	2.	.3	154.2
27	SEP	1415	10	0.	.0	154.0	* 28	SEP	0100	53	23.	2.1	155.3	* 28	SEP	1145	96	2.	.3	154.2
27	SEP	1430	11	0.	.0	154.0	* 28	SEP	0115	54	24.	2.2	155.3	* 28	SEP	1200	97	2.	.3	154.2
27	SEP	1445	12	0.	.0	154.0	* 28	SEP	0130	55	24.	2.2	155.3	* 28	SEP	1215	98	2.	.3	154.2
27	SEP	1500	13	0.	.0	154.0	* 28	SEP	0145	56	22.	2.1	155.3	* 28	SEP	1230	99	2.	.3	154.2
27	SEP	1515	14	0.	.0	154.0	* 28	SEP	0200	57	20.	2.0	155.2	* 28	SEP	1245	100	2.	.3	154.2
27	SEP	1530	15	0.	.0	154.0	* 28	SEP	0215	58	18.	1.8	155.1	* 28	SEP	1300	101	1.	.3	154.2
27	SEP	1545	16	0.	.0	154.0	* 28	SEP	0230	59	16.	1.6	155.0	* 28	SEP	1315	102	1.	.2	154.2
27	SEP	1600	17	0.	.0	154.0	* 28	SEP	0245	60	14.	1.5	154.9	* 28	SEP	1330	103	1.	.2	154.1
27	SEP	1615	18	0.	.0	154.0	* 28	SEP	0300	61	12.	1.4	154.8	* 28	SEP	1345	104	1.	.2	154.1
27	SEP	1630	19	0.	.0	154.0	* 28	SEP	0315	62	11.	1.3	154.8	* 28	SEP	1400	105	1.	.2	154.1
27	SEP	1645	20	0.	.0	154.0	* 28	SEP	0330	63	9.	1.2	154.7	* 28	SEP	1415	106	1.	.2	154.1
27	SEP	1700	21	0.	.1	154.0	* 28	SEP	0345	64	8.	1.1	154.7	* 28	SEP	1430	107	1.	.1	154.1
27	SEP	1715	22	0.	.1	154.0	* 28	SEP	0400	65	8.	1.0	154.6	* 28	SEP	1445	108	1.	.1	154.1
27	SEP	1730	23	0.	.1	154.0	* 28	SEP	0415	66	7.	.9	154.6	* 28	SEP	1500	109	1.	.1	154.1
27	SEP	1745	24	0.	.1	154.0	* 28	SEP	0430	67	6.	.9	154.5	* 28	SEP	1515	110	1.	.1	154.1
27	SEP	1800	25	0.	.1	154.0	* 28	SEP	0445	68	6.	.8	154.5	* 28	SEP	1530	111	1.	.1	154.1
27	SEP	1815	26	0.	.1	154.0	* 28	SEP	0500	69	5.	.8	154.5	* 28	SEP	1545	112	0.	.1	154.1
27	SEP	1830	27	0.	.1	154.0	* 28	SEP	0515	70	5.	.7	154.5	* 28	SEP	1600	113	0.	.1	154.0
27	SEP	1845	28	0.	.1	154.1	* 28	SEP	0530	71	4.	.7	154.4	* 28	SEP	1615	114	0.	.1	154.0
27	SEP	1900	29	1.	.1	154.1	* 28	SEP	0545	72	4.	.7	154.4	* 28	SEP	1630	115	0.	.1	154.0
27	SEP	1915	30	1.	.1	154.1	* 28	SEP	0600	73	4.	.6	154.4	* 28	SEP	1645	116	0.	.1	154.0
27	SEP	1930	31	1.	.1	154.1	* 28	SEP	0615	74	4.	.6	154.4	* 28	SEP	1700	117	0.	.0	154.0
27	SEP	1945	32	1.	.1	154.1	* 28	SEP	0630	75	3.	.6	154.4	* 28	SEP	1715	118	0.	.0	154.0
27	SEP	2000	33	1.	.1	154.1	* 28	SEP	0645	76	3.	.5	154.3	* 28	SEP	1730	119	0.	.0	154.0
27	SEP	2015	34	1.	.1	154.1	* 28	SEP	0700	77	3.	.5	154.3	* 28	SEP	1745	120	0.	.0	154.0
27	SEP	2030	35	1.	.1	154.1	* 28	SEP	0715	78	3.	.5	154.3	* 28	SEP	1800	121	0.	.0	154.0
27	SEP	2045	36	1.	.2	154.1	* 28	SEP	0730	79	3.	.5	154.3	* 28	SEP	1815	122	0.	.0	154.0
27	SEP	2100	37	1.	.2	154.1	* 28	SEP	0745	80	3.	.5	154.3	* 28	SEP	1830	123	0.	.0	154.0
27	SEP	2115	38	1.	.2	154.1	* 28	SEP	0800	81	3.	.5	154.3	* 28	SEP	1845	124	0.	.0	154.0

27 SEP 2130	39	1.	.2	154.1	* 28 SEP 0815	82	3.	.5	154.3	* 28 SEP 1900	125	0.	.0	154.0
27 SEP 2145	40	1.	.2	154.1	* 28 SEP 0830	83	3.	.5	154.3	* 28 SEP 1915	126	0.	.0	154.0
27 SEP 2200	41	1.	.2	154.1	* 28 SEP 0845	84	3.	.4	154.3	* 28 SEP 1930	127	0.	.0	154.0
SEP 2215	42	1.	.3	154.2	* 28 SEP 0900	85	2.	.4	154.3	* 28 SEP 1945	128	0.	.0	154.0
SEP 2230	43	2.	.3	154.2	* 28 SEP 0915	86	2.	.4	154.3	* 28 SEP 2000	129	0.	.0	154.0

\*\*\*\*\*

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	32.00-HR	
24.	13.25	12.	4.	3.	3.	
		(INCHES)	4.533	6.208	6.275	6.275
		(AC-FT)	6.	8.	8.	8.

PEAK STORAGE + (AC-FT)	TIME (HR)	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	32.00-HR
2.	13.25	1.	1.	0.	0.

PEAK STAGE + (FEET)	TIME (HR)	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	32.00-HR
155.34	13.25	154.83	154.33	154.25	154.25

CUMULATIVE AREA = .03 SQ MI

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*****
*
51 KK * BAS1 *
*
*****

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52 KO      OUTPUT CONTROL VARIABLES
          IPRNT      5 PRINT CONTROL
          IPLOT      5 PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE

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*****
*
67 KK * BAS1&P *
*
*****

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68 KO      OUTPUT CONTROL VARIABLES
          IPRNT      5 PRINT CONTROL
          IPLOT      5 PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE

```

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS



RATIOS APPLIED TO PRECIPITATION

OPERATION	STATION	AREA	PLAN		RATIO 1
					7.80
HYDROGRAPH AT					
+	OFF	.01	1	FLOW	17.
				TIME	12.00
HYDROGRAPH AT					
+	BAS2	.02	1	FLOW	29.
				TIME	12.75
2 COMBINED AT					
+	OFF&2	.03	1	FLOW	32.
				TIME	12.75
ROUTED TO					
+	POND	.03	1	FLOW	24.
				TIME	13.25

\*\* PEAK STAGES IN FEET \*\*

1	STAGE	155.34
	TIME	13.25



HYDROGRAPH AT					
+	BAS1	.01	1	FLOW	12.
				TIME	12.50
2 COMBINED AT					
+	BAS1&P	.03	1	FLOW	32.
				TIME	13.00

\*\*\* NORMAL END OF HEC-1 \*\*\*



SWS Line #1.txt

100 j,	149.0000	100	1	12	11				
110 t,	Creekside at Pembroke SWS Line #1								
120 i,	160	0.00	0.00	0.00	0.00	0.00	1.60	15.00	158.72
130 i,	150	0.00	0.00	0.00	0.00	0.00	1.36	15.00	158.72
140 i,	140	0.00	0.00	0.00	0.00	0.00	1.66	15.00	158.00
150 i,	130	0.00	0.00	0.00	0.00	0.00	1.02	15.00	158.00
160 i,	125	0.00	0.00	0.00	0.00	0.00	0.83	15.00	161.62
170 i,	124	0.00	0.00	0.00	0.00	0.00	0.69	15.00	161.62
180 i,	123	0.00	0.00	0.00	0.00	0.00	1.69	15.00	158.00
190 i,	122	0.00	0.00	0.00	0.00	0.00	1.00	15.00	158.00
200 i,	120	0.00	0.00	0.00	0.00	0.00	1.85	15.00	158.72
210 i,	110	0.00	0.00	0.00	0.00	0.00	1.26	15.00	158.72
220 m,	121	162.26							
230 m,	100	149.00							
240 p,	160	150	30.00	15	0.013	0.00	0.00		
250 p,	150	140	130.00	15	0.013	0.00	0.00		
260 p,	140	130	170.00	15	0.013	0.00	0.00		
270 p,	130	120	100.00	15	0.013	0.00	0.00		
280 p,	125	124	30.00	15	0.013	0.00	0.00		
290 p,	124	123	125.00	15	0.013	90.00	0.00		
300 p,	123	122	170.00	15	0.013	0.00	0.00		
310 p,	122	121	75.00	15	0.013	75.00	0.00		
320 p,	121	120	320.00	15	0.013	75.00	0.00		
330 p,	120	110	30.00	24	0.013	45.00	0.00		
340 p,	110	100	120.00	24	0.013	0.00	0.00		
350 e									



STORM12.OUT

Date: 04-29-2004  
Time: 11:57:49

Creekside at Pembrook SWS Line #1

Input File: c:\storm\sws1

Storm Frequency = 2-Year

\* \* \* H Y D R A U L I C S \* \* \*

Node	Hyd-slope (Ft/Ft)	Friction (Ft)	Bend (Ft)	Transition (Ft)	Manhole (Ft)	Deflection (Ft)	Junction (Ft)	Total (Ft)	Hyd-GJ Elevation	Desired Elevation	Diff.
160	.00061	.0184	.0000	.0000	.0000	.0000	.0000	.0184	152.1940	158.7200	6.53
150	.00208	.2701	.0000	.0063	.0000	.0000	.1330	.4094	152.1756	158.7200	6.54
140	.00495	.8407	.0000	.0123	.0000	.0000	.2648	1.1179	151.7663	158.0000	6.23
130	.00726	.7259	.0000	.0100	.0000	.0000	.2300	.9658	150.6484	158.0000	7.35
125	.00017	.0050	.0000	.0000	.0000	.0000	.0000	.0050	152.1023	161.6200	9.52
124	.00054	.0678	.0000	.0016	.0000	.0000	.0343	.1038	152.0974	161.6200	9.52
123	.00227	.3865	.0000	.0074	.0000	.0117	.1563	.5619	151.9936	158.0000	6.01
122	.00380	.2853	.0000	.0066	.0000	.0000	.1471	.4390	151.4317	158.0000	6.57
120	.00221	.0663	.0000	.0269	.0000	.0000	.1372	.2303	149.6825	158.7200	9.04
110	.00268	.3216	.0000	.0038	.0000	.0387	.0881	.4522	149.4522	158.7200	9.27
121	.00380	1.2172	.0000	.0000	.0082	.0657	.0191	1.3102	150.9927	162.2600	11.27
100	.00000	.0000	.0000	.0000	.0000	.0000	.0000	.0000	149.0000	149.0000	.00

\*\*\*\*\*

KS-2-5

County	Expected 24-hour Storm Rainfall in Inches						Normal Annual Precipitation Inches
	Storm Frequency in Years						
	100	50	25	10	5	2	
Pawnee	6.6	6.0	5.2	4.5	3.7	2.8	23.3
Phillips	6.0	5.5	4.8	4.1	3.4	2.5	23.6
Pottawatomie	7.5	6.6	5.9	5.1	4.3	3.4	33.6
Pratt	7.2	6.4	5.6	4.8	4.1	3.0	24.6
Rawlins	5.5	5.0	4.3	3.6	3.1	2.3	21.0
Reno	7.4	6.6	5.8	5.0	4.2	3.2	27.7
Republic	6.8	6.0	5.4	4.6	3.9	2.9	28.6
Rice	7.3	6.4	5.6	4.8	4.1	3.0	26.6
Riley	7.4	6.5	5.8	5.1	4.3	3.3	33.5
Rooks	6.1	5.7	4.9	4.1	3.4	2.5	23.9
Rush	6.5	5.9	5.0	4.3	3.6	2.7	23.3
Russell	6.7	5.9	5.2	4.4	3.7	2.8	26.8
Saline	7.3	6.4	5.7	4.9	4.1	3.1	28.4
Scott	5.7	5.3	4.5	3.8	3.2	2.4	20.2
Sedgwick	7.8	7.0	6.1	5.3	4.5	3.5	30.6
Seward	6.0	5.7	4.8	4.2	3.5	2.6	19.8
Shawnee	7.8	6.8	6.1	5.3	4.5	3.5	34.7
Sheridan	5.7	5.3	4.5	3.8	3.2	2.4	21.3
Sherman	5.3	4.8	4.2	3.5	3.0	2.2	16.7
Smith	6.3	5.7	5.0	4.2	3.5	2.6	24.4
Stafford	7.1	6.2	5.5	4.7	4.0	2.9	25.1
Stanton	5.6	5.2	4.5	3.8	3.2	2.4	15.8
Stevens	5.9	5.5	4.7	4.1	3.4	2.5	19.7
Sumner	8.0	7.1	6.2	5.4	4.6	3.6	34.0

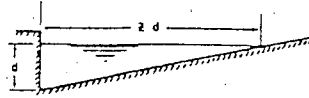
$x\text{-slope} = \frac{3}{8} \frac{1}{4} = 6.03125\%$

$z = \frac{1}{x}\text{-slope} = \frac{1}{6.03125} = 32$

$n = 0.016$

$\frac{z}{n} = \frac{32}{0.016} = 2000$

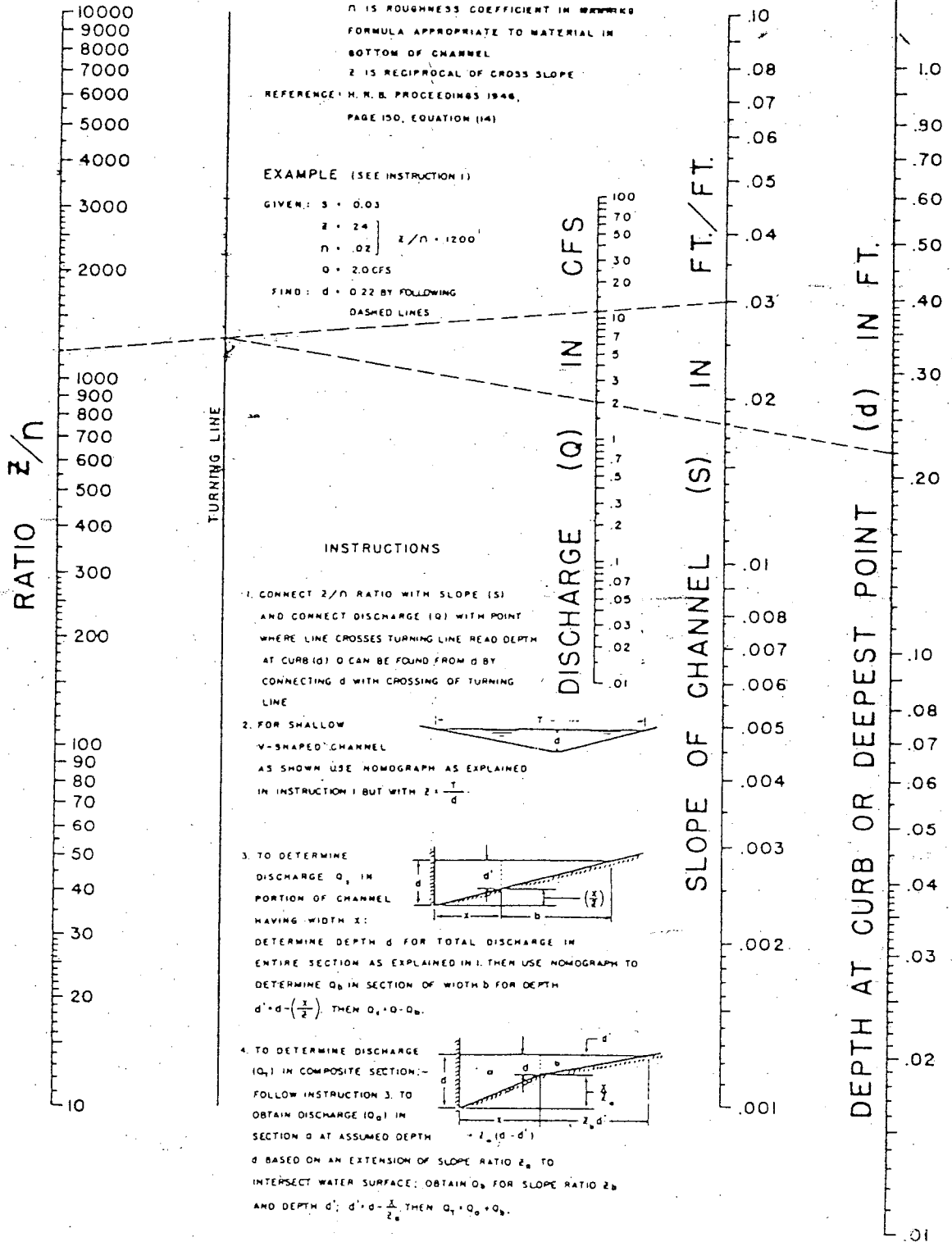
always



EQUATION:  $Q = 0.56 \left(\frac{z}{n}\right)^{5/3} d^{8/3}$   
 $n$  IS ROUGHNESS COEFFICIENT IN MKS  
 FORMULA APPROPRIATE TO MATERIAL IN  
 BOTTOM OF CHANNEL  
 $z$  IS RECIPROCAL OF CROSS SLOPE  
 REFERENCE: H. R. B. PROCEEDINGS 1948,  
 PAGE 150, EQUATION (14)

EXAMPLE (SEE INSTRUCTION 1)

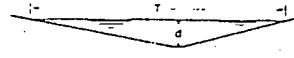
GIVEN:  $s = 0.03$   
 $z = 24$   
 $n = .02$  }  $z/n = 1200$   
 $Q = 2.0 \text{ CFS}$   
 FIND:  $d = 0.22$  BY FOLLOWING  
 DASHED LINES



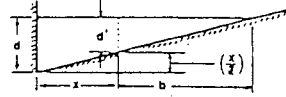
INSTRUCTIONS

1. CONNECT  $z/n$  RATIO WITH SLOPE (S) AND CONNECT DISCHARGE (Q) WITH POINT WHERE LINE CROSSES TURNING LINE READ DEPTH AT CURB (d). d CAN BE FOUND FROM Q BY CONNECTING d WITH CROSSING OF TURNING LINE

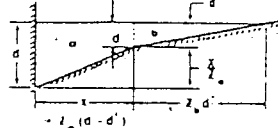
2. FOR SHALLOW V-SHAPED CHANNEL AS SHOWN USE NOMOGRAPH AS EXPLAINED IN INSTRUCTION 1 BUT WITH  $z = \frac{T}{d}$

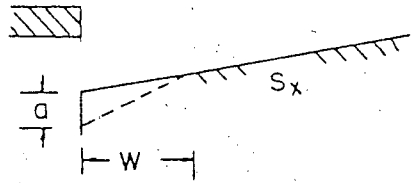


3. TO DETERMINE DISCHARGE  $Q_1$  IN PORTION OF CHANNEL HAVING WIDTH  $x$ : DETERMINE DEPTH  $d$  FOR TOTAL DISCHARGE IN ENTIRE SECTION AS EXPLAINED IN 1. THEN USE NOMOGRAPH TO DETERMINE  $Q_0$  IN SECTION OF WIDTH  $b$  FOR DEPTH  $d' = d - (\frac{x}{z})$ . THEN  $Q_1 = Q - Q_0$ .



4. TO DETERMINE DISCHARGE ( $Q_1$ ) IN COMPOSITE SECTION:- FOLLOW INSTRUCTION 3. TO OBTAIN DISCHARGE ( $Q_0$ ) IN SECTION  $b$  AT ASSUMED DEPTH  $d$  BASED ON AN EXTENSION OF SLOPE RATIO  $z_0$  TO INTERSECT WATER SURFACE; OBTAIN  $Q_0$  FOR SLOPE RATIO  $z_0$  AND DEPTH  $d'$ ;  $d' = d - \frac{x}{z_0}$ . THEN  $Q_1 = Q_0 + Q_2$ .

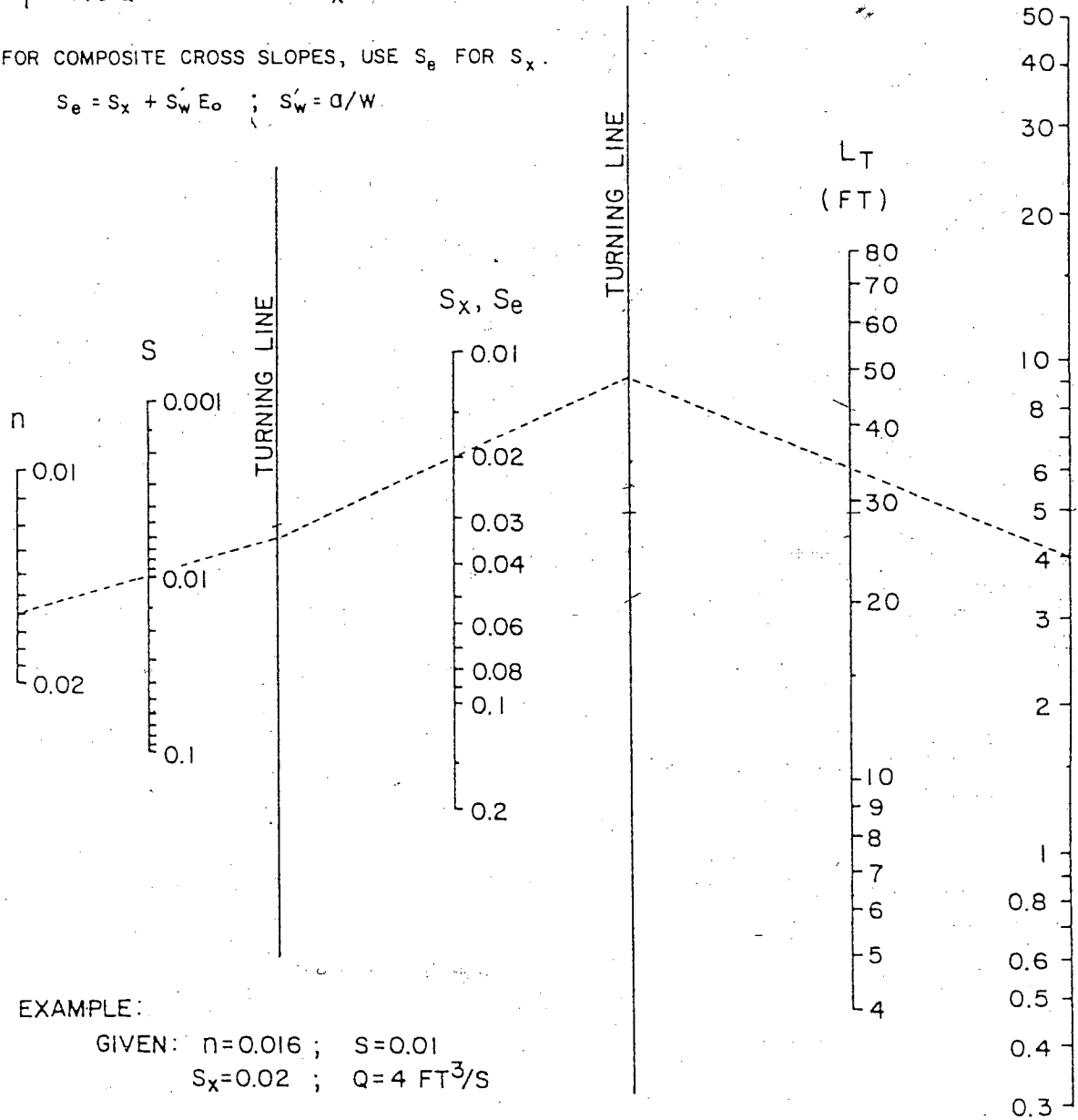




$$L_T = 0.6Q^{0.42} S^{0.3} (1/nS_x)^{0.6}$$

FOR COMPOSITE CROSS SLOPES, USE  $S_e$  FOR  $S_x$ .

$$S_e = S_x + S_w E_o ; S_w = a/w$$



EXAMPLE:

GIVEN:  $n=0.016$  ;  $S=0.01$   
 $S_x=0.02$  ;  $Q=4 \text{ FT}^3/\text{S}$

FIND:  $L_T = 34 \text{ FT}$

**CHART 9. Curb-opening and slotted drain inlet length for total interception.**

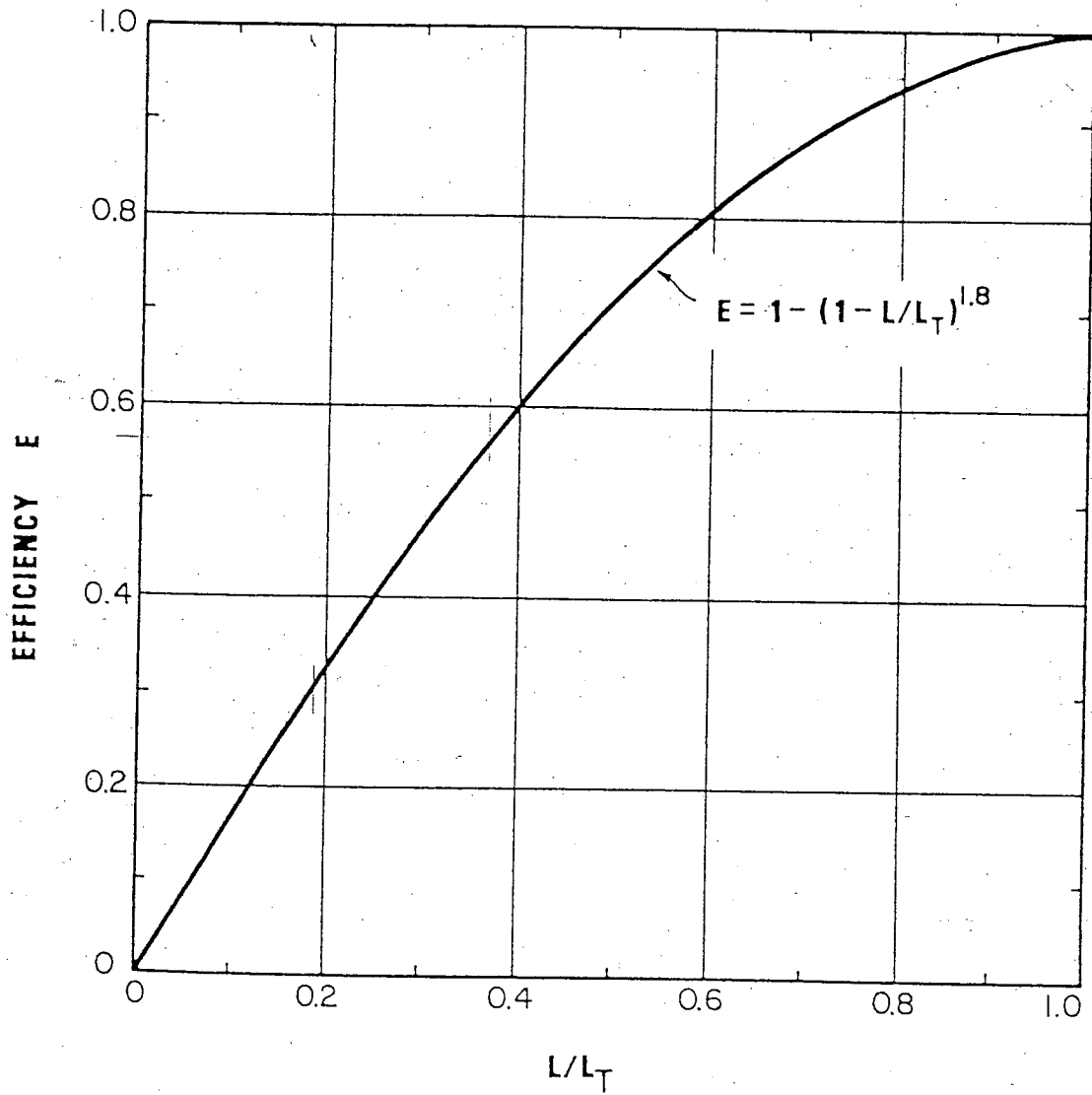


CHART 10. Curb-opening and slotted drain inlet interception efficiency.

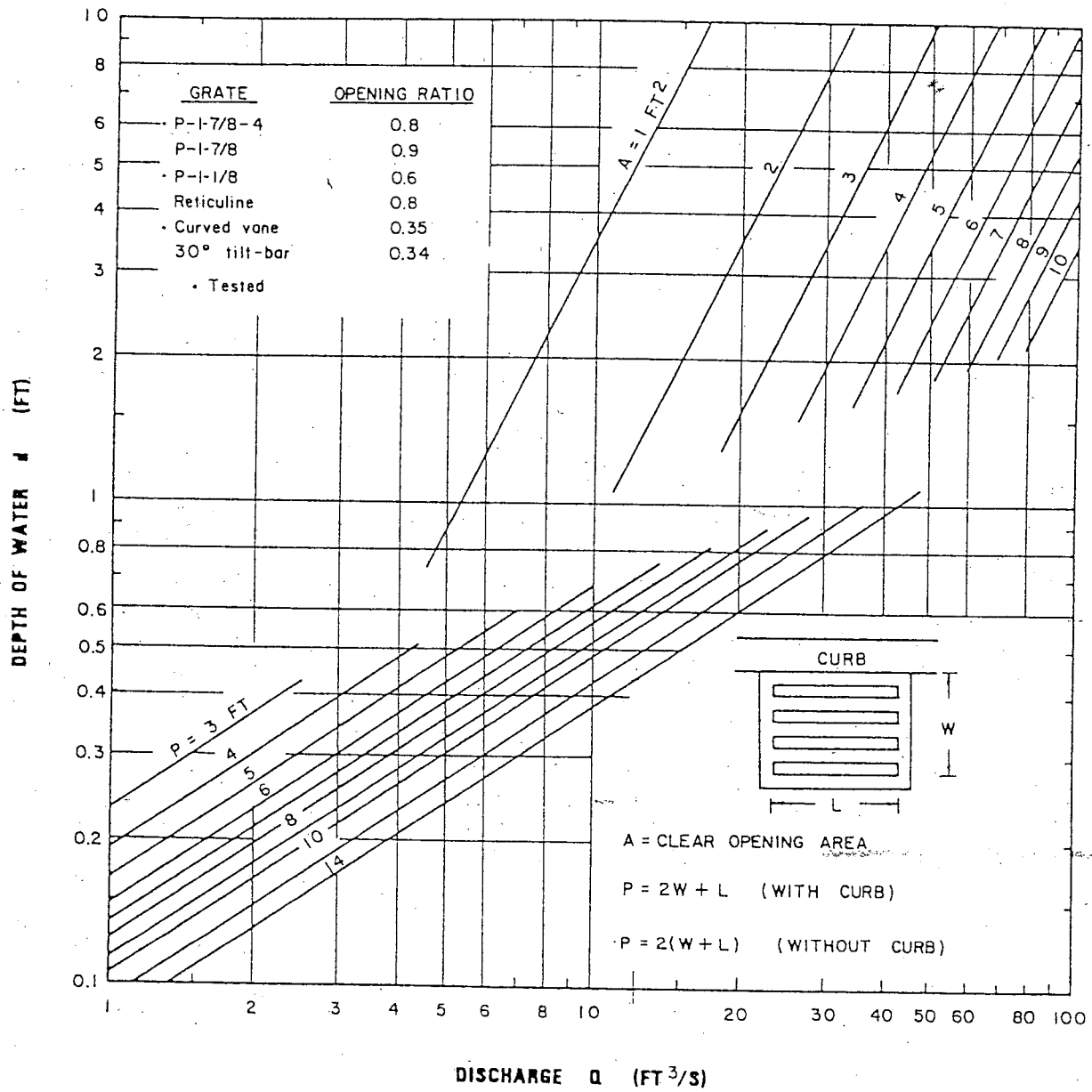


CHART 11. Grate inlet capacity in sump conditions.

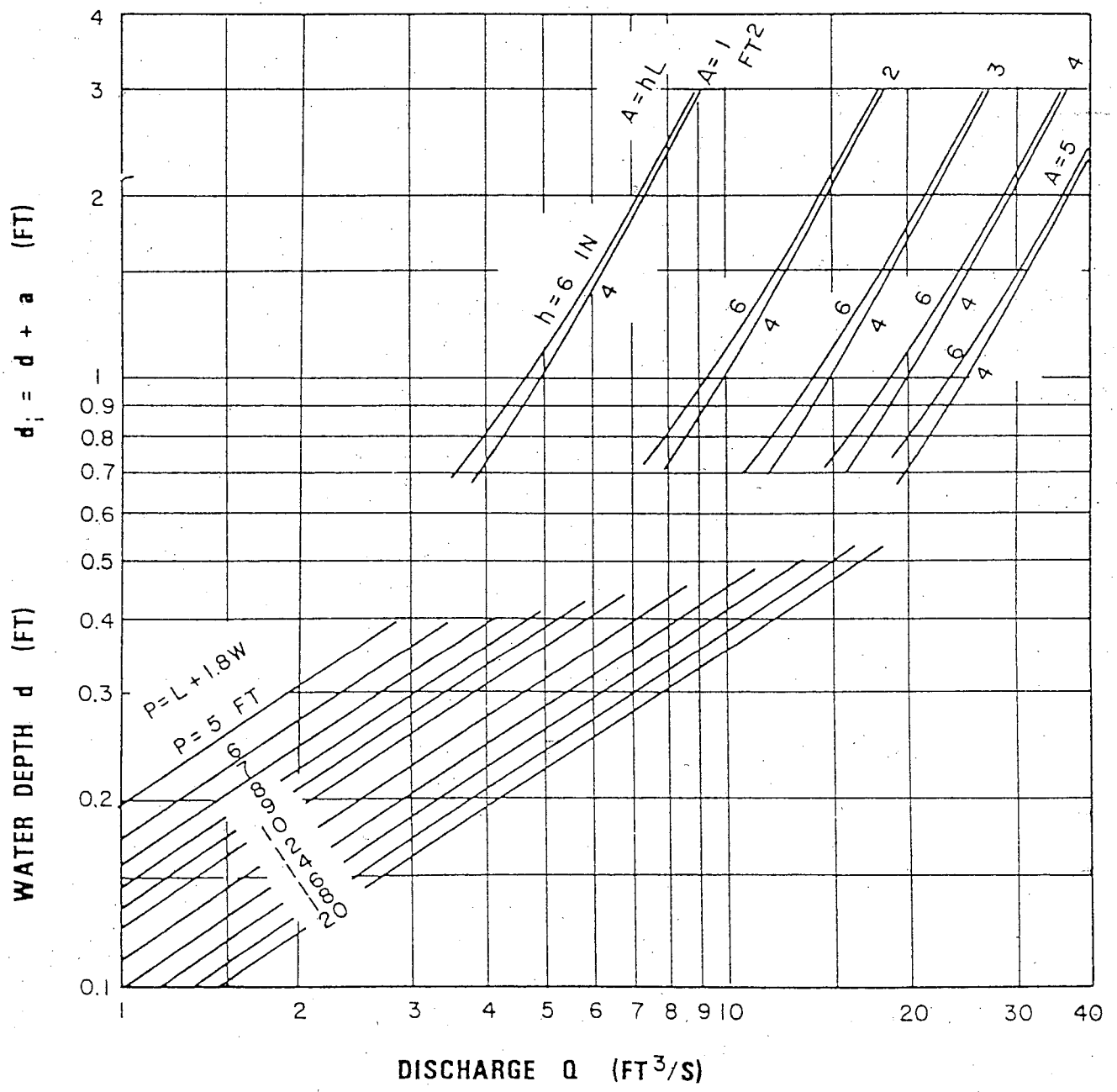
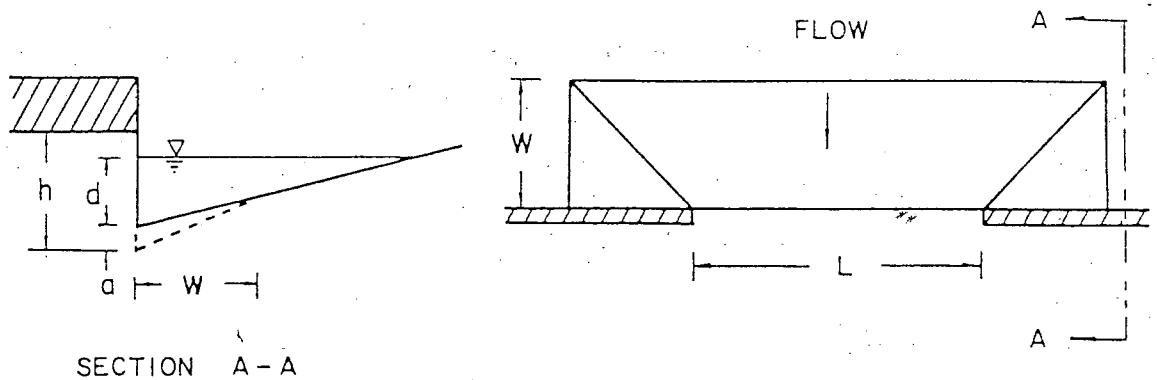


CHART 12. Depressed curb-opening inlet capacity in sump locations.

April 15, 1986

- ATTACHMENT A  
DRAINAGE CRITERIA MANUAL

RAINFALL INTENSITY TABLE FOR SEDGWICK COUNTY, KANSAS

The following tabulation contains rainfall intensity in inches per hour as derived from ESSA Weather Bureau Technical Paper 40 Modified to NWS Hydro-35, 1977 During First Hour

DURATION IN MINUTES ( $\frac{1}{2}$ )	RETURN PERIODS OF						
	1-YR	2-YR	5-YR	10-YR	25-YR	50-YR	100-YR
5	$i = 4.18$	5.57	6.53	7.41	8.52	9.48	10.32
6	3.99	5.32	6.25	7.09	8.16	9.09	9.89
7	3.81	5.09	5.99	6.81	7.84	8.74	9.50
8	3.66	4.89	5.75	6.55	7.55	8.42	9.15
9	3.52	4.70	5.54	6.31	7.28	8.13	8.83
10	3.39	4.52	5.34	6.09	7.04	7.86	8.54
11	3.27	4.36	5.16	5.89	6.81	7.61	8.27
12	3.18	4.21	4.99	5.71	6.60	7.38	8.02
13	3.05	4.08	4.84	5.53	6.41	7.17	7.79
14	2.96	3.95	4.69	5.37	6.23	6.97	7.57
15	2.87	3.83	4.56	5.22	6.06	6.78	7.37
16	2.78	3.72	4.43	5.08	5.90	6.60	7.18
17	2.71	3.61	4.31	4.95	5.75	6.44	7.00
18	2.63	3.51	4.20	4.83	5.61	6.29	6.84
19	2.56	3.42	4.10	4.71	5.47	6.14	6.68
20	2.50	3.33	4.00	4.60	5.35	6.00	6.53
21	2.44	3.25	3.90	4.50	5.23	5.87	6.39
22	2.38	3.17	3.81	4.40	5.12	5.75	6.26
23	2.32	3.10	3.73	4.31	5.01	5.63	6.13
24	2.27	3.03	3.65	4.22	4.91	5.52	6.01
25	2.22	2.96	3.57	4.13	4.81	5.41	5.90
26	2.20	2.90	3.50	4.05	4.72	5.31	5.79
27	2.16	2.84	3.43	3.98	4.63	5.21	5.69
28	2.14	2.78	3.37	3.90	4.55	5.12	5.59
29	2.11	2.72	3.30	3.83	4.47	5.03	5.49
30	2.08	2.67	3.24	3.76	4.39	4.94	5.40
31	2.05	2.62	3.19	3.70	4.32	4.86	5.32
32	2.02	2.57	3.10	3.63	4.25	4.79	5.22
33	1.99	2.52	3.05	3.57	4.18	4.71	5.14
34	1.96	2.48	3.01	3.51	4.11	4.63	5.07
35	1.93	2.44	2.98	3.46	4.05	4.56	5.00
36	1.91	2.39	2.93	3.41	3.99	4.50	4.93
37	1.89	2.35	2.88	3.36	3.93	4.43	4.86
38	1.87	2.32	2.84	3.31	3.87	4.37	4.79
39	1.85	2.28	2.80	3.26	3.82	4.31	4.73
40	1.83	2.24	2.76	3.22	3.76	4.25	4.66
41	1.81	2.21	2.72	3.17	3.71	4.19	4.60
42	1.79	2.18	2.68	3.13	3.66	4.13	4.54
43	1.77	2.14	2.64	3.09	3.61	4.08	4.49
44	1.75	2.11	2.61	3.05	3.57	4.03	4.43
45	1.73	2.08	2.57	3.01	3.52	3.98	4.38

DURATION IN MINUTES	RETURN PERIODS OF						
	1-YR	2-YR	5-YR	10-YR	25-YR	50-YR	100-YR
46	1.70	2.05	2.54	2.97	3.48	3.93	4.33
47	1.67	2.02	2.50	2.93	3.44	3.88	4.28
48	1.66	2.00	2.47	2.90	3.39	3.84	4.23
49	1.64	1.97	2.44	2.86	3.35	3.79	4.18
50	1.61	1.95	2.41	2.83	3.32	3.75	4.13
51	1.59	1.92	2.38	2.79	3.28	3.71	4.09
52	1.56	1.89	2.35	2.76	3.24	3.67	4.05
53	1.54	1.86	2.33	2.73	3.20	3.63	4.00
54	1.52	1.84	2.30	2.70	3.17	3.59	3.96
55	1.50	1.81	2.27	2.67	3.14	3.55	3.92
56	1.47	1.79	2.25	2.64	3.10	3.51	3.88
57	1.45	1.76	2.22	2.61	3.07	3.48	3.84
58	1.43	1.74	2.20	2.59	3.04	3.44	3.81
59	1.42	1.72	2.18	2.56	3.01	3.41	3.77
60	1.40	1.69	2.15	2.53	2.98	3.37	3.73
61	1.38	1.67	2.13	2.51	2.95	3.34	3.70
62	1.36	1.65	2.11	2.48	2.92	3.31	3.67
63	1.34	1.63	2.09	2.46	2.89	3.28	3.63
64	1.33	1.61	2.07	2.44	2.86	3.25	3.60
65	1.31	1.59	2.05	2.41	2.84	3.22	3.57
66	1.30	1.57	2.03	2.39	2.81	3.19	3.54
67	1.28	1.56	2.01	2.37	2.79	3.16	3.51
68	1.26	1.54	1.99	2.35	2.76	3.13	3.48
69	1.25	1.52	1.97	2.33	2.74	3.10	3.45
70	1.24	1.50	1.95	2.31	2.71	3.08	3.42
71	1.22	1.49	1.93	2.28	2.69	3.05	3.39
72	1.21	1.47	1.92	2.26	2.67	3.02	3.36
73	1.20	1.46	1.90	2.25	2.64	3.00	3.34
74	1.18	1.44	1.88	2.23	2.63	2.98	3.31
75	1.17	1.43	1.86	2.21	2.61	2.95	3.29
76	1.16	1.41	1.85	2.19	2.58	2.93	3.26
77	1.15	1.40	1.83	2.17	2.55	2.90	3.24
78	1.13	1.38	1.82	2.15	2.53	2.88	3.22
79	1.12	1.37	1.80	2.14	2.50	2.86	3.19
80	1.11	1.36	1.79	2.12	2.48	2.84	3.16
81	1.10	1.34	1.77	2.10	2.46	2.82	3.13
82	1.09	1.33	1.76	2.08	2.43	2.79	3.10
83	1.08	1.32	1.74	2.06	2.41	2.76	3.07
84	1.07	1.31	1.73	2.04	2.39	2.74	3.04
85	1.06	1.30	1.72	2.02	2.37	2.71	3.01
86	1.05	1.28	1.70	2.00	2.34	2.69	2.99
87	1.04	1.27	1.69	1.99	2.32	2.66	2.96
88	1.03	1.26	1.68	1.97	2.30	2.64	2.93
89	1.02	1.25	1.68	1.95	2.28	2.62	2.91
90	1.01	1.24	1.66	1.93	2.26	2.59	2.88

ATTACHMENT A CONTINUED  
Page 3

<u>DURATION IN MINUTES</u>	<u>RETURN PERIODS OF</u>						
	<u>1-YR</u>	<u>2-YR</u>	<u>5-YR</u>	<u>10-YR</u>	<u>25-YR</u>	<u>50-YR</u>	<u>100-YR</u>
91	1.00	1.23	1.65	1.92	2.24	2.57	2.86
92	1.00	1.22	1.63	1.90	2.22	2.55	2.83
93	0.99	1.21	1.62	1.89	2.20	2.53	2.81
94	0.98	1.20	1.61	1.87	2.19	2.51	2.79
95	0.97	1.19	1.59	1.85	2.17	2.49	2.76
96	0.96	1.18	1.58	1.84	2.15	2.46	2.74
97	0.96	1.17	1.57	1.82	2.13	2.44	2.72
98	0.95	1.16	1.56	1.81	2.12	2.42	2.70
99	0.94	1.15	1.54	1.80	2.10	2.41	2.67
100	0.93	1.14	1.53	1.78	2.08	2.39	2.65
101	0.93	1.13	1.52	1.77	2.07	2.39	2.65
102	0.92	1.13	1.51	1.75	2.05	2.35	2.61
103	0.91	1.12	1.50	1.74	2.04	2.33	2.59
104	0.90	1.11	1.49	1.73	2.02	2.31	2.57
105	0.90	1.10	1.47	1.72	2.01	2.30	2.55
106	0.89	1.09	1.46	1.70	1.99	2.28	2.54
107	0.88	1.09	1.45	1.69	1.98	2.26	2.52
108	0.88	1.08	1.44	1.68	1.96	2.25	2.50
109	0.87	1.07	1.43	1.67	1.95	2.23	2.48
110	0.87	1.06	1.42	1.65	1.93	2.21	2.46
111	0.86	1.06	1.41	1.64	1.92	2.20	2.45
112	0.85	1.05	1.40	1.63	1.91	2.18	2.43
113	0.85	1.04	1.39	1.62	1.89	2.17	2.41
114	0.84	1.03	1.38	1.61	1.88	2.15	2.40
115	0.84	1.03	1.37	1.60	1.87	2.14	2.38
116	0.83	1.02	1.36	1.59	1.86	2.12	2.36
117	0.82	1.01	1.36	1.58	1.84	2.11	2.35
118	0.82	1.01	1.35	1.57	1.83	2.09	2.33
119	0.81	1.00	1.34	1.56	1.82	2.08	2.32
120	0.81	0.99	1.33	1.55	1.81	2.07	2.30

<u>DURATION IN HOURS</u>	<u>RETURN PERIODS OF</u>						
	<u>1-YR</u>	<u>2-YR</u>	<u>5-YR</u>	<u>10-YR</u>	<u>25-YR</u>	<u>50-YR</u>	<u>100-YR</u>
2	0.81	0.99	1.33	1.55	1.81	2.07	2.30
3	0.59	0.72	0.97	1.13	1.32	1.51	1.68
4	0.47	0.58	0.78	0.91	1.06	1.21	1.35
5	0.40	0.49	0.66	0.77	0.89	1.02	1.14
6	0.35	0.42	0.57	0.67	0.78	0.89	0.99
8	0.28	0.34	0.46	0.53	0.62	0.71	0.79
10	0.23	0.29	0.39	0.45	0.52	0.60	0.67
12	0.20	0.25	0.33	0.39	0.45	0.52	0.58
18	0.15	0.18	0.24	0.28	0.33	0.38	0.42
24	0.12	0.15	0.20	0.23	0.27	0.31	0.34

ATTACHMENT B  
DRAINAGE CRITERIA MANUAL

INCREMENTAL INFILTRATION VALUES IN INCHES

Time Minutes**	SCS Hydrologic Soil Group			
	A	B	C	D
5	.33	.26	.19	.12
10	.25	.17	.09	.04
15	.18	.11	.05	.02
20	.13	.07	.03	.02
25	.10	.05	.03	.02
30	.08	.05	.03	.02
35	.08	.05	.03	.02
40	.08	.05	.03	.02
45	.08	.05	.03	.02
50	.08	.05	.03	.02
55	.08	.05	.03	.02
60	.08	.05	.03	.02
65	.08	.05	.03	.02
70	.08	.05	.03	.02
75	.08	.05	.03	.02
80	.08	.05	.03	.02
85	.08	.05	.03	.02
90	.08	.05	.03	.02
95	.08	.05	.03	.02
100	.08	.05	.03	.02
105	.08	.05	.03	.02
110	.08	.05	.03	.02
115	.08	.05	.03	.02
120	.08	.05	.03	.02

\*\*Time at end of the time increment

NOTE: Values for 125 minutes and additional 5 minute increments shall be the same as those shown for 120 minutes.

ATTACHMENT C

DRAINAGE CRITERIA MANUAL

DEPRESSION STORAGE LOSSES

<u>Surface Type</u>	<u>Total Loss (Inches)</u>
Impervious:	
Paved Areas	0.1
Flat Roofs	0.1
Sloped Roofs	0.05
Pervious:	
Lawns and Grass	0.3
Wooded Areas and Open Fields	0.4

## ATTACHMENT D

## DRAINAGE CRITERIA

RECOMMENDED RUNOFF COEFFICIENTS FOR RATIONAL METHOD  
AND PERCENT IMPERVIOUS FOR UNIT HYDROGRAPH METHOD

Land Use or Surface Characteristics	Percent Impervious	Frequency			
		<u>2</u>	<u>5</u>	<u>10</u>	<u>100</u>
1. Business:					
Downtown Areas	95	0.84	0.85	0.87	0.91
Neighborhood Areas	70	0.68	0.69	0.73	0.80
2. Residential:					
Single Family (Soil Group D)					
1/8 Acre	50	0.57	0.61	0.66	0.79
1/4 Acre	38	0.50	0.54	0.62	0.76
1/3 Acre	30	0.46	0.50	0.59	0.73
1/2 Acre	25	0.42	0.48	0.56	0.72
3/4 Acre	22	0.42	0.46	0.55	0.71
1 Acre	20	0.41	0.45	0.54	0.71
Multi-Family (Soil Group D)					
Multi-Unit (detached)	60	0.62	0.66	0.72	0.82
Multi-Unit (attached)	65	0.64	0.68	0.73	0.83
Apartments	75	0.70	0.73	0.79	0.86
Single Family (Soil Group C)					
1/8 Acre	50	0.55	0.58	0.64	0.73
1/4 Acre	38	0.48	0.51	0.57	0.68
1/3 Acre	30	0.43	0.46	0.53	0.65
1/2 Acre	25	0.40	0.43	0.50	0.63
3/4 Acre	22	0.39	0.42	0.49	0.62
1 Acre	20	0.37	0.40	0.48	0.61
Multi-Family (Soil Group C)					
Multi-Unit (detached)	60	0.60	0.63	0.69	0.77
Multi-Unit (attached)	65	0.63	0.66	0.71	0.79
Apartments	75	0.68	0.72	0.77	0.83
Single-Family (Soil Group B)					
1/8 Acre	50	0.52	0.54	0.59	0.67
1/4 Acre	38	0.44	0.46	0.52	0.61
1/3 Acre	30	0.39	0.41	0.47	0.57
1/2 Acre	25	0.36	0.38	0.44	0.54
3/4 Acre	22	0.34	0.36	0.42	0.52
1 Acre	20	0.33	0.35	0.40	0.51
Multi-Family (Soil Group B)					
Multi-Unit (detached)	60	0.58	0.60	0.65	0.72
Multi-Unit (attached)	65	0.61	0.64	0.68	0.75
Apartments	75	0.67	0.70	0.74	0.80

Land Use or Surface Characteristics	Percent Impervious	Frequency			
		2	5	10	100
<u>Single Family (Soil Group A)</u>					
1/8 Acre	50	0.47	0.50	0.54	0.60
1/4 Acre	38	0.39	0.41	0.45	0.52
1/3 Acre	30	0.33	0.35	0.39	0.47
1/2 Acre	25	0.30	0.31	0.35	0.44
3/4 Acre	22	0.28	0.29	0.33	0.42
1 Acre	20	0.26	0.28	0.32	0.40
<u>Multi-Family (Soil Group A)</u>					
Multi-Unit (detached)	60	0.55	0.57	0.61	0.67
Multi-Unit (attached)	65	0.58	0.60	0.64	0.70
Apartments	75	0.65	0.68	0.72	0.77
3. Industrial:					
Light Areas	70	0.68	0.69	0.73	0.80
Heavy Areas	80	0.74	0.76	0.79	0.84
4. Playgrounds:	15	0.33	0.35	0.42	0.55
5. Schools:	40	0.49	0.51	0.56	0.66
6. Railroad Yard Areas:	30	0.43	0.45	0.50	0.62
Undeveloped Urban Areas:					
Offsite Flow Analysis (when land use not defined)	45	0.52	0.54	0.59	0.68
8. Streets:					
Paved	99	0.87	0.88	0.90	0.93
Gravel	00	0.24	0.26	0.33	0.48
9. Drive, Parking Lots and Walks:	96	0.87	0.87	0.88	0.89
10. Roofs:	90	0.80	0.85	0.90	0.93
11. Urban Lawn Areas (See Note No. 1 below):					
<u>Soil Group A</u>					
Slope less than 1%	00	0.08	0.09	0.13	0.23
Slope 1% to 4%	00	0.12	0.13	0.17	0.27
Slope more than 4%	00	0.16	0.17	0.21	0.31
<u>Soil Group B</u>					
Slope less than 1%	00	0.16	0.18	0.24	0.37
Slope 1% to 4%	00	0.20	0.22	0.28	0.41
Slope more than 4%	00	0.24	0.26	0.32	0.45
<u>Soil Group C</u>					
Slope less than 1%	00	0.24	0.27	0.35	0.51
Slope 1% to 4%	00	0.26	0.29	0.37	0.53
Slope more than 4%	00	0.28	0.31	0.39	0.55

<u>Land Use or Surface Characteristics</u>	<u>Percent Impervious</u>	<u>Frequency</u>			
		<u>2</u>	<u>5</u>	<u>10</u>	<u>100</u>
<u>Soil Group D</u>					
Slope less than 1%	00	0.28	0.33	0.43	0.63
Slope 1% to 4%	00	0.30	0.35	0.45	0.65
Slope more than 4%	00	0.32	0.37	0.47	0.67

Note No. 1: Coefficients shown in the above table are for pervious open space areas with thick turf which includes pervious areas in parks and cemeteries. Coefficients shown above must be increased 0.02 for use with agricultural pasture areas. Coefficients shown above must be reduced by 0.04 for use with agricultural cultivated areas. Group A soils are well-drained, coarse textured sands with high infiltration rates. Group B soils are moderately well-drained, moderately coarse textured soils with moderate infiltration rates. Group C soils are moderately poor-drained, moderately fine textured soils with slow infiltration rates. Group D soils are poor-drained, fine textured soils with very slow infiltration rates.

GENERAL NOTE: These Rational Formula Coefficients may not be valid for basins 320 acres or larger.

ATTACHMENT E

DRAINAGE CRITERIA

AVERAGE OVERLAND FLOW VELOCITY FOR USE WITH URBANIZED AREAS

Surface Type	VELOCITY IN FEET/SECOND FOR SLOPES IN PERCENT SHOWN																			
	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0	20.0
Forest with Heavy Ground Litter or Meadow	0.03	0.04	0.06	0.07	0.08	0.09	0.10	0.11	0.12	0.13	0.16	0.21	0.28	0.33	0.39	0.46	0.53	0.60	0.72	1.10
Fallow or Minimum Tillage Cultivation	0.06	0.08	0.10	0.12	0.13	0.14	0.16	0.17	0.18	0.19	0.29	0.40	0.51	0.66	0.78	0.91	1.05	1.20	1.44	2.10
Short Grass Pasture or Lawns	0.09	0.13	0.15	0.18	0.20	0.21	0.23	0.25	0.26	0.28	0.45	0.60	0.77	0.96	1.17	1.33	1.50	1.68	1.98	3.20
Almost Bare Ground	0.16	0.22	0.28	0.31	0.35	0.38	0.41	0.44	0.46	0.49	0.70	0.85	1.05	1.26	1.50	1.75	2.03	2.32	2.79	4.40
Grassed Waterway	0.35	0.48	0.58	0.67	0.77	0.84	0.91	0.98	1.05	1.12	1.54	1.82	2.10	2.38	2.78	3.20	3.66	4.14	4.56	7.00
Paved Areas (Sheet Flow) or Shallow Gutter Flow	0.44	0.62	0.77	0.91	1.05	1.12	1.19	1.26	1.33	1.40	2.00	2.55	3.20	3.83	4.41	5.04	5.70	6.00	6.20	9.00

ATTACHMENT F

DETERMINATION OF DIMENSIONLESS  
WATERSHED CONVEYANCE FACTOR ( $\emptyset$ )

$$\emptyset = \emptyset_1 + \emptyset_2$$

$\emptyset_1$	Classification
0.6	Extensive channel improvement and storm sewer system, closed conduit channel system
0.7	Moderate channel improvement and storm sewer system.
0.8	Some channel improvement and storm sewers, mainly cleaning and enlargement of existing channel.
0.9	Little channel improvement and storm sewers.
1.0	Natural channel conditions.
$\emptyset_2$	Classification
0.0	No channel vegetation.
0.1	Light channel vegetation.
0.2	Moderate channel vegetation.
0.3	Heavy channel vegetation.

## EXHIBIT NO. 1

## SOIL LEGEND

<u>SYMBOL</u>	<u>HYDROLOGIC GROUP</u>	<u>NAME</u>
Aa	B	Albion-Shellabarger sandy loams, 1 to 4 percent slopes
Ab	B	Albion and Shellabarger sandy loams, 7 to 15 percent slopes
Ba	C	Blanket silt loam, 0 to 1 percent slopes
Bb	C	Blanket silt loam, 1 to 3 percent slopes**
Ca	B	Canadian fine sandy loam
Cb	B	Canadian-Waldeck fine sandy loams
Cc	D	Carwile fine sandy loam
Cd	B	Clark-Ost clay loams, 1 to 4 percent slopes
Ce	C	Clime silty clay, 3 to 6 percent slopes
Ea	B	Elandco silt loam
Eb	B	Elandco silt loam, occasionally flooded
Ec	B	Elandco silt loam, frequently flooded
Fa	B	Farnum loam, 0 to 1 percent slopes
Fb	B	Farnum loam, 1 to 3 percent slopes
Fc	B	Farnum loam, sandy substratum, 0 to 1 percent slopes
Ga	D	Goessel silty clay, 0 to 1 percent slopes
Gb	D	Goessel silty clay, 1 to 2 percent slopes
Ia	D	Irwin silty clay loam, 1 to 3 percent slopes
Ib	D	Irwin silty clay loam, 3 to 6 percent slopes
Ic	D	Irwin silty clay loam, 2 to 6 percent slopes, eroded
La	C	Lesho loam
Lb	A	Lincoln soils
Ma	B	Milan loam, 1 to 3 percent slopes
Mb	B	Milan form, 3 to 6 percent slopes
Mc	B	Milan clay loam, 2 to 6 percent slopes, eroded
Na	B	Naron fine sandy loam
Oc	D	Owens clay loam, 1 to 3 percent slopes
Od	D	Owens-Rock outcrop complex, 3 to 10 percent slopes
Pa		Pits
Pb	D	Plevna fine sandy loam
Pc	A	Pratt loamy fine sand, undulating
Pd	A	Pratt-Tivoli complex, rolling
Ra	D	Renfrow silty clay loam, 1 to 3 percent slopes
Rb	D	Renfrow silty clay loam, 3 to 6 percent slopes
Rc	D	Renfrow-Owens clay loams, 1 to 4 percent slopes
Rd	D	Rosehill silty clay, 1 to 3 percent slopes
Sa	B	Shellabarger sandy loam, 1 to 3 percent slopes
Sb	B	Shellabarger sandy loam, 3 to 6 percent slopes
Sc	B	Shellabarger sandy loam, 3 to 6 percent slopes, eroded
Ta	D	Tabler silty clay loam
Tb	D	Tabler-Drummond complex
Ua	B	Urban land-Canadian complex
Ub	B	Urban land-Elandco complex
Uc	B	Urban land-Farnum complex, 0 to 3 percent slopes
Ud	D	Urban land-Irwin complex, 1 to 3 percent slopes
Ue	D	Urban land-Tabler complex
Va	B	Vanoss silt loam, 0 to 1 percent slopes
Vb	B	Vanoss silt loam, 1 to 3 percent slopes
Vc	B	Vanoss silt loam, 3 to 6 percent slopes
Vd	B	Vanoss silt loam, 3 to 6 percent slopes, eroded
Ve	D	Vernon sandy loam, 1 to 3 percent slopes
Vf	D	Vernon sandy loam, 3 to 6 percent slopes
Wa	C	Waldeck sandy loam





# LETTER OF TRANSMITTAL

**Professional Engineering Consultants, P.A.**  
303 S. TOPEKA - WICHITA, KANSAS 67202 - 316-262-2691 - FAX 316-262-3003  
www.pec1.com - designers@pec1.com

TO: Dept. of Public Works  
7<sup>th</sup> Floor City Hall  
455 N. Main  
Wichita, Ks. 67202

PROJECT NO.: 36-04165-3104  
PROJECT: Creekside at Pembroke

ATTENTION: Vicky Huang

DATE: 6/28/04

WE ARE SENDING YOU:  Attached  Under separate cover via \_\_\_\_\_ the following items:  
 Shop drawings  Prints  Plans  Samples  Specifications  
 Copy of letter  Change order  \_\_\_\_\_

COPIES	DATE	NO.	DESCRIPTION
2			Drainage plan

THESE ARE TRANSMITTED as checked below:

- For approval  Approved as submitted  Resubmit \_\_\_\_\_ copies for approval
- For your use  Approved as noted  Submit \_\_\_\_\_ copies for distribution
- As requested  Returned for corrections  \_\_\_\_\_ corrected prints
- For review and comment  \_\_\_\_\_
- FOR BIDS DUE \_\_\_\_\_  PRINTS RETURNED AFTER LOAN TO US

REMARKS:

**RECEIVED**  
**JUN 28 2004**  
**CITY - ENGINEERING**

COPY TO: file

SIGNED Rob Hartman

If enclosures are not as noted, kindly notify us at once.