



Professional Engineering Consultants, P.A.

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Remington Place 2nd **Wichita, Sedgwick County, Kansas**

9/16/02

Remington Place 2nd is a development in northeast Wichita containing both commercial and residential areas. It consists of a 2.6 acre area for commercial use and 14 residential lots. Development plans include commercial office buildings, parking, open space, patio homes, three landscaped ponds, and utilities. The drainage plan and supporting calculations for Remington Place 2nd are presented herein.

Hydrology

The proposed plat lies in the E ½, NW ¼, Section 9, T27S, R2E of the 6th P.M. The soils on-site consist of Goessel silty clay and Irwin silty clay loam. These soils are classified in hydrologic group D. The existing landscape is vacant posture with trees on all sides and across the middle of the property. The plat generally drains to the northeast corner of the plat and then to a Four Mile Creek tributary.

For runoff calculations, the plat was divided into 3 major basins, each with its own discharge. Additional runoff on the site will come from the south via a future storm sewer and street flow from Remington Place Addition. The offsite runoff combined with Basin 1 runoff will discharge to Pond No. 1. Pond No. 1 will discharge to Pond No. 2, which also accepts runoff from Basin 2. Pond No. 2 will then discharge to Pond No. 3, which also accepts runoff from Basin 3. The net effect of the three ponds is to reduce the plat runoff from 74.6 cfs for existing conditions to 64.0 cfs for proposed conditions.

Using the Army Corp of Engineer's program HEC-1, all systems were modeled with runoff based on the Rational Method. In the model, minor basins 1B, 1C, 1D, and 1E were combined with the offsite basin due to the small size of the basins and to the fact that the runoff from the minor basins joins the offsite runoff before entering Pond No. 1. The minimum time of concentration was assumed for all basins, so the basins could be combined with negligible lag time. The ponds were included to determine water elevations in the 100-year design storm and to determine the outfall from the ponds via weirs.

Runoff coefficients were estimated based on existing land use and the tables presented in the Design Aids section. A map showing the basin boundaries, drainage calculations, and HEC-1 model are included. The analysis made is based on the available site data which includes the following: 1"=100' topographic map with 2' contours of the site and adjacent areas, USGS topographic map, Sedgwick County Soil Survey Map, and references noted herein.

Storm Sewer Design

For the storm sewer hydrologic analysis, the Rational Method was again used. Runoff coefficients were estimated using the charts in the design aids section of this report. For this development, a uniform assumption of the minimum time of concentration of 15 minutes was deemed appropriate. Travel time for flow through defined channels, pipes, etc, for these basins was estimated on the basis of Manning's Equation.

In the hydraulic analysis, the storm sewers are designed for the minor storm, with major storm overflows to be routed through easements and rights-of-way to an appropriate outlet. The minor storm has a recurrence interval of two years. The major storm evaluated has a recurrence interval of one hundred years. To simplify this analysis, the time of concentration is identical for both the major and the minor storms.

For each inlet, street flooding and inlet capacity were checked for the minor storm. Conveyance in the street is based on the Modified Manning's Equation, as expressed in the Design of Urban Highway Drainage-The State of the Art, Equation (5-1), page 5-9. It has been assumed that T_c for street flow is equal to T_c for pipe flow. This is a simplifying, but conservative, assumption, since pipe flow velocities generally exceed street flow velocities.

Inlet capacities were determined by the methods described in Drainage of Highway Pavements, Hydraulic Engineering Circular #12, using Chart #12 as found in the Design Aids section. City of Wichita Type 1A inlets and 3/8 inch per foot cross slopes have been assumed. Streets have been assumed to have 6-5/8 inch standard curb, unless otherwise noted.

The storm sewer for this plat is designed to tie into the future storm sewer from Remington Place Addition and Cranbrook Street. Hydraulic computation for the pipe system was performed using PEC's STORM computer program. This program uses Manning's Equation to calculate friction losses for pipes flowing full. Minor losses are computed by momentum principles at each structure. All pipe area is assumed to be reinforced concrete with a Manning's "n" of 0.013. It is desirable to keep the hydraulic grade line at least one foot below the top of curb for the minor storm. The STORM analysis for the combined storm sewer is

included in this report. Note that the inlet at node 130 and, subsequently, the pipe system connecting node 130 to Pond 1 was sized to handle flows from the 100-year storm in order to greatly reduce overflow between lots 11 and 12 during storms greater than the 2-year storm. (The STORM analysis showing the sizing of inlet 130 and the analysis showing the actual 2-year storm flow rates are both included.)

Design Aids

This section includes material used to assist in designing the drainage system. A 1"=50' scale drainage plan map is enclosed in the pocket.

References

Design of Urban Highway Drainage – The State of the Art, by Reitz & Jens, Inc., April 1980.

Drainage of Highway Pavements, Hydraulic Engineering Circular #12, by Tye Engineering, Inc., March 1984.

Interim Drainage and Storm Sewer Policy for Design Criteria and Documentation, City of Wichita, Kansas, 1985.

Soil Survey of Sedgwick County, Kansas, US Department of Agriculture, Soil Conservation Service, 1979.



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Project REMINGTON PLACE 2NDDate 9/12/02

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Item HYDROLOGY

By _____

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EXISTING CONDITIONS

THE DISCHARGE FROM THIS SITE IS AN OVERLAND SWALE AT THE NORTHEAST CORNER OF THE PLAT. OPPOSITE RUNOFF FROM REMINGTON PLACE ADDITION ALSO DISCHARGES AT THIS POINT.

FIND EXISTING RUNOFF USING THE RATIONAL METHOD, $Q = CIA$

1. AREA = 15.5 A₂

2. RUNOFF COEFFICIENTS, C
PERVIOUS OPEN SPACE
SOIL GROUP "D", 1-4% SLOPE
 $C_{100} = 0.65$

3. INTENSITY, i
ASSUME MINIMUM TIME OF CONCENTRATION, $T_c = 15 \text{ MIN}$
 $i_{100} = 7.4 \text{ IN/HR}$

4. $Q_{100} = C_{100} i_{100} A$

$$Q_{100} = 0.65(7.4 \text{ IN/HR})(15.5 \text{ A}_2) = 74.6 \text{ CFS}$$

THEREFORE, THE EXISTING CONDITIONS RUNOFF FROM THIS SITE IS 74.6 CFS FOR THE 100-YR STORM. THE PROPOSED CONDITIONS RUNOFF FOR THIS PLAT SHOULD NOT EXCEED 74.6 CFS. PROPOSED CONDITIONS INCLUDE THE PROPOSED DEVELOPMENT OF THIS PLAT AND THE DEVELOPMENT OF THE AREA IN REMINGTON PLACE ADDITION WHOSE RUNOFF ENTERS THIS SITE.



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PROPOSED CONDITIONS

FIND PROPOSED CONDITIONS RUNOFF

1. AREAS: 2.2 AC OFFICE
1.9 AC POND RESERVE
11.4 AC RESIDENTIAL

2. RUNOFF COEFFICIENTS, C

2.2 AC OFFICE
BUSINESS NEIGHBORHOOD AREAS
 $C_{100} = 0.80$

1.9 AC POND RESERVE
"D" 1-4% SLOPE
 $C_{100} = 0.65$

11.4 AC RESIDENTIAL
1/4 AC RES. SINGLEFAMILY "D"
 $C_{100} = 0.76$

$$C_{100} = \frac{2.2 (0.80)}{15.5} + \frac{1.9 (0.65)}{15.5} + \frac{11.4 (0.76)}{15.5} = 0.75$$

3. INTENSITY, i

$T_c = 15 \text{ MIN}$

$i_{100} = 7.4 \text{ IN/HR}$

4. $Q_{100} = C_{100} i_{100} A$

$$Q_{100} = 0.75 (7.4 \text{ IN/HR}) (15.5 \text{ AC}) = 86.0 \text{ CFS}$$

THEREFORE, NEED TO HAVE DETENTION TRENDS
IN ORDER TO REDUCE RUNOFF FROM THE SITE
SINCE $86.0 \text{ CFS} > \text{EXISTING RUNOFF}$.



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POND #1

INFLOW

BASIN 1 AND OFFSITE FROM REMINGTON PUMP ADDITION

BASIN 1: 0.6 AC OFFICE, $C_{100} = 0.80$
4.3 AC 1/4 AC RES, $C_{100} = 0.76$

$$C_{100} = \frac{0.6}{4.9} (0.80) + \frac{4.3}{4.9} (0.76) = 0.76$$

$$t_c = 15 \text{ MIN}, i_{100} = 7.4 \text{ IN/HR} \quad (* \text{ USE } t_c = 15 \text{ MIN FOR ALL BASINS})$$

$$Q_{100} = 0.76 (7.4 \text{ IN/HR}) (4.9 \text{ AC}) = \underline{27.6 \text{ CFS}}$$

OFFSITE: 6.8 AC 1/4 AC RES, $C_{100} = 0.76$

$$i_{100} = 7.4 \text{ IN/HR}$$

$$Q_{100} = 0.76 (7.4 \text{ IN/HR}) (6.8 \text{ AC}) = \underline{38.2 \text{ CFS}}$$

$$\therefore \text{INFLOW} = 27.6 + 38.2 = 65.8 \text{ CFS}$$

$$\text{STATIC POOL EL} = 202.0'$$

SURFACE AREA

$$\begin{aligned} @ 202.0' &= 0.20 \text{ AC} \\ @ 204.0' &= 0.27 \text{ AC} \end{aligned}$$

OUTFALL

ASSUME 10' BROAD-CRESTED WEIR @ 202.0'

FROM HEC-1 USING WEIR EQUATION $Q = CLH^{1.5}$
WITH $C = 3.2$

$$\begin{aligned} \text{DWS}_{100} &= 203.0' \\ Q_{100} &= 64 \text{ CFS} \end{aligned}$$



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POND # 2

INFLOW

BASIN 2 AND POND 1 OUTFALL

BASIN 2: 2.1 AC OFFICE, $C_{100} = 0.80$
0.9 AC 1/2 ACRES, $C_{100} = 0.79$

$$C_{100} = 0.80$$

$$i_{100} = 7.4 \text{ in/hr}$$

$$Q_{100} = 0.80(7.4 \text{ in/hr})(3.0 \text{ AC}) = \underline{17.8 \text{ CFS}}$$

$$\text{POND 1} = \underline{64 \text{ CFS}}$$

$$\therefore \text{INFLOW} = 17.8 + 64 = 81.8 \text{ CFS}$$

$$\text{STATIC EL} = 199^{\circ}$$

SURFACE AREA

$$@ 199^{\circ} = 0.43 \text{ AC}$$

$$@ 202^{\circ} = 0.64 \text{ AC}$$

OUTFALL

5' WEIR @ 199° , $C = 3.2$

FROM HEC-1

$$DWS_{100} = 201^{\circ}$$

$$Q_{100} = 67 \text{ CFS}$$



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POND #3

INFLOW

BASIN 3 AND POND 2 OUTFALL

BASIN 3: 0.6 AC OFFICE, $C_{100} = 0.80$
0.2 AC 1/3 AC RES, $C_{100} = 0.79$

$$C_{100} = 0.80$$

$$I_{100} = 7.4 \text{ IN/HR}$$

$$Q_{100} = 0.80(7.4 \text{ IN/HR})(0.8 \text{ AC}) = \underline{4.7 \text{ CFS}}$$

POND 2 = 67 CFS

$$\therefore \text{INFLOW} = 4.7 + 67 = 71.7 \text{ CFS}$$

STATIC EL = 195'

SURFACE AREA

$$\text{@ } 195' = 0.30 \text{ AC}$$

$$\text{@ } 198' = 0.50 \text{ AC}$$

OUTFALL

5' WEIR @ 195', $C = 3.2$

FROM HEC-1

$$DWS_{100} = 197.5$$

$$Q_{100} = 64 \text{ CFS}$$

POND 3 OUTFALL IS THE RUNOFF LEAVING THE SITE.
 \therefore RUNOFF LEAVING THE SITE IS 64 CFS WHICH IS LESS
THAN EXISTING RUNOFF FROM THE SITE EQUAL TO
74.6 CFS.



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PROPOSED SWS

THE PROPOSED SWS FOR REMINGTON PLACE 2ND IS DESIGNED TO TIE INTO SWS FROM REMINGTON PLACE ADDITION ALONG CRANBROOK. THE STORM COMPUTER ANALYSIS OF THE ENTIRE SWS SYSTEM IS INCLUDED IN THIS REPORT.

1. HYDROLOGY USING RATIONAL METHOD, $Q = CIA$

DETERMINE AREAS, A

BASIN	NODE	AREA (AC)
IB	130	2.84
IC	150	0.61
ID	160	0.47
IE	170	0.31

DETERMINE RUNOFF COEFFICIENTS, C

BASIN	NODE	SOIL GROUP	LAND USE	C_2	C_{100}
IB	130	D	1/4 ACRES	0.50	0.76
IC	150	D	1/4 ACRES	0.50	0.76
ID	160	D	1/4 ACRES	0.50	0.76
IE	170	D	1/4 ACRES	0.50	0.76

DETERMINE INTENSITY, i

ASSUME MINIMUM TIME OF CONCENTRATION, $T_c = 15$ MIN FOR ALL BASINS

$\therefore i_2 = 3.8 \text{ IN/HR}$



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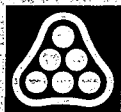
DETERMINE FLOW RATES, (Q)

BASIN	NODE	C ₂	C ₁₀₀	C ₂	C ₁₀₀	A (ft ²)	Q ₂ (CFS)	Q ₁₀₀ (CFS)
1B	130	0.50	0.76	3.8	7.4	2.84	5.4	16.0
1C	150	0.50	0.76	3.8	7.4	0.61	1.2	3.4
1D	160	0.50	0.76	3.8	7.4	0.47	0.9	2.6
1E	170	0.50	0.76	3.8	7.4	0.31	0.6	1.7

2. INLET SIZING / FLOOD ROUTING (2-4R)

BASIN	NODE	INLET	Q (CFS)	Q _{MAX} (5' INLET)	Q _{MAX} (10' INLET)	Q _{IN}	Q _{BY}	USE
1B	130	SUMP	*16.0	11.0	22.0	16.0	—	L=10'
1C	150	R4826	1.2	N/A	N/A	1.2	—	1-2x2
1D	160	R4826	0.9	N/A	N/A	0.9	—	1-2x2
1E	170	R4826	0.6	N/A	N/A	0.6	—	1-2x2

* NOTE THAT Q₁₀₀ WAS USED TO SIZE THE INLET AT NODE 130. BY SIZING THE INLET TO INTERCEPT THE 100-YR STORM FLOW, OVERLAND FLOW BETWEEN LOTS 11 AND 12 FROM THE STREET SHOULD BE DRASTICALLY REDUCED IN STORMS EXCEEDING THE 2-4R STORM, THUS PREVENTING SEVERE WASHOUT.



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3. STREET FLOW

2-YR

NODE	BASIN	Q_2	DISTRIBUTION	STREET SLOPE	d	d_{max}	COMMENT
130	1B	5.4	100% (E) = 5.4	0.5%	0.36'	0.55'	OK

100-YR

LOCATION	CONTRIBUTING AREA	Q_{100}	Q_{pipe}	Q_{street}	STREET SLOPE	Q_{max}	COMMENT
NODE 130	100% 1B	16.0	-	16.0	0.5%	29.2	OK

* Q_{max} IS THE MAX FLOW THE STREET CAN HANDLE W/O OVERDROPPING THE CURB

4. OVERFLOW

100-YR FLOW AT NODES 150, 160, AND 170 WILL FLOW TO CRANBROOK STREET AND BE CARRIED TO POND 1 VIA CRANBROOK STREET FLOW, WHICH IS DESIGNED WITH SUFFICIENT CAPACITY TO HANDLE THIS FLOW.

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* FEBRUARY 1981 *
* REVISED 02 AUG 88 *
* RUN DATE 09/13/2002 TIME 08:36:26 *

* U.S. ARMY CORPS OF ENGINEERS *
* THE HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *

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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Remington Place Second
2 ID 2, 10, 25 & 100 year storms
3 ID Professional Engineering Consultants
4 ID Wichita, Ks
5 ID SPL 08/23/02
6 ID File: 0:\SPL\HEC1\REM4.IH1
7 IT 6 12DEC97 0000 300
8 IN 30 12DEC97 0600
9 IO 3 0
10 JR PREC .448718 .679487 .78947 1.000

DIAGRAM

11 KK BAS1 Basin to Pond 1 via street and SWS (offsite, 1B, 1C, 1D, and 1E)
12 BA .01672
13 PB 7.8
14 PC 0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
15 PC .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
16 PC .880 .890 .900 .910 .916 .925 .934 .943 .952 .958
17 PC .964 .970 .976 .982 .988 .994 1.000
18 LS 0 87 0
19 UD .15

20 KK BAS1A Basin 1A directly to pond 1 including pond 1
21 BA .00156
22 PB 7.8
23 PC 0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
24 PC .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
25 PC .880 .890 .900 .910 .916 .925 .934 .943 .952 .958
26 PC .964 .970 .976 .982 .988 .994 1.000
27 LS 0 94 0
28 UD .15

29 KK COMB1
30 KO 5
31 HC 2

32 KK POND1
33 RS 1 ELEV 202
34 SA .20 27
35 SE 202 204
36 SS 202 10 3.2 1.5

37 KK BAS2 Basin 2 to Pond 2
38 BA .00469
39 PB 7.8
40 PC 0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
41 PC .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
42 PC .880 .890 .900 .910 .916 .925 .934 .943 .952 .958

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
43 PC .964 .970 .976 .982 .988 .994 1.000
44 LS 0 94 0
45 UD .15

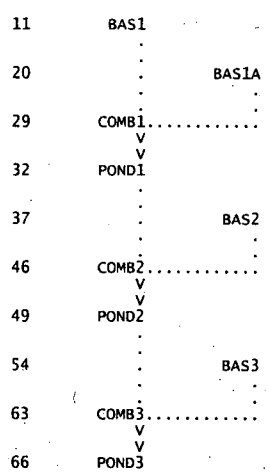
46 KK COMB2
47 KO 5
48 HC 2

49 KK POND2
50 RS 1 ELEV 199
51 SA .43 64
52 SE .199 202
53 SS 199.0 5 3.2 1.5

54 KK BAS3 Basin 3 to Pond 3
55 BA .00125
56 PB 7.8
57 PC 0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
58 PC .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
59 PC .880 .890 .900 .910 .916 .925 .934 .943 .952 .958

60	PC	.964	.970	.976	.982	.988	REM4.OH1	
61	LS	0	94	0			.994	1.000
62	UD	.15						
	*							
	*							
63	KK	COMB3						
64	KD	5						
65	HC	2						
	*							
	*							
66	KK	POND3						
67	RS	1	ELEV	195				
68	SA	.30	.50					
69	SE	195	198					
70	SS	195.0	5	3.2	1.5			
	*							
	*							
71	ZZ							

1
 SCHEMATIC DIAGRAM OF STREAM NETWORK
 INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW



(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

 FLOOD HYDROGRAPH PACKAGE: (HEC-1)
 FEBRUARY 1981
 REVISED 02 AUG 88
 *
 * RUN DATE 09/13/2002 TIME 08:36:26 *
 *

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 *

Remington Place Second
 2, 10, 25 & 100-year storms
 Professional Engineering Consultants
 Wichita, Ks
 SPL 08/23/02
 File: O:\SPL\HEC1\REM4.IH1

9 IO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IT HYDROGRAPH TIME DATA
 NMIN 6 MINUTES IN COMPUTATION INTERVAL
 IDATE 12DEC97 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 13DEC97 ENDING DATE
 NDTIME 0554 ENDING TIME
 ICENT 19 CENTURY MARK
 COMPUTATION INTERVAL .10 HOURS
 TOTAL TIME BASE 29:90 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-Feet
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .45 .68 .79 1.00

*** **

 *
 * BAS1 * Basin to Pond 1 via street and SWS (offsite, 1B, 1C, 1D, and 1E)
 *

8 IN TIME DATA FOR INPUT TIME SERIES
 TXMTN 30 TIME INTERVAL IN MINUTES

REM4.OHI

CUMULATIVE AREA = .00 SQ MI

*** **

HYDROGRAPH AT STATION BAS1A
FOR PLAN 1, RATIO = .79

TOTAL RAINFALL = 6.16, TOTAL LOSS = .70, TOTAL EXCESS = 5.45

PEAK FLOW	TIME	6-HR	24-HR	72-HR	29.90-HR
(CFS)	(HR)	(CFS)	(CFS)	(CFS)	(CFS)
+	5.	12.00	1.	0.	0.
			4.400	5.453	5.453
			(INCHES)	0.	0.
			(AC-FT)	0.	0.

CUMULATIVE AREA = .00 SQ MI

*** **

HYDROGRAPH AT STATION BAS1A
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = .72, TOTAL EXCESS = 7.08

PEAK FLOW	TIME	6-HR	24-HR	72-HR	29.90-HR
(CFS)	(HR)	(CFS)	(CFS)	(CFS)	(CFS)
+	6.	12.00	1.	0.	0.
			5.681	7.083	7.083
			(INCHES)	1.	1.
			(AC-FT)	0.	0.

CUMULATIVE AREA = .00 SQ MI

29 KK *****
* *
* COMB1 *
* *

30 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

32 KK *****
* *
* POND1 *
* *

HYDROGRAPH ROUTING DATA

33 RS STORAGE ROUTING
NSTPS 1 NUMBER OF SUBREACHES
ITYP ELEV TYPE OF INITIAL CONDITION
RSVRIC 202.00 INITIAL CONDITION
X .00 WORKING R AND D COEFFICIENT

34 SA AREA .2 .3

35 SE ELEVATION 202.00 204.00

36 SS SPILLWAY
CREL 202.00 SPILLWAY CREST ELEVATION
SPWID 10.00 SPILLWAY WIDTH
COQW 3.20 WEIR COEFFICIENT
EXPW 1.50 EXPONENT OF HEAD

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	.47
ELEVATION	202.00	204.00

COMPUTED OUTFLOW-ELEVATION DATA

OUTFLOW	.00	.00	.02	.12	.42	.99	1.94	3.35	5.32	7.95
ELEVATION	202.00	202.00	202.01	202.02	202.06	202.10	202.15	202.22	202.30	202.40
OUTFLOW	11.31	15.52	20.66	26.82	34.10	42.59	52.38	63.57	76.25	90.51
ELEVATION	202.50	202.62	202.75	202.89	203.04	203.21	203.39	203.58	203.78	204.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	.00	.01	.02	.03	.05	.06	.08	.10	.13
OUTFLOW	.00	.12	.42	.99	1.94	3.35	5.32	7.95	11.31	15.52
ELEVATION	202.00	202.02	202.06	202.10	202.15	202.22	202.30	202.40	202.50	202.62
STORAGE	.16	.19	.23	.27	.31	.36	.41	.47		
OUTFLOW	20.66	26.82	34.10	42.59	52.38	63.57	76.25	90.51		
ELEVATION	202.75	202.89	203.04	203.21	203.39	203.58	203.78	204.00		

** WARNING *** MODIFIED PULS ROUTING MAY BE NUMERICALLY UNSTABLE FOR OUTFLOWS BETWEEN 76 TO 91.
THE ROUTED HYDROGRAPH SHOULD BE EXAMINED FOR OSCILLATIONS OR OUTFLOWS GREATER THAN PEAK INFLOWS.
THIS CAN BE CORRECTED BY DECREASING THE TIME INTERVAL OR INCREASING STORAGE (USE A LONGER REACH.)

*** **

HYDROGRAPH AT STATION POND1
FOR PLAN 1, RATIO = .45

PEAK FLOW	TIME	6-HR	24-HR	72-HR	29.90-HR
(CFS)	(HR)	(CFS)	(CFS)	(CFS)	(CFS)
+	23.	12.10	1	1	1

46 KK

 * COMB2 *
 * *

47 KO
 OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

49 KK

 * POND2 *
 * *

HYDROGRAPH ROUTING DATA

50 RS STORAGE ROUTING
 NSTPS 1 NUMBER OF SUBREACHES
 ITYP ELEV TYPE OF INITIAL CONDITION
 RSVRIC 199.00 INITIAL CONDITION
 X .00 WORKING R AND D COEFFICIENT

51 SA AREA .4 .6

52 SE ELEVATION 199.00 202.00

53 SS SPILLWAY
 CREL 199.00 SPILLWAY CREST ELEVATION
 SPWID 5.00 SPILLWAY WIDTH
 COOW 3.20 WEIR COEFFICIENT
 EXPW 1.50 EXPONENT OF HEAD

COMPUTED STORAGE-ELEVATION DATA

STORAGE .00 1.59
 ELEVATION 199.00 202.00

COMPUTED OUTFLOW-ELEVATION DATA

OUTFLOW	.00	.00	.01	.11	.38	.91	1.78	3.08	4.89	7.30
ELEVATION	199.00	199.00	199.01	199.04	199.08	199.15	199.23	199.33	199.45	199.59
OUTFLOW	10.39	14.26	18.97	24.63	31.32	39.12	48.11	58.39	70.04	83.14
ELEVATION	199.75	199.93	200.12	200.33	200.56	200.81	201.08	201.37	201.68	202.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	.02	.04	.06	.10	.15	.20	.27	.34	.43
OUTFLOW	.00	.11	.38	.91	1.78	3.08	4.89	7.30	10.39	14.26
ELEVATION	199.00	199.04	199.08	199.15	199.23	199.33	199.45	199.59	199.75	199.93
STORAGE	.52	.63	.75	.89	1.04	1.21	1.39	1.59		
OUTFLOW	18.97	24.63	31.32	39.12	48.11	58.39	70.04	83.14		
ELEVATION	200.12	200.33	200.56	200.81	201.08	201.37	201.68	202.00		

*** **

HYDROGRAPH AT STATION POND2
 FOR PLAN 1, RATIO = .45

PEAK FLOW	TIME	6-HR	24-HR	72-HR	29.90-HR
+	(CFS)				
+	23.	12.20	5.	1.	1.
	(INCHES)	1.912	2.359	2.359	2.359
	(AC-FT)	2.	3.	3.	3.
PEAK STORAGE	TIME	6-HR	24-HR	72-HR	29.90-HR
+	(AC-FT)				
+	1.	12.20	0.	0.	0.
PEAK STAGE	TIME	6-HR	24-HR	72-HR	29.90-HR
+	(FEET)				
+	200.26	12.20	199.39	199.15	199.12

CUMULATIVE AREA = .02 SQ MI

*** **

HYDROGRAPH AT STATION POND2
 FOR PLAN 1, RATIO = .68

PEAK FLOW	TIME	6-HR	24-HR	72-HR	29.90-HR
+	(CFS)				
+	41.	12.20	8.	3.	2.
	(INCHES)	3.290	4.054	4.054	4.054
	(AC-FT)	4.	5.	5.	5.
PEAK STORAGE	TIME	6-HR	24-HR	72-HR	29.90-HR
+	(AC-FT)				
+	1.	12.20	0.	0.	0.
PEAK STAGE	TIME	6-HR	24-HR	72-HR	29.90-HR
+	(FEET)				
+	200.88	12.20	199.56	199.21	199.17

CUMULATIVE AREA = .02 SQ MI

*** **

HYDROGRAPH AT STATION POND2
 FOR PLAN 1, RATIO = .79

*** **

HYDROGRAPH AT STATION BAS3
FOR PLAN 1, RATIO = .45

TOTAL RAINFALL = 3.50, TOTAL LOSS = .66, TOTAL EXCESS = 2.84

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR MAXIMUM AVERAGE FLOW	72-HR MAXIMUM AVERAGE FLOW	29.90-HR MAXIMUM AVERAGE FLOW
2.	12.00	0.	0.	0.	0.
		(INCHES) 2.316	2.836	2.836	2.836
		(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = .00 SQ MI

*** **

HYDROGRAPH AT STATION BAS3
FOR PLAN 1, RATIO = .68

TOTAL RAINFALL = 5.30, TOTAL LOSS = .70, TOTAL EXCESS = 4.60

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR MAXIMUM AVERAGE FLOW	72-HR MAXIMUM AVERAGE FLOW	29.90-HR MAXIMUM AVERAGE FLOW
3.	12.00	1.	0.	0.	0.
		(INCHES) 3.729	4.604	4.604	4.604
		(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = .00 SQ MI

*** **

HYDROGRAPH AT STATION BAS3
FOR PLAN 1, RATIO = .79

TOTAL RAINFALL = 6.16, TOTAL LOSS = .70, TOTAL EXCESS = 5.45

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR MAXIMUM AVERAGE FLOW	72-HR MAXIMUM AVERAGE FLOW	29.90-HR MAXIMUM AVERAGE FLOW
4.	12.00	1.	0.	0.	0.
		(INCHES) 4.400	5.453	5.453	5.453
		(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = .00 SQ MI

*** **

HYDROGRAPH AT STATION BAS3
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = .72, TOTAL EXCESS = 7.08

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR MAXIMUM AVERAGE FLOW	72-HR MAXIMUM AVERAGE FLOW	29.90-HR MAXIMUM AVERAGE FLOW
5.	12.00	1.	0.	0.	0.
		(INCHES) 5.681	7.083	7.083	7.083
		(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = .00 SQ MI

63 KK *****
* *
* COMB3 *
* *

64 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

66 KK *****
* *
* POND3 *
* *

HYDROGRAPH ROUTING DATA

67 RS STORAGE ROUTING
NSTPS 1 NUMBER OF SUBREACHES
ITYP ELEV TYPE OF INITIAL CONDITION
RSVRIC 195.00 INITIAL CONDITION
X .00 WORKING R AND D COEFFICIENT

68 SA AREA .3 .5

69 SE ELEVATION 195.00 198.00

70 SS SPILLWAY
CREL 195.00 SPILLWAY CREST ELEVATION
SPWID 5.00 SPILLWAY WIDTH
COQW 3.20 WEIR COEFFICIENT
EXPW 1.50 EXPONENT OF HEAD

COMPUTED STORAGE-ELEVATION DATA

STORAGE :00 1.19

COMPUTED OUTFLOW-ELEVATION DATA

OUTFLOW	.00	.00	.01	.11	.38	.91	1.78	3.08	4.89	7.30
ELEVATION	195.00	195.00	195.01	195.04	195.08	195.15	195.23	195.33	195.45	195.59
OUTFLOW	10.39	14.26	18.97	24.63	31.32	39.12	48.11	58.39	70.04	83.14
ELEVATION	195.75	195.93	196.12	196.33	196.56	196.81	197.08	197.37	197.68	198.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	.01	.03	.05	.07	.10	.14	.19	.24	.30
OUTFLOW	.00	.11	.38	.91	1.78	3.08	4.89	7.30	10.39	14.26
ELEVATION	195.00	195.04	195.08	195.15	195.23	195.33	195.45	195.59	195.75	195.93
STORAGE	.37	.45	.54	.65	.76	.89	1.03	1.19		
OUTFLOW	18.97	24.63	31.32	39.12	48.11	58.39	70.04	83.14		
ELEVATION	196.12	196.33	196.56	196.81	197.08	197.37	197.68	198.00		

*** **

HYDROGRAPH AT STATION POND3
FOR PLAN 1, RATIO = .45

PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	29.90-HR
+	(CFS)		24-HR	
+	20.	12.40	72-HR	
	(CFS)	5.	1.	1.
	(INCHES)	1.919	2.381	2.381
	(AC-FT)	2.	3.	3.
PEAK STORAGE	TIME	6-HR	MAXIMUM AVERAGE STORAGE	29.90-HR
+	(AC-FT)		24-HR	
+	0.	12.40	72-HR	
	(AC-FT)	0.	0.	0.
PEAK STAGE	TIME	6-HR	MAXIMUM AVERAGE STAGE	29.90-HR
+	(FEET)		24-HR	
+	196.17	12.40	72-HR	
	(FEET)	195.42	195.16	195.13

CUMULATIVE AREA = .02 SQ MI

*** **

HYDROGRAPH AT STATION POND3
FOR PLAN 1, RATIO = .68

PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	29.90-HR
+	(CFS)		24-HR	
+	38.	12.30	72-HR	
	(CFS)	9.	3.	2.
	(INCHES)	3.300	4.080	4.080
	(AC-FT)	4.	5.	5.
PEAK STORAGE	TIME	6-HR	MAXIMUM AVERAGE STORAGE	29.90-HR
+	(AC-FT)		24-HR	
+	1.	12.30	72-HR	
	(AC-FT)	0.	0.	0.
PEAK STAGE	TIME	6-HR	MAXIMUM AVERAGE STAGE	29.90-HR
+	(FEET)		24-HR	
+	196.78	12.30	72-HR	
	(FEET)	195.59	195.23	195.18

CUMULATIVE AREA = .02 SQ MI

*** **

HYDROGRAPH AT STATION POND3
FOR PLAN 1, RATIO = .79

PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	29.90-HR
+	(CFS)		24-HR	
+	47.	12.30	72-HR	
	(CFS)	10.	3.	3.
	(INCHES)	3.967	4.907	4.907
	(AC-FT)	5.	6.	6.
PEAK STORAGE	TIME	6-HR	MAXIMUM AVERAGE STORAGE	29.90-HR
+	(AC-FT)		24-HR	
+	1.	12.30	72-HR	
	(AC-FT)	0.	0.	0.
PEAK STAGE	TIME	6-HR	MAXIMUM AVERAGE STAGE	29.90-HR
+	(FEET)		24-HR	
+	197.05	12.30	72-HR	
	(FEET)	195.67	195.25	195.20

CUMULATIVE AREA = .02 SQ MI

*** **

HYDROGRAPH AT STATION POND3
FOR PLAN 1, RATIO = 1.00

PEAK FLOW	TIME	6-HR	MAXIMUM AVERAGE FLOW	29.90-HR
+	(CFS)		24-HR	
+	64.	12.30	72-HR	
	(CFS)	14.	4.	3.
	(INCHES)	5.250	6.507	6.507
	(AC-FT)	7.	8.	8.
PEAK STORAGE	TIME	6-HR	MAXIMUM AVERAGE STORAGE	29.90-HR
+	(AC-FT)		24-HR	
+	1.	12.30	72-HR	
	(AC-FT)	0.	0.	0.
PEAK STAGE	TIME	6-HR	MAXIMUM AVERAGE STAGE	29.90-HR
+	(FEET)		24-HR	
+	197.51	12.30	72-HR	
	(FEET)	195.80	195.31	195.25

CUMULATIVE AREA = .02 SQ MI

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION			
				RATIO 1 .45	RATIO 2 .68	RATIO 3 .79	RATIO 4 1.00
HYDROGRAPH AT +	BAS1	.02	1 FLOW TIME	21. 12.00	38. 12.00	46. 12.00	60. 12.00
HYDROGRAPH AT +	BAS1A	.00	1 FLOW TIME	3. 12.00	4. 12.00	5. 12.00	6. 12.00
2 COMBINED AT +	COMB1	.02	1 FLOW TIME	24. 12.00	42. 12.00	50. 12.00	67. 12.00
ROUTED TO +	POND1	.02	1 FLOW TIME	23. 12.10	40. 12.10	48. 12.00	64. 12.00
			** PEAK STAGES IN FEET **				
			1 STAGE TIME	202.80 12.10	203.15 12.10	203.31 12.00	203.59 12.00
HYDROGRAPH AT +	BAS2	.00	1 FLOW TIME	8. 12.00	12. 12.00	14. 12.00	18. 12.00
2 COMBINED AT +	COMB2	.02	1 FLOW TIME	30. 12.00	52. 12.00	62. 12.00	83. 12.00
ROUTED TO +	POND2	.02	1 FLOW TIME	23. 12.20	41. 12.20	50. 12.20	67. 12.20
			** PEAK STAGES IN FEET **				
			1 STAGE TIME	200.26 12.20	200.88 12.20	201.15 12.20	201.61 12.20
HYDROGRAPH AT +	BAS3	.00	1 FLOW TIME	2. 12.00	3. 12.00	4. 12.00	5. 12.00
2 COMBINED AT +	COMB3	.02	1 FLOW TIME	24. 12.20	43. 12.20	53. 12.20	71. 12.10
ROUTED TO +	POND3	.02	1 FLOW TIME	20. 12.40	38. 12.30	47. 12.30	64. 12.30
			** PEAK STAGES IN FEET **				
			1 STAGE TIME	196.17 12.40	196.78 12.30	197.05 12.30	197.51 12.30

*** NORMAL END OF HEC-1 ***

STORM11

Date: 09-12-2002
Time: 17:22:12

Input File: rem10.inp

Remington 10

Storm Frequency = 2-Year

* * * H Y D R O L O G Y * *

Node to Node	C	Area (Ac)	Slope (%)	Tributary Area (FT)	Length (Min)	TC (Min)	I (In/Hr)	Q(0) (CFS)	TC (Min)	I (In/Hr)	Sum-Q (CFS)	Sum-Q (CFS)	Size	Velocity (Ft/Sec)	Length (FT)	TT (Min)	TT+TC (Min)
200 190	.50	1.19	.00	.0	15.00	3.83	2.30	15.00	3.83	2.30	2.30	2.30	15"	1.87	155.00	1.38	16.38
195 190	.57	.52	.00	.0	15.00	3.83	.60	15.00	3.83	.60	.60	.60	15"	.49	35.00	1.19	16.19
190 180	.57	.97	.00	.0	15.00	3.83	.90	16.38	3.68	.86	3.76	3.76	15"	3.06	240.00	1.31	17.68
185 180	.57	.70	.00	.0	15.00	3.83	.90	15.00	3.83	.90	.90	.90	15"	.73	35.00	.80	15.80
180 140	.57	1.72	.00	.0	15.00	3.83	1.60	17.68	3.54	1.48	6.10	6.10	18"	3.45	135.00	.65	18.34
170 160	.50	.31	.00	.0	15.00	3.83	.60	15.00	3.83	.60	.60	.60	15"	.49	80.00	2.73	17.73
160 150	.50	.47	.00	.0	15.00	3.83	.90	17.73	3.54	.83	1.43	1.43	15"	1.17	240.00	3.43	21.15
150 140	.50	.61	.00	.0	15.00	3.83	1.20	21.15	3.24	1.02	2.45	2.45	18"	1.38	125.00	1.50	22.66
145 140	.57	.11	.00	.0	15.00	3.83	.60	15.00	3.83	.60	.60	.60	18"	.34	35.00	1.72	16.72
140 120	.57	.18	.00	.0	15.00	3.83	1.30	18.34	3.48	1.18	9.83	9.83	24"	3.13	130.00	.69	19.03
130 120	.50	2.84	.00	.0	15.00	3.83	5.40	15.00	3.83	5.40	5.40	5.40	18"	3.06	125.00	.68	15.68
125 120	.57	.11	.00	.0	15.00	3.83	.50	15.00	3.83	.50	.50	.50	18"	.28	35.00	2.06	17.06
120 110	.57	.22	.00	.0	15.00	3.83	1.10	19.03	3.42	.98	16.21	16.21	30"	3.30	195.00	.98	20.01
115 110	.57	.16	.00	.0	15.00	3.83	.70	15.00	3.83	.70	.70	.70	18"	.40	35.00	1.47	16.47
110 100	.57	.34	.00	.0	15.00	3.83	2.50	20.01	3.33	2.18	19.02	19.02	30"	3.88	50.00	.22	20.23

* * * H Y D R A U L I C S * * *

Node	Hyd-Slope (Ft/Ft)	Friction (Ft)	Bend (Ft)	Transition (Ft)	Manhole (Ft)	Deflection (Ft)	Junction (Ft)	Total (Ft)	Hyd-GI Elevation	Desired Elevation	Diff. (Ft)
100	.00000	.0000	.0000	.0000	.0000	.0000	.0000	.0000	202.8000	202.8000	.00
110	.00127	.0636	.0000	.0064	.0000	.4768	.1319	.6787	203.4787	205.5000	2.02
115	.00003	.0009	.0000	.0000	.0000	.0000	.0000	.0009	203.4796	205.5000	2.02
120	.00092	.1802	.0000	.0017	.0000	.3419	.0526	.5764	204.0551	207.1000	3.04
125	.00001	.0005	.0000	.0000	.0000	.0000	.0000	.0005	204.0556	207.1000	3.04
130	.00156	.1955	.0000	.0000	.0000	.0000	.0000	.1955	204.2506	209.6000	5.35
140	.00112	.1453	.0000	.0065	.0000	.4633	.0954	.7105	204.7655	208.2000	3.43
145	.00002	.0007	.0000	.0000	.0000	.0000	.0000	.0007	204.7662	208.2000	3.43
150	.00032	.0401	.0000	.0009	.0000	.0028	.0372	.0811	204.8466	206.1000	1.25
160	.00029	.0698	.0000	.0017	.0000	.0005	.0358	.1078	204.9545	207.3000	2.35
170	.00005	.0041	.0000	.0000	.0000	.0000	.0000	.0041	204.9585	209.1000	4.14
180	.00199	.2690	.0000	.0039	.0000	.3279	.1941	.7949	205.5605	209.5000	3.94
185	.00011	.0040	.0000	.0000	.0000	.0000	.0000	.0040	205.5645	209.5000	3.94
190	.00201	.4814	.0000	.0091	.0000	.1368	.1834	.8107	206.3712	211.4000	5.03
195	.00005	.0018	.0000	.0000	.0000	.0000	.0000	.0018	206.3730	211.4000	5.03
200	.00075	.1163	.0000	.0000	.0000	.0000	.0000	.1163	206.4874	208.3000	1.81

Date: 09-12-2002
Time: 17:29:41

STORM11

Input File: rem12.inp
**Analysis with 100-yr flow to node 130

Storm Frequency = 2-Year

Remington 12

* * * H Y D R O L O G Y * * *

Node to Node	C	Area (AC)	Slope (%)	Length (FT)	TC (Min)	I (In/Hr)	Q(0) (CFS)	TC (Min)	I (In/Hr)	Q Sum (CFS)	Sum Q (CFS)	Conduit Size	Velocity (Ft/Sec)	Length (FT)	TT (Min)	TT+TC (Min)
200 190	.50	1.19	.00	.0	15.00	3.83	2.30	15.00	3.83	2.30	2.30	15"	1.87	155.00	1.38	16.38
195 190	.57	.52	.00	.0	15.00	3.83	.60	15.00	3.83	.60	.60	15"	.49	35.00	1.19	16.19
190 180	.57	.97	.00	.0	15.00	3.83	.90	16.38	3.68	.86	3.76	15"	3.06	240.00	1.31	17.68
185 180	.57	.70	.00	.0	15.00	3.83	.90	15.00	3.83	.90	.90	15"	.73	35.00	.80	15.80
180 140	.57	1.72	.00	.0	15.00	3.83	1.60	17.68	3.54	1.48	6.10	18"	3.45	135.00	.65	18.34
170 160	.50	.31	.00	.0	15.00	3.83	.60	15.00	3.83	.60	.60	15"	.49	80.00	2.73	17.73
160 150	.50	.47	.00	.0	15.00	3.83	.90	17.73	3.54	.83	1.43	15"	1.17	240.00	3.43	21.15
150 140	.50	.61	.00	.0	15.00	3.83	1.20	21.15	3.24	1.02	2.45	18"	1.38	125.00	1.50	22.66
145 140	.57	.11	.00	.0	15.00	3.83	.60	15.00	3.83	.60	.60	18"	.34	35.00	1.72	16.72
140 120	.57	.18	.00	.0	15.00	3.83	1.30	18.34	3.48	1.18	9.83	24"	3.13	130.00	.69	19.03
130 120	.50	2.84	.00	.0	15.00	3.83	16.00	15.00	3.83	16.00	16.00	18"	9.05	125.00	.23	15.23
125 120	.57	.11	.00	.0	15.00	3.83	.50	15.00	3.83	.50	.50	18"	.28	35.00	2.06	17.06
120 110	.57	.22	.00	.0	15.00	3.83	1.10	19.03	3.42	.98	25.67	30"	5.23	195.00	.62	19.65
115 110	.57	.16	.00	.0	15.00	3.83	.70	15.00	3.83	.70	.70	18"	.40	35.00	1.47	16.47
110 100	.57	.34	.00	.0	15.00	3.83	2.50	19.65	3.36	2.20	28.51	30"	5.81	50.00	.14	19.79

Input File: rem12.inp
**Analysis with 100-yr flow to node 130

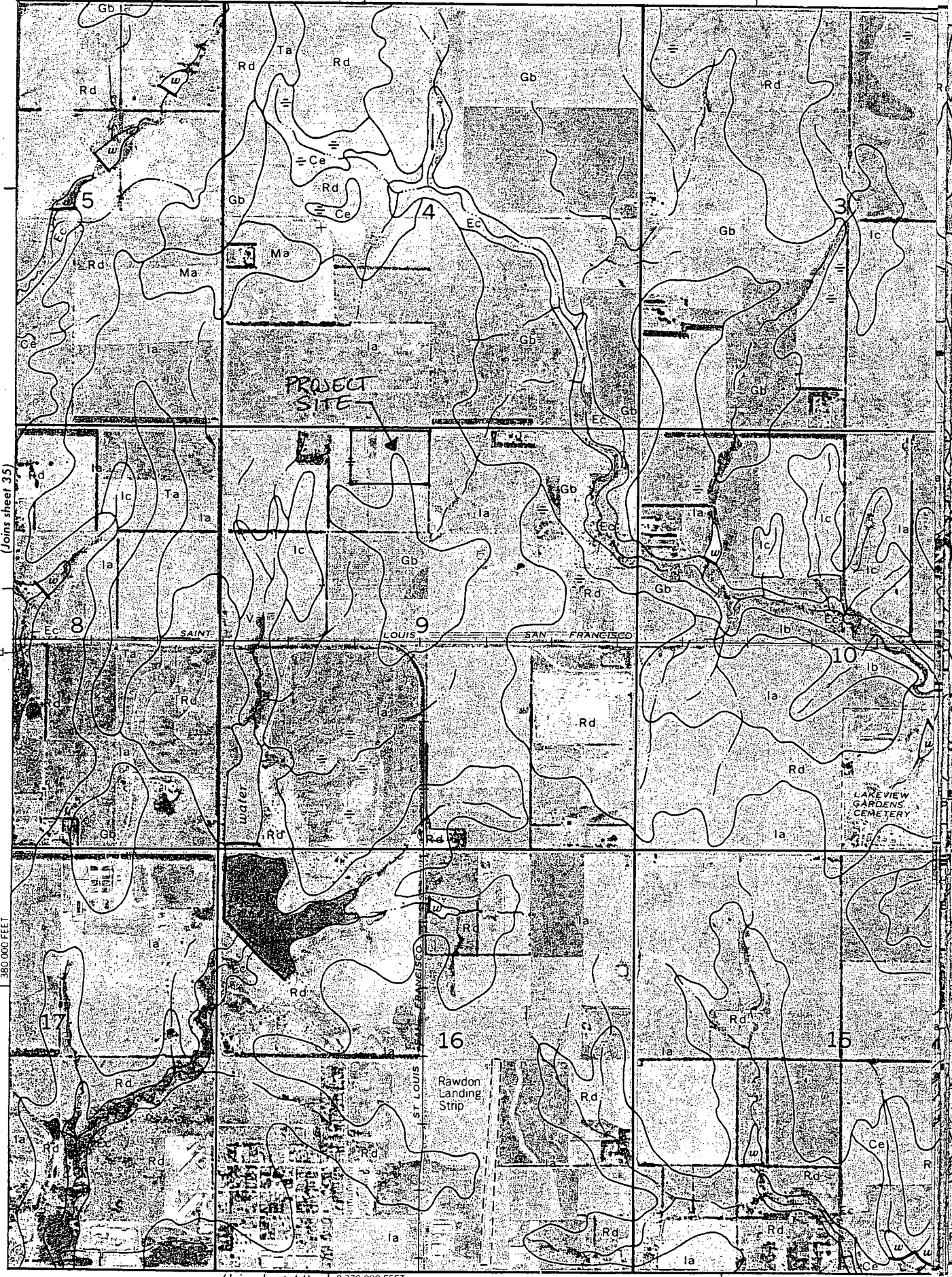
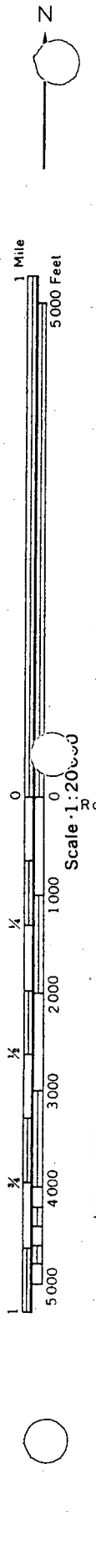
Remington 12

Storm Frequency = 2-Year

* * * H Y D R A U L I C S * * *

Node	Hyd-Slope (Ft/Ft)	Friction (Ft)	Bend (Ft)	Transition (Ft)	Manhole (Ft)	Deflection (Ft)	Junction (Ft)	Total (Ft)	Hyd-GI Elevation	Desired Elevation	Diff.
100	.00000	.0000	.0000	.0000	.0000	.0000	.0000	.0000	202.8000	202.8000	.00
110	.00286	.1430	.0000	.0099	.0000	1.1962	.2101	1.5591	204.3591	205.5000	1.14
115	.00003	.0009	.0006	.0000	.0000	.0000	.0000	.0016	204.3606	205.5000	1.14
120	.00232	.4521	.0000	.1696	.0000	.0112	-.2625	.3704	204.7294	207.1000	2.37
125	.00001	.0005	.0000	.0000	.0000	.0000	.0000	.0005	204.7299	207.1000	2.37
130	.01373	1.7160	.0000	.0000	.0000	.0000	.0000	1.7160	206.4455	209.6000	3.15
140	.00112	.1453	.0000	.0065	.0000	.4633	.0954	.7105	205.4399	208.2000	2.76
145	.00002	.0007	.0000	.0000	.0000	.0000	.0000	.0007	205.4406	208.2000	2.76
150	.00032	.0401	.0000	.0009	.0000	.0028	.0372	.0811	205.5210	206.1000	.58
160	.00029	.0698	.0000	.0017	.0000	.0005	.0358	.1078	205.6288	207.3000	1.67
170	.00005	.0041	.0000	.0000	.0000	.0000	.0000	.0041	205.6329	209.1000	3.47
180	.00199	.2690	.0000	.0039	.0000	.3279	.1941	.7949	206.2348	209.5000	3.27
185	.00011	.0040	.0000	.0000	.0000	.0000	.0000	.0040	206.2388	209.5000	3.26
190	.00201	.4814	.0000	.0091	.0000	.1368	.1834	.8107	207.0455	211.4000	4.35
195	.00005	.0018	.0000	.0000	.0000	.0000	.0000	.0018	207.0473	211.4000	4.35
200	.00075	.1163	.0000	.0000	.0000	.0000	.0000	.1163	207.1618	208.3000	1.14

(Joins sheet 28)



(Joins sheet 44) 1 2 370 000 FEET

SOIL LEGEND

SYMBOL	NAME
Aa	Albion-Shellabarger sandy loams, 1 to 4 percent slopes
Ab	Albion and Shellabarger sandy loams, 7 to 15 percent slopes
Ba	Blanket silt loam, 0 to 1 percent slopes
Bb	Blanket silt loam, 1 to 3 percent slopes
Ca	Canadian fine sandy loam
Cb	Canadian-Waldeck fine sandy loams
Cc	Carwile fine sandy loam
Cd	Clark-Ost clay loams, 1 to 4 percent slopes
Ce	Clime silty clay, 3 to 6 percent slopes
Ea	Elandco silt loam
Eb	Elandco silt loam, occasionally flooded
Ec	Elandco silt loam, frequently flooded
Fa	Farnum loam, 0 to 1 percent slopes
Fb	Farnum loam, 1 to 3 percent slopes
Fc	Farnum loam, sandy substratum, 0 to 1 percent slopes
Ga	Goessel silty clay, 0 to 1 percent slopes
Gb	Goessel silty clay, 1 to 2 percent slopes
Ia	Irwin silty clay loam, 1 to 3 percent slopes
Ib	Irwin silty clay loam, 3 to 6 percent slopes
Ic	Irwin silty clay loam, 2 to 6 percent slopes, eroded
La	Lesho loam
Lb	Lincoln soils
Ma	Milan loam, 1 to 3 percent slopes
Mb	Milan loam, 3 to 6 percent slopes
Mc	Milan clay loam, 2 to 6 percent slopes, eroded
Na	Naron fine sandy loam
Oc	Owens clay loam, 1 to 3 percent slopes
Od	Owens-Rock outcrop complex, 3 to 10 percent slopes
Pa	Pits
Pb	Plevna fine sandy loam
Pc	Pratt loamy fine sand, undulating
Pd	Pratt-Tivoli complex, rolling
Ra	Renfrow silty clay loam, 1 to 3 percent slopes
Rb	Renfrow silty clay loam, 3 to 6 percent slopes
Rc	Renfrow-Owens clay loams, 1 to 4 percent slopes
Rd	Rosehill silty clay, 1 to 3 percent slopes
Sa	Shellabarger sandy loam, 1 to 3 percent slopes
Sb	Shellabarger sandy loam, 3 to 6 percent slopes
Sc	Shellabarger sandy loam, 3 to 6 percent slopes, eroded
Ta	Tabler silty clay loam
Tb	Tabler-Drummond complex
Ua	Urban land-Canadian complex
Ub	Urban land-Elandco complex
Uc	Urban land-Farnum complex, 0 to 3 percent slopes
Ud	Urban land-Irwin complex, 1 to 3 percent slopes
Ue	Urban land-Tabler complex
Va	Vanoss silt loam, 0 to 1 percent slopes
Vb	Vanoss silt loam, 1 to 3 percent slopes
Vc	Vanoss silt loam, 3 to 6 percent slopes
Vd	Vanoss silt loam, 3 to 6 percent slopes, eroded
Ve	Vernon sandy loam, 1 to 3 percent slopes
Vf	Vernon sandy loam, 3 to 6 percent slopes
Wa	Waldeck sandy loam
Wb	Waurika silt loam

KS-2-5

County	Expected 24-hour Storm Rainfall in Inches						Normal Annual Precipitation Inches
	Storm Frequency in Years						
	100	50	25	10	5	2	
Pawnee	6.6	6.0	5.2	4.5	3.7	2.8	23.3
Phillips	6.0	5.5	4.8	4.1	3.4	2.5	23.6
Pottawatomie	7.5	6.6	5.9	5.1	4.3	3.4	33.6
Pratt	7.2	6.4	5.6	4.8	4.1	3.0	24.6
Rawlins	5.5	5.0	4.3	3.6	3.1	2.3	21.0
Reno	7.4	6.6	5.8	5.0	4.2	3.2	27.7
Republic	6.8	6.0	5.4	4.6	3.9	2.9	28.6
Rice	7.3	6.4	5.6	4.8	4.1	3.0	26.6
Riley	7.4	6.5	5.8	5.1	4.3	3.3	33.5
Rooks	6.1	5.7	4.9	4.1	3.4	2.5	23.9
Rush	6.5	5.9	5.0	4.3	3.6	2.7	23.3
Russell	6.7	5.9	5.2	4.4	3.7	2.8	26.8
Saline	7.3	6.4	5.7	4.9	4.1	3.1	28.4
Scott	5.7	5.3	4.5	3.8	3.2	2.4	20.2
Sedgwick	7.8	7.0	6.1	5.3	4.5	3.5	30.6
Seward	6.0	5.7	4.8	4.2	3.5	2.6	19.8
Shawnee	7.8	6.8	6.1	5.3	4.5	3.5	34.7
Sheridan	5.7	5.3	4.5	3.8	3.2	2.4	21.3
Sherman	5.3	4.8	4.2	3.5	3.0	2.2	16.7
Smith	6.3	5.7	5.0	4.2	3.5	2.6	24.4
Stafford	7.1	6.2	5.5	4.7	4.0	2.9	25.1
Stanton	5.6	5.2	4.5	3.8	3.2	2.4	15.8
Stevens	5.9	5.5	4.7	4.1	3.4	2.5	19.7
Sumner	8.0	7.1	6.2	5.4	4.6	3.6	34.0

ATTACHMENT D

(3 pages)

DRAINAGE CRITERIA

CITY OF WICHITA, KANSAS

RECOMMENDED RUNOFF COEFFICIENTS FOR RATIONAL METHOD
AND PERCENT IMPERVIOUS FOR UNIT HYDROGRAPH METHOD

Land Use or Surface Characteristics	Percent Impervious	Frequency			
		<u>2</u>	<u>5</u>	<u>10</u>	<u>100</u>
1. Business:					
Downtown Areas	95	0.84	0.85	0.87	0.91
Neighborhood Areas	70	0.68	0.69	0.73	0.80
2. Residential:					
<u>Single Family (Soil Group D)</u>					
1/8 Acre	50	0.57	0.61	0.66	0.79
1/4 Acre	38	0.50	0.54	0.62	0.76
1/3 Acre	30	0.46	0.50	0.59	0.73
1/2 Acre	25	0.42	0.48	0.56	0.72
3/4 Acre	22	0.42	0.46	0.55	0.71
1 Acre	20	0.41	0.45	0.54	0.71
<u>Multi-Family (Soil Group D)</u>					
Multi-Unit (detached)	60	0.62	0.66	0.72	0.82
Multi-Unit (attached)	65	0.64	0.68	0.73	0.83
Apartments	75	0.70	0.73	0.79	0.86
<u>Single Family (Soil Group C)</u>					
1/8 Acre	50	0.55	0.58	0.64	0.73
1/4 Acre	38	0.48	0.51	0.57	0.68
1/3 Acre	30	0.43	0.46	0.53	0.65
1/2 Acre	25	0.40	0.43	0.50	0.63
3/4 Acre	22	0.39	0.42	0.49	0.62
1 Acre	20	0.37	0.40	0.48	0.61
<u>Multi-Family (Soil Group C)</u>					
Multi-Unit (detached)	60	0.60	0.63	0.69	0.77
Multi-Unit (attached)	65	0.63	0.66	0.71	0.79
Apartments	75	0.68	0.72	0.77	0.83
<u>Single-Family (Soil Group B)</u>					
1/8 Acre	50	0.52	0.54	0.59	0.67
1/4 Acre	38	0.44	0.46	0.52	0.61
1/3 Acre	30	0.39	0.41	0.47	0.57
1/2 Acre	25	0.36	0.38	0.44	0.54
3/4 Acre	22	0.34	0.36	0.42	0.52
1 Acre	20	0.33	0.35	0.40	0.51
<u>Multi-Family (Soil Group B)</u>					
Multi-Unit (detached)	60	0.58	0.60	0.65	0.72
Multi-Unit (attached)	65	0.61	0.64	0.68	0.75
Apartments	75	0.67	0.70	0.74	0.80

Land Use or Surface Characteristics	Percent Impervious	Frequency				
		2	5	10	25	100
<u>Single Family (Soil Group A)</u>						
1/8 Acre	50	0.47	0.50	0.54		0.60
1/4 Acre	38	0.39	0.41	0.45		0.52
1/3 Acre	30	0.33	0.35	0.39		0.47
1/2 Acre	25	0.30	0.31	0.35		0.44
3/4 Acre	22	0.28	0.29	0.33		0.42
1 Acre	20	0.26	0.28	0.32		0.40
<u>Multi-Family (Soil Group A)</u>						
Multi-Unit (detached)	60	0.55	0.57	0.61		0.67
Multi-Unit (attached)	65	0.58	0.60	0.64		0.70
Apartments	75	0.65	0.68	0.72		0.77
3. Industrial:						
Light Areas	70	0.68	0.69	0.73		0.80
Heavy Areas	80	0.74	0.76	0.79		0.84
4. Playgrounds:	15	0.33	0.35	0.42		0.55
Schools:	40	0.49	0.51	0.56		0.66
Railroad Yard Areas:	30	0.43	0.45	0.50		0.62
7. Undeveloped Urban Areas:						
Offsite Flow Analysis (when land use not defined)	45	0.52	0.54	0.59		0.68
8. Streets:						
Paved	99	0.87	0.88	0.90		0.93
Gravel	00	0.24	0.26	0.33		0.48
9. Drive, Parking Lots and Walks:	96	0.87	0.87	0.88		0.89
10. Roofs:	90	0.80	0.85	0.90		0.93
11. Urban Lawn Areas (See Note No. 1 below):						
<u>Soil Group A</u>						
Slope less than 1%	00	0.08	0.09	0.13		0.23
Slope 1% to 4%	00	0.12	0.13	0.17		0.27
Slope more than 4%	00	0.16	0.17	0.21		0.31
<u>Soil Group B</u>						
Slope less than 1%	00	0.16	0.26	0.18		0.37
Slope 1% to 4%	00	0.20	0.22	0.28		0.41
Slope more than 4%	00	0.24	0.26	0.32		0.45
<u>Soil Group C</u>						
Slope less than 1%	00	0.24	0.27	0.35		0.51
Slope 1% to 4%	00	0.26	0.29	0.37	0.40	0.53
Slope more than 4%	00	0.28	0.31	0.39		0.55

<u>Land Use or Surface Characteristics</u>	<u>Percent Impervious</u>	<u>Frequency</u>			
		<u>2</u>	<u>5</u>	<u>10</u>	<u>100</u>
<u>Soil Group D</u>					
Slope less than 1%	00	0.28	0.33	0.43	0.63
Slope 1% to 4%	00	0.30	0.35	0.45	0.65
Slope more than 4%	00	0.32	0.37	0.47	0.67

Note No. 1: Coefficients shown in the above table are for pervious open space areas with thick turf which includes pervious areas in parks and cemeteries. Coefficients shown above must be increased 0.02 for use with agricultural pasture areas. Coefficients shown above must be reduced by 0.04 for use with agricultural cultivated areas. Group A soils are well-drained, coarse textured sands with high infiltration rates. Group B soils are moderately well-drained, moderately coarse textured soils with moderate infiltration rates. Group C soils are moderately poor-drained, moderately fine textured soils with slow infiltration rates. Group D soils are poor-drained, fine textured soils with very slow infiltration rates.

GENERAL NOTE: These Rational Formula Coefficients may not be valid for large basins.

RAINFALL INTENSITIES

SEDGWICK COUNTY KANSAS (revised June 1997)

This table contains average rainfall intensities in inches per hour.

DURATION, HR:MIN	RETURN PERIOD						
	1 YR	2 YR	5 YR	10 YR	25 YR	50 YR	100 YR
0:05	4.91	5.64	6.64	7.38	8.48	9.34	10.20
0:06	4.62	5.34	6.33	7.07	8.15	9.00	9.84
0:07	4.38	5.09	6.08	6.80	7.86	8.69	9.52
0:08	4.17	4.87	5.85	6.56	7.60	8.41	9.22
0:09	4.00	4.68	5.63	6.33	7.34	8.14	8.93
0:10	3.84	4.50	5.43	6.11	7.10	7.87	8.64
0:11	3.70	4.34	5.25	5.90	6.86	7.61	8.36
0:12	3.56	4.19	5.07	5.71	6.64	7.36	8.09
0:13	3.44	4.05	4.91	5.53	6.43	7.14	7.84
0:14	3.33	3.92	4.76	5.36	6.24	6.92	7.61
0:15	3.22	3.80	4.62	5.21	6.06	6.73	7.40
0:16	3.12	3.69	4.49	5.07	5.91	6.56	7.21
0:17	3.03	3.58	4.37	4.94	5.76	6.40	7.04
0:18	2.94	3.48	4.26	4.82	5.63	6.26	6.88
0:19	2.85	3.39	4.16	4.71	5.50	6.12	6.74
0:20	2.77	3.30	4.06	4.60	5.38	5.99	6.60
0:21	2.70	3.22	3.97	4.50	5.27	5.87	6.47
0:22	2.63	3.14	3.88	4.41	5.17	5.76	6.35
0:23	2.56	3.07	3.80	4.32	5.07	5.65	6.23
0:24	2.50	3.00	3.72	4.23	4.97	5.54	6.12
0:25	2.44	2.93	3.64	4.15	4.88	5.44	6.01
0:26	2.38	2.87	3.57	4.07	4.79	5.35	5.90
0:27	2.33	2.81	3.50	4.00	4.70	5.26	5.80
0:28	2.27	2.75	3.44	3.92	4.62	5.17	5.71
0:29	2.23	2.69	3.37	3.86	4.54	5.08	5.61
0:30	2.18	2.64	3.31	3.79	4.47	4.99	5.52
0:31	2.14	2.59	3.26	3.72	4.39	4.91	5.43
0:32	2.09	2.54	3.20	3.66	4.32	4.83	5.34
0:33	2.05	2.50	3.14	3.60	4.25	4.76	5.26
0:34	2.02	2.45	3.09	3.54	4.18	4.68	5.18
0:35	1.98	2.41	3.04	3.48	4.12	4.61	5.10
0:36	1.94	2.37	2.99	3.43	4.05	4.54	5.02
0:37	1.91	2.33	2.94	3.38	3.99	4.47	4.95
0:38	1.88	2.29	2.90	3.32	3.93	4.40	4.87
0:39	1.85	2.25	2.85	3.27	3.87	4.34	4.80
0:40	1.82	2.22	2.81	3.23	3.82	4.28	4.73
0:41	1.79	2.18	2.77	3.18	3.76	4.22	4.67
0:42	1.76	2.15	2.73	3.13	3.71	4.16	4.60
0:43	1.73	2.12	2.69	3.09	3.66	4.10	4.54
0:44	1.71	2.09	2.65	3.05	3.61	4.04	4.48
0:45	1.68	2.06	2.62	3.01	3.56	3.99	4.42
0:46	1.66	2.03	2.58	2.96	3.51	3.94	4.36
0:47	1.63	2.00	2.55	2.93	3.47	3.89	4.30
0:48	1.61	1.97	2.51	2.89	3.42	3.84	4.25
0:49	1.59	1.95	2.48	2.85	3.38	3.79	4.20
0:50	1.57	1.92	2.45	2.81	3.34	3.74	4.15

RAINFALL INTENSITY TABLE

SEDGWICK COUNTY KANSAS (revised June 1997)

This table contains average rainfall intensities in inches per hour.

DURATION, HR:MIN	RETURN PERIOD						
	1 YR	2 YR	5 YR	10 YR	25 YR	50 YR	100 YR
0:51	1.55	1.90	2.42	2.78	3.30	3.70	4.10
0:52	1.53	1.87	2.39	2.75	3.26	3.65	4.05
0:53	1.51	1.85	2.36	2.71	3.22	3.61	4.00
0:54	1.49	1.83	2.33	2.68	3.18	3.57	3.95
0:55	1.47	1.80	2.30	2.65	3.14	3.53	3.91
0:56	1.45	1.78	2.28	2.62	3.11	3.49	3.86
0:57	1.43	1.76	2.25	2.59	3.07	3.45	3.82
0:58	1.41	1.74	2.22	2.56	3.04	3.41	3.78
0:59	1.40	1.72	2.20	2.53	3.01	3.37	3.74
1:00	1.38	1.70	2.17	2.50	2.97	3.34	3.70
1:05	1.30	1.61	2.06	2.38	2.82	3.17	3.52
1:10	1.23	1.53	1.96	2.26	2.69	3.02	3.35
1:15	1.17	1.45	1.87	2.16	2.57	2.89	3.20
1:20	1.11	1.38	1.79	2.06	2.46	2.77	3.07
1:25	1.06	1.32	1.71	1.98	2.36	2.65	2.95
1:30	1.01	1.27	1.64	1.90	2.27	2.55	2.83
1:35	0.97	1.21	1.58	1.83	2.18	2.46	2.73
1:40	0.93	1.16	1.52	1.76	2.10	2.37	2.63
1:45	0.89	1.12	1.46	1.70	2.03	2.29	2.54
1:50	0.86	1.08	1.41	1.64	1.96	2.21	2.46
1:55	0.82	1.04	1.36	1.58	1.89	2.13	2.38
2:00	0.79	1.00	1.31	1.53	1.83	2.07	2.30
2:05	0.76	0.97	1.27	1.48	1.77	2.00	2.23
2:10	0.74	0.93	1.23	1.43	1.72	1.94	2.16
2:15	0.71	0.90	1.19	1.39	1.67	1.88	2.10
2:20	0.69	0.87	1.15	1.35	1.62	1.83	2.04
2:25	0.66	0.85	1.12	1.31	1.57	1.78	1.98
2:30	0.64	0.82	1.09	1.27	1.53	1.73	1.93
2:35	0.62	0.80	1.06	1.24	1.49	1.68	1.88
2:40	0.61	0.78	1.03	1.21	1.45	1.64	1.83
2:45	0.59	0.75	1.01	1.18	1.42	1.60	1.79
2:50	0.57	0.74	0.98	1.15	1.38	1.56	1.74
2:55	0.56	0.72	0.96	1.12	1.35	1.53	1.70
3:00	0.55	0.70	0.94	1.10	1.32	1.49	1.67
3:15	0.51	0.66	0.88	1.03	1.24	1.40	1.57
3:30	0.48	0.62	0.83	0.97	1.17	1.32	1.48
3:45	0.45	0.59	0.78	0.92	1.11	1.26	1.40
4:00	0.43	0.56	0.75	0.88	1.06	1.20	1.34
4:15	0.41	0.53	0.71	0.84	1.01	1.14	1.28
4:30	0.40	0.51	0.68	0.80	0.97	1.10	1.22
4:45	0.38	0.49	0.66	0.77	0.93	1.05	1.17
5:00	0.37	0.47	0.63	0.74	0.89	1.01	1.13
5:15	0.36	0.46	0.61	0.72	0.86	0.98	1.09
5:30	0.35	0.44	0.59	0.69	0.83	0.94	1.05
5:45	0.34	0.43	0.57	0.67	0.81	0.91	1.02
6:00	0.33	0.42	0.55	0.65	0.78	0.88	0.98

@ L=5' : P=5+1.8(2')=8.6

@ L=10' : P=10'+1.8(2)=13.6

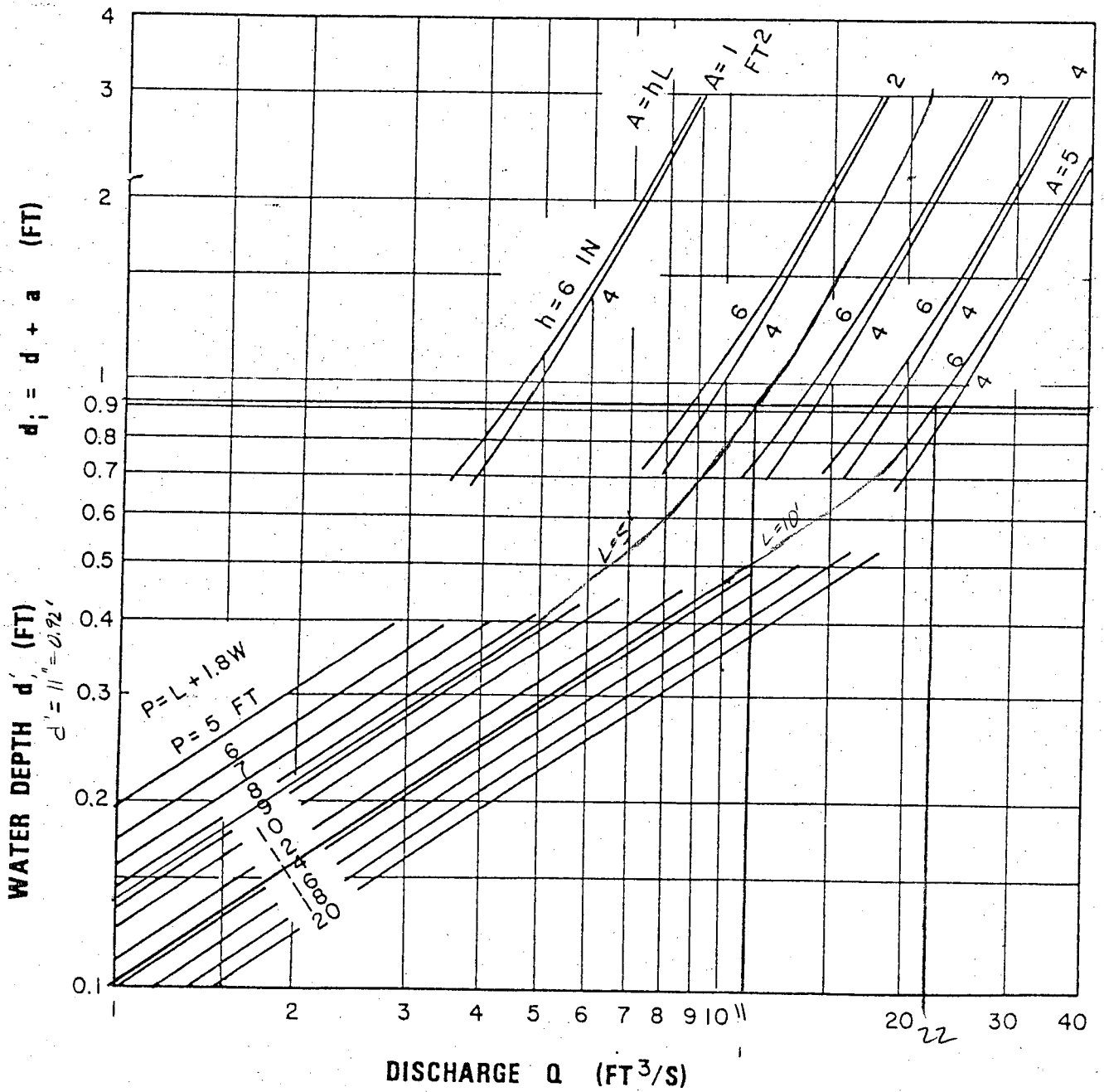
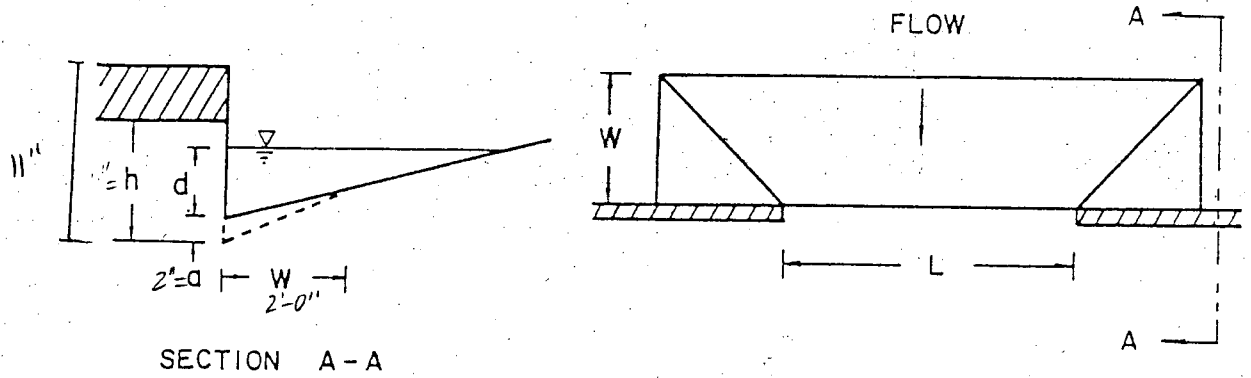


CHART 12. Depressed curb-opening inlet capacity in sump locations.



303 S. TOPEKA - WICHITA, KANSAS 67202

Project _____

Date _____

316-262-2691 - FAX 316-262-3003

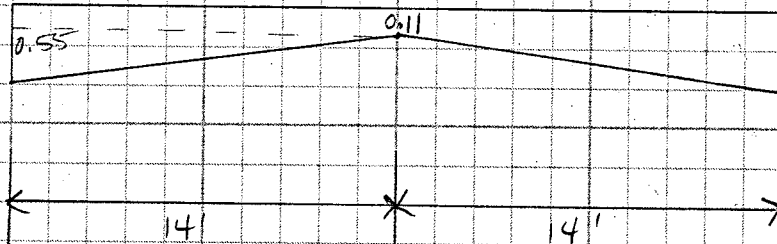
Item _____

By _____

www.pec1.com - designers@pec1.com

DETERMINE CAPACITIES OF STANDARD CURB STREETS
(32' R-O-W)

* ASSUME FLOW CARRIED BY STREET ONLY



$$n = \frac{(2 \times 2.55 \times 0.013) + (2 \times 12 \times 0.016)}{29.1} = 0.01547$$

$$A = (2 \times \frac{1}{2} \times 14 \times 0.44) + (0.11 \times 28) = 9.24 \text{ SF}$$

$$P = 29.1$$

$$R = \frac{A}{P} = \frac{9.24}{29.1} = 0.318$$

$$Q = \frac{1.486}{n} A R^{2/3} S^{1/2}$$

$$Q = \frac{1.486}{0.01547} (9.24)(0.318)^{2/3} (S)^{1/2}$$

$$Q = 413.5 \sqrt{S}$$