



Prairie Pointe **Wichita, Sedgwick County, Kansas**

4/28/03

Prairie Pointe is a residential development in northwest Wichita. Development consists of single-family, ¼ acre lots, utilities, and two ponds. The drainage plan and supporting calculations for Prairie Pointe are presented herein.

Hydrology

The proposed plat lies in the S ½, SE ¼, Section 30, T26S, R1W of the 6th P.M. The soils on-site consist of Vanoss silt loam, Farnum loam, Milan loam (all hydrologic group B), Blanket silt loam (hydrologic group C), Waurika silt loam, and Carwile fine sandy loam (both hydrologic group D). The existing landscape is vacant pasture save an existing house at the south end of the site whose lot is lined with trees. The plat generally drains to the south end.

This hydrologic study analyzes the Prairie Pointe site along with the land between it and Maize Road. This additional area is planned for future commercial use. For runoff calculations under existing conditions, the site plus the additional area was divided into 3 major basins, each with its own discharge. The site also accepts runoff from approximately 116 acres to the north. (See existing conditions calculations.)

Under developed conditions, Basin 1 and the minor storm runoff from offsite will drain to Pond 1. Note that the inlets in the back of the lots at the north end of the site are designed to handle the 2-year storm runoff from the offsite basin and then discharge to Pond 1. The backs of the lots are graded to have a 0.3% slope from high point to high point in order to carry overflow to Pond 2. Pond 2 is designed to accept overflow from the offsite basin, Basin 2 runoff, and future developed conditions runoff from the commercial area. Pond 1 discharges to Pond 2, and Pond 2 discharges to 37th Street North via a weir. (See calculations.)

Using the Army Corp of Engineer's program HEC-1, all systems were modeled with runoff based on the Rational Method. The minimum time of concentration was assumed for all basins, so the basins could be combined with negligible lag

time. The ponds were included to determine water elevations in the 100-year design storm and to determine the outfall from the ponds via weirs. A 2-year storm model of the system is enclosed which shows the minor storm runoff from offsite draining to Pond 1. A 100-year storm model of the system is also enclosed, and it shows the overflow from the offsite basin draining to pond 2. The pond elevations in the 100-year design storm eventually equalize and reach maximum stage at 1357.9.

Runoff coefficients were estimated based on existing land use and the tables presented in the Design Aids section. A map showing the basin boundaries, drainage calculations, and HEC-1 model are included. The analysis made is based on the available site data which includes the following: 1"=100' topographic map with 1' contours of the site and adjacent areas, USGS topographic map, Sedgwick County Soil Survey Map, and references noted herein.

Storm Sewer Design

For the storm sewer hydrologic analysis, the Rational Method was again used. Runoff coefficients were estimated using the charts in the design aids section of this report. For this development, a uniform assumption of the minimum time of concentration of 15 minutes was deemed appropriate. Travel time for flow through defined channels, pipes, etc, for these basins was estimated on the basis of Manning's Equation.

In the hydraulic analysis, the storm sewers are designed for the minor storm, with major storm overflows to be routed through easements and rights-of-way to an appropriate outlet. The minor storm has a recurrence interval of two years. The major storm evaluated has a recurrence interval of one hundred years. To simplify this analysis, the time of concentration is identical for both the major and the minor storms.

For each inlet, street flooding and inlet capacity were checked for the minor storm. Conveyance in the street is based on the Modified Manning's Equation, as expressed in the Design of Urban Highway Drainage-The State of the Art, Equation (5-1), page 5-9. It has been assumed that T_c for street flow is equal to T_c for pipe flow. This is a simplifying, but conservative, assumption, since pipe flow velocities generally exceed street flow velocities.

Inlet capacities were determined by the methods described in Drainage of Highway Pavements, Hydraulic Engineering Circular #12, using Chart #12 as found in the Design Aids section. City of Wichita Type 1A inlets and 3/8 inch per foot cross slopes have been assumed. Streets have been assumed to have 6-5/8 inch standard curb, unless otherwise noted.

Hydraulic computation for the pipe system was performed using PEC's STORM computer program. This program uses Manning's Equation to calculate friction losses for pipes flowing full. Minor losses are computed by momentum principles at each structure. All pipe area is assumed to be reinforced concrete with a Manning's "n" of 0.013. It is desirable to keep the hydraulic grade line at least one foot below the top of curb for the minor storm. The STORM analyses for the storm sewer systems are included in this report. Note that the inlets in the back of the lots at the north end of the site are designed to handle the 2-year storm runoff from the offsite basin and then discharge to Pond 1. The backs of the lots are graded to have a 0.3% slope from high point to high point in order to carry overflow to Pond 2. See Plan Map.

Design Aids

This section includes material used to assist in designing the drainage system. A 1"=100' scale drainage plan map is enclosed in the pocket.

References

Design of Urban Highway Drainage – The State of the Art, by Reitz & Jens, Inc., April 1980.

Drainage of Highway Pavements, Hydraulic Engineering Circular #12, by Tye Engineering, Inc., March 1984.

Interim Drainage and Storm Sewer Policy for Design Criteria and Documentation, City of Wichita, Kansas, 1985.

Soil Survey of Sedgwick County, Kansas, US Department of Agriculture, Soil Conservation Service, 1979.

Prairie Pointe

Existing Conditions Hydrology

Rational Method, $Q=ciA$

Offsite Basin to the North

Runoff Coefficients

Agricultural pasture areas, $S < 1\%$

	Gr. B	Gr. D
$c_2 =$	0.28	0.30
$c_{100} =$	0.39	0.65

Intensity

Velocity: Attachment E. Short grass pasture or lawns @ $S=0.3\%$

$Vel=0.38$ f/s

$L=3075'$

$$T_c = \frac{3075'}{0.38f} \left| \frac{\text{sec}}{60 \text{ sec}} \right| \left| \frac{1 \text{ min}}{60 \text{ sec}} \right| = 135 \text{ MIN}$$

$T_c = 2:15$

$i_2 = 0.90$ in/hr

$i_{100} = 2.10$ in/hr

Basin	Soil Group	Area (Ac.)	Total Area	c_2	c_{100}	Q_2	Q_{100}
offsite	B	94.7	116	0.28	0.44	29.2	107.2
	D	21.3					

Results

The runoff from offsite enters the from the north and is carried through the site to 37th Street North at the south end of the site.

Site Analysis

*The Prairie Pointe site combined with the area to the east between the site and Maize Road was divided into three existing conditions basins (Basins 1-3) for analysis.

Runoff Coefficients

Agricultural pasture areas, $S < 1\%$

	Gr. B	Gr. C	Gr. D
$c_2 =$	0.28	0.26	0.30
$c_{100} =$	0.39	0.53	0.65

Intensity

Velocity: Attachment E. Short grass pasture or lawns

Basin	L (ft)	S (%)	Vel (f/s)	T _c (hr:min)	i ₂ (in/hr)	i ₁₀₀ (in/hr)
1	2440	0.25	0.35	1:55	1.04	2.38
2	1135	0.62	0.54	0:35	2.41	5.1
3	1275	0.63	0.55	0:39	2.25	4.8

Sample Calculation

Vel=0.35 f/s

L=2440'

$$T_c = \frac{2440'}{0.35f} \left| \frac{\text{sec}}{60 \text{ sec}} \right| 1 \text{ min} = 116 \text{ MIN}$$

Basin	Soil Group	Area (Ac.)	Total Area	c ₂	c ₁₀₀	Q ₂	Q ₁₀₀
1	B	15.1	41.6	0.27	0.48	11.7	47.5
	C	25.6					
	D	0.9					
2	B	11.5	18.1	0.27	0.44	11.8	40.6
	C	6.6					
3	B	8.5	17.2	0.29	0.52	11.2	42.9
	D	8.7					

Results

Basin 1 runoff discharges to the southeast corner of the site by the intersection of 37th Street North and Maize Road. Basin 2 discharges to the south end of the site to 37th Street. Basin 3 runoff flows to a depression at the southwest end of the site then overflows to the 37th Street ditch.

Runoff from Basin 1 and Basin 2 flows east along 37th Street to Maize Road.

$$Q_{100\text{exist}} = 47.5 \text{ cfs} + 40.6 \text{ cfs} = 88.1 \text{ cfs}$$

Runoff from Basin 3 flows west along 37th Street and enters a swale that runs along the west end of the site and continues south.

$$Q_{100\text{exist}} = 42.9 \text{ cfs}$$

Basin north of site draining to Maize Road culverts at the 37th Street intersection
(runoff does not pass through site.)

Runoff Coefficients

Agricultural pasture areas, S<1%

Gr. B

$$c_2 = 0.28$$

$$c_{100} = 0.39$$

Intensity

Velocity: Attachment E. Short grass pasture or lawns @ S=0.3%

Vel=0.38 f/s

L=2960'

$$T_c = \frac{2960'}{0.38f} \text{ sec} \quad \left| \quad \frac{1 \text{ min} = 60 \text{ sec}}{60} \right| \quad 130 \text{ MIN}$$

$T_c = 2:10$

$i_2 = 0.93 \text{ in/hr}$

$i_{100} = 2.16 \text{ in/hr}$

Basin	Soil Group	Area (Ac.)	Total Area	c_2	c_{100}	Q_2	Q_{100}
Maize	B	24.3	24.3	0.28	0.39	6.3	20.5

Prairie Pointe

Developed Conditions Hydrology

Rational Method, $Q=ciA$

Runoff Coefficients

Single Family Residential, 1/4 Acre Lots

	Gr. B	Gr. C	Gr. D
$c_2=$	0.44	0.48	0.50
$c_{100}=$	0.61	0.68	0.76

Intensity

Assume minimum time of concentration for all basins

$$T_c = 15 \text{ Min}$$

$$i_2 = 3.8 \text{ in/hr}$$

$$i_{100} = 7.4 \text{ in/hr}$$

* Runoff from offsite can be found in existing conditions calculations

Basin 1 Analysis

Basin	Node	Soil Group	Area (Ac.)	Total Area	c		Q		Offsite		Total			
					c_2	c_{100}	Q_2	Q_{100}	Q_2	Q_{100}	Q_2	Q_{100}		
1A		B	7.08	9.05	0.45	0.64	15.5	42.9			15.5	42.9		
		C	0.56											
		D	1.41											
1B	110	B	0.33	0.33	0.44	0.61	0.6	1.5	2.4	8.9	3.0	10.4		
1C	120	B	0.19	0.27	0.46	0.65	0.5	1.3	2.4	8.8	2.9	10.1		
		D	0.08											
1D	130	B	0.26	0.51	0.47	0.68	0.9	2.6	4.8	17.7	5.7	20.3		
		D	0.25											
1E	140	B	0.31	0.31	0.44	0.61	0.5	1.4	2.2	8	2.7	9.4		
1F	210	B	1.77	2.01	0.45	0.62	3.4	9.2			3.4	9.2		
		C	0.21											
		D	0.03											
1G	220	B	1.86	2.11	0.44	0.62	3.5	9.7			3.5	9.7		
		C	0.25											
1H	230	B	0.36	0.36	0.44	0.61	0.6	1.6	2.5	9.3	3.1	10.9		
1I	240	B	0.39	0.39	0.44	0.61	0.7	1.8	2.8	10.4	3.5	12.2		
1J	250	B	0.03	0.21	0.49	0.73	0.4	1.1	1.4	5.1	1.8	6.2		
		C	0.03											
		D	0.15											
1K	310	B	1.3	1.3	0.44	0.61	2.2	5.9			2.2	5.9		
1L	320	B	3.19	3.95	0.45	0.62	6.8	18.1			6.8	18.1		
		C	0.76											
1M	330	B	0.46	0.46	0.44	0.61	0.8	2.1			0.8	2.1		
1N	410	B	0.15	0.15	0.44	0.61	0.3	0.7			0.3	0.7		

Basin	Node	Soil Group	Area (Ac.)	Total Area	c_2	c_{100}	Q_2	Q_{100}	Offsite Q_2	Offsite Q_{100}	Total Q_2	Total Q_{100}
1O	420	B	0.43	0.43	0.44	0.61	0.7	1.9			0.7	1.9
1P	510	B	0.77	1.23	0.46	0.67	2.2	6.1			2.2	6.1
		D	0.46									
1Q	520	B	1.8	2.28	0.45	0.64	3.9	10.8			3.9	10.8
		D	0.48									
1R	530	B	0.48	0.48	0.44	0.61	0.8	2.2			0.8	2.2
1S	540	B	0.56	1	0.47	0.68	1.8	5.0			1.8	5
		D	0.44									
1T	610	D	1.36	1.36	0.5	0.76	2.6	7.6			2.6	7.6
1U	620	B	0.84	2.23	0.48	0.7	4.1	11.6			4.1	11.6
		D	1.39									
1V	710	B	0.07	1.15	0.48	0.68	2.1	5.8			2.1	5.8
		C	1.08									
1W	720	C	1.44	1.44	0.48	0.68	2.6	7.2			2.6	7.2

Results

Runoff from Basin 1 enters Pond 1. Pond 1 then discharges to Pond 2 via a 15" RCP. Runoff not picked up by the SWS which is designed for the 2-year storm in Basins 1B-1E and 1H-1J will overflow along the north property line of the site and enter Pond 2.

Basin 2 Analysis

Basin	Node	Soil Group	Area (Ac.)	Total Area	c_2	c_{100}	Q_2	Q_{100}	Offsite Q_2	Offsite Q_{100}	Total Q_2	Total Q_{100}
2		B	0.84	9.03	0.48	0.68	16.5	45.4	7.1	26.2	15.5	42.9
		C	7.43									
		D	0.76									

Results

Runoff from Basin 2 enters Pond 2 along with outflow from Pond 1 and overflow from Basins 1B-1E and 1H-1J. Pond 2 then discharges from the site via a 2' weir at the south end of the pond. ($Q_{100}=49$ cfs. See HEC-1 Analysis.)

Basin 3 Analysis

Basin	Node	Soil Group	Area (Ac.)	Total Area	c_2	c_{100}	Q_2	Q_{100}	Offsite Q_2	Offsite Q_{100}	Total Q_2	Total Q_{100}
3		B	3.36	5.99	0.47	0.68	10.7	30.1	0	0	10.7	30.1
		D	2.63									

Results

Runoff discharges to the southwest corner of the site.

$$Q_{100DEV}=30.1 < Q_{100EXIST}=42.9 \text{ cfs}$$

Basin 4 Analysis

Basin	Node	Soil Group	Area (Ac.)	Total Area	c_2	c_{100}	Q_2	Q_{100}	Offsite Q_2	Offsite Q_{100}	Total Q_2	Total Q_{100}
4		B	1.97	4.55	0.46	0.65	8.0	21.9	0	0	8	21.9
		C	2.58									

Results

Runoff discharges south to 37th Street North and is then carried east to Maize Road.

Basin 5 Analysis

Basin 5 is the area between the Prairie Pointe site and Maize Road. Future development is proposed to be commercial. The Prairie Pointe pond system has been designed to handle this future development of Basin 5.

Runoff Coefficients

Commercial Area (80% impervious)

$$c_2 = 0.76$$

$$c_{100} = 0.86$$

Basin	Node	Soil Group	Area (Ac.)	Total Area	c_2	c_{100}	Q_2	Q_{100}	Offsite Q_2	Offsite Q_{100}	Total Q_2	Total Q_{100}
5		B,C	23.6	23.6	0.76	0.86	68.2	150.2	3.5	12.8	71.7	163.0

Results

Runoff from Basin 5 enters Pond 2 along with Basin 2 runoff, Pond 1 outflow, and Basin 1B-1E and 1H-1J overflow. Pond 2 then discharges from the site via a 2' weir at the south end of the pond. ($Q_{100}=49$ cfs. See HEC-1 Analysis.)

The discharge enters a channel along 37th Street North, joins runoff from Basin 4, and is carried east to Maize Road. The combined 100-year runoff from Pond 2 and Basin 4 is approximately 70 cfs. The overall developed conditions runoff is less than the existing conditions runoff at this location. ($Q_{100DEV}=88$ cfs < $Q_{100EXIST}=70$ cfs.) However, in order to be conservative, this study assumes that future development will occur in the area south of 37th Street. In keeping with this assumption, the combined outflow from Pond 2 and Basin 4 travels east to Maize Road and is picked up by Maize Road drainage structures. At this intersection, three culverts run parallel to Maize Road. (See Maize Road excerpts in the Design Aids Section.) Prairie Pointe drainage was designed in accordance with and to match design flows of the culverts. Runoff from the north in the amount of 20 cfs flows to these culverts without passing through the Prairie Pointe site. (See existing conditions calculations.) Therefore, a total of 90 cfs will reach the culverts in a 100-year storm. At this flow rate, the culverts are designed to have a head water elevation of 1355.21. The centerline of Maize Road is 1355.5. Therefore, the runoff from the 100-year storm should not overtop Maize Road.

Prairie Pointe

Street Flow

2-Year Storm

Node	Q ₂	Street Slope	d	d _{max}	Comment
320	6.8	0.5	0.40'	0.55'	ok

*by inspection, all nodes are ok

100-Year Storm

Location	Q ₁₀₀	Q _{pipe}	Q _{street}	S	Q _{max}	Comment
approaching nodes 310 and 320	24	9	15	0.5	61.3	ok

*By inspection, all nodes are ok.

Prairie Pointe

Inlet Sizing

*All inlets in sump

Curb Inlet Sizing

Node	Q ₂	Q _{max} L=5'	Q _{max} L=10'	Q _{in}	Use L=
210	3.4	11	22	3.4	5
220	3.5	11	22	3.5	5
310	2.2	11	22	2.2	5
320	6.8	11	22	6.8	5
510	2.2	11	22	2.2	5
520	3.9	11	22	3.9	5
610	2.6	11	22	2.6	5
620	4.1	11	22	4.1	5
710	2.1	11	22	2.1	5
720	2.6	11	22	2.6	5

Area Inlet Sizing

Node	Q ₁₀₀	Size	Ponding Depth
110	10.4	2'x2'	0.59'
120	10.1	2'x2'	0.57'
130	20.3	2'x4'	0.75'
140	9.4	2'x2'	0.55'
230	10.9	2'x2'	0.60'
240	12.2	2'x2'	0.65'
250	6.2	2'x2'	0.42'
330	2.1	2'x2'	0.2'
410	0.7	2'x2'	0'
420	1.9	2'x2'	0.19'
530	2.2	2'x2'	0.2'
540	5.0	2'x2'	0.36'

Area inlets were sized as follows:

2'x2' Area Inlet--Neenah Grate R4826

1.3 SF of open area

8 F Perimeter

2'x4' Area Inlet--Neenah Grate R4853A

3.1 SF of open area

11.5 F Perimeter

FLOOD HYDROGRAPH PACKAGE (HEC-1)
 FEBRUARY 1981
 REVISED 02 AUG 88

RUN DATE 04/24/2003 TIME 15:44:21

U.S. ARMY CORPS OF ENGINEERS
 THE HYDROLOGIC ENGINEERING CENTER
 609 SECOND STREET
 DAVIS, CALIFORNIA 95616
 (916) 551-1748

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X   X   XXXXXXX   XXXXX   X
X   X   X         X   X   XX
X   X   X         X         X
XXXXXXX   XXXX   X   XXXXX
X   X   X         X         X
X   X   X         X   X   X
X   X   XXXXXXX   XXXXX   XXX
    
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Prairie Pointe
2 ID 2-YEAR STORM ANALYSIS
3 ID 2 year storm
4 ID Professional Engineering Consultants
5 ID Wichita, Ks
6 ID SPL 3/25/03
7 ID File: X:\HEC1\PP2:IH1
8 IT 15 12DEC97 0000 300
9 IN 30 12DEC97 0600
10 IO 3 0
11 JR PREC .448718
*
*DIAGRAM
*
12 KK OFF1
13 KM OFFSITE TO BACKYARD NORTH LINE SWS CARRIED TO POND 1
14 BA .11547
15 PB 7.8
16 PC 0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
17 PC .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
18 PC .880 .890 .900 .910 .916 .925 .934 .943 .952 .958
19 PC .964 .970 .976 .982 .988 .994 1.000
20 LS 0 70 0
21 UD 1.35
*
22 KK BAS1
23 KM BASIN 1 TO POND 1 INCLUDING NORTH LINE SWS
24 BA .05158
25 PB 7.8
26 PC 0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
27 PC .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
28 PC .880 .890 .900 .910 .916 .925 .934 .943 .952 .958
29 PC .964 .970 .976 .982 .988 .994 1.000
30 LS 0 84 0
31 UD .15
*
32 KK COMB1
33 KO 5
34 HC 2
*
35 KK POND1
36 KM 15" RCP CULVERT FROM POND 1 TO POND 2
37 RS 1 ELEV 1354.00
38 SA 4.05 4.98
39 SE 1354.0 1358.00
40 SQ 0 1.00 2.00 3.00 4.00
41 SE 1354.0 1354.73 1356.36 1358.52 1359.45
    
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HEC-1 INPUT

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42 KK OFF2
43 KM OFFSITE TO POND 2
44 BA .04422
45 PB 7.8
46 PC 0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
47 PC .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
48 PC .880 .890 .900 .910 .916 .925 .934 .943 .952 .958
49 PC .964 .970 .976 .982 .988 .994 1.000
50 LS 0 70 0
51 UD 1.35
*
52 KK BAS2
53 KM BASIN DIRECTLY TO POND 2
54 BA .01411
55 PB 7.8
    
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57	PC	.235	.283	.663	.735	.772	.799	.820	.835	.850	.865
58	PC	.880	.890	.900	.910	.916	.925	.934	.943	.952	.958
59	PC	.964	.970	.976	.982	.988	.994	1.000			
60	LS	0	.86	0							
61	UD	.15									
*											
62	KK	COMB2									
63	KO	5									
64	HC	2									
*											
65	KK	COMB3									
66	KO	5									
67	HC	2									
*											
68	KK	OFF3									
69	KM	OFFSITE TO COMMERCIAL									
70	BA	.02172									
71	PB	7.8									
72	PC	0.08	.09	.10	.11	.12	.133	.147	.163	.181	.204
73	PC	.235	.283	.663	.735	.772	.799	.820	.835	.850	.865
74	PC	.880	.890	.900	.910	.916	.925	.934	.943	.952	.958
75	PC	.964	.970	.976	.982	.988	.994	1.000			
76	LS	0	.69	0							
77	UD	1.35									
*											
78	KK	BAS3									
79	KM	COMMERCIAL BASIN DIRECTLY TO POND 2									
80	BA	.03688									
81	PB	7.8									
82	PC	0.08	.09	.10	.11	.12	.133	.147	.163	.181	.204
83	PC	.235	.283	.663	.735	.772	.799	.820	.835	.850	.865
84	PC	.880	.890	.900	.910	.916	.925	.934	.943	.952	.958
85	PC	.964	.970	.976	.982	.988	.994	1.000			

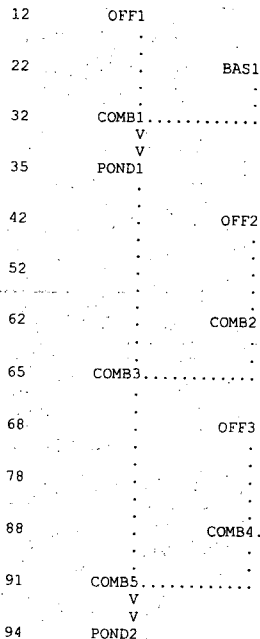
HEC-1 INPUT

PAGE 3

LINE	ID	1	2	3	4	5	6	7	8	9	10
86	LS	.0	98	0							
87	UD	.15									
*											
88	KK	COMB4									
89	KO	5									
90	HC	2									
*											
91	KK	COMB5									
92	KO	5									
93	HC	2									
*											
94	KK	POND2									
95	RS	1	ELEV	1354							
96	SA	5.47	6.63								
97	SE	1354	1358								
98	SS	1354	3.5	3.2	1.5						
*											
99	ZZ										

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW



(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
 * FEBRUARY 1981 *
 * REVISED 02 AUG 88 *
 * RUN DATE 04/24/2003 TIME 15:44:21 *

PP2A.OH1

* U.S. ARMY CORPS OF ENGINEERS *
 * THE HYDROLOGIC ENGINEERING CENTER *
 * 609 SECOND STREET *
 * DAVIS, CALIFORNIA 95616 *
 * (916) 551-1748 *

Prairie Pointe
 2-YEAR STORM ANALYSIS
 2 year storm
 Professional Engineering Consultants
 Wichita, Ks
 SPL 3/25/03
 File: X:\HEC1\PP2.IH1

10 IO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 15 MINUTES IN COMPUTATION INTERVAL
 IDATE 12DEC97 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 15DEC97 ENDING DATE
 NDTIME 0245 ENDING TIME
 ICENT 19 CENTURY MARK
 COMPUTATION INTERVAL .25 HOURS
 TOTAL TIME BASE 74.75 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-Feet
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .45

12 KK *****
 * OFF1 *

OFFSITE TO BACKYARD NORTH LINE SWS CARRIED TO POND 1

9 IN TIME DATA FOR INPUT TIME SERIES
 JKMIN 30 TIME INTERVAL IN MINUTES
 JKDATE 12DEC97 STARTING DATE
 JKTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

14 BA SUBBASIN CHARACTERISTICS
 TAREA .12 SUBBASIN AREA

PRECIPITATION DATA

15 PB STORM 7.80 BASIN TOTAL PRECIPITATION

16 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.01	.01	.01	.00	.01	.00
.01	.00	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.02	.02	.02	.02	.19	.19	.04	.04
.02	.02	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.00	.00	.00	.00	.01	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

20 LS SCS LOSS RATE
 STRTL .86 INITIAL ABSTRACTION
 CRVNR 70.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

21 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 1.35 LAG

UNIT HYDROGRAPH
 29 END-OF-PERIOD ORDINATES

3.	9.	18.	30.	36.	38.	36.	31.	25.	18.
13.	10.	8.	6.	4.	3.	3.	2.	1.	1.
1.	1.	0.	0.	0.	0.	0.	0.	0.	

HYDROGRAPH AT STATION OFF1
 FOR PLAN 1, RATIO = .00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 3.51, TOTAL EXCESS = 4.29

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	74.75-HR
90.	13.25	42.	13.	4.	4.
		(INCHES) 3.390	4.293	4.293	4.293
		(AC-FT) 21.	26.	26.	26.

CUMULATIVE AREA = .12 SQ MI

HYDROGRAPH AT STATION OFF1
FOR PLAN 1, RATIO = .45

TOTAL RAINFALL = 3.50, TOTAL LOSS = 2.49, TOTAL EXCESS = 1.01

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	74.75-HR
18.	13.50	9.	3.	1.	1.
		(INCHES) .740	1.008	1.008	1.008
		(AC-FT) 5.	6.	6.	6.

CUMULATIVE AREA = .12 SQ MI

22 KK *****
BAS1 *****

BASIN 1 TO POND 1 INCLUDING NORTH LINE SWS

9 IN TIME DATA FOR INPUT TIME SERIES *
JKMIN 30 TIME INTERVAL IN MINUTES
JXDATE 12DEC97 STARTING DATE
JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

24 BA SUBBASIN CHARACTERISTICS
TAREA .05 SUBBASIN AREA

PRECIPITATION DATA

25 PB STORM 7.80 BASIN TOTAL PRECIPITATION

26 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.01	.01	.01	.00	.01	.00
.01	.00	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.02	.02	.02	.02	.19	.19	.04	.04
.02	.02	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.00	.00	.00	.00	.01	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

30 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNR 84.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

31 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .15 LAG

UNIT HYDROGRAPH
5 END-OF-PERIOD ORDINATES
0.

89. 34. 8. 2.

HYDROGRAPH AT STATION BAS1
FOR PLAN 1, RATIO = .00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 1.90, TOTAL EXCESS = 5.90

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	74.75-HR
170.	12.00	27.	8.	3.	3.
		(INCHES) 4.838	5.903	5.903	5.903
		(AC-FT) 13.	16.	16.	16.

CUMULATIVE AREA = .05 SQ MI

HYDROGRAPH AT STATION BAS1
FOR PLAN 1, RATIO = .45

TOTAL RAINFALL = 3.50, TOTAL LOSS = 1.56, TOTAL EXCESS = 1.94

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	74.75-HR

+	(CFS)	(HR)	(CFS)				
+	56.	12.00	9.	3.	1.	1.	
			(INCHES)	1.591	1.936	1.936	1.936
			(AC-FT)	4.	5.	5.	5.

CUMULATIVE AREA = .05 SQ MI

```

*****
*          *
* 32 KK    *
*          *
*  COMB1  *
*          *
*****

```

33 KO. OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLST	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE

```

*****
*          *
* 35 KK    *
*          *
*  POND1  *
*          *
*****

```

15" RCP CULVERT FROM POND 1 TO POND 2

HYDROGRAPH ROUTING DATA

37 RS STORAGE ROUTING

NSTPS	1	NUMBER OF SUBREACHES
ITYP	ELEV	TYPE OF INITIAL CONDITION
RSVRIC	1354.00	INITIAL CONDITION
X	.00	WORKING R AND D COEFFICIENT

38 SA AREA 4.1 5.0

39 SE ELEVATION 1354.00 1358.00

40 SQ DISCHARGE 0. 1. 2. 3. 4.

41 SE ELEVATION 1354.00 1354.73 1356.36 1358.52 1359.45

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	18.03
ELEVATION	1354.00	1358.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	3.02	10.19	18.03	20.65	25.51
OUTFLOW	.00	1.00	2.00	2.76	3.00	4.00
ELEVATION	1354.00	1354.73	1356.36	1358.00	1358.52	1359.45

HYDROGRAPH AT STATION POND1 FOR PLAN 1, RATIO = .45

PEAK FLOW	TIME		6-HR	24-HR	72-HR	74.75-HR
+	(CFS)	(HR)	(CFS)	(CFS)	(CFS)	(CFS)
+	2.	24.50	2.	2.	1.	1.
			(INCHES)	.400	.882	.882
			(AC-FT)	4.	8.	8.

PEAK STORAGE	TIME		6-HR	24-HR	72-HR	74.75-HR
+	(AC-FT)	(HR)	(AC-FT)	(AC-FT)	(AC-FT)	(AC-FT)
+	10.	24.75	9.	9.	6.	6.

PEAK STAGE	TIME		6-HR	24-HR	72-HR	74.75-HR
+	(FEET)	(HR)	(FEET)	(FEET)	(FEET)	(FEET)
+	1356.23	24.75	1356.20	1356.03	1355.37	1355.32

CUMULATIVE AREA = .17 SQ MI

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*****
*          *
* 42 KK    *
*          *
*  OFF2   *
*          *
*****

```

OFFSITE TO POND 2

9 IN TIME DATA FOR INPUT TIME SERIES

JXMIN	30	TIME INTERVAL IN MINUTES
JXDATE	12DEC97	STARTING DATE
JXTIME	600	STARTING TIME

SUBBASIN RUNOFF DATA

44 BA

SUBBASIN CHARACTERISTICS
TAREA .04 SUBBASIN AREA

PP2A.OH1

PRECIPITATION DATA

45 PB

STORM 7.80 BASIN TOTAL PRECIPITATION

46 PI

INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.01	.01	.01	.01	.00	.01	.00
.01	.00	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.02	.02	.02	.02	.02	.19	.19	.04	.04
.02	.02	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.00	.00	.00	.00	.00	.01	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

50 LS

SCS LOSS RATE
STRTL .86 INITIAL ABSTRACTION
CRVNR 70.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

51 UD

SCS DIMENSIONLESS UNITGRAPH
TLAG 1.35 LAG

UNIT HYDROGRAPH
29 END-OF-PERIOD ORDINATES

1.	3.	7.	11.	14.	14.	14.	12.	9.	7.
5.	4.	3.	2.	2.	1.	1.	1.	1.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

HYDROGRAPH AT STATION OFF2
FOR PLAN 1, RATIO = .00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 3.51, TOTAL EXCESS = 4.29

PEAK FLOW	TIME	6-HR	24-HR	72-HR	74.75-HR
(CFS)	(HR)	(CFS)	(INCHES)	(AC-FT)	(INCHES)
35.	13.25	16.	3.390	8.	3.390
		5.	4.293	10.	4.293
		2.	4.293	10.	4.293
		2.	4.293	10.	4.293

CUMULATIVE AREA = .04 SQ MI

HYDROGRAPH AT STATION OFF2
FOR PLAN 1, RATIO = .45

TOTAL RAINFALL = 3.50, TOTAL LOSS = 2.49, TOTAL EXCESS = 1.01

PEAK FLOW	TIME	6-HR	24-HR	72-HR	74.75-HR
(CFS)	(HR)	(CFS)	(INCHES)	(AC-FT)	(INCHES)
7.	13.50	4.	.740	2.	.740
		1.	1.008	2.	1.008
		0.	1.008	2.	1.008
		0.	1.008	2.	1.008

CUMULATIVE AREA = .04 SQ MI

52 KK

* BAS2 *

BASIN DIRECTLY TO POND 2

9 IN

TIME DATA FOR INPUT TIME SERIES
JXMIN 30 TIME INTERVAL IN MINUTES
JXDATE 12DEC97 STARTING DATE
JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

54 BA

SUBBASIN CHARACTERISTICS
TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

55 PB

STORM 7.80 BASIN TOTAL PRECIPITATION

56 PI

INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.01	.01	.01	.00	.01	.00
.01	.00	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.02	.02	.02	.02	.02	.19	.19	.04	.04
.02	.02	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.00	.00	.00	.00	.00	.01	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

60 LS

SCS LOSS RATE
STRTL .33 INITIAL ABSTRACTION

CRVNER 86.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

PP2A:OH1

61 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .15 LAG

UNIT HYDROGRAPH
 5 END-OF-PERIOD ORDINATES
 24. 9. 2. 0. 0.

HYDROGRAPH AT STATION BAS2
 FOR PLAN 1, RATIO = .00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 1.66, TOTAL EXCESS = 6.14

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	74.75-HR
48.	12.00	8.	2.	1.	1.
		(INCHES) 5.019	6.138	6.138	6.138
		(AC-FT) 4.	5.	5.	5.

CUMULATIVE AREA = .01 SQ MI

HYDROGRAPH AT STATION BAS2
 FOR PLAN 1, RATIO = .45

TOTAL RAINFALL = 3.50, TOTAL LOSS = 1.40, TOTAL EXCESS = 2.10

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	74.75-HR
17.	12.00	3.	1.	0.	0.
		(INCHES) 1.725	2.098	2.098	2.098
		(AC-FT) 1.	2.	2.	2.

CUMULATIVE AREA = .01 SQ MI

62 KK

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*****
*          *
*   COMB2   *
*          *
*****
  
```

63 KO

OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

65 KK

```

*****
*          *
*   COMB3   *
*          *
*****
  
```

66 KO

OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

68 KK

```

*****
*          *
*   OFF3    *
*          *
*****
  
```

OFFSITE TO COMMERCIAL

9 IN

TIME DATA FOR INPUT TIME SERIES
 JXMIN 30 TIME INTERVAL IN MINUTES
 JXDATE 12DEC97 STARTING DATE
 JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

70 BA

SUBBASIN CHARACTERISTICS
 TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

71 PB

STORM 7.80 BASIN TOTAL PRECIPITATION

72 PI

INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.01	.01	.00	.00	.01	.01	.00
.01	.00	.01	.01	.01	.01	.01	.01	.01	.01	.01

PP2A.OH1

.01	.01	.02	.02	.02	.02	.19	.19	.04	.04
.02	.02	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.00	.00	.00	.00	.01	.01
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

76 LS SCS LOSS RATE
 STRTL .90 INITIAL ABSTRACTION
 CRVNR 69.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

77 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 1.35 LAG

UNIT HYDROGRAPH
 29 END-OF-PERIOD ORDINATES

1.	2.	3.	6.	7.	7.	6.	5.	3.
3.	2.	1.	1.	1.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.

HYDROGRAPH AT STATION OFF3
 FOR PLAN 1, RATIO = .45

TOTAL RAINFALL = 7.80, TOTAL LOSS = 3.62, TOTAL EXCESS = 4.18

PEAK FLOW	TIME	6-HR	24-HR	72-HR	74.75-HR
(CFS)	(HR)	(CFS)	(INCHES)	(AC-FT)	
16.	13.25	8.	3.294	4.180	4.180
		2.	4.	5.	5.
		1.	4.180	5.	5.
		1.	4.180	5.	5.

CUMULATIVE AREA = .02 SQ MI

HYDROGRAPH AT STATION OFF3
 FOR PLAN 1, RATIO = .45

TOTAL RAINFALL = 3.50, TOTAL LOSS = 2.55, TOTAL EXCESS = .95

PEAK FLOW	TIME	6-HR	24-HR	72-HR	74.75-HR
(CFS)	(HR)	(CFS)	(INCHES)	(AC-FT)	
3.	13.50	2.	.696	1.	.954
		1.	1.	1.	1.
		0.	.954	1.	1.
		0.	.954	1.	1.

CUMULATIVE AREA = .02 SQ MI

78 KK

 * BAS3 *

COMMERCIAL BASIN DIRECTLY TO POND 2

9 IN

TIME DATA FOR INPUT TIME SERIES
 JXMIN 30 TIME INTERVAL IN MINUTES
 JXDATE 12DEC97 STARTING DATE
 JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

80 BA

SUBBASIN CHARACTERISTICS
 TAREA .04 SUBBASIN AREA

PRECIPITATION DATA

81 PB

STORM 7.80 BASIN TOTAL PRECIPITATION

82 PI

INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.01	.01	.01	.01	.01	.01
.01	.00	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.02	.02	.02	.02	.19	.19	.04	.04
.02	.02	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.00	.00	.00	.00	.01	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

86 LS

SCS LOSS RATE
 STRTL .04 INITIAL ABSTRACTION
 CRVNR 98.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

87 UD

SCS DIMENSIONLESS UNITGRAPH
 TLAG .15 LAG

UNIT HYDROGRAPH
 5 END-OF-PERIOD ORDINATES

64.	24.	6.	1.	0.
-----	-----	----	----	----

HYDROGRAPH AT STATION BAS3
FOR PLAN 1, RATIO = .00

TOTAL RAINFALL = 7.80, TOTAL LOSS = .24, TOTAL EXCESS = 7.56
 PEAK FLOW TIME 6-HR MAXIMUM AVERAGE FLOW 74.75-HR
 + (CFS) (HR) (CFS) 24-HR 72-HR
 + 143. 12.00 (CFS) 23. 7. 2. 2.
 (INCHES) 5.909 7.560 7.560 7.560
 (AC-FT) 12. 15. 15. 15.
 CUMULATIVE AREA = .04 SQ MI

HYDROGRAPH AT STATION BAS3
FOR PLAN 1, RATIO = .45

TOTAL RAINFALL = 3.50, TOTAL LOSS = .23, TOTAL EXCESS = 3.27
 PEAK FLOW TIME 6-HR MAXIMUM AVERAGE FLOW 74.75-HR
 + (CFS) (HR) (CFS) 24-HR 72-HR
 + 63. 12.00 (CFS) 10. 3. 1. 1.
 (INCHES) 2.596 3.266 3.266 3.266
 (AC-FT) 5. 6. 6. 6.
 CUMULATIVE AREA = .04 SQ MI

88 KK

* COMB4 *

89 KO

OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

91 KK

* COMB5 *

92 KO

OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

94 KK

* POND2 *

HYDROGRAPH ROUTING DATA

95 RS STORAGE ROUTING:
 NSTPS 1 NUMBER OF SUBREACHES
 ITYP ELEV TYPE OF INITIAL CONDITION
 RSVRIC 1354.00 INITIAL CONDITION
 X .00 WORKING R AND D COEFFICIENT
 96 SA AREA 5.5 6.6
 97 SE ELEVATION 1354.00 1358.00
 98 SS SPILLWAY
 CREL 1354.00 SPILLWAY CREST ELEVATION
 SPWID 3.50 SPILLWAY WIDTH
 COQW 3.20 WEIR COEFFICIENT
 EXPW 1.50 EXPONENT OF HEAD

COMPUTED STORAGE-ELEVATION DATA

STORAGE .00 24.16
 ELEVATION 1354.00 1358.00

COMPUTED OUTFLOW-ELEVATION DATA

OUTFLOW .00 .00 .02 .12 .41 .98 1.92 3.32 5.27 7.87
 ELEVATION 1354.00 1354.00 1354.01 1354.05 1354.11 1354.20 1354.31 1354.44 1354.60 1354.79
 OUTFLOW 11.20 15.36 20.45 26.55 33.75 42.16 51.85 62.93 75.48 89.60
 ELEVATION 1355.00 1355.23 1355.49 1355.78 1356.09 1356.42 1356.78 1357.16 1357.57 1358.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	.07	.27	.61	1.09	1.70	2.46	3.36	4.41	5.61
OUTFLOW	.00	.02	.12	.41	.98	1.92	3.32	5.27	7.87	11.20
ELEVATION	1354.00	1354.01	1354.05	1354.11	1354.20	1354.31	1354.44	1354.60	1354.79	1355.00
STORAGE	6.97	8.48	10.17	12.02	14.06	16.28	18.70	21.33	24.16	
OUTFLOW	15.36	20.45	26.55	33.75	42.16	51.85	62.93	75.48	89.60	
ELEVATION	1355.23	1355.49	1355.78	1356.09	1356.42	1356.78	1357.16	1357.57	1358.00	

*** *** *** *** ***

HYDROGRAPH AT STATION POND2
FOR PLAN 1, RATIO = .45

PEAK FLOW (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	74.75-HR
12.	14.50		11.	6.	3.	3.
		(INCHES)	.351	.845	1.196	1.196
		(AC-FT)	5.	13.	18.	18.
PEAK STORAGE (AC-FT)	TIME (HR)		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	74.75-HR
6.	14.50		5.	4.	2.	2.
PEAK STAGE (FEET)	TIME (HR)		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	74.75-HR
1355.03	14.50		1354.97	1354.67	1354.38	1354.36

CUMULATIVE AREA = .28 SQ MI

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	TIME
HYDROGRAPH AT	OFF1	.12	1	.45	18.
					13.50
HYDROGRAPH AT	BAS1	.05	1		56.
					12.00
2 COMBINED AT	COMB1	.17	1		57.
					12.00
ROUTED TO	POND1	.17	1		2.
					24.50
				** PEAK STAGES IN FEET **	
			1	STAGE	1356.23
				TIME	24.75
HYDROGRAPH AT	OFF2	.04	1		7.
					13.50
HYDROGRAPH AT	BAS2	.01	1		17.
					12.00
2 COMBINED AT	COMB2	.06	1		17.
					12.00
2 COMBINED AT	COMB3	.23	1		18.
					12.00
HYDROGRAPH AT	OFF3	.02	1		3.
					13.50
HYDROGRAPH AT	BAS3	.04	1		63.
					12.00
2 COMBINED AT	COMB4	.06	1		63.
					12.00
2 COMBINED AT	COMB5	.28	1		81.
					12.00
ROUTED TO	POND2	.28	1		12.
					14.50
				** PEAK STAGES IN FEET **	
			1	STAGE	1355.03
				TIME	14.50

*** NORMAL END OF HEC-1 ***

FLOOD HYDROGRAPH PACKAGE (HEC-1)
 FEBRUARY 1981
 REVISED 02 AUG 88

RUN DATE 04/24/2003 TIME 15:45:15

U.S. ARMY CORPS OF ENGINEERS
 THE HYDROLOGIC ENGINEERING CENTER
 609 SECOND STREET
 DAVIS, CALIFORNIA 95616
 (916) 551-1748

```

X   X   XXXXXXX   XXXXX   X
X   X   X       X   X     XX
X   X   X       X         X
XXXXXXXX XXXX   X   XXXXX  X
X   X   X       X         X
X   X   X       X   X     X
X   X   XXXXXXX   XXXXX   XXX
    
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION.
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10.....

```

1 ID Prairie Point
2 ID 100-YEAR STORM ANALYSIS
3 ID 100 year storm
4 ID Professional Engineering Consultants
5 ID Wichita, Ks
6 ID SPL 3/25/03
7 ID File: X:\HEC1\PP100.IH1
8 IT 15 12DEC97 0000 300
9 IN 30 12DEC97 0600
10 IO 3 0
11 JR PREC1.000
    
```

*DIAGRAM

```

12 KK OFF1
13 KM BACKYARD NORTH LINE SWS CARRIED TO POND 1 VIA SWS (Q2) BOTH OFF AND ON SITE
14 BA .03258
15 PB 7.8
16 PC 0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
17 PC .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
18 PC .880 .890 .900 .910 .916 .925 .934 .943 .952 .958
19 PC .964 .970 .976 .982 .988 .994 1.000
20 LS 0 66 0
21 UD 1.35
    
```

```

22 KK BAS1
23 KM BASIN 1 TO POND 1 EXCLUDING NORTH LINE SWS OVERFLOW
24 BA .04786
25 PB 7.8
26 PC 0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
27 PC .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
28 PC .880 .890 .900 .910 .916 .925 .934 .943 .952 .958
29 PC .964 .970 .976 .982 .988 .994 1.000
30 LS 0 78 0
31 UD .15
    
```

```

32 KK COMB1
33 KO 5
34 HC 2
    
```

```

35 KK POND1
36 KM 15" RCP CULVERT FROM POND 1 TO POND 2
37 RS 1 ELEV 1354.00
38 SA 4.05 4.98
39 SE 1354.0 1358.00
40 SQ 0 1.00 2.00 3.00 4.00
41 SE 1354.0 1354.73 1356.36 1358.52 1359.45
    
```

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10.....

```

42 KK CHANN
43 KM OVERFLOW FROM NORTH SWS TO POND 2
44 BA .09605
45 PB 7.8
46 PC 0.08 .09 .10 .11 .12 .133 .147 .163 .181 .204
47 PC .235 .283 .663 .735 .772 .799 .820 .835 .850 .865
48 PC .880 .890 .900 .910 .916 .925 .934 .943 .952 .958
49 PC .964 .970 .976 .982 .988 .994 1.000
50 LS 0 61 0
51 UD 1.35
    
```

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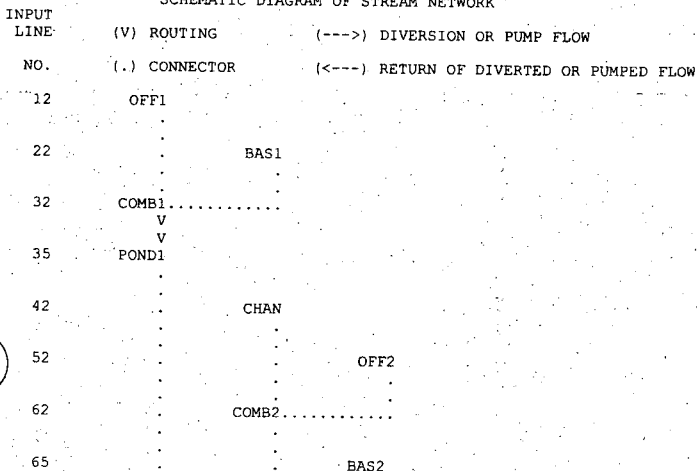
52 KK OFF2
53 KM OFFSITE TO POND 2
54 BA .04422
55 PB 7.8
    
```

PF100A.OH1											
56	PC	0.08	.09	.10	.11	.12	.133	.147	.163	.181	.204
57	PC	.235	.283	.663	.735	.772	.799	.820	.835	.850	.865
58	PC	.880	.890	.900	.910	.916	.925	.934	.943	.952	.958
59	PC	.964	.970	.976	.982	.988	.994	1.000			
60	LS	0	62	0							
61	UD	1.35									
*											
62	KK	COMB2									
63	KO	5									
64	HC	2									
*											
65	KK	BAS2									
66	KM	BASIN DIRECTLY TO POND 2									
67	BA	.01411									
68	PB	7.8									
69	PC	0.08	.09	.10	.11	.12	.133	.147	.163	.181	.204
70	PC	.235	.283	.663	.735	.772	.799	.820	.835	.850	.865
71	PC	.880	.890	.900	.910	.916	.925	.934	.943	.952	.958
72	PC	.964	.970	.976	.982	.988	.994	1.000			
73	LS	0	81	0							
74	UD	.15									
*											
75	KK	COMB3									
76	KO	5									
77	HC	2									
*											
78	KK	COMB4									
79	KO	5									
80	HC	2									
*											

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
81	KK	OFF3									
82	KM	OFFSITE TO COMMERCIAL									
83	BA	.02172									
84	PB	7.8									
85	PC	0.08	.09	.10	.11	.12	.133	.147	.163	.181	.204
86	PC	.235	.283	.663	.735	.772	.799	.820	.835	.850	.865
87	PC	.880	.890	.900	.910	.916	.925	.934	.943	.952	.958
88	PC	.964	.970	.976	.982	.988	.994	1.000			
89	LS	0	62	0							
90	UD	1.35									
*											
91	KK	BAS3									
92	KM	COMMERCIAL BASIN DIRECTLY TO POND 2									
93	BA	.03688									
94	PB	7.8									
95	PC	0.08	.09	.10	.11	.12	.133	.147	.163	.181	.204
96	PC	.235	.283	.663	.735	.772	.799	.820	.835	.850	.865
97	PC	.880	.890	.900	.910	.916	.925	.934	.943	.952	.958
98	PC	.964	.970	.976	.982	.988	.994	1.000			
99	LS	0	98	0							
100	UD	.15									
*											
101	KK	COMB5									
102	KO	5									
103	HC	2									
*											
104	KK	COMB6									
105	KO	5									
106	HC	2									
*											
107	KK	POND2									
108	RS	1	ELEV	1354							
109	SA	5.47	6.63								
110	SE	1354	1358								
111	SS	1354	2.0	3.2	1.5						
112	ZZ										

SCHEMATIC DIAGRAM OF STREAM NETWORK



75 COMB3.....
 78 COMB4.....
 81 OFF3.....
 91 BAS3.....
 101 COMB5.....
 104 COMB6.....
 V
 V
 107 POND2

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   FEBRUARY 1981                 *
*   REVISED 02 AUG 88             *
* RUN DATE 04/24/2003 TIME 15:45:15 *
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*****
* U.S. ARMY CORPS OF ENGINEERS *
* THE HYDROLOGIC ENGINEERING CENTER *
*   609 SECOND STREET           *
*   DAVIS, CALIFORNIA 95616     *
*   (916) 551-1748             *
*****
  
```

Prairie Pointe
 100-YEAR STORM ANALYSIS
 100 year storm
 Professional Engineering Consultants
 Wichita, Ks
 SPL 3/25/03
 File: X:\HEC1\PP100.IH1

10 IO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 15 MINUTES IN COMPUTATION INTERVAL
 LDATE 12DEC97 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 15DEC97 ENDING DATE
 NDTIME 0245 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .25 HOURS
 TOTAL TIME BASE 74.75 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-Feet
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 1.00

12 KK OFF1

BACKYARD NORTH LINE SWS CARRIED TO POND 1 VIA SWS (Q2) BOTH OFF AND ON SITE

9 IN TIME DATA FOR INPUT TIME SERIES
 JXMIN 30 TIME INTERVAL IN MINUTES
 JXDATE 12DEC97 STARTING DATE
 JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

14 BA SUBBASIN CHARACTERISTICS
 TAREA .03 SUBBASIN AREA

PRECIPITATION DATA

15 PB STORM 7.80 BASIN TOTAL PRECIPITATION

16 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.01	.01	.01	.00	.00	.00	.00
.01	.00	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.02	.02	.02	.01	.19	.19	.04	.04	.04
.02	.02	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.00	.00	.00	.00	.01	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00

20 LS SCS LOSS RATE
STRTL 1.03 INITIAL ABSTRACTION
CRVNR 66.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

21 UD SCS DIMENSIONLESS UNITGRAPH
TLAG 1.35 LAG

UNIT HYDROGRAPH
29 END-OF-PERIOD ORDINATES

1. 3. 5. 8. 10. 11. 10. 9. 7. 5.
4. 3. 2. 2. 1. 1. 1. 1. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0. 0. 0.

HYDROGRAPH AT STATION OFF1
FOR PLAN 1, RATIO = .00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 3.96, TOTAL EXCESS = 3.84

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
+ (CFS) (HR) 6-HR 24-HR 72-HR 74.75-HR
+ 22. 13.25 (CFS) 11. 3. 1. 1.
(INCHES) 3.005 3.844 3.844 3.844
(AC-FT) 5. 7. 7. 7.

CUMULATIVE AREA = .03 SQ MI

HYDROGRAPH AT STATION OFF1
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 3.96, TOTAL EXCESS = 3.84

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
+ (CFS) (HR) 6-HR 24-HR 72-HR 74.75-HR
+ 22. 13.25 (CFS) 11. 3. 1. 1.
(INCHES) 3.005 3.844 3.844 3.844
(AC-FT) 5. 7. 7. 7.

CUMULATIVE AREA = .03 SQ MI

22 KK *****
* BAS1 *

BASIN 1 TO POND 1 EXCLUDING NORTH LINE SWS OVERFLOW

9 IN TIME DATA FOR INPUT TIME SERIES
JXMIN 30 TIME INTERVAL IN MINUTES
JXDATE 12DEC97 STARTING DATE
JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

24 BA SUBBASIN CHARACTERISTICS
TAREA .05 SUBBASIN AREA

PRECIPITATION DATA

25 PB STORM 7.80 BASIN TOTAL PRECIPITATION

26 PI INCREMENTAL PRECIPITATION PATTERN
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .01 .01 .01 .00 .01 .00
.01 .00 .01 .01 .01 .01 .01 .01 .01 .01
.01 .01 .02 .02 .02 .02 .02 .19 .19 .04
.02 .02 .01 .01 .01 .01 .01 .01 .01 .01
.01 .01 .01 .01 .01 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00

30 LS SCS LOSS RATE
STRTL .56 INITIAL ABSTRACTION
CRVNR 78.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

31 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .15 LAG

UNIT HYDROGRAPH
5 END-OF-PERIOD ORDINATES

83. 32. 7. 2. 0.

HYDROGRAPH AT STATION BAS1
FOR PLAN 1, RATIO = .00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 2.59, TOTAL EXCESS = 5.21

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	74.75-HR	
140.	12.00	22.	7.	2.	2.	
		(INCHES)	4.278	5.206	5.206	5.206
		(AC-FT)	11.	13.	13.	13.

CUMULATIVE AREA = .05 SQ MI

HYDROGRAPH AT STATION BAS1
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 2.59, TOTAL EXCESS = 5.21

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	74.75-HR	
140.	12.00	22.	7.	2.	2.	
		(INCHES)	4.278	5.206	5.206	5.206
		(AC-FT)	11.	13.	13.	13.

CUMULATIVE AREA = .05 SQ MI

32 KK

* COMB1 *

33 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

35 KK

* POND1 *

15" RCP CULVERT FROM POND 1 TO POND 2

HYDROGRAPH ROUTING DATA

STORAGE ROUTING	NSTPS ITYP RSVRIC X	1 ELEV 1354.00 .00	NUMBER OF SUBREACHES TYPE OF INITIAL CONDITION INITIAL CONDITION WORKING R AND D COEFFICIENT			
			4.1	5.0		
37 RS						
38 SA	AREA	4.1	5.0			
39 SE	ELEVATION	1354.00	1358.00			
40 SQ	DISCHARGE	0.	1.	2.	3.	4.
41 SE	ELEVATION	1354.00	1354.73	1356.36	1358.52	1359.45

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	18.03
ELEVATION	1354.00	1358.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	3.02	10.19	18.03	20.65	25.51
OUTFLOW	.00	1.00	2.00	2.76	3.00	4.00
ELEVATION	1354.00	1354.73	1356.36	1358.00	1358.52	1359.45

HYDROGRAPH AT STATION POND1
FOR PLAN 1, RATIO = 1.00

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	74.75-HR	
3.	24.25	3.	3.	2.	2.	
		(INCHES)	.308	1.183	2.735	2.735
		(AC-FT)	1.	5.	12.	12.

PEAK STORAGE (AC-FT)	TIME (HR)	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	74.75-HR
17.	24.25	17.	16.	11.	11.

PEAK STAGE (FEET)	TIME (HR)	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	74.75-HR
1357.84	24.25	1357.79	1357.57	1356.56	1356.46

CUMULATIVE AREA = .08 SQ MI

42 KK

```

*****
*   CHAN   *
*         *
*****
    
```

OVERFLOW FROM NORTH SWS TO POND 2

9 IN

TIME DATA FOR INPUT TIME SERIES
 JXMIN 30 TIME INTERVAL IN MINUTES
 JXDATE 12DEC97 STARTING DATE
 JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

44 BA

SUBBASIN CHARACTERISTICS
 TAREA .10 SUBBASIN AREA

PRECIPITATION DATA

45 PB

STORM 7.80 BASIN TOTAL PRECIPITATION

46 PI

INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.01	.00	.01	.01	.01	.01	.01	.01	.01	.01	.00
.01	.01	.02	.02	.02	.02	.02	.19	.19	.04	.04
.02	.02	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.00	.00	.00	.00	.00	.01	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

50 LS

SCS LOSS RATE
 STRTL 1.28 INITIAL ABSTRACTION
 CRVNR 61.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

51 UD

SCS DIMENSIONLESS UNITGRAPH
 TLAG 1.35 LAG

UNIT HYDROGRAPH

2.	7.	15.	25.	30.	31.	30.	26.	20.	15.
11.	8.	6.	5.	4.	3.	2.	2.	1.	1.
1.	1.	0.	0.	0.	0.	0.	0.	0.	0.

HYDROGRAPH AT STATION CHAN
 FOR PLAN 1, RATIO = .00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 4.51, TOTAL EXCESS = 3.29

PEAK FLOW	TIME	6-HR	24-HR	72-HR	74.75-HR
(CFS)	(HR)	(CFS)	(CFS)	(CFS)	(CFS)
54.	13.50	26.	9.	3.	3.
		(INCHES)	(INCHES)	(INCHES)	(INCHES)
		2.531	3.293	3.293	3.293
		(AC-FT)	(AC-FT)	(AC-FT)	(AC-FT)
		13.	17.	17.	17.

CUMULATIVE AREA = .10 SQ MI

HYDROGRAPH AT STATION CHAN
 FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 4.51, TOTAL EXCESS = 3.29

PEAK FLOW	TIME	6-HR	24-HR	72-HR	74.75-HR
(CFS)	(HR)	(CFS)	(CFS)	(CFS)	(CFS)
54.	13.50	26.	9.	3.	3.
		(INCHES)	(INCHES)	(INCHES)	(INCHES)
		2.531	3.293	3.293	3.293
		(AC-FT)	(AC-FT)	(AC-FT)	(AC-FT)
		13.	17.	17.	17.

CUMULATIVE AREA = .10 SQ MI

52 KK

```

*****
*   OFF2  *
*         *
*****
    
```

OFFSITE TO POND 2

9 IN

TIME DATA FOR INPUT TIME SERIES
 JXMIN 30 TIME INTERVAL IN MINUTES
 JXDATE 12DEC97 STARTING DATE
 JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

PP100A.OH1

54 BA SUBBASIN CHARACTERISTICS
TAREA .04 SUBBASIN AREA

PRECIPITATION DATA

55 PB STORM 7.80 BASIN TOTAL PRECIPITATION

56 PI INCREMENTAL PRECIPITATION PATTERN
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .01 .01 .01 .01 .00 .01 .00
.01 .00 .01 .01 .01 .01 .01 .01 .01 .01 .01
.01 .01 .02 .02 .02 .02 .02 .19 .19 .04 .04
.02 .02 .01 .01 .01 .01 .01 .01 .01 .01 .01
.01 .01 .01 .01 .00 .00 .00 .00 .00 .01 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00

60 LS SCS LOSS RATE
STRTL 1.23 INITIAL ABSTRACTION
CRVNR 62.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

61 UD SCS DIMENSIONLESS UNITGRAPH
TLAG 1.35 LAG

UNIT HYDROGRAPH
29 END-OF-PERIOD ORDINATES

1. 3. 7. 11. 14. 14. 14. 12. 9. 7.
5. 4. 3. 2. 2. 1. 1. 1. 1. 0.
0. 0. 0. 0. 0. 0. 0. 0. 0. 0.

HYDROGRAPH AT STATION OFF2
FOR PLAN 1, RATIO = .00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 4.40, TOTAL EXCESS = 3.40

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
+ (CFS) (HR) 6-HR 24-HR 72-HR 74.75-HR
+ 26. 13.25 (CFS) 12. 4. 1. 1.
(INCHES) 2.625 3.402 1. 3.402
(AC-FT) 6. 8. 8. 8.

CUMULATIVE AREA = .04 SQ MI

HYDROGRAPH AT STATION OFF2
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 4.40, TOTAL EXCESS = 3.40

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
+ (CFS) (HR) 6-HR 24-HR 72-HR 74.75-HR
+ 26. 13.25 (CFS) 12. 4. 1. 1.
(INCHES) 2.625 3.402 1. 3.402
(AC-FT) 6. 8. 8. 8.

CUMULATIVE AREA = .04 SQ MI

62 KK *****
* COMB2 *

63 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

65 KK *****
* BAS2 *

BASIN DIRECTLY TO POND 2

9 IN TIME DATA FOR INPUT TIME SERIES
JXMIN 30 TIME INTERVAL IN MINUTES
JXDATE 12DEC97 STARTING DATE
JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

67 BA SUBBASIN CHARACTERISTICS
TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

PP100A:OH1

68 PB STORM 7.80 BASIN TOTAL PRECIPITATION

69 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.01	.00	.01	.01	.01	.01	.01	.01	.00	.01	.00
.01	.01	.02	.02	.02	.02	.02	.19	.19	.04	.04
.02	.02	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.00	.00	.00	.00	.00	.01	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

73 LS SCS LOSS RATE
 STRTL .47 INITIAL ABSTRACTION
 CRVNBR 81.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

74 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .15 LAG

UNIT HYDROGRAPH
 5 END-OF-PERIOD ORDINATES
 0.

24. 9. 2. 0.

*** *** *** *** ***

HYDROGRAPH AT STATION BAS2
 FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 2.25, TOTAL EXCESS = 5.55

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	74.75-HR
44.	12.00	7.	2.	1.	1.
		(INCHES) 4.560	5.554	5.554	5.554
		(AC-FT) 3.	4.	4.	4.

CUMULATIVE AREA = .01 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BAS2
 FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 2.25, TOTAL EXCESS = 5.55

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	74.75-HR
44.	12.00	7.	2.	1.	1.
		(INCHES) 4.560	5.554	5.554	5.554
		(AC-FT) 3.	4.	4.	4.

CUMULATIVE AREA = .01 SQ MI

75 KK

 * COMB3 *

76 KO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

78 KK

 * COMB4 *

79 KO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

81 KK

 * OFF3 *

OFFSITE TO COMMERCIAL

9 IN TIME DATA FOR INPUT TIME SERIES

JXMIN 30 TIME INTERVAL IN MINUTES
JXDATE 12DEC97 STARTING DATE
JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

83 BA SUBBASIN CHARACTERISTICS
TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

84 PB STORM 7.80 BASIN TOTAL PRECIPITATION

85 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.01	.01	.01	.00	.01	.00
.01	.00	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.02	.02	.02	.02	.19	.19	.04	.04	.04
.02	.02	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.00	.00	.00	.00	.01	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

89 LS SCS LOSS RATE
STRTL 1.23 INITIAL ABSTRACTION
CRVNR 62.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

90 UD SCS DIMENSIONLESS UNITGRAPH
TLAG 1.35 LAG

UNIT HYDROGRAPH
29 END-OF-PERIOD ORDINATES

1.	2.	3.	6.	7.	7.	7.	6.	5.	3.
3.	2.	1.	1.	1.	1.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

HYDROGRAPH AT STATION OFF3
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 4.40, TOTAL EXCESS = 3.40

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (INCHES)	74.75-HR (INCHES)
13.	13.25	6.	2.625	2.	1.
		(AC-FT)	3.	3.402	3.402
			4.	4.	4.

CUMULATIVE AREA = .02 SQ MI

HYDROGRAPH AT STATION OFF3
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 4.40, TOTAL EXCESS = 3.40

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (INCHES)	74.75-HR (INCHES)
13.	13.25	6.	2.625	2.	1.
		(AC-FT)	3.	3.402	3.402
			4.	4.	4.

CUMULATIVE AREA = .02 SQ MI

91 KK

* BAS3 *

COMMERCIAL BASIN DIRECTLY TO POND 2

9 IN TIME DATA FOR INPUT TIME SERIES
JXMIN 30 TIME INTERVAL IN MINUTES
JXDATE 12DEC97 STARTING DATE
JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

93.BA SUBBASIN CHARACTERISTICS
TAREA .04 SUBBASIN AREA

PRECIPITATION DATA

94 PB STORM 7.80 BASIN TOTAL PRECIPITATION

95 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.01	.01	.01	.00	.01	.00
.01	.00	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.02	.02	.02	.02	.19	.19	.04	.04	.04
.02	.02	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.00	.00	.00	.00	.01	.00	.00

PP100A.OH1

.00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00

99 LS SCS LOSS RATE
STRTL .04 INITIAL ABSTRACTION
CRVNR 98.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

100 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .15 LAG

UNIT HYDROGRAPH
5 END-OF-PERIOD ORDINATES
0.

64. 24. 6. 1.

*** *** *** *** ***

HYDROGRAPH AT STATION BAS3
FOR PLAN 1, RATIO = .00

TOTAL RAINFALL = 7.80, TOTAL LOSS = .24, TOTAL EXCESS = 7.56

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	74.75-HR
+ 143.	12.00	(CFS) 23.	7.	2.	2.
		(INCHES) 5.909	7.560	7.560	7.560
		(AC-FT) 12.	15.	15.	15.

CUMULATIVE AREA = .04 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION BAS3
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = .24, TOTAL EXCESS = 7.56

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	74.75-HR
+ 143.	12.00	(CFS) 23.	7.	2.	2.
		(INCHES) 5.909	7.560	7.560	7.560
		(AC-FT) 12.	15.	15.	15.

CUMULATIVE AREA = .04 SQ MI

101 KK *****
* COMB5 *

102 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

104 KK *****
* COMB6 *

105 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

107 KK *****
* POND2 *

HYDROGRAPH ROUTING DATA

108 RS STORAGE ROUTING
NSTPS 1 NUMBER OF SUBREACHES
ITYP ELEV TYPE OF INITIAL CONDITION
RSVRIC 1354.00 INITIAL CONDITION
X .00 WORKING R AND D COEFFICIENT

109 SA AREA 5.5 6.6

110 SE ELEVATION 1354.00 1358.00

111 SS SPILLWAY
CREL 1354.00 SPILLWAY CREST ELEVATION

SPWID 2.00 SPILLWAY WIDTH
 COOW 3.20 WEIR COEFFICIENT
 EXPW 1.50 EXPONENT OF HEAD

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	24.16
ELEVATION	1354.00	1358.00

COMPUTED OUTFLOW-ELEVATION DATA

OUTFLOW	.00	.00	.01	.07	.24	.56	1.10	1.90	3.01	4.50
ELEVATION	1354.00	1354.00	1354.01	1354.05	1354.11	1354.20	1354.31	1354.44	1354.60	1354.79
OUTFLOW	6.40	8.78	11.68	15.17	19.29	24.09	29.63	35.96	43.13	51.20
ELEVATION	1355.00	1355.23	1355.49	1355.78	1356.09	1356.42	1356.78	1357.16	1357.57	1358.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	.07	.27	.61	1.09	1.70	2.46	3.36	4.41	5.61
OUTFLOW	.00	.01	.07	.24	.56	1.10	1.90	3.01	4.50	6.40
ELEVATION	1354.00	1354.01	1354.05	1354.11	1354.20	1354.31	1354.44	1354.60	1354.79	1355.00
STORAGE	6.97	8.48	10.17	12.02	14.06	16.28	18.70	21.33	24.16	
OUTFLOW	8.78	11.68	15.17	19.29	24.09	29.63	35.96	43.13	51.20	
ELEVATION	1355.23	1355.49	1355.78	1356.09	1356.42	1356.78	1357.16	1357.57	1358.00	

*** *** *** *** ***

HYDROGRAPH AT STATION POND2
 FOR PLAN 1, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	74.75-HR	
49.	15.25	43.	24.	10.	9.	
		(INCHES)	1.373	3.013	3.649	3.649
		(AC-FT)	21.	47.	57.	57.

PEAK STORAGE + (AC-FT)	TIME (HR)	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	74.75-HR
23.	15.25	21.	13.	6.	6.

PEAK STAGE + (FEET)	TIME (HR)	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	74.75-HR
1357.87	15.25	1357.57	1356.30	1355.10	1355.06

CUMULATIVE AREA = .29 SQ MI

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	1.00
HYDROGRAPH AT	OFF1	.03	1	FLOW	22.
				TIME	13.25
HYDROGRAPH AT	BAS1	.05	1	FLOW	140.
				TIME	12.00
2 COMBINED AT	COMB1	.08	1	FLOW	143.
				TIME	12.00
ROUTED TO	POND1	.08	1	FLOW	3.
				TIME	24.25
				** PEAK STAGES IN FEET **	
				1 STAGE	1357.84
				TIME	24.25
HYDROGRAPH AT	CHAN	.10	1	FLOW	54.
				TIME	13.50
HYDROGRAPH AT	OFF2	.04	1	FLOW	26.
				TIME	13.25
2 COMBINED AT	COMB2	.14	1	FLOW	80.
				TIME	13.50
HYDROGRAPH AT	BAS2	.01	1	FLOW	44.
				TIME	12.00
2 COMBINED AT	COMB3	.15	1	FLOW	84.
				TIME	13.25
2 COMBINED AT	COMB4	.23	1	FLOW	86.
				TIME	13.25

HYDROGRAPH AT

+	OFF3	.02	1	FLOW TIME	13. 13.25
+	HYDROGRAPH AT				
+	BAS3	.04	1	FLOW TIME	143. 12.00
+	2 COMBINED AT				
+	COMB5	.06	1	FLOW TIME	144. 12.00
+	2 COMBINED AT				
+	COMB6	.29	1	FLOW TIME	198. 12.00
+	ROUTED TO				
+	POND2	.29	1	FLOW TIME	49. 15.25

** PEAK STAGES IN FEET **
1 STAGE 1357.87
TIME 15.25

*** NORMAL END OF HEC-1 ***

PRAIRIE POINTE 1
Input File: ppl.inp
Flow rate includes undeveloped runoff from north offsite basin

Storm Frequency = 2-Year

* * * H Y D R O L O G Y * *

```

*****
Tributary Area
*****
Node to C Area Slope Length TC(0) I(0) Q(0) I TC Sum Q
(Ft) (Min) (In/Hr) (CFS) (Min) (In/Hr) (CFS) (CFS)
*****
140 110 .44 .31 .00 .0 15.00 3.83 2.70 15.00 3.83 2.70 2.70
130 120 .47 .51 .00 .0 15.00 3.83 5.70 15.00 3.83 5.70 5.70
120 110 .46 .27 .00 .0 15.00 3.83 2.90 15.90 3.73 2.82 8.52
110 100 .44 .33 .00 .0 15.00 3.83 3.00 16.95 3.62 2.83 14.00
*****
Conduit Data
*****
Size Velocity Length TT TT+TC
(Ft/Sec) (Ft) (Min) (Min)
*****
15" 2.20 165.00 1.25 16.25
18" 3.23 173.50 .90 15.90
24" 2.71 171.75 1.06 16.95
24" 4.46 340.00 1.27 18.22
*****

```

Date: 03-27-2003
Time: 09:39:05

STOR OUT

Input File: pp1.inp
PRAIRIE POINTE 1
Flow rate includes undeveloped runoff from north offsite basin

Storm Frequency = 2-Year

* * * H Y D R A U L I C S * *

Node	Hyd-Slope (Ft/Ft)	Friction (Ft)	Bend (Ft)	Transition (Ft)	Manhole (Ft)	Deflection (Ft)	Junction (Ft)	Total (Ft)	Hyd-Gl Elevation	Desired Elevation	Diff.
100	.00000	.0000	.0000	.0000	.0000	.0000	.0000	.0000	1356.0000	1356.0000	.00
110	.00227	.7710	.0000	.0194	.0000	.3321	.3461	1.4686	1357.4690	1359.0000	1.53
120	.00084	.1443	.0000	.0094	.0000	.0216	.0666	.2419	1357.7110	1359.3000	1.59
130	.00174	.3023	.0000	.0000	.0000	.0000	.0000	.3023	1358.0130	1359.6000	1.59
140	.00103	.1706	.0000	.0000	.0000	.0000	.0000	.1706	1357.6390	1359.3000	1.66

Date: 03-27-2003
Time: 09:48:09

STORM OUT

Input File: pp2.inp

PRAIRIE POINTE 2

Flow rates (230-250) include undeveloped runoff from north offsite b

Storm Frequency = 2-Year

* * * HYDROLOGY * *

Tributary Area		Hydrology			Summation			Conduit Data							
Node to	C	Area (Ac)	Slope (%)	Length (Ft)	TC (Min)	I (In/Hr)	Q (CFS)	I (In/Hr)	Q (CFS)	Sum Q (CFS)	Size	Velocity (Ft/Sec)	Length (Ft)	TT (Min)	TT+TC (Min)
250	230	.49	.21	.00	.0	15.00	3.83	1.80	1.80	1.80	18"	1.02	124.00	2.03	17.03
240	230	.44	.39	.00	.0	15.00	3.83	3.50	3.50	3.50	18"	1.98	204.00	1.72	16.72
230	220	.44	.36	.00	.0	15.00	3.83	3.10	2.92	8.19	24"	2.61	149.90	.96	17.99
220	210	.44	2.11	.00	.0	15.00	3.83	3.50	3.51	3.21	24"	3.63	44.00	.20	18.19
210	200	.45	2.01	.00	.0	15.00	3.83	3.40	3.50	3.10	24"	4.62	146.00	.53	18.72

□

Date: 03-27-2003
Time: 09:48:09

STORM OUT

Input File: pp2.inp

PRAIRIE POINTE 2
Flow rates (230-250) include undeveloped runoff from north offsite b

Storm Frequency = 2-Year

* * * H Y D R A U L I C S * *

Node	Hyd-Slope (Ft/Ft)	Friction (Ft)	Bend (Ft)	Transition (Ft)	Manhole (Ft)	Deflection (Ft)	Junction (Ft)	Total (Ft)	Hyd-Gl. Elevation	Desired Elevation	Diff.
200	.00000	.0000	.0000	.0000	.0000	.0000	.0000	.0000	1356.0000	1356.0000	.00
210	.00243	.3554	.0000	.0127	.0000	.0274	.2635	.6589	1356.6590	1361.0000	4.34
220	.00150	.0662	.0000	.0099	.0000	.0141	.2042	.2944	1356.9530	1361.0000	4.05
230	.00078	.1163	.0000	.0045	.0000	.1770	.1663	.4641	1357.4170	1359.0000	1.58
240	.00066	.1340	.0000	.0000	.0000	.0000	.0000	.1340	1357.5520	1359.3000	1.75
250	.00017	.0215	.0000	.0000	.0000	.0000	.0000	.0215	1357.4390	1359.3000	1.86

Date: 03-27-2003
Time: 10:00:35

STORM OUT

Input File: pp3.inp

Storm Frequency = 2-Year

PRAIRIE POINTE 3

* * * H Y D R O L O G Y * * *

Tributary Area		Hydrology Summation				Conduit Data										
Node	C	Area (Ac)	Slope (%)	Length (Ft)	TC (Min)	I (In/Hr)	Q (0) (CFS)	TC (Min)	I (In/Hr)	Q (CFS)	Sum Q (CFS)	Size	Velocity (Ft/Sec)	Length (Ft)	TT (Min)	TT+TC (Min)
330	320	.44	.00	.0	15.00	3.83	.80	15.00	3.83	.80	.80	15"	.65	111.00	2.84	17.84
320	310	.45	.00	.0	15.00	3.83	6.80	15.00	3.83	6.80	7.47	18"	4.23	44.00	.17	15.17
310	300	.44	.00	.0	15.00	3.83	2.20	15.17	3.81	2.19	9.66	24"	3.08	146.00	.79	15.96

□

Input File: pp3.inp

Storm Frequency = 2-Year

PRAIRIE POINTE. 3

* * * H Y D R A U L I C S * * *

Node	Hyd-Slope (Ft/Ft)	Friction (Ft)	Bend (Ft)	Transition (Ft)	Manhole (Ft)	Deflection (Ft)	Junction (Ft)	Total (Ft)	Hyd-GI Elevation	Desired Elevation	Diff.
300	.00000	.0000	.0000	.0000	.0000	.0000	.0000	.0000	1356.0000	1356.0000	.00
310	.00108	.1576	.0000	.0262	.0000	.6243	-.0137	.7943	1356.7940	1360.6000	3.81
320	.00299	.1318	.0000	.0271	.0000	.0151	.6535	.8275	1357.6220	1360.6000	2.98
330	.00009	.0101	.0000	.0000	.0000	.0000	.0000	.0101	1357.6320	1359.2000	1.57

Date: 03-27-2003
Time: 10:08:09

STORM OUT

Input File: pp4.inp

Storm Frequency = 2-Year

PRAIRIE POINTE 4

* * * H Y D R O L O G Y * * *

Tributary Area		Hydrology Summation				Conduit Data							
Node to	C	Area (Ac)	Slope (%)	Length (Ft)	TC (Min)	I (In/Hr)	Q (CFS)	Sum Q (CFS)	Size	Velocity (Ft/Sec)	Length (Ft)	TT (Min)	TT+TC (Min)
420	410	.44	.00	.0	15.00	3.83	1.90	1.90	15"	1.55	62.70	.67	15.67
410	400	.44	.00	.0	15.00	3.83	.30	2.19	15"	1.79	116.00	1.08	16.76

□

Input File: pp4.inp

Storm Frequency = 2-Year

PRAIRIE POINTE 4

* * * H Y D R A U L I C S * *

```

*****
Node  Hyd-Slope  Friction  Bend  Transition  Manhole  Deflection  Junction  Total  Hyd-Gl  Desired  Diff.
      (Ft/Ft)    (Ft)      (Ft)    (Ft)        (Ft)      (Ft)      (Ft)      (Ft)    Elevation Elevation (Ft)
*****
400   .00000    .0000    .0000    .0000    .0000    .0000    .0000    .0000  1356.0000  1356.0000    .00
410   .00068    .0792    .0000    .0012    .0000    .0933    .0279    .2016  1356.2020  1359.7000    3.50
420   .00051    .0321    .0000    .0000    .0000    .0000    .0000    .0321  1356.2340  1359.0000    2.77
*****

```

Input File: pp5.inp

Storm Frequency = 2-Year

PRAIRIE POINTE 5

* * * H Y D R O L O G Y * * *

Tributary Area		Hydrology				Conduit Data											
Node to Node	C	Area (Ac)	Slope (%)	Length (Ft)	TC (Min)	I(0) (In/Hr)	Q(0) (CFS)	TC (Min)	I (In/Hr)	Q (CFS)	Sum Q (CFS)	Size	Velocity (Ft/Sec)	length (Ft)	TT (Min)	TT+TC (Min)	
540	530	.47	1.00	.00	.0	15.00	3.83	1.80	15.00	3.83	1.80	1.80	15"	1.47	216.80	2.46	17.46
530	520	.44	.48	.00	.0	15.00	3.83	.80	17.46	3.57	.75	2.55	15"	2.07	92.50	.74	18.21
520	510	.45	2.28	.00	.0	15.00	3.83	3.90	18.21	3.49	3.56	6.10	15"	4.97	45.00	.15	18.36
510	500	.46	1.23	.00	.0	15.00	3.83	2.20	18.36	3.48	2.00	8.10	18"	4.59	150.50	.55	18.90

□

Input File: pp5.inp

Storm Frequency = 2-Year

PRAIRIE POINTE 5

* * * H Y D R A U L I C S * * *

Node	Hyd-Slope (Ft/Ft)	Friction (Ft)	Bend (Ft)	Transition (Ft)	Manhole (Ft)	Deflection (Ft)	Junction (Ft)	Total (Ft)	Hyd-GI Elevation	Desired Elevation	Diff.
500	.00000	.0000	.0000	.0000	.0000	.0000	.0000	.0000	1356.0000	1356.0000	.00
510	.00352	.5301	.0000	.0115	.0000	.0514	.1634	.7564	1356.7560	1361.0000	4.24
520	.00528	.2378	.0000	.0317	.0000	.0089	.6516	.9300	1357.6860	1361.0000	3.31
530	.00092	.0850	.0000	.0033	.0000	.0794	.0703	.2381	1357.9240	1359.7000	1.78
540	.00046	.0996	.0000	.0000	.0000	.0000	.0000	.0996	1358.0240	1359.5000	1.48

Date: 03-27-2003
Time: 10:36:49

Storm Frequency = 2-Year

Input File: pb6.inp

PRAIRIE POINTE 6

* * * H Y D R O L O G Y * * *

Tributary Area		Hydrology Summation				Conduit Data											
Node	C Area	Slope (%)	Length (Ft)	TC (Min)	I (In/Hr)	Q (CFS)	Sum Q (CFS)	TC (Min)	Length (Ft)	Velocity (Ft/Sec)	TT (Min)	TT+TC (Min)					
620	610	.48	2.23	.00	.0	15.00	3.83	4.10	15.00	3.83	4.10	4.10	18"	2.32	44.00	.32	15.32
610	600	.50	1.36	.00	.0	15.00	3.83	2.60	15.32	3.79	2.58	6.68	18"	3.78	146.00	.64	15.96

Input File: pp6.inp

Storm Frequency = 2-Year

PRAIRIE POINTE 6

* * * H Y D R A U L I C S * * *

```

*****
Node  Hyd-Slope  Friction  Bend  Transition  Manhole  Deflection  Junction  Total  Hyd-Gl  Desired  Diff.
      (Ft/Ft)    (Ft)      (Ft)    (Ft)        (Ft)      (Ft)      (Ft)    (Ft)    (Ft)    Elevation  Elevation (Ft)
*****
600    .00000    .0000    .0000    .0000    .0000    .0000    .0000    .0000  1356.0000  1356.0000    .00
610    .00239    .3489    .0000    .0138    .0000    .0112    .2847    .6586  1356.6590  1361.0000    4.34
620    .00090    .0397    .0000    .0000    .0000    .0000    .0000    .0397  1356.6980  1361.0000    4.30
*****

```

Date: 03-27-2003
Time: 10:41:37

STORM1

Input File: pp7.inp

Storm Frequency = 2-Year

PRAIRIE POINTE 7

* * * H Y D R O L O G Y * *

```
*****  
Tributary Area  
*****  
Node to C Area Slope Length TC(0) I(0) Q(0) Q(0) Sum Q  
Node (Ac) (%) (Ft) (Min) (In/Hr) (CFS) (Min) (In/Hr) (CFS) (CFS)  
*****  
720 710 .48 1.44 .00 .0 15.00 3.83 2.60 15.00 3.83 2.60 2.60  
710 700 .48 1.15 .00 .0 15.00 3.83 2.10 15.50 3.77 2.07 4.67  
*****  
Conduit Data  
*****  
Size Velocity Length TT TT+TC  
(Ft) (Ft/Sec) (Ft) (Min) (Min)  
*****  
18" 1.47 44.00 .50 15.50  
18" 2.64 145.00 .91 16.41  
*****
```

□

Input File: pp7.inp

Storm Frequency = 2-Year

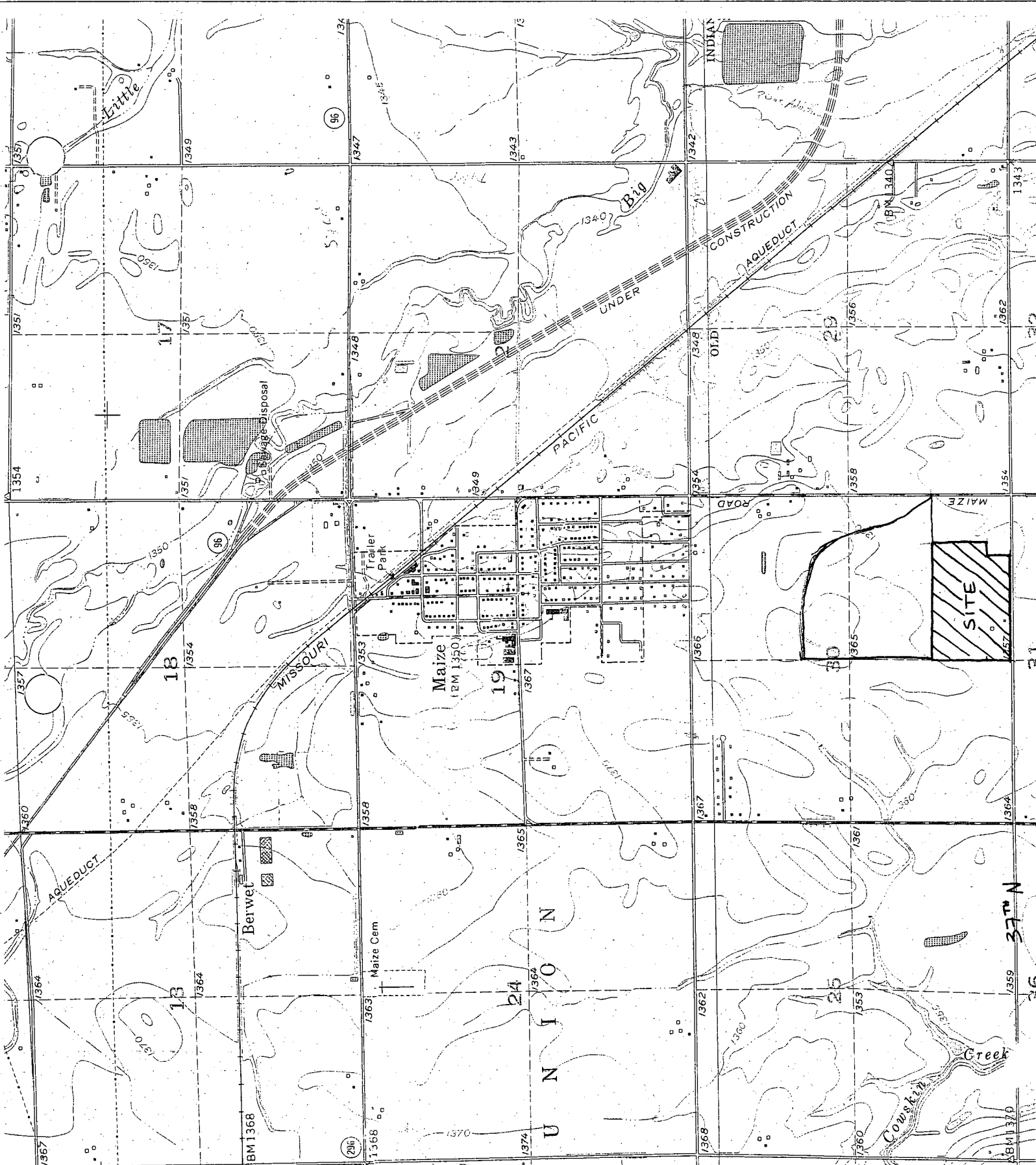
PRAIRIE POINTE 7

* * * H Y D R A U L I C S * * *

```

*****
Node  Hyd-Slope  Friction  Bend  Transition  Manhole  Deflection  Junction  Total  Hyd-G1  Desired  Diff.
      (Ft/Ft)    (Ft)      (Ft)    (Ft)      (Ft)      (Ft)      (Ft)      (Ft)      (Ft)      Elevation  Elevation  (Ft)
*****
700   .00000    .0000    .0000    .0000    .0000    .0000    .0000    .0000  1356.0000  1356.0000    .00
710   .00117    .1695    .0000    .0075    .0000    .0045    .1537    .3351  1356.3350  1361.0000    4.66
720   .00036    .0160    .0000    .0000    .0000    .0000    .0000    .0160  1356.3510  1361.0000    4.65
*****

```

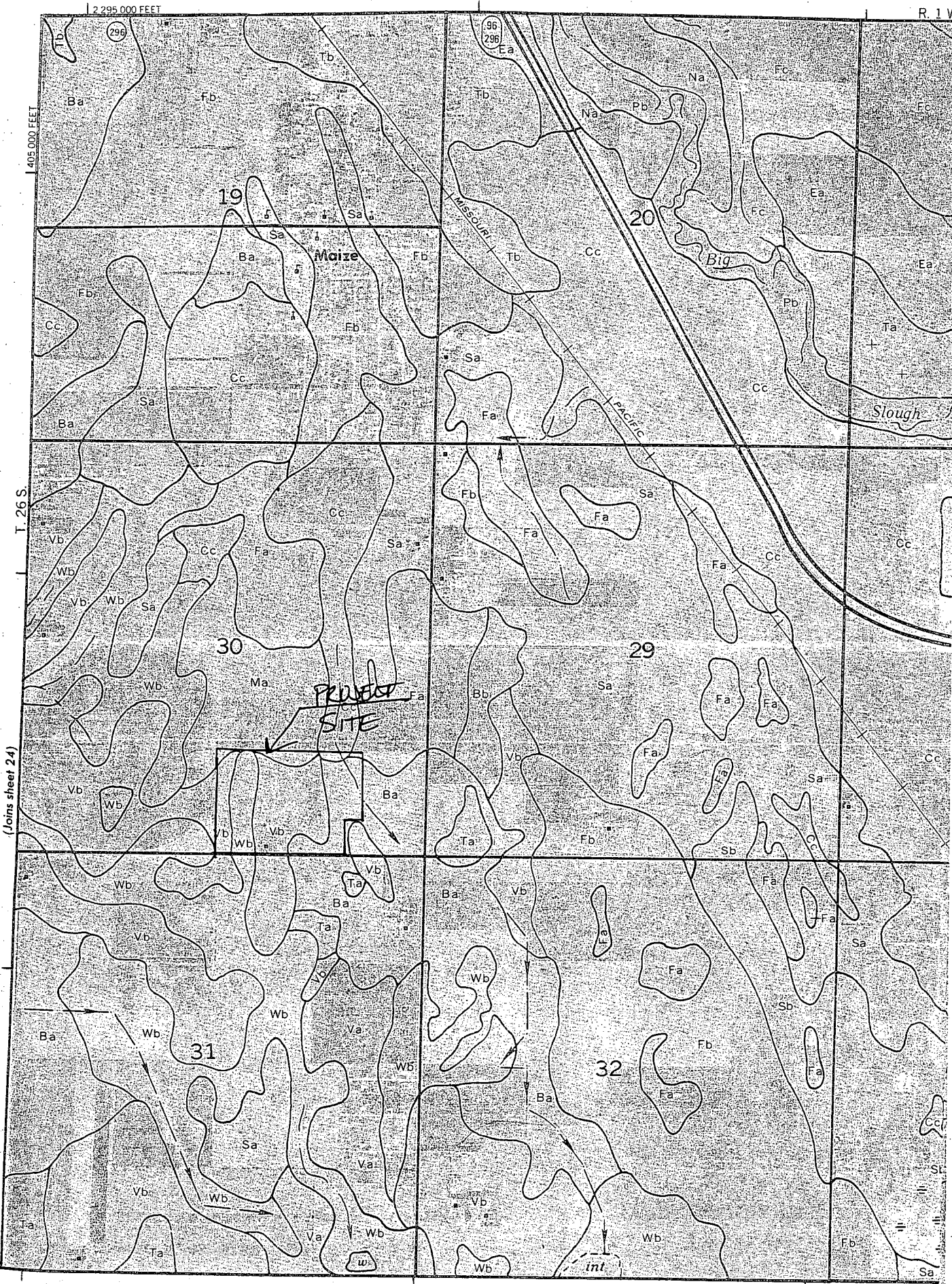


↑
N
1" = 2000'

HUTCHINSON 42 MI.
COLWICH 21 MI.

400 000
FEET

75
E QUADRANGLE
SAS-SEDGWICK CO
DPO



(Joins sheet 24)

PROJECT SITE

int

SOIL LEGEND

SYMBOL	NAME
Aa	Albion-Shellabarger sandy loams, 1 to 4 percent slopes
Ab	Albion and Shellabarger sandy loams, 7 to 15 percent slopes
Ba	Blanket silt loam, 0 to 1 percent slopes
Bb	Blanket silt loam, 1 to 3 percent slopes
Ca	Canadian fine sandy loam
Cb	Canadian-Waldeck fine sandy loams
Cc	Carville fine sandy loam
Cd	Clark-Ost clay loams, 1 to 4 percent slopes
Ce	Clime silty clay, 3 to 6 percent slopes
Ea	Elandco silt loam
Eb	Elandco silt loam, occasionally flooded
Ec	Elandco silt loam, frequently flooded
Fa	Farnum loam, 0 to 1 percent slopes
Fb	Farnum loam, 1 to 3 percent slopes
Fc	Farnum loam, sandy substratum, 0 to 1 percent slopes
Ga	Goessel silty clay, 0 to 1 percent slopes
Gb	Goessel silty clay, 1 to 2 percent slopes
Ia	Irwin silty clay loam, 1 to 3 percent slopes
Ib	Irwin silty clay loam, 3 to 6 percent slopes
Ic	Irwin silty clay loam, 2 to 6 percent slopes, eroded
La	Lesho loam
Lb	Lincoln soils
Ma	Milan loam, 1 to 3 percent slopes
Mb	Milan loam, 3 to 6 percent slopes
Mc	Milan clay loam, 2 to 6 percent slopes, eroded
Na	Naron fine sandy loam
Oc	Owens clay loam, 1 to 3 percent slopes
Od	Owens-Rock outcrop complex, 3 to 10 percent slopes
Pa	Pits
Pb	Plevna fine sandy loam
Pc	Pratt loamy fine sand, undulating
Pd	Pratt-Tivoli complex, rolling
Ra	Renfrow silty clay loam, 1 to 3 percent slopes
Rb	Renfrow silty clay loam, 3 to 6 percent slopes
Rc	Renfrow-Owens clay loams, 1 to 4 percent slopes
Rd	Rosehill silty clay, 1 to 3 percent slopes
Sa	Shellabarger sandy loam, 1 to 3 percent slopes
Sb	Shellabarger sandy loam, 3 to 6 percent slopes
Sc	Shellabarger sandy loam, 3 to 6 percent slopes, eroded
Ta	Tabler silty clay loam
Tb	Tabler-Drummond complex
Ua	Urban land-Canadian complex
Ub	Urban land-Elandco complex
Uc	Urban land-Farnum complex, 0 to 3 percent slopes
Ud	Urban land-Irwin complex, 1 to 3 percent slopes
Ue	Urban land-Tabler complex
Va	Vanoss silt loam, 0 to 1 percent slopes
Vb	Vanoss silt loam, 1 to 3 percent slopes
Vc	Vanoss silt loam, 3 to 6 percent slopes
Vd	Vanoss silt loam, 3 to 6 percent slopes, eroded
Ve	Vernon sandy loam, 1 to 3 percent slopes
Vf	Vernon sandy loam, 3 to 6 percent slopes
Wa	Waldeck sandy loam
Wb	Waurika silt loam



S. TOPEKA - WICHITA, KANSAS 67202
316-262-2691 - FAX 316-262-3003
www.pec1.com - designers@pec1.com

Project 37TH AND MAIZE PLAT

Date 1/29/03

Item _____

By _____

SOIL TYPE

- Vb: VANOSS SILT LOAM, 1-3% SLOPES
- Wb: WAURIKA SILT LOAM
- Ba: BLANKET SILT LOAM, 0-1% SLOPES
- Cc: CARWILE FINE SANDY LOAM
- Fa: FARNUM LOAM, 0-1% SLOPES
- Ma: MILAN LOAM, 1-3% SLOPES

HYDROLOGIC GROUP

B
C
D
E
F

KS-2-5

County	Expected 24-hour Storm Rainfall in Inches						Normal Annual Precipitation Inches
	Storm Frequency in Years						
	100	50	25	10	5	2	
Pawnee	6.6	6.0	5.2	4.5	3.7	2.8	23.3
Phillips	6.0	5.5	4.8	4.1	3.4	2.5	23.6
Pottawatomie	7.5	6.6	5.9	5.1	4.3	3.4	33.6
Pratt	7.2	6.4	5.6	4.8	4.1	3.0	24.6
Rawlins	5.5	5.0	4.3	3.6	3.1	2.3	21.0
Reno	7.4	6.6	5.8	5.0	4.2	3.2	27.7
Republic	6.8	6.0	5.4	4.6	3.9	2.9	28.6
Rice	7.3	6.4	5.6	4.8	4.1	3.0	26.6
Riley	7.4	6.5	5.8	5.1	4.3	3.3	33.5
Rooks	6.1	5.7	4.9	4.1	3.4	2.5	23.9
Rush	6.5	5.9	5.0	4.3	3.6	2.7	23.3
Russell	6.7	5.9	5.2	4.4	3.7	2.8	26.8
Saline	7.3	6.4	5.7	4.9	4.1	3.1	28.4
Scott	5.7	5.3	4.5	3.8	3.2	2.4	20.2
Sedgwick	7.8	7.0	6.1	5.3	4.5	3.5	30.6
Seward	6.0	5.7	4.8	4.2	3.5	2.6	19.8
Shawnee	7.8	6.8	6.1	5.3	4.5	3.5	34.7
Sheridan	5.7	5.3	4.5	3.8	3.2	2.4	21.3
Sherman	5.3	4.8	4.2	3.5	3.0	2.2	16.7
Smith	6.3	5.7	5.0	4.2	3.5	2.6	24.4
Stafford	7.1	6.2	5.5	4.7	4.0	2.9	25.1
Stanton	5.6	5.2	4.5	3.8	3.2	2.4	15.8
Stevens	5.9	5.5	4.7	4.1	3.4	2.5	19.7
Sumner	8.0	7.1	6.2	5.4	4.6	3.6	34.0

ATTACHMENT D

(3 pages)

DRAINAGE CRITERIA

CITY OF WICHITA, KANSAS

RECOMMENDED RUNOFF COEFFICIENTS FOR RATIONAL METHOD
AND PERCENT IMPERVIOUS FOR UNIT HYDROGRAPH METHOD

Land Use or Surface Characteristics	Percent Impervious	Frequency			
		2	5	10	100
1. Business:					
Downtown Areas	95	0.84	0.85	0.87	0.91
Neighborhood Areas	70	0.68	0.69	0.73	0.80
2. Residential:					
<u>Single Family (Soil Group D)</u>					
1/8 Acre	50	0.57	0.61	0.66	0.79
1/4 Acre	38	0.50	0.54	0.62	0.76
1/3 Acre	30	0.46	0.50	0.59	0.73
1/2 Acre	25	0.42	0.48	0.56	0.72
3/4 Acre	22	0.42	0.46	0.55	0.71
1 Acre	20	0.41	0.45	0.54	0.71
<u>Multi-Family (Soil Group D)</u>					
Multi-Unit (detached)	60	0.62	0.66	0.72	0.82
Multi-Unit (attached)	65	0.64	0.68	0.73	0.83
Apartments	75	0.70	0.73	0.79	0.86
<u>Single Family (Soil Group C)</u>					
1/8 Acre	50	0.55	0.58	0.64	0.73
1/4 Acre	38	0.48	0.51	0.57	0.68
1/3 Acre	30	0.43	0.46	0.53	0.65
1/2 Acre	25	0.40	0.43	0.50	0.63
3/4 Acre	22	0.39	0.42	0.49	0.62
1 Acre	20	0.37	0.40	0.48	0.61
<u>Multi-Family (Soil Group C)</u>					
Multi-Unit (detached)	60	0.60	0.63	0.69	0.77
Multi-Unit (attached)	65	0.63	0.66	0.71	0.79
Apartments	75	0.68	0.72	0.77	0.83
<u>Single-Family (Soil Group B)</u>					
1/8 Acre	50	0.52	0.54	0.59	0.67
1/4 Acre	38	0.44	0.46	0.52	0.61
1/3 Acre	30	0.39	0.41	0.47	0.57
1/2 Acre	25	0.36	0.38	0.44	0.54
3/4 Acre	22	0.34	0.36	0.42	0.52
1 Acre	20	0.33	0.35	0.40	0.51
<u>Multi-Family (Soil Group B)</u>					
Multi-Unit (detached)	60	0.58	0.60	0.65	0.72
Multi-Unit (attached)	65	0.61	0.64	0.68	0.75
Apartments	75	0.67	0.70	0.74	0.80

Land Use or Surface Characteristics	Percent Impervious	Frequency				
		<u>2</u>	<u>5</u>	<u>10</u>	<u>25</u>	<u>100</u>
<u>Single Family (Soil Group A)</u>						
1/8 Acre	50	0.47	0.50	0.54		0.60
1/4 Acre	38	0.39	0.41	0.45		0.52
1/3 Acre	30	0.33	0.35	0.39		0.47
1/2 Acre	25	0.30	0.31	0.35		0.44
3/4 Acre	22	0.28	0.29	0.33		0.42
1 Acre	20	0.26	0.28	0.32		0.40
<u>Multi-Family (Soil Group A)</u>						
Multi-Unit (detached)	60	0.55	0.57	0.61		0.67
Multi-Unit (attached)	65	0.58	0.60	0.64		0.70
Apartments	75	0.65	0.68	0.72		0.77
3. Industrial:						
Light Areas	70	0.68	0.69	0.73		0.80
Heavy Areas	80	0.74	0.76	0.79		0.84
4. Playgrounds:	15	0.33	0.35	0.42		0.55
Schools:	40	0.49	0.51	0.56		0.66
Railroad Yard Areas:	30	0.43	0.45	0.50		0.62
7. Undeveloped Urban Areas: Offsite Flow Analysis (when land use not defined)	45	0.52	0.54	0.59		0.68
8. Streets:						
Paved	99	0.87	0.88	0.90		0.93
Gravel	00	0.24	0.26	0.33		0.48
9. Drive, Parking Lots and Walks:	96	0.87	0.87	0.88		0.89
10. Roofs:	90	0.80	0.85	0.90		0.93
11. Urban Lawn Areas (See Note No. 1 below):						
<u>Soil Group A</u>						
Slope less than 1%	00	0.08	0.09	0.13		0.23
Slope 1% to 4%	00	0.12	0.13	0.17		0.27
Slope more than 4%	00	0.16	0.17	0.21		0.31
<u>Soil Group B</u>						
Slope less than 1%	00	0.16	0.26	0.24		0.37
Slope 1% to 4%	00	0.20	0.22	0.28		0.41
Slope more than 4%	00	0.24	0.26	0.32		0.45
<u>Soil Group C</u>						
Slope less than 1%	00	0.24	0.27	0.35		0.51
Slope 1% to 4%	00	0.26	0.29	0.37	0.40	0.53
Slope more than 4%	00	0.28	0.31	0.39		0.55

<u>Land Use or Surface Characteristics</u>	<u>Percent Impervious</u>	<u>Frequency</u>			
		<u>2</u>	<u>5</u>	<u>10</u>	<u>100</u>
<u>Soil Group D</u>					
Slope less than 1%	00	0.28	0.33	0.43	0.63
Slope 1% to 4%	00	0.30	0.35	0.45	0.65
Slope more than 4%	00	0.32	0.37	0.47	0.67

Note No. 1: Coefficients shown in the above table are for pervious open space areas with thick turf which includes pervious areas in parks and cemeteries. Coefficients shown above must be increased 0.02 for use with agricultural pasture areas. Coefficients shown above must be reduced by 0.04 for use with agricultural cultivated areas. Group A soils are well-drained, coarse textured sands with high infiltration rates. Group B soils are moderately well-drained, moderately coarse textured soils with moderate infiltration rates. Group C soils are moderately poor-drained, moderately fine textured soils with slow infiltration rates. Group D soils are poor-drained, fine textured soils with very slow infiltration rates.

GENERAL NOTE: These Rational Formula Coefficients may not be valid for large basins.

RAINFALL INTENSITIES

SEDGWICK COUNTY KANSAS (revised June 1997)

This table contains average rainfall intensities in inches per hour.

DURATION, HR:MIN	RETURN PERIOD						
	1 YR	2 YR	5 YR	10 YR	25 YR	50 YR	100 YR
0:05	4.91	5.64	6.64	7.38	8.48	9.34	10.20
0:06	4.62	5.34	6.33	7.07	8.15	9.00	9.84
0:07	4.38	5.09	6.08	6.80	7.86	8.69	9.52
0:08	4.17	4.87	5.85	6.56	7.60	8.41	9.22
0:09	4.00	4.68	5.63	6.33	7.34	8.14	8.93
0:10	3.84	4.50	5.43	6.11	7.10	7.87	8.64
0:11	3.70	4.34	5.25	5.90	6.86	7.61	8.36
0:12	3.56	4.19	5.07	5.71	6.64	7.36	8.09
0:13	3.44	4.05	4.91	5.53	6.43	7.14	7.84
0:14	3.33	3.92	4.76	5.36	6.24	6.92	7.61
0:15	3.22	3.80	4.62	5.21	6.06	6.73	7.40
0:16	3.12	3.69	4.49	5.07	5.91	6.56	7.21
0:17	3.03	3.58	4.37	4.94	5.76	6.40	7.04
0:18	2.94	3.48	4.26	4.82	5.63	6.26	6.88
0:19	2.85	3.39	4.16	4.71	5.50	6.12	6.74
0:20	2.77	3.30	4.06	4.60	5.38	5.99	6.60
0:21	2.70	3.22	3.97	4.50	5.27	5.87	6.47
0:22	2.63	3.14	3.88	4.41	5.17	5.76	6.35
0:23	2.56	3.07	3.80	4.32	5.07	5.65	6.23
0:24	2.50	3.00	3.72	4.23	4.97	5.54	6.12
0:25	2.44	2.93	3.64	4.15	4.88	5.44	6.01
0:26	2.38	2.87	3.57	4.07	4.79	5.35	5.90
0:27	2.33	2.81	3.50	4.00	4.70	5.26	5.80
0:28	2.27	2.75	3.44	3.92	4.62	5.17	5.71
0:29	2.23	2.69	3.37	3.86	4.54	5.08	5.61
0:30	2.18	2.64	3.31	3.79	4.47	4.99	5.52
0:31	2.14	2.59	3.26	3.72	4.39	4.91	5.43
0:32	2.09	2.54	3.20	3.66	4.32	4.83	5.34
0:33	2.05	2.50	3.14	3.60	4.25	4.76	5.26
0:34	2.02	2.45	3.09	3.54	4.18	4.68	5.18
0:35	1.98	2.41	3.04	3.48	4.12	4.61	5.10
0:36	1.94	2.37	2.99	3.43	4.05	4.54	5.02
0:37	1.91	2.33	2.94	3.38	3.99	4.47	4.95
0:38	1.88	2.29	2.90	3.32	3.93	4.40	4.87
0:39	1.85	2.25	2.85	3.27	3.87	4.34	4.80
0:40	1.82	2.22	2.81	3.23	3.82	4.28	4.73
0:41	1.79	2.18	2.77	3.18	3.76	4.22	4.67
0:42	1.76	2.15	2.73	3.13	3.71	4.16	4.60
0:43	1.73	2.12	2.69	3.09	3.66	4.10	4.54
0:44	1.71	2.09	2.65	3.05	3.61	4.04	4.48
0:45	1.68	2.06	2.62	3.01	3.56	3.99	4.42
0:46	1.66	2.03	2.58	2.96	3.51	3.94	4.36
0:47	1.63	2.00	2.55	2.93	3.47	3.89	4.30
0:48	1.61	1.97	2.51	2.89	3.42	3.84	4.25
0:49	1.59	1.95	2.48	2.85	3.38	3.79	4.20
0:50	1.57	1.92	2.45	2.81	3.34	3.74	4.15

RAINFALL INTENSITY TABLE

SEDGWICK COUNTY KANSAS

(revised June 1997)

This table contains average rainfall intensities in inches per hour.

DURATION, HR:MIN	RETURN PERIOD						
	1 YR	2 YR	5 YR	10 YR	25 YR	50 YR	100 YR
0:51	1.55	1.90	2.42	2.78	3.30	3.70	4.10
0:52	1.53	1.87	2.39	2.75	3.26	3.65	4.05
0:53	1.51	1.85	2.36	2.71	3.22	3.61	4.00
0:54	1.49	1.83	2.33	2.68	3.18	3.57	3.95
0:55	1.47	1.80	2.30	2.65	3.14	3.53	3.91
0:56	1.45	1.78	2.28	2.62	3.11	3.49	3.86
0:57	1.43	1.76	2.25	2.59	3.07	3.45	3.82
0:58	1.41	1.74	2.22	2.56	3.04	3.41	3.78
0:59	1.40	1.72	2.20	2.53	3.01	3.37	3.74
1:00	1.38	1.70	2.17	2.50	2.97	3.34	3.70
1:05	1.30	1.61	2.06	2.38	2.82	3.17	3.52
1:10	1.23	1.53	1.96	2.26	2.69	3.02	3.35
1:15	1.17	1.45	1.87	2.16	2.57	2.89	3.20
1:20	1.11	1.38	1.79	2.06	2.46	2.77	3.07
1:25	1.06	1.32	1.71	1.98	2.36	2.65	2.95
1:30	1.01	1.27	1.64	1.90	2.27	2.55	2.83
1:35	0.97	1.21	1.58	1.83	2.18	2.46	2.73
1:40	0.93	1.16	1.52	1.76	2.10	2.37	2.63
1:45	0.89	1.12	1.46	1.70	2.03	2.29	2.54
1:50	0.86	1.08	1.41	1.64	1.96	2.21	2.46
1:55	0.82	1.04	1.36	1.58	1.89	2.13	2.38
2:00	0.79	1.00	1.31	1.53	1.83	2.07	2.30
2:05	0.76	0.97	1.27	1.48	1.77	2.00	2.23
2:10	0.74	0.93	1.23	1.43	1.72	1.94	2.16
2:15	0.71	0.90	1.19	1.39	1.67	1.88	2.10
2:20	0.69	0.87	1.15	1.35	1.62	1.83	2.04
2:25	0.66	0.85	1.12	1.31	1.57	1.78	1.98
2:30	0.64	0.82	1.09	1.27	1.53	1.73	1.93
2:35	0.62	0.80	1.06	1.24	1.49	1.68	1.88
2:40	0.61	0.78	1.03	1.21	1.45	1.64	1.83
2:45	0.59	0.75	1.01	1.18	1.42	1.60	1.79
2:50	0.57	0.74	0.98	1.15	1.38	1.56	1.74
2:55	0.56	0.72	0.96	1.12	1.35	1.53	1.70
3:00	0.55	0.70	0.94	1.10	1.32	1.49	1.67
3:15	0.51	0.66	0.88	1.03	1.24	1.40	1.57
3:30	0.48	0.62	0.83	0.97	1.17	1.32	1.48
3:45	0.45	0.59	0.78	0.92	1.11	1.26	1.40
4:00	0.43	0.56	0.75	0.88	1.06	1.20	1.34
4:15	0.41	0.53	0.71	0.84	1.01	1.14	1.28
4:30	0.40	0.51	0.68	0.80	0.97	1.10	1.22
4:45	0.38	0.49	0.66	0.77	0.93	1.05	1.17
5:00	0.37	0.47	0.63	0.74	0.89	1.01	1.13
5:15	0.36	0.46	0.61	0.72	0.86	0.98	1.09
5:30	0.35	0.44	0.59	0.69	0.83	0.94	1.05
5:45	0.34	0.43	0.57	0.67	0.81	0.91	1.02
6:00	0.33	0.42	0.55	0.65	0.78	0.88	0.98

ATTACHMENT E

DRAINAGE CRITERIA

CITY OF WICHITA, KANSAS

AVERAGE OVERLAND FLOW VELOCITY FOR USE WITH URBANIZED AREAS

Surface Type	VELOCITY IN FEET/SECOND FOR SLOPES IN PERCENT SHOWN																			
	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0	20.0
Forest with Heavy Ground Litter or Meadow	0.08	0.11	0.14	0.16	0.18	0.19	0.20	0.22	0.23	0.25	0.35	0.42	0.50	0.55	0.60	0.66	0.70	0.75	0.80	1.10
Fallow or Minimum Tillage Cultivation	0.15	0.21	0.26	0.29	0.33	0.35	0.39	0.41	0.44	0.46	0.65	0.80	0.92	1.10	1.20	1.30	1.40	1.50	1.60	2.10
Short Grass Pasture or Lawns	0.23	0.32	0.38	0.44	0.50	0.53	0.58	0.62	0.66	0.70	1.00	1.20	1.40	1.60	1.80	1.90	2.00	2.10	2.20	3.20
Almost Bare Ground	0.32	0.44	0.53	0.62	0.69	0.75	0.82	0.87	0.92	0.98	1.40	1.70	1.90	2.10	2.30	2.50	2.70	2.90	3.10	4.40
Grassed Waterway	0.50	0.68	0.83	0.95	1.10	1.20	1.30	1.40	1.50	1.60	2.20	2.60	3.00	3.40	3.70	4.00	4.30	4.60	4.80	7.00
Paved Areas (Sheet Flow) or Shallow Gutter Flow	0.63	0.89	1.10	1.30	1.50	1.60	1.70	1.80	1.90	2.00	2.80	3.40	4.00	4.50	4.90	5.30	5.70	6.00	6.20	9.00

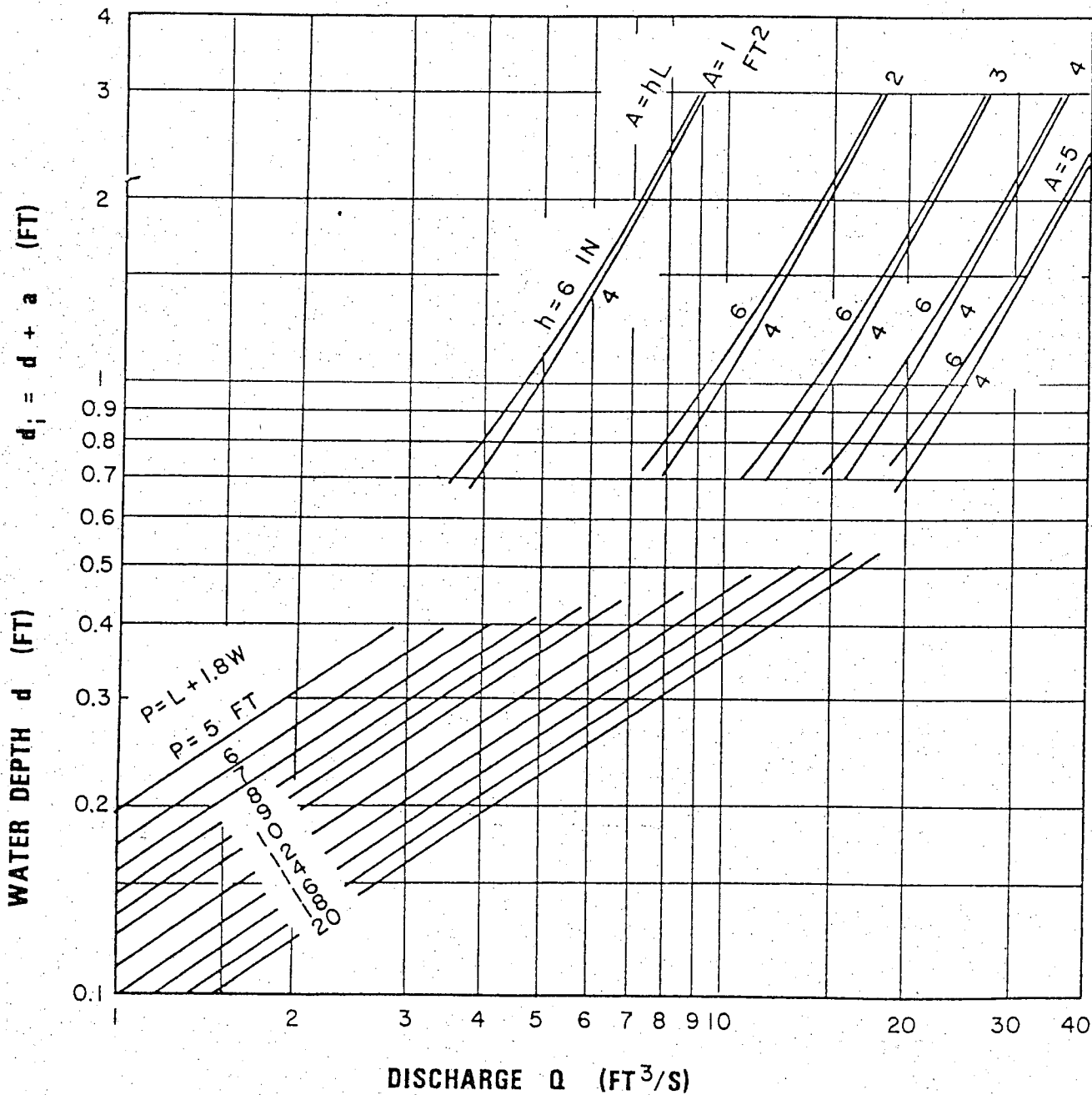
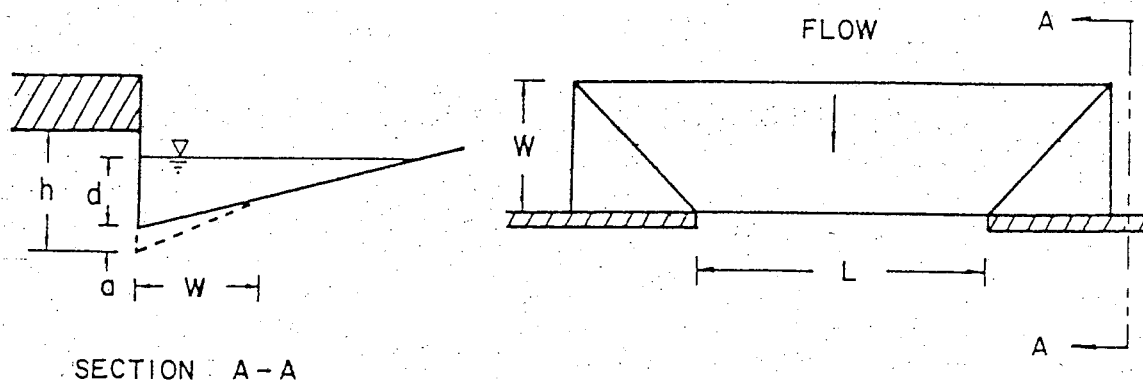


CHART 12. Depressed curb-opening inlet capacity in sump locations.

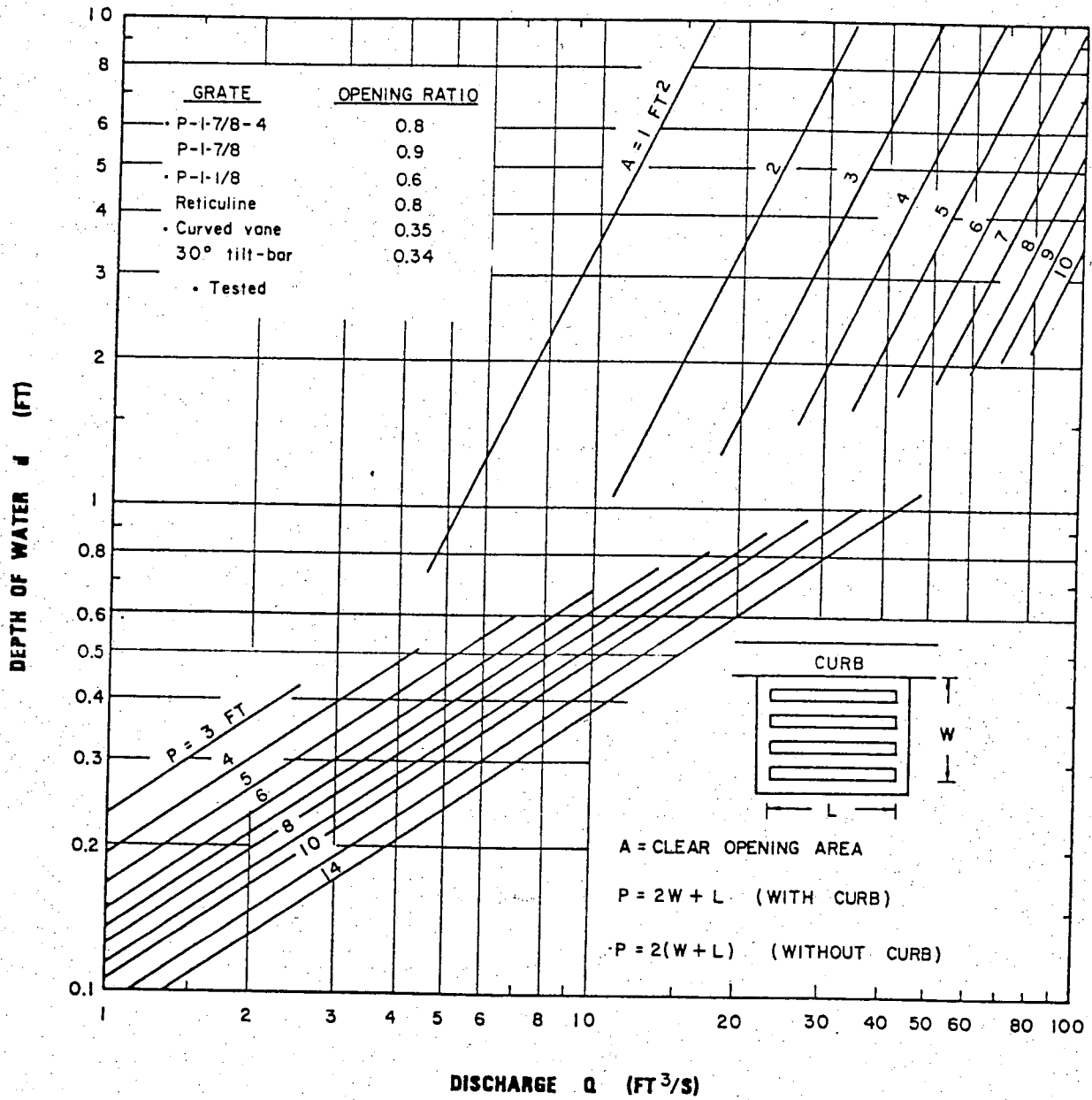


CHART 11. Grate inlet capacity in sump conditions.

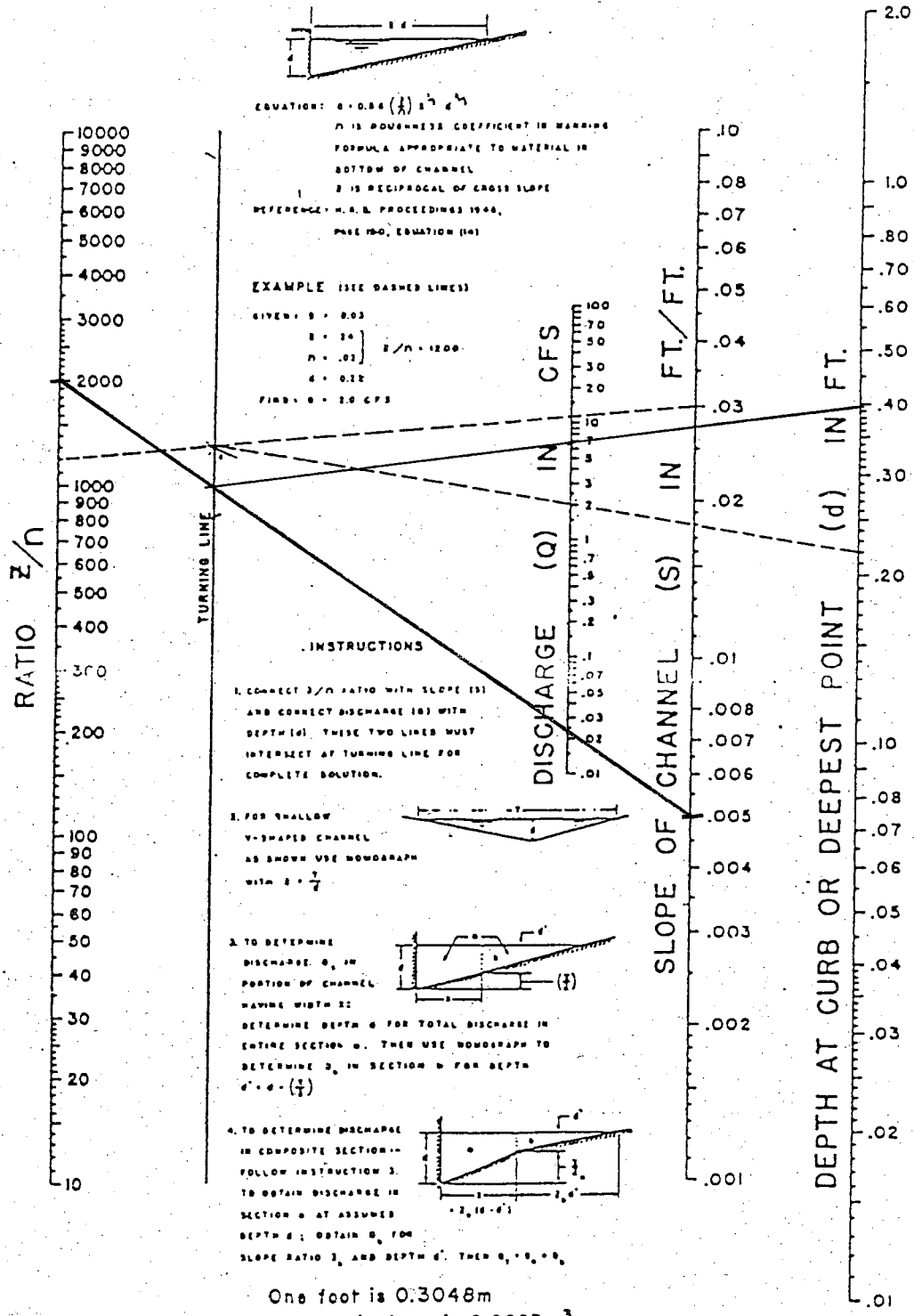
$n = 0.016$
 $Z = \frac{1}{0.031} = 32.26$
 $Z/n = 2016$

@ N 320 $Q_2 = 6.8$
 $S = 0.5\%$

PRAIRIE POINT
 3/25/03

0.4' (0.55') SO OK
 - BY INSPECTION ALL NOTES OK

NOMOGRAPH FOR FLOW IN TRIANGULAR CHANNELS





03 S. TOPEKA • WICHITA, KANSAS 67202

316-262-2691 • FAX 316-262-3003

www.pec1.com • designers@pec1.com

Project _____

Date _____

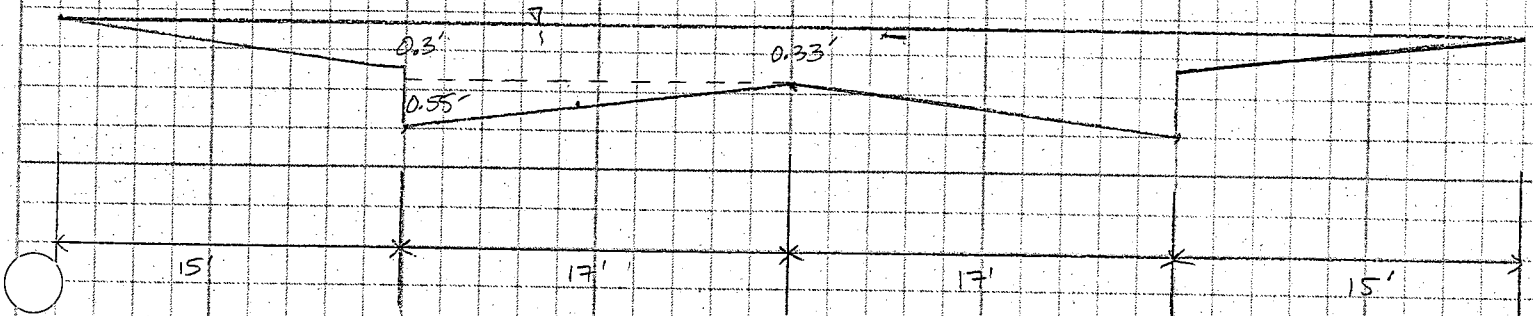
Item _____

By _____

DETERMINE CAPACITIES OF STANDARD CURB STREETS W/
VARIOUS WALK GRADES FOR 100-YR SIDEN ANALYSIS

(64' R.O.W.)

0.3' WALK GRADE



$$n = \frac{(2 \times 14.5 \times 0.03) + (2 \times 3.05 \times 0.013) + (2 \times 15 \times 0.016)}{65.1} = 0.02196$$

$$A = (2 \times \frac{1}{2} \times 15 \times 0.3) + (34 \times 0.33) + (2 \times \frac{1}{2} \times 17 \times 0.52) = 24.56 \text{ SF}$$

$$P = 65.1'$$

$$R = \frac{A}{P} = \frac{24.56 \text{ SF}}{65.1} = 0.377$$

$$R^{2/3} = (0.377)^{2/3} = 0.522$$

$$Q = \frac{1.486}{n} A R^{2/3} S^{1/2}$$

$$Q = \frac{1.486}{0.02196} (24.56) (0.522) (S^{1/2})$$

$$Q = 867.5 (S^{1/2})$$

CURRENT DATE: 04-24-2003
 CURRENT TIME: 15:45:54

FILE DATE: 04-24-2003
 FILE NAME: PP

FHWA CULVERT ANALYSIS
 HY-8, VERSION 6.1

C U L V NO.	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (ft)	OUTLET ELEV. (ft)	CULVERT LENGTH (ft)	BARRELS SHAPE MATERIAL	SPAN (ft)	RISE (ft)	MANNING n	INLET TYPE
1	1350.75	1350.60	370.00	1 RCP	1.25	1.25	.012	CONVENTIONAL
2								
3								
4								
5								
6								

15" RCP FROM
 POND 1 TO POND 2

SUMMARY OF CULVERT FLOWS (cfs) FILE: PP DATE: 04-24-2003

ELEV (ft)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
1354.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1354.73	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1356.36	2.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1358.52	3.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1359.45	4.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1360.27	5.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1361.26	6.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1362.44	7.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1363.80	8.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1365.34	9.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1367.06	10.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
0.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: PP DATE: 04-24-2003

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
1354.00	0.000	0.00	0.00	0.00
1354.73	0.000	1.00	0.00	0.00
1356.36	0.000	2.00	0.00	0.00
1358.52	0.000	3.00	0.00	0.00
1359.45	0.000	4.00	0.00	0.00
1360.27	0.000	5.00	0.00	0.00
1361.26	0.000	6.00	0.00	0.00
1362.44	0.000	7.00	0.00	0.00
1363.80	0.000	8.00	0.00	0.00
1365.34	0.000	9.00	0.00	0.00
1367.06	0.000	10.00	0.00	0.00

<1> TOLERANCE (ft) = 0.010

<2> TOLERANCE (%) = 1.000

PRINT DATE: 04-24-2003
 PRINT TIME: 15:45:54

FILE DATE: 04-24-2003
 FILE NAME: PP

PERFORMANCE CURVE FOR CULVERT 1 - 1(1.25 (ft) BY 1.25 (ft)) RCP

DIS- CHARGE FLOW (cfs)	HEAD- WATER ELEV. (ft)	INLET CONTROL DEPTH (ft)	OUTLET CONTROL DEPTH (ft)	FLOW NORMAL TYPE <F4>	NORMAL DEPTH (ft)	CRIT. DEPTH (ft)	OUTLET DEPTH (ft)	TW DEPTH (ft)	OUTLET VEL. (fps)	TW VEL. (fps)
0.00	1354.00	0.00	3.25	0-NF	0.00	0.00	0.00	3.40	0.00	0.00
1.00	1354.73	0.53	3.98	4-FFt	0.78	0.39	1.25	4.04	0.81	0.00
2.00	1356.36	0.82	5.61	4-FFt	1.25	0.56	1.25	5.40	1.63	0.00
3.00	1358.52	1.05	7.77	4-FFt	1.25	0.69	1.25	7.10	2.44	0.00
4.00	1359.45	1.26	8.70	4-FFt	1.25	0.81	1.25	7.40	3.26	0.00
5.00	1360.27	1.50	9.52	4-FFt	1.25	0.90	1.25	7.40	4.07	0.00
6.00	1361.26	1.78	10.51	4-FFt	1.25	0.99	1.25	7.40	4.89	0.00
7.00	1362.44	2.12	11.69	4-FFt	1.25	1.05	1.25	7.40	5.70	0.00
8.00	1363.80	2.51	13.05	4-FFt	1.25	1.11	1.25	7.40	6.52	0.00
9.00	1365.34	2.97	14.59	4-FFt	1.25	1.17	1.25	7.40	7.33	0.00
10.00	1367.06	3.47	16.31	4-FFt	1.25	1.23	1.25	7.40	8.15	0.00

El. inlet face invert 1350.75 ft El. outlet invert 1350.60 ft
 El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

SITE DATA ***** CULVERT INVERT *****
 INLET STATION 0.00 ft
 INLET ELEVATION 1350.75 ft
 OUTLET STATION 370.00 ft
 OUTLET ELEVATION 1350.60 ft
 NUMBER OF BARRELS 1
 SLOPE (V/H) 0.0004
 CULVERT LENGTH ALONG SLOPE 370.00 ft

***** CULVERT DATA SUMMARY *****
 BARREL SHAPE CIRCULAR
 BARREL DIAMETER 1.25 ft
 BARREL MATERIAL CONCRETE
 BARREL MANNING'S n 0.012
 INLET TYPE CONVENTIONAL
 INLET EDGE AND WALL SQUARE EDGE WITH HEADWALL
 INLET DEPRESSION NONE

REPORT DATE: 04-24-2003
REPORT TIME: 15:45:54

FILE DATE: 04-24-2003
FILE NAME: PP

TAILWATER

TAILWATER RATING CURVE

FLOW (cfs)	W.S.E.(ft)	DEPTH (ft)
0	1354.00	3.40
1	1354.64	4.04
2	1356.00	5.40
3	1357.70	7.10
4	1358.00	7.40
5	1358.00	7.40
6	1358.00	7.40
7	1358.00	7.40
8	1358.00	7.40
9	1358.00	7.40
10	1358.00	7.40

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH	64.00 ft
CREST LENGTH	300.00 ft
OVERTOPPING CREST ELEVATION	1360.17 ft

CURRENT DATE: 04-24-2003
 CURRENT TIME: 13:50:59

FILE DATE: 04-24-2003
 FILE NAME: POINT

FHWA CULVERT ANALYSIS
 HY-8, VERSION 6.1

CULVERT UNDER
 EAST ENTRANCE

C U L V N O.	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (ft)	OUTLET ELEV. (ft)	CULVERT LENGTH (ft)	BARRELS SHAPE MATERIAL	SPAN (ft)	RISE (ft)	MANNING n	INLET TYPE
1	1354.00	1353.80	85.00	1 RCPE	1.92	1.17	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (cfs) FILE: POINT DATE: 04-24-2003

ELEV (ft)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
1354.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1354.66	2.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1355.01	4.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1355.30	6.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1355.68	8.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1356.28	10.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1356.92	12.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1357.63	14.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1358.44	16.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1359.36	18.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
1360.40	20.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
0.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: POINT DATE: 04-24-2003

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
1354.00	0.000	0.00	0.00	0.00
1354.66	0.000	2.00	0.00	0.00
1355.01	0.000	4.00	0.00	0.00
1355.30	0.000	6.00	0.00	0.00
1355.68	0.000	8.00	0.00	0.00
1356.28	0.000	10.00	0.00	0.00
1356.92	0.000	12.00	0.00	0.00
1357.63	0.000	14.00	0.00	0.00
1358.44	0.000	16.00	0.00	0.00
1359.36	0.000	18.00	0.00	0.00
1360.40	0.000	20.00	0.00	0.00

<1> TOLERANCE (ft) = 0.010

<2> TOLERANCE (%) = 1.000

PRINT DATE: 04-24-2003
 PRINT TIME: 13:50:59

FILE DATE: 04-24-2003
 FILE NAME: POINT

PERFORMANCE CURVE FOR CULVERT 1 - 1(1.92 (ft) BY 1.17 (ft)) RCPE

DIS-CHARGE FLOW (cfs)	HEAD- WATER ELEV. (ft)	INLET CONTROL DEPTH (ft)	OUTLET CONTROL DEPTH (ft)	FLOW TYPE <F4>	NORMAL DEPTH (ft)	CRIT. DEPTH (ft)	OUTLET DEPTH (ft)	TW DEPTH (ft)	OUTLET VEL. (fps)	TW VEL. (fps)
0.00	1354.00	0.00	0.00	0-NF	0.00	0.00	0.00	0.10	0.00	0.00
2.00	1354.66	0.59	0.66	2-M2c	0.48	0.42	0.42	0.10	3.27	0.00
4.00	1355.01	0.91	1.01	2-M2c	0.74	0.62	0.62	0.10	4.05	0.00
6.00	1355.30	1.21	1.30	2-M2c	1.04	0.78	0.78	0.10	4.79	0.00
8.00	1355.67	1.55	1.67	2-M2c	1.17	0.91	0.91	0.10	5.43	0.00
10.00	1356.28	1.98	2.28	2-M2c	1.17	1.00	1.00	0.10	6.19	0.00
12.00	1356.92	2.50	2.92	2-M2c	1.17	1.09	1.09	0.10	6.90	0.00
14.00	1357.63	3.13	3.63	6-FFc	1.17	1.17	1.17	0.10	7.87	0.00
16.00	1358.44	3.88	4.44	6-FFc	1.17	1.17	1.17	0.10	8.99	0.00
18.00	1359.37	4.75	5.37	6-FFc	1.17	1.17	1.17	0.10	10.12	0.00
20.00	1360.40	5.73	6.40	6-FFc	1.17	1.17	1.17	0.10	11.24	0.00

El. inlet face invert 1354.00 ft El. outlet invert 1353.80 ft
 El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

SITE DATA ***** CULVERT INVERT *****

INLET STATION 0.00 ft
 INLET ELEVATION 1354.00 ft
 OUTLET STATION 85.00 ft
 OUTLET ELEVATION 1353.80 ft
 NUMBER OF BARRELS 1
 SLOPE (V/H) 0.0024
 CULVERT LENGTH ALONG SLOPE 85.00 ft

***** CULVERT DATA SUMMARY *****

BARREL SHAPE ELLIPTICAL
 BARREL SPAN 1.92 ft
 BARREL RISE 1.17 ft
 BARREL MATERIAL CONCRETE
 BARREL MANNING'S n 0.012
 INLET TYPE CONVENTIONAL
 INLET EDGE AND WALL SQ. EDGE WITH HEADWALL
 INLET DEPRESSION NONE

EVENT DATE: 04-24-2003
CURRENT TIME: 13:50:59

FILE DATE: 04-24-2003
FILE NAME: POINT

TAILWATER

CONSTANT WATER SURFACE ELEVATION
1353.90

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH	70.00 ft
CREST LENGTH	300.00 ft
OVERTOPPING CREST ELEVATION	1356.30 ft

CURRENT DATE: 08-26-1999
 CURRENT TIME: 09:45:29

FILE DATE: 08-26-1999
 FILE NAME: 37MZW

MAIZE ROAD
 West CULVERTS

FHWA CULVERT ANALYSIS
 HY-8, VERSION 3.2

C	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
U								
L	INLET	OUTLET	CULVERT	BARRELS				
V	ELEV.	ELEV.	LENGTH	SHAPE	SPAN	RISE	MANNING	INLET
	(FT)	(FT)	(FT)	MATERIAL	(FT)	(FT)	n	TYPE
1	52.19	52.11	80.00	3 RCPE	2.50	1.58	.012	CONVENTIONAL
2								
3								
4								
5								
6								

A = 140 acres
 10% Q = 55 cfs
 overlap @ 54.
 By putting in 3-30" RCPE
 I am increasing the area
 from 5.0' to 9.9'

SUMMARY OF CULVERT FLOWS (CFS) FILE: 37MZW DATE: 08-26-1999

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
52.19	0	0	0	0	0	0	0	0	1
53.08	12	12	0	0	0	0	0	0	1
53.53	24	24	0	0	0	0	0	0	1
53.93	36	36	0	0	0	0	0	0	1
54.41	48	48	0	0	0	0	0	0	1
54.84	60	57	0	0	0	0	0	3	6
55.01	72	60	0	0	0	0	0	12	4
55.15	84	62	0	0	0	0	0	22	4
55.27	96	64	0	0	0	0	0	31	3
55.38	108	66	0	0	0	0	0	41	3
55.49	120	68	0	0	0	0	0	51	3
54.72	54	54	0	0	0	0	0	0	OVERTOPPING

There is a pipe about at
 the intersection but the
 north end of the pipe is
 out of the ground and it is
 not really a pipe. I
 ignored it.

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: 37MZW DATE: 08-26-1999

HEAD ELEV(FT)	HEAD ERROR(FT)	TOTAL FLOW(CFS)	FLOW ERROR(CFS)	% FLOW ERROR
52.19	0.00	0	0	0.00
53.08	0.00	12	0	0.00
53.53	0.00	24	0	0.00
53.93	0.00	36	0	0.00
54.41	0.00	48	0	0.00
54.84	-0.00	60	0	0.73
55.01	-0.00	72	0	0.58
55.15	-0.01	84	0	0.23
55.27	-0.00	96	1	0.61
55.38	-0.00	108	1	0.48
55.49	-0.00	120	0	0.35

<1> TOLERANCE (FT) = 0.010

<2> TOLERANCE (%) = 1.000

CURRENT DATE: 08-26-1999
TIME: 09:45:29

FILE DATE: 08-26-1999
FILE NAME: 37MZW

TAILWATER

***** REGULAR CHANNEL CROSS SECTION *****

BOTTOM WIDTH (FT) 6.00
SIDE SLOPE H/V (X:1) %20.0
CHANNEL SLOPE V/H (FT/FT) 0.001
MANNING'S N (.01-0.1) 0.020
CHANNEL INVERT ELEVATION (FT) 52.11
CULVERT NO.1 OUTLET INVERT ELEVATION 52.11 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	52.11	0.000	0.00	0.00
12.00	52.69	0.270	1.17	0.04
24.00	52.90	0.277	1.39	0.05
36.00	53.05	0.281	1.55	0.06
48.00	53.17	0.284	1.66	0.07
60.00	53.27	0.287	1.76	0.07
72.00	53.37	0.290	1.84	0.08
84.00	53.45	0.292	1.91	0.08
96.00	53.52	0.293	1.98	0.09
108.00	53.59	0.295	2.04	0.09
120.00	53.66	0.297	2.09	0.10

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE PAVED
EMBANKMENT TOP WIDTH (FT) 28.00
CREST LENGTH (FT) 25.00
OVERTOPPING CREST ELEVATION (FT) 54.72

DRAINAGE PLAN PRAIRIE POINTE AN ADDITION TO WICHITA, SEDGWICK COUNTY, KANSAS

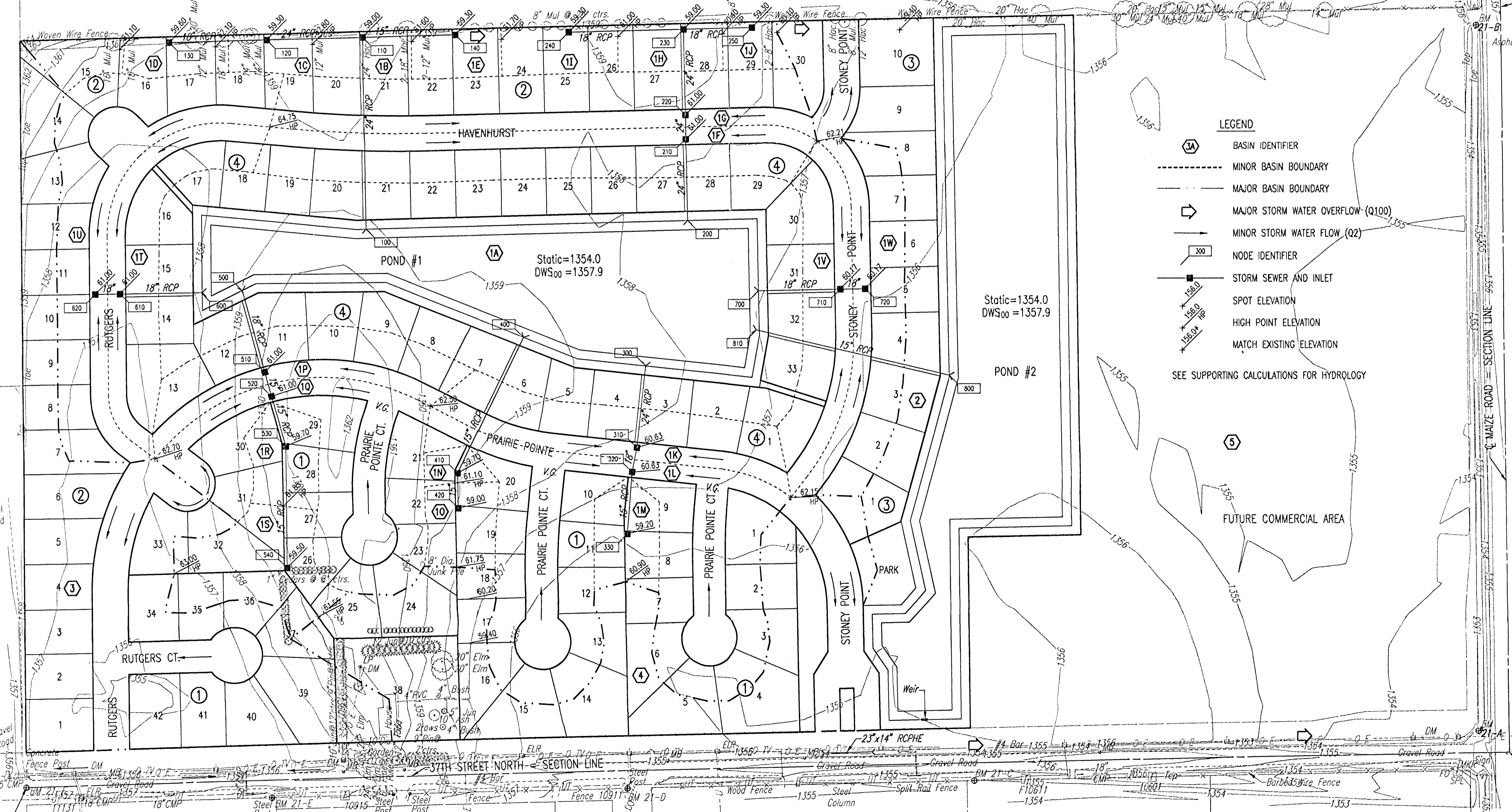
Center of
Sec. 30, T26S, R1W
Found Slope 30" Deep
Reset 3/4" Pipe
w/PEC Cap

- BENCHMARKS:**
- BM 21-A CHISELED SQUARE ON NORTH END 30"x19" RCP ON WEST SIDE OF TRIPLE PIPE AT THE NORTHWEST CORNER OF 37TH ST. NORTH AND MAIZE ROAD.
ELEV. = 1354.18 N.G.V.D.
(166.78 CITY DATUM)
 - BM 21-C STEP NAILS ON NORTH FACE OF CORNER POST ON SOUTH SIDE OF 37TH ST. NORTH 950± WEST OF 37TH ST. NORTH AND MAIZE ROAD.
ELEV. = 1356.24 N.G.V.D.
(168.84 CITY DATUM)
 - BM 21-D CHISELED SQUARE ON CONCRETE BASE OF BRICK FENCE POST ON SOUTH SIDE OF 37TH ST. NORTH 1070± EAST OF 1/2 MILE LINE.
ELEV. = 1355.56 N.G.V.D.
(168.16 CITY DATUM)
 - BM 21-E CHISELED SQUARE ON CONCRETE BASE OF BRICK FENCE POST ON SOUTH SIDE OF 37TH ST. NORTH 440± EAST OF 1/2 MILE LINE.
ELEV. = 1357.01 N.G.V.D.
(169.61 CITY DATUM)
 - BM 21-F 1" PIPE AT Q OF 37TH ST. NORTH = 1/4 CORNER 1/2 MILE WEST OF 37TH ST. NORTH AND MAIZE ROAD.
ELEV. = 1357.24 N.G.V.D.
(169.84 CITY DATUM)

MINIMUM OPENINGS	ELEVATION (N.G.V.D.)	CITY DATUM
BLOCK 1		
LOTS 4-6, 13-16, 40-42	1359.0	171.6
LOT 39	1360.0	172.6
LOTS 1-3, 7, 17, 24	1360.5	173.1
LOTS 8-12, 18-23	1361.9	174.5
LOT 25	1361.6	174.2
LOTS 28-30	1362.3	174.9
LOTS 26-27, 31-37	1362.6	175.2
BLOCK 2		
LOTS 1-6	1359.0	171.6
LOTS 7-10	1360.0	172.6
LOTS 11-12	1361.0	173.6
LOTS 27-30	1361.6	174.2
LOTS 13-14, 24-26	1362.0	174.6
LOTS 20-23	1362.7	175.3
LOTS 15-19	1363.8	176.4
BLOCK 3		
LOTS 1-10	1360.5	173.1
BLOCK 4		
LOTS 1-33	1360.5	173.1

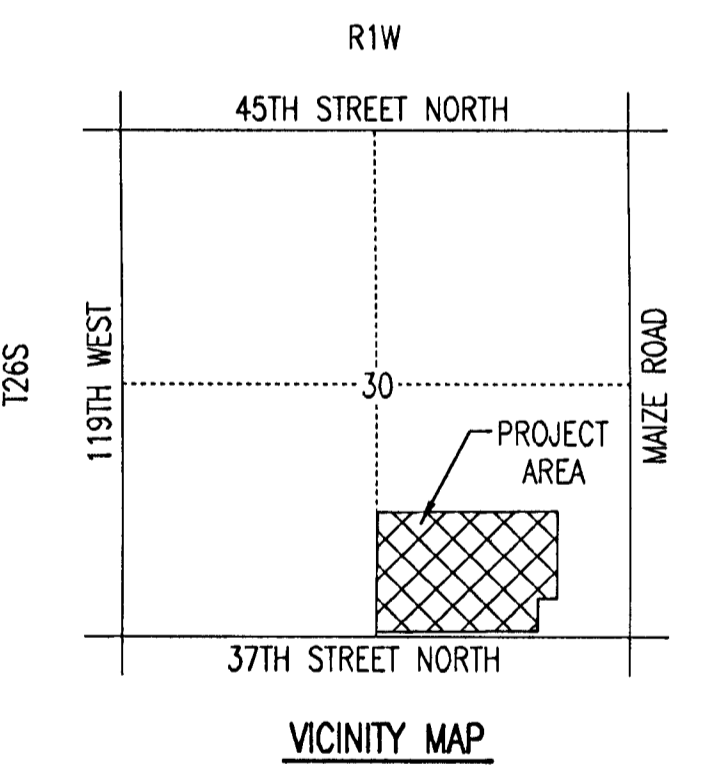
E 1/4 Corner, Sec. 30
Twp. 26S, R1W
Found #4 Bar w/ Moehring
Cap

N.E. Cor. SE 1/4, SE 1/4
Sec. 30, T26S, R1W
No Monument Found



- LEGEND**
- ① BASIN IDENTIFIER
 - MINOR BASIN BOUNDARY
 - MAJOR BASIN BOUNDARY
 - ➔ MAJOR STORM WATER OVERFLOW (Q100)
 - ➔ MINOR STORM WATER FLOW (Q2)
 - 300 NODE IDENTIFIER
 - STORM SEWER AND INLET
 - SPOT ELEVATION
 - HIGH POINT ELEVATION
 - MATCH EXISTING ELEVATION
- SEE SUPPORTING CALCULATIONS FOR HYDROLOGY

SCALE: 1" = 100'



DATE: 04-25-2003 03:54:56 pm
PROJECT: 611DD 02726.dwg DRAINAGE
DRAWN BY: JAVELLE

JAMES M. & TERRIE M. RAMSEY
Gravel Road
ZONED: RR

DAVID D. CRANMER
ZONED: SF-20

ANGELA A. & KELLY E. KENDALL
ZONED: SF-20

MARY GRADY REV. TRUST
ZONED: SF-20

MUNIR & BARBARA RAZZAQ
ZONED: SF-20

DANE & JENNIFER WADLEY
ZONED: SF-20

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