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## **SUPPLEMENTAL DRAINAGE STUDY**

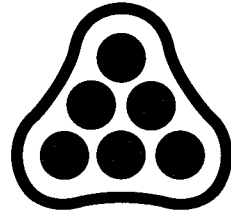
**FOREST LAKES; REFLECTION RIDGE**  
**6TH, 7TH AND 8TH ADDITIONS;**  
**UNPLATTED LAND IN NORTHWEST QUARTER**  
**SECTION 4 AND SOUTHWEST QUARTER SECTION 33**

PREPARED BY

PROFESSIONAL ENGINEERING CONSULTANTS, P.A.  
WICHITA, KANSAS

FEBRUARY 10, 1993

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February 10, 1993

Mr. Michael E. Lindebak, P.E.  
City Engineer  
7th Floor, City Hall  
455 N. Main  
Wichita, KS 67202

Attention: Ms. Vicky Huang, P.E.

Reference: Forest Lakes Drainage Plan  
PEC Project No. 32-92431-2273

Dear Mr. Lindebak:

In accordance with your request in our meeting of December 6, 1992, transmitted herewith are two copies of a Supplemental Drainage Report relative to Forest Lakes Addition. The purpose of the report is to address the interrelationship of developments in the area and the ultimate impact on drainage.

We would be happy to review this report with you upon your request at a mutually convenient time.

Very truly yours,

PROFESSIONAL ENGINEERING CONSULTANTS, P.A.

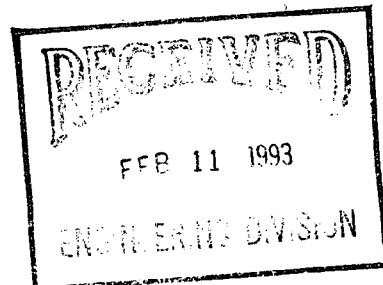
*Michael W. Berry*

Michael W. Berry, P.E.  
Manager  
Land Development Division

MWB:st

Encl.

cc: Marvin Schellenberg  
Harlan D. Foraker, P.E.



## FOREST LAKES

### Major Channels/Structures

In the development of the Drainage Plan for this plat, consideration must be given to routing of the major flows through the development. These flows and hydrographs were developed using the SCS methodology in the US Army Corps of Engineers HEC-1 hydrologic computer model. Reference is made to Figure A. This figure shows a schematic of storm routing thorough existing/proposed channels, structures, and ponds.

The Drainage Plan for Reflection Ridge 6th Addition provided a pond at the southeast corner of 29th and Ridge, and a box culvert at Wild Rose. All of these features have been constructed. The channel and culvert were sized to convey the 100-year flow from the area now platted as Reflection Ridge 7th and 8th Additions, estimated to be 568 cfs at hydrograph time 6.1 hr. This flow is depicted as B on Figure A, and the Wild Rose culvert is depicted as Structure No. 4 (existing 3 - 8' X 4' RCBB).

In the 6th Addition Drainage Plan, areas lying north of 29th St. were assumed to be collected north of the roadway and conveyed across 29th St. to Lake #3 in the 6th Addition. This lake and downstream structure were sized to accommodate these flows (Flows B and C on Figure A).

The property currently owned by Mr. Kastens lying in the NW Quarter of Section 4, has not been studied in as much detail. A preliminary plat layout dated 8/3/92, along with a preliminary drainage study dated 9/30/92, are available. (See Exhibit B in map pocket.)

The referenced drainage study proposes a series of ponds lying along the present KG&E transmission line. For purposes of this study, no detention has been assumed and the northerly 70 acres is assumed to flow to the northeast corner of the property. The reader should note that in the Preliminary Drainage Study, a portion of the same 70 acres is assumed to flow south and east through the golf course driving range. However, for this report it was felt that the exact ridge line between basins is not definite based on the design performed to date. Thus, a conservative (large) value of drainage area has been assumed.

In the development of the Forest Lakes Drainage Plan, the area north of 29th St. has been studied in greater detail. The basin is composed of two subareas: the first containing 195 acres flows to a poorly defined channel flowing through the plat. This drainage is intercepted near

the northwest corner of the plat and is conveyed through a series of culverts and ponds to discharge to 29th St. just east of Wild Rose (Flow C).

The west portion of the basin is defined by a ridge line along the 1340 elevation contour. This area is rolling, but has no defined channel. The natural low area discharges to 29th St. at the existing homestead in the SW corner of the SE 1/4 of Section 33 (the area being excepted from the plat). This flow is designated as A and is estimated to be 444 cfs at hydrograph time 6.9 hours.

Both flows A and C must be conveyed to the 6th Addition Pond #3 at 29th and Ridge. Open channels provide the most economical alternative, and are compatible with the developments' water amenities. Rather than providing a second open channel on the north side of 29th, conveyance of flows across 29th St. to the south side is proposed.

The proposed system has the following components:

Structure No. 6. Future box culvert beneath 29th St. to convey flows from the area west of Forest Lakes to the south road ditch. This culvert will be required when the SW 1/4 of Section 33 develops, and would be the responsibility of that developer. This structure was not sized for this report.

An Open Channel from Structure No. 6 to Structure No. 5 (Tee Time South). This channel would be sized to carry flow A and Flow D. This channel is a ten-foot trapezoidal channel on 1% grade. To carry Flow D (Q100 = 290 cfs),  $d = 2.1'$  for Retardance Class E, requiring a 3.0' deep ditch. To carry both A and D (Q100 = 486 cfs),  $d = 2.8'$  for Retardance Class E and a 4.0' deep ditch is required. The ditch will require a minimum 60' half street right-of-way.

Structure No. 5. Future box culvert beneath Tee Time (south) at 29th St. This structure would carry Flow A and D (Q100 = 486 cfs) and is sized as 3 - 7' X 4' RCB.

An Open Channel from Structure No. 5 to Wild Rose (Structure No. 4) This channel would be sized to convey Flows A, B, and D (Q100 = 608 cfs). A ten foot trapezoidal channel to be provided on 0.8% slope. For Class E Retardance,  $d = 3.2'$  and a 4.25' ditch is required, necessitating a minimum 62' half street right-of-way (75' has been provided).

Structure No. 4. The existing Wild Rose culvert has been analyzed and is shown to be at capacity for Flow B Q100 = 608 cfs, with a headwater elevation = 1326.9. The road grade (at R/W line) should be set at 1327.0; in addition, the south side of the road ditch should be protected by a berm at elevation 1327 (139.82 City).

Structure No. 3. This structure serves as the outlet for Forest Lakes Pond No. 3. It has been sized as a 2 - 8' X 4' RCB carrying Q100 = 216 cfs at a headwater elevation of 1324.90, assuming a free discharge.

Open Channel from Structure Nos. 3 and 4 to Lake No. 3 in the 6th Addition. In the course of the investigation, it was determined that the Lake No. 3 in the 6th Addition causes a high tailwater condition for the outlet from Lake No. 3 in Forest Lakes. Therefore, these two lakes have been modeled to function together as one large pond.

Structure Nos. 2 and 1 (Not shown on Figure A). These structures are the outlet control structures for Ponds Nos. 2 and 1 respectively in Forest Lakes, are in discussed in the Forest Lakes Drainage Plan (February 1, 1993).

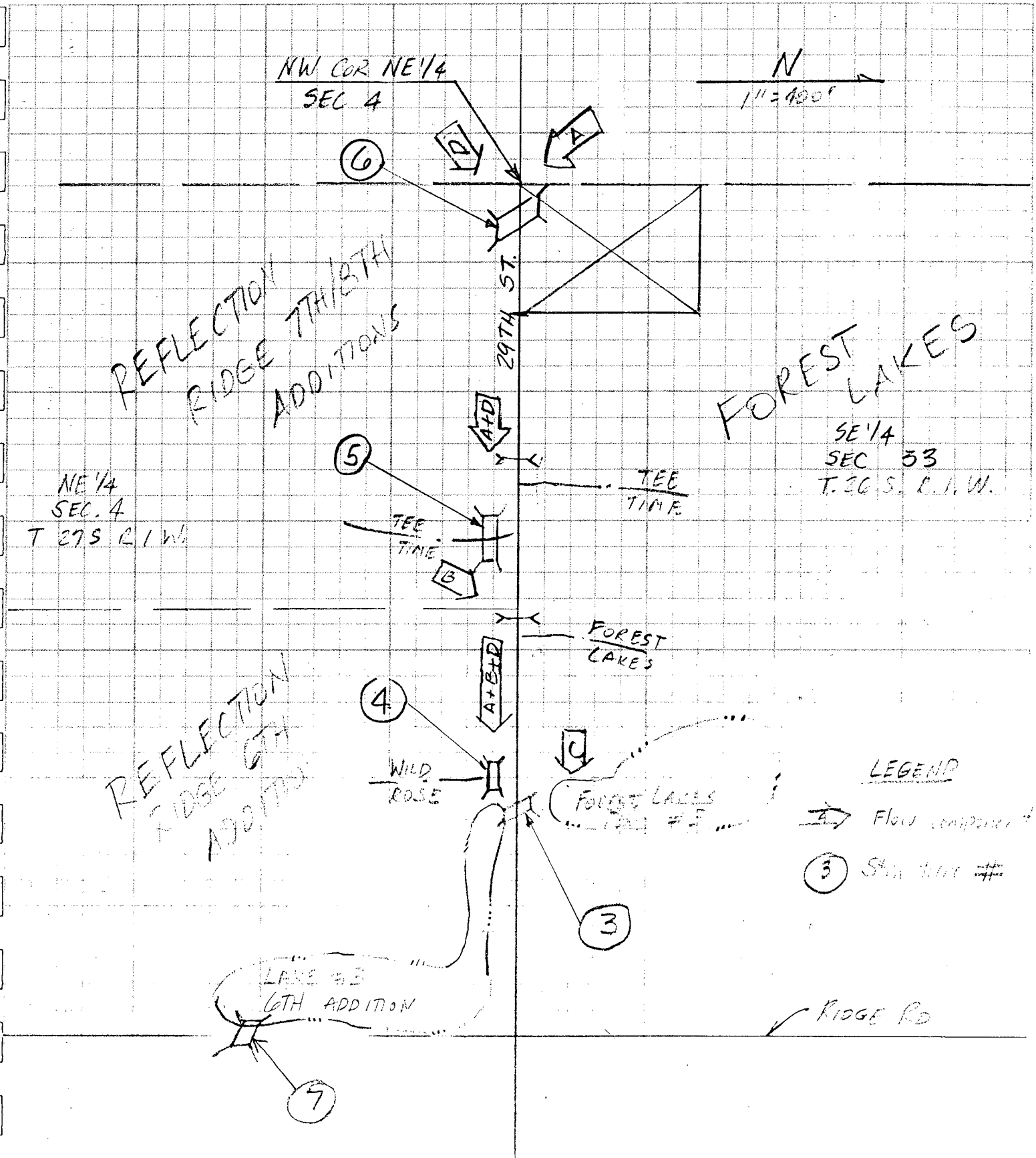
Structure No. 7. In the HEC-1 hydrologic analysis included herein, the outlet across Ridge Road was evaluated. The existing outlet is a single 10' X 3' reinforced concrete box culvert. Under existing outlet conditions and with the ultimate development, the 100-yr. design water surface in Pond No. 3 is 1327.27. This is to be compared to the minimum pad elevation in Reflection Ridge 6th Addition of 1328.00. Thus, approximately 9" of freeboard is provided to homes in the 6th Addition without any additional culvert capacity at Ridge Road.

The ultimate proposed outlet at this location is a 3 - 10' X 3' reinforced concrete box bridge. One barrel must be added at the time of development in the NW 1/4 Sec. 4, and the other at the time of development in the SW 1/4 Sec. 33. If Ridge Road is to be improved to arterial standards, the additional barrels should be added at that time.

Ditch capacity charts and printed results of culvert analysis using the FHWA computer program HY-8 are included. Please note that the computer results do not exactly agree with the results of the HEC-1 analysis; they do agree to within  $\pm 0.1$  ft., which is of sufficient accuracy for hydraulic analysis.



REV 2/8/93  
 Date 10/25/92 MMB Page \_\_\_\_\_ of \_\_\_\_\_  
 Project FOREST LAKES  
 Item MAJOR CHANNELS FIGURE A





Date 10-24-92 MMB Page \_\_\_\_\_ of \_\_\_\_\_

Project FOREST LAKES PLAT

Item OFF SITE DRAINAGE BASIN

WEST OF PLAT & N/O 29TH ST.

SCS PARAMETERS

15% D SOIL

85% B SOIL

CULTIVATED - WHEAT 0% INT 0% HLM

GOOD COND., straight row + residue

$$CN = 0.15 \times 83 + 0.85 \times 72 = 73.65 \text{ SAY } 74.$$

$$CN = 74$$

DETERMINE LAG

No defined channel.  $L = 5800 \text{ ft.}$

Hydraulically most remote point @ NW cor sec 33 Elev 1343

Outlet @ SW cor SE 1/4 Sec 33 (Farmstead) Elev 1336

$$7/5800 = 0.12\%$$

7 ft

ESTIMATE 1 FT/SEC OVERLAND FLOW VELOCITY

$$T_c = \frac{5800}{1} = 5800 \text{ SEC} = 97 \text{ MIN} = 1.6 \text{ HR}$$

$$\text{LAG} = 0.6 T_c = \frac{6}{10} \times 1.6 = 0.97 \text{ HR}$$

FROM PROPOSED CONDITION HEC-1 MODEL (AREA W FOR LK)

$Q_5 = 182 \text{ CFS}$

$Q_{10} = 239 \text{ CFS}$

$Q_{50} = 381 \text{ CFS}$

$Q_{100} = 444 \text{ CFS}$

TIME TO PEAK = 6.9 HR

TIME TO PEAK = 6.9 HR

TIME TO PEAK = 6.9 HR

TIME TO PEAK = 6.9 HR

SEE HEC-1 PRINTOUT  
FOR PROPOSED CONDITIONS



Date 1/30/93 NMB Page \_\_\_\_\_ of \_\_\_\_\_

Project FOREST LAKES DRAINAGE PLAN

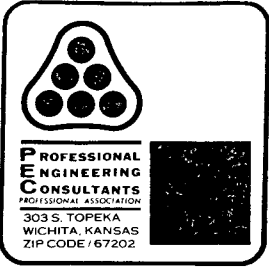
Item EVALUATION OF TW CONDITIONS

CHECK STRUCTURE NO 3 TAILWATER CONDITION FROM POND NO 4. (Q100 ONLY)

TIME	Q OUT POND 3	STAGE POND 3	3 BBL STAGE POND 4	4 BBL STAGE POND 4
1224	143	1324.3	1324.9	1323.9
1236	171	1324.6	1325.3	1324.0
1248	191	1324.8	1325.5	1324.0
1300	207	1324.9	1325.4	1323.9
1312	215	1324.9	1325.3	1323.8
1324	215	1324.9	1324.9	1323.3
1336	208	1324.9	1324.4	1323.0

CONCLUSION:

FOREST LAKES POND # 3 & REFLECTION RIDGE 6TH POND FLOW TOGETHER.



Date 2/4/93 MWB Page \_\_\_\_\_ of \_\_\_\_\_

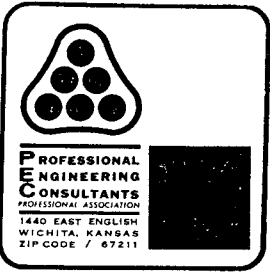
Project FOREST LAKES

Item COMBINED STORAGE

	REFLECTOR RIDGE STA POND # 4 STORAGE	FOREST LAKE POND # 3 STORAGE	Σ
ELEV			
1319.6	0		0
1321.6	5.4		5.4
1322	6.6*	0	6.6
1322.2	7.2		
1322.9	9.3		
1323.6	11.6	8.9	20.5
1324.0		11.2	
1324.4	14.3	13.5	27.8
1324.8		15.9	
1325.2		18.3	
1325.4	18.0	19.5*	37.5
1325.6		20.7	
1325.7	19.1		
1326.0	20.3*	23.2	43.5
1326.5	22.4		
1327.0	24.8	25*	50*
1327.2	25.8		
1328	30.4	30*	60*

\* Estimated

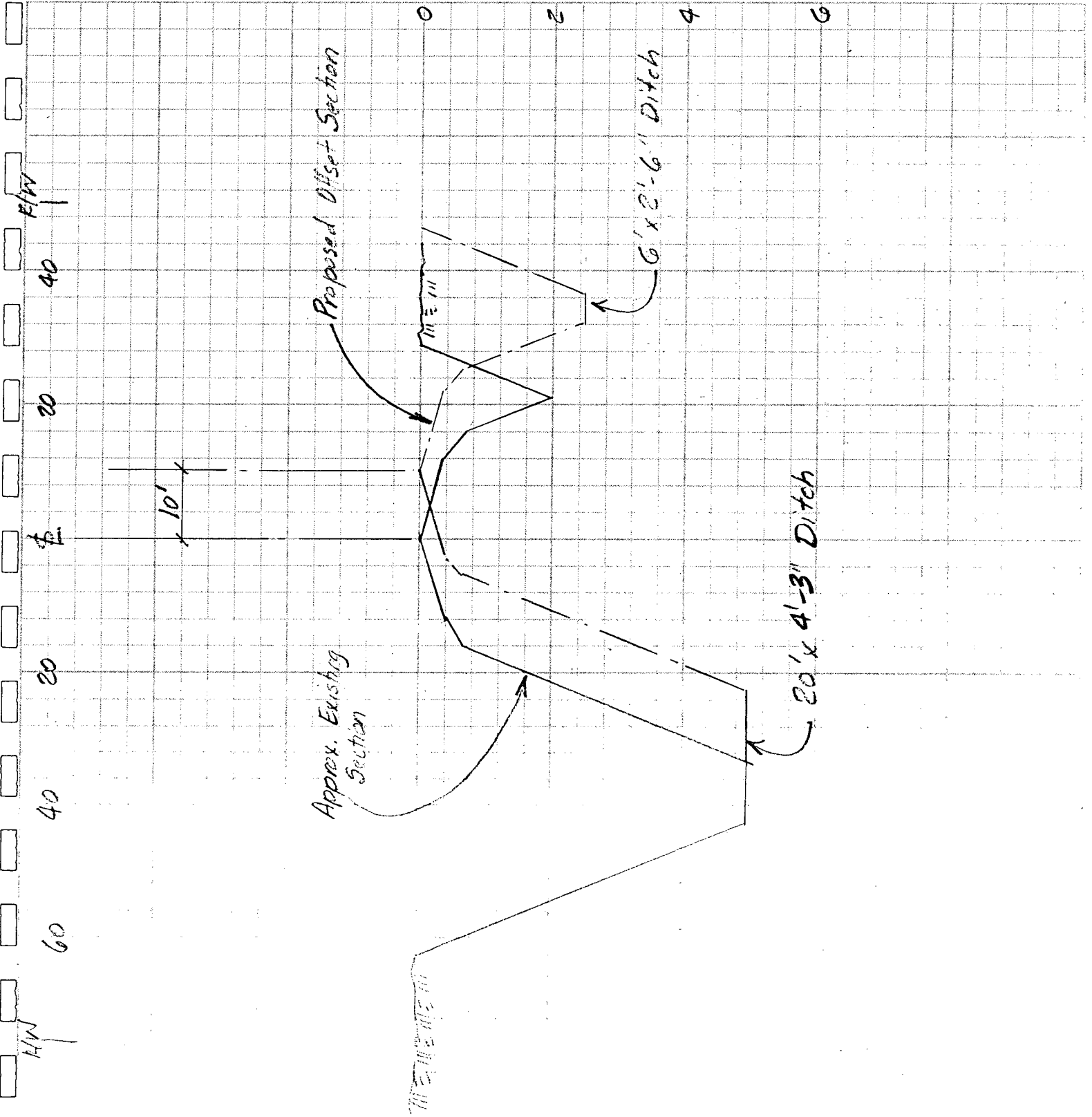
\* Interpolated



Date 10/25/92 MMB Page \_\_\_\_\_ of \_\_\_\_\_

Project FOREST LAKES

Item 29TH ST TYP SEC - POSSIBLE OFFSET SECTION



Tee Time (South) RCBB

CURRENT DATE: 02-09-1993  
 CURRENT TIME: 09:52:34

FILE DATE: 02-06-1993  
 FILE NAME: TEETIMES

\*\*\*\*\*  
 \*\*\*\*\* FHWA CULVERT ANALYSIS \*\*\*\*\*  
 \*\*\*\*\* HY-8, VERSION 3.2 \*\*\*\*\*  
 \*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	1324.00	1323.80	80.00	3 RCB	7.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*

\*\*\*\*\*  
 SUMMARY OF CULVERT FLOWS (CFS) FILE: TEETIMES DATE: 02-06-1993

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
1324.00	0	0	0	0	0	0	0	0	1
1325.51	100	100	0	0	0	0	0	0	1
1326.35	200	200	0	0	0	0	0	0	1
1327.03	300	300	0	0	0	0	0	0	1
1327.63	400	400	0	0	0	0	0	0	1
1328.11	486	486	0	0	0	0	0	0	1
1328.73	600	600	0	0	0	0	0	0	1
1329.31	700	686	0	0	0	0	0	52	14
1329.55	800	700	0	0	0	0	0	122	16
1329.78	900	700	0	0	0	0	0	209	8
1330.01	1000	700	0	0	0	0	0	309	7
1329.00	600	600	0	0	0	0	0	0	OVERTOPPING

\*\*\*\*\*

\*\*\*\*\*  
 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: TEETIMES DATE: 02-06-1993

HEAD ELEV(FT)	HEAD ERROR(FT)	TOTAL FLOW(CFS)	FLOW ERROR(CFS)	% FLOW ERROR
1324.00	0.00	0	0	0.00
1325.51	0.00	100	0	0.00
1326.35	0.00	200	0	0.00
1327.03	0.00	300	0	0.00
1327.63	0.00	400	0	0.00
1328.11	0.00	486	0	0.00
1328.73	0.00	600	0	0.00
1329.31	0.00	700	-38	-5.38
1329.55	0.00	800	-22	-2.79
1329.78	0.00	900	-9	-0.97
1330.01	0.01	1000	-9	-0.95

\*\*\*\*\*

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000  
 \*\*\*\*\*

Tee Time (South) RCBB

CURRENT DATE: 02-09-1993  
 CURRENT TIME: 09:52:34

FILE DATE: 02-06-1993  
 FILE NAME: TEETIMES

\*\*\*\*\*  
 \*\*\*\*\* CULVERT # 1 \*\*\*\*\*  
 \*\*\*\*\*

PERFORMANCE CURVE FOR 3 BARREL(S)

Q (cfs)	HWE (ft)	TWE (ft)	ICH (ft)	OCH (ft)	FLOW TYPE	CCE (ft)	FCE (ft)	TCE (ft)	VO (fps)
0	1324.00	1323.80	0.00	-0.20	0-NF	0.00	1324.00	0.00	0.00
100	1325.51	1325.22	1.33	1.51	3-M1	0.00	0.00	0.00	3.36
200	1326.35	1325.82	2.11	2.35	3-M1	0.00	0.00	0.00	4.71
300	1327.03	1326.27	2.82	3.03	3-M1	0.00	0.00	0.00	5.78
400	1327.63	1326.64	3.46	3.63	3-M1	0.00	0.00	0.00	6.71
486	1328.11	1326.92	4.01	4.11	3-M1	0.00	0.00	0.00	7.43
600	1328.73	1327.24	4.73	4.71	3-M1	0.00	0.00	0.00	8.30
686	1329.30	1327.50	5.30	5.14	3-M1	0.00	0.00	0.00	8.83
700	1329.40	1327.73	5.40	5.19	3-M2	0.00	0.00	0.00	8.48
700	1329.51	1327.95	5.40	5.51	4-FF	0.00	0.00	0.00	8.33
700	1329.71	1328.15	5.40	5.71	4-FF	0.00	0.00	0.00	8.33

El. inlet face invert 1324.00 ft El. outlet invert 1323.80 ft  
 El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

\*\*\*\*\*

\*\*\*\*\* SITE DATA \*\*\*\*\* CULVERT INVERT \*\*\*\*\*  
 INLET STATION (FT) 0.00  
 INLET ELEVATION (FT) 1324.00  
 OUTLET STATION (FT) 80.00  
 OUTLET ELEVATION (FT) 1323.80  
 NUMBER OF BARRELS 3.00  
 SLOPE (V-FT/H-FT) 0.0025  
 CULVERT LENGTH ALONG SLOPE (FT) 80.00

\*\*\*\*\* CULVERT DATA SUMMARY \*\*\*\*\*  
 BARREL SHAPE BOX  
 BARREL SPAN 7.00 FT  
 BARREL RISE 4.00 FT  
 BARREL MATERIAL CONCRETE  
 BARREL MANNING'S N 0.012  
 INLET TYPE CONVENTIONAL  
 INLET EDGE AND WALL 1:1 BEVEL (45 DEG. FLARE)  
 INLET DEPRESSION NONE

\*\*\*\*\*

Tee Time (South) RCBB

CURRENT DATE: 02-09-1993  
CURRENT TIME: 09:52:34

FILE DATE: 02-06-1993  
FILE NAME: TEETIMES

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 4.0  
CHANNEL SLOPE V/H (FT/FT) 0.008  
MANNING'S N (.01-0.1) 0.030  
CHANNEL INVERT ELEVATION (FT) 1323.80  
CULVERT NO.1 OUTLET INVERT ELEVATION 1323.80 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	1323.80	0.000	0.00	0.00
100.00	1325.22	0.666	4.50	0.71
200.00	1325.82	0.677	5.47	1.01
300.00	1326.27	0.685	6.11	1.23
400.00	1326.64	0.690	6.59	1.42
486.00	1326.92	0.693	6.94	1.56
600.00	1327.24	0.697	7.34	1.72
700.00	1327.50	0.700	7.64	1.85
800.00	1327.73	0.703	7.91	1.96
900.00	1327.95	0.705	8.15	2.07
1000.00	1328.15	0.708	8.38	2.17

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 50.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 1329.00

\*\*\*\*\*

CURRENT DATE: 02-06-1993  
 CURRENT TIME: 14:26:57

FILE DATE: 10-24-1992  
 FILE NAME: NEWLDROS

\*\*\*\*\*  
 \*\*\*\*\* FHWA CULVERT ANALYSIS \*\*\*\*\*  
 \*\*\*\*\* HY-8, VERSION 3.2 \*\*\*\*\*  
 \*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	1320.60	1320.50	72.00	3 RCB	8.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*  
 \*\*\*\*\* SUMMARY OF CULVERT FLOWS (CFS) FILE: NEWLDROS DATE: 10-24-1992 \*\*\*\*\*

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
1320.60	0	0	0	0	0	0	0	0	1
1322.97	100	100	0	0	0	0	0	0	1
1323.98	200	200	0	0	0	0	0	0	1
1324.71	300	300	0	0	0	0	0	0	1
1325.48	400	400	0	0	0	0	0	0	1
1326.18	500	500	0	0	0	0	0	0	1
1326.87	600	600	0	0	0	0	0	0	1
1326.92	608	608	0	0	0	0	0	0	1
1327.69	800	624	0	0	0	0	0	172	3
1327.97	900	611	0	0	0	0	0	288	3
1328.22	1000	592	0	0	0	0	0	408	3
1327.00	800	800	0	0	0	0	0	0	OVERTOPPING

\*\*\*\*\*  
 \*\*\*\*\* SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: NEWLDROS DATE: 10-24-1992 \*\*\*\*\*

HEAD ELEV(FT)	HEAD ERROR(FT)	TOTAL FLOW(CFS)	FLOW ERROR(CFS)	% FLOW ERROR
1320.60	0.00	0	0	0.00
1322.97	0.00	100	0	0.00
1323.98	0.00	200	0	0.00
1324.71	0.00	300	0	0.00
1325.48	0.00	400	0	0.00
1326.18	0.00	500	0	0.00
1326.87	0.00	600	0	0.00
1326.92	0.00	608	0	0.00
1327.69	-0.00	800	3	0.42
1327.97	-0.00	900	1	0.16
1328.22	0.00	1000	-0	-0.01

\*\*\*\*\*  
 <1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000  
 \*\*\*\*\*

Wild Rose (South) RCBB

CURRENT DATE: 02-06-1993  
 CURRENT TIME: 14:26:57

FILE DATE: 10-24-1992  
 FILE NAME: NEWLDROS

\*\*\*\*\*  
 \*\*\*\*\* CULVERT # 1 \*\*\*\*\*  
 \*\*\*\*\*

PERFORMANCE CURVE FOR 3 BARREL(S)

Q (cfs)	HWE (ft)	TWE (ft)	ICH (ft)	OCH (ft)	FLOW TYPE	CCE (ft)	FCE (ft)	TCE (ft)	VO (fps)
0	1320.60	1320.50	0.00	-0.10	0-NF	0.00	1320.60	0.00	0.00
100	1322.97	1322.90	1.22	2.37	3-M1	0.00	0.00	0.00	1.74
200	1323.98	1323.85	1.93	3.38	3-M1	0.00	0.00	0.00	2.49
300	1324.71	1324.54	2.56	4.11	3-M1	0.00	0.00	0.00	2.49
400	1325.48	1325.10	3.15	4.88	4-FF	0.00	0.00	0.00	4.17
500	1326.18	1325.59	3.70	5.58	4-FF	0.00	0.00	0.00	5.21
600	1326.87	1326.02	4.25	6.27	4-FF	0.00	0.00	0.00	6.25
608	1326.92	1326.05	4.30	6.32	4-FF	0.00	0.00	0.00	6.33
624	1327.68	1326.76	4.39	7.08	4-FF	0.00	0.00	0.00	6.50
611	1327.97	1327.08	4.31	7.37	4-FF	0.00	0.00	0.00	6.36
592	1328.22	1327.39	4.21	7.62	4-FF	0.00	0.00	0.00	6.16

El. inlet face invert 1320.60 ft El. outlet invert 1320.50 ft  
 El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

\*\*\*\*\*

\*\*\*\*\* SITE DATA \*\*\*\*\* CULVERT INVERT \*\*\*\*\*  
 INLET STATION (FT) 0.00  
 INLET ELEVATION (FT) 1320.60  
 OUTLET STATION (FT) 72.00  
 OUTLET ELEVATION (FT) 1320.50  
 NUMBER OF BARRELS 3.00  
 SLOPE (V-FT/H-FT) 0.0014  
 CULVERT LENGTH ALONG SLOPE (FT) 72.00

\*\*\*\*\* CULVERT DATA SUMMARY \*\*\*\*\*  
 BARREL SHAPE BOX  
 BARREL SPAN 8.00 FT  
 BARREL RISE 4.00 FT  
 BARREL MATERIAL CONCRETE  
 BARREL MANNING'S N 0.012  
 INLET TYPE CONVENTIONAL  
 INLET EDGE AND WALL 1:1 BEVEL (45 DEG. FLARE)  
 INLET DEPRESSION NONE

\*\*\*\*\*

CURRENT DATE: 02-06-1993  
CURRENT TIME: 14:26:57

FILE DATE: 10-24-1992  
FILE NAME: NEWLDROS

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 4.0  
CHANNEL SLOPE V/H (FT/FT) 0.001  
MANNING'S N (.01-0.1) 0.030  
CHANNEL INVERT ELEVATION (FT) 1320.50  
CULVERT NO.1 OUTLET INVERT ELEVATION 1320.50 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	1320.50	0.000	0.00	0.00
100.00	1322.90	0.242	2.12	0.15
200.00	1323.85	0.246	2.55	0.21
300.00	1324.54	0.249	2.84	0.25
400.00	1325.10	0.251	3.06	0.29
500.00	1325.59	0.253	3.24	0.32
600.00	1326.02	0.255	3.39	0.34
608.00	1326.05	0.255	3.40	0.35
800.00	1326.76	0.257	3.65	0.39
900.00	1327.08	0.258	3.76	0.41
1000.00	1327.39	0.259	3.86	0.43

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 60.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 1327.00

\*\*\*\*\*

Existing 10'x 3' RCB in Ridge Rd

CURRENT DATE: 01-30-1993  
 CURRENT TIME: 15:56:38

FILE DATE: 01-30-1993  
 FILE NAME: RIDG1BBL

-----  
 FHWA CULVERT ANALYSIS  
 HY-8, VERSION 3.2  
 -----

SITE DATA			CULVERT SHAPE, MATERIAL, INLET						
L	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE	
1	1319.60	1319.30	106.00	1 RCB	10.00	3.00	.012	CONVENTIONAL	
2									
3									
4									
5									
6									

SUMMARY OF CULVERT FLOWS (CFS)                      FILE: RIDG1BBL                      DATE: 01-30-1993

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
1319.60	0	0	0	0	0	0	0	0	1
1322.90	150	150	0	0	0	0	0	0	1
1326.49	300	300	0	0	0	0	0	0	1
1327.12	450	319	0	0	0	0	0	129	11
1327.21	600	321	0	0	0	0	0	275	6
1327.27	750	323	0	0	0	0	0	423	5
1327.33	900	325	0	0	0	0	0	568	4
1327.37	1000	326	0	0	0	0	0	669	4
1327.44	1200	328	0	0	0	0	0	866	4
1327.48	1350	330	0	0	0	0	0	1017	4
1327.53	1500	331	0	0	0	0	0	1157	3
1327.00	315	315	0	0	0	0	0	0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS                      FILE: RIDG1BBL                      DATE: 01-30-1993

HEAD ELEV(FT)	HEAD ERROR(FT)	TOTAL FLOW(CFS)	FLOW ERROR(CFS)	% FLOW ERROR
1319.60	0.00	0	0	0.00
1322.90	0.00	150	0	0.00
1326.49	0.00	300	0	0.00
1327.12	-0.00	450	2	0.44
1327.21	-0.00	600	3	0.54
1327.27	-0.00	750	4	0.51
1327.33	-0.01	900	7	0.80
1327.37	-0.00	1000	4	0.45
1327.44	-0.00	1200	6	0.48
1327.48	-0.00	1350	4	0.28
1327.53	-0.01	1500	12	0.80

<1> TOLERANCE (FT) = 0.010

<2> TOLERANCE (%) = 1.000

Existing 10'x 3' RCB in Ridge Rd

CURRENT DATE: 01-30-1993  
 CURRENT TIME: 15:56:38

FILE DATE: 01-30-1993  
 FILE NAME: RIDG1BBL

-----  
 CULVERT # 1  
 -----

PERFORMANCE CURVE FOR 1 BARREL(S)

Q (cfs)	HWE (ft)	TWE (ft)	ICH (ft)	OCH (ft)	FLOW TYPE	CCE (ft)	FCE (ft)	TCE (ft)	VO (fps)
0	1319.60	1318.50	0.00	-0.30	0-NF	0.00	1319.60	0.00	0.00
150	1322.90	1318.50	3.30	2.96	6-FF	0.00	0.00	0.00	8.04
300	1326.49	1318.50	6.89	5.91	4-FF	0.00	0.00	0.00	10.00
319	1327.12	1318.50	7.52	6.33	4-FF	0.00	0.00	0.00	10.64
321	1327.20	1318.50	7.60	6.38	4-FF	0.00	0.00	0.00	10.72
323	1327.26	1318.50	7.66	6.43	4-FF	0.00	0.00	0.00	10.78
325	1327.32	1318.50	7.72	6.47	4-FF	0.00	0.00	0.00	10.84
326	1327.36	1318.50	7.76	6.49	4-FF	0.00	0.00	0.00	10.87
328	1327.43	1318.50	7.83	6.54	4-FF	0.00	0.00	0.00	10.94
330	1327.47	1318.50	7.87	6.57	4-FF	0.00	0.00	0.00	10.99
331	1327.52	1318.50	7.92	6.60	4-FF	0.00	0.00	0.00	11.03

El. inlet face invert 1319.60 ft El. outlet invert 1319.30 ft  
 El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

\*\*\*\*\* SITE DATA \*\*\*\*\* CULVERT INVERT \*\*\*\*\*  
 INLET STATION (FT) 0.00  
 INLET ELEVATION (FT) 1319.60  
 OUTLET STATION (FT) 106.00  
 OUTLET ELEVATION (FT) 1319.30  
 NUMBER OF BARRELS 1.00  
 SLOPE (V-FT/H-FT) 0.0028  
 CULVERT LENGTH ALONG SLOPE (FT) 106.00

\*\*\*\*\* CULVERT DATA SUMMARY \*\*\*\*\*  
 BARREL SHAPE BOX  
 BARREL SPAN 10.00 FT  
 BARREL RISE 3.00 FT  
 BARREL MATERIAL CONCRETE  
 BARREL MANNING'S N 0.012  
 INLET TYPE CONVENTIONAL  
 INLET EDGE AND WALL SQUARE EDGE (0 DEG. FLARE)  
 INLET DEPRESSION NONE

Existing 10'x 3' RCB in Ridge Rd

CURRENT DATE: 01-30-1993  
CURRENT TIME: 15:56:38

FILE DATE: 01-30-1993  
FILE NAME: RIDG1BBL

-----  
TAILWATER  
-----

CONSTANT WATER SURFACE ELEVATION  
1318.50

-----  
ROADWAY OVERTOPPING DATA  
-----

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH (FT)	30.00
CREST LENGTH (FT)	1000.00
OVERTOPPING CREST ELEVATION (FT)	1327.00

-----

CURRENT DATE: 01-30-1993  
CURRENT TIME: 00:32:21

FILE DATE: 01-30-1993  
FILE NAME: RIDG2BBL

-----  
FHWA CULVERT ANALYSIS  
HY-8, VERSION 3.2  
-----

# C #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET					#		
# U	L #	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	# BARRELS	SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE	#
# 1	# 1	1319.60	1319.30	106.00	# 2	RCB	10.00	3.00	.012	CONVENTIONAL	#
# 2	#				#						#
# 3	#				#						#
# 4	#				#						#
# 5	#				#						#
# 6	#				#						#

-----  
SUMMARY OF CULVERT FLOWS (CFS) FILE: RIDG2BBL DATE: 01-30-1993

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY ITR
1319.60	0	0	0	0	0	0	0	0 1
1321.61	150	150	0	0	0	0	0	0 1
1322.90	300	300	0	0	0	0	0	0 1
1324.43	450	450	0	0	0	0	0	0 1
1326.49	600	600	0	0	0	0	0	0 1
1327.11	750	638	0	0	0	0	0	109 11
1327.19	900	642	0	0	0	0	0	250 5
1327.26	1050	646	0	0	0	0	0	399 5
1327.32	1200	650	0	0	0	0	0	543 4
1327.38	1350	653	0	0	0	0	0	691 4
1327.43	1500	656	0	0	0	0	0	840 4
1327.00	631	631	0	0	0	0	0	OVERTOPPING

-----  
SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: RIDG2BBL DATE: 01-30-1993

HEAD ELEV(FT)	HEAD ERROR(FT)	TOTAL FLOW(CFS)	FLOW ERROR(CFS)	% FLOW ERROR
1319.60	0.00	0	0	0.00
1321.61	0.00	150	0	0.00
1322.90	0.00	300	0	0.00
1324.43	0.00	450	0	0.00
1326.49	0.00	600	0	0.00
1327.11	-0.00	750	3	0.45
1327.19	-0.00	900	8	0.88
1327.26	-0.00	1050	4	0.42
1327.32	-0.01	1200	7	0.62
1327.38	-0.00	1350	6	0.44
1327.43	-0.00	1500	5	0.31

<1> TOLERANCE (FT) = 0.010

<2> TOLERANCE (%) = 1.000

CURRENT DATE: 01-30-1993  
 CURRENT TIME: 00:32:21

FILE DATE: 01-30-1993  
 FILE NAME: RIDG2BBL

-----  
 CULVERT # 1  
 -----

PERFORMANCE CURVE FOR 2 BARREL(S)

Q (cfs)	HWE (ft)	TWE (ft)	ICH (ft)	OCH (ft)	FLOW TYPE	CCE (ft)	FCE (ft)	TCE (ft)	VO (fps)
0	1319.60	1318.50	0.00	-0.30	0-NF	0.00	1319.60	0.00	0.00
150	1321.61	1318.50	2.01	2.00	6-FF	0.00	0.00	0.00	6.39
300	1322.90	1318.50	3.30	2.96	6-FF	0.00	0.00	0.00	8.04
450	1324.43	1318.50	4.83	4.26	6-FF	0.00	0.00	0.00	9.21
600	1326.49	1318.50	6.89	5.91	4-FF	0.00	0.00	0.00	10.00
638	1327.10	1318.50	7.50	6.32	4-FF	0.00	0.00	0.00	10.63
642	1327.18	1318.50	7.58	6.38	4-FF	0.00	0.00	0.00	10.70
646	1327.25	1318.50	7.65	6.42	4-FF	0.00	0.00	0.00	10.77
650	1327.31	1318.50	7.71	6.46	4-FF	0.00	0.00	0.00	10.83
653	1327.37	1318.50	7.77	6.50	4-FF	0.00	0.00	0.00	10.88
656	1327.42	1318.50	7.82	6.53	4-FF	0.00	0.00	0.00	10.93

El. inlet face invert 1319.60 ft El. outlet invert 1319.30 ft  
 El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

-----  
 \*\*\*\*\* SITE DATA \*\*\*\*\* CULVERT INVERT \*\*\*\*\*  
 INLET STATION (FT) 0.00  
 INLET ELEVATION (FT) 1319.60  
 OUTLET STATION (FT) 106.00  
 OUTLET ELEVATION (FT) 1319.30  
 NUMBER OF BARRELS 2.00  
 SLOPE (V-FT/H-FT) 0.0028  
 CULVERT LENGTH ALONG SLOPE (FT) 106.00

\*\*\*\*\* CULVERT DATA SUMMARY \*\*\*\*\*  
 BARREL SHAPE BOX  
 BARREL SPAN 10.00 FT  
 BARREL RISE 3.00 FT  
 BARREL MATERIAL CONCRETE  
 BARREL MANNING'S N 0.012  
 INLET TYPE CONVENTIONAL  
 INLET EDGE AND WALL SQUARE EDGE (0 DEG. FLARE)  
 INLET DEPRESSION NONE

CURRENT DATE: 01-30-1993  
CURRENT TIME: 00:32:21

FILE DATE: 01-30-1993  
FILE NAME: RIDG2BBL

-----  
TAILWATER  
-----

CONSTANT WATER SURFACE ELEVATION  
1318.50

-----  
ROADWAY OVERTOPPING DATA  
-----

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH (FT)	30.00
CREST LENGTH (FT)	1000.00
OVERTOPPING CREST ELEVATION (FT)	1327.00

-----

CURRENT DATE: 01-30-1993  
CURRENT TIME: 00:31:43

FILE DATE: 01-30-1993  
FILE NAME: RIDG3BBL

-----  
FHWA CULVERT ANALYSIS  
HY-8, VERSION 3.2  
-----

C	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
L	INLET	OUTLET	CULVERT	BARRELS	SPAN	RISE	MANNING	INLET
V	ELEV.	ELEV.	LENGTH	SHAPE	(FT)	(FT)	n	TYPE
	(FT)	(FT)	(FT)	MATERIAL				
1	1319.60	1319.30	106.00	3 RCB	10.00	3.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

-----  
SUMMARY OF CULVERT FLOWS (CFS)      FILE: RIDG3BBL      DATE: 01-30-1993  
-----

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
1319.60	0	0	0	0	0	0	0	0	1
1321.35	150	150	0	0	0	0	0	0	1
1322.04	300	300	0	0	0	0	0	0	1
1322.90	450	450	0	0	0	0	0	0	1
1323.87	600	600	0	0	0	0	0	0	1
1325.05	750	750	0	0	0	0	0	0	1
1326.49	900	900	0	0	0	0	0	0	1
1327.10	1050	955	0	0	0	0	0	89	11
1327.18	1200	963	0	0	0	0	0	228	5
1327.25	1350	969	0	0	0	0	0	369	4
1327.31	1500	974	0	0	0	0	0	517	4
1327.00	947	947	0	0	0	0	0	0	OVERTOPPING

-----  
SUMMARY OF ITERATIVE SOLUTION ERRORS      FILE: RIDG3BBL      DATE: 01-30-1993  
-----

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
1319.60	0.00	0	0	0.00
1321.35	0.00	150	0	0.00
1322.04	0.00	300	0	0.00
1322.90	0.00	450	0	0.00
1323.87	0.00	600	0	0.00
1325.05	0.00	750	0	0.00
1326.49	0.00	900	0	0.00
1327.10	-0.01	1050	6	0.55
1327.18	-0.01	1200	9	0.73
1327.25	-0.01	1350	12	0.89
1327.31	-0.01	1500	9	0.59

<1> TOLERANCE (FT) = 0.010

<2> TOLERANCE (%) = 1.000

CURRENT DATE: 01-30-1993  
 CURRENT TIME: 00:31:43

FILE DATE: 01-30-1993  
 FILE NAME: RIDG3BBL

-----  
 CULVERT # 1  
 -----

PERFORMANCE CURVE FOR 3 BARREL(S)

Q (cfs)	HWE (ft)	TWE (ft)	ICH (ft)	OCH (ft)	FLOW TYPE	CCE (ft)	FCE (ft)	TCE (ft)	VO (fps)
0	1319.60	1318.50	0.00	-0.30	0-NF	0.00	1319.60	0.00	0.00
150	1321.35	1318.50	1.55	1.75	6-FF	0.00	0.00	0.00	5.43
300	1322.04	1318.50	2.44	2.29	6-FF	0.00	0.00	0.00	7.07
450	1322.90	1318.50	3.30	2.96	6-FF	0.00	0.00	0.00	8.04
600	1323.87	1318.50	4.27	3.79	6-FF	0.00	0.00	0.00	8.91
750	1325.05	1318.50	5.45	4.77	6-FF	0.00	0.00	0.00	9.45
900	1326.49	1318.50	6.89	5.91	4-FF	0.00	0.00	0.00	10.00
955	1327.10	1318.50	7.50	6.32	4-FF	0.00	0.00	0.00	10.62
963	1327.18	1318.50	7.58	6.37	4-FF	0.00	0.00	0.00	10.70
969	1327.25	1318.50	7.65	6.42	4-FF	0.00	0.00	0.00	10.77
974	1327.31	1318.50	7.71	6.46	4-FF	0.00	0.00	0.00	10.83

El. inlet face invert 1319.60 ft El. outlet invert 1319.30 ft  
 El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

\*\*\*\*\* SITE DATA \*\*\*\*\* CULVERT INVERT \*\*\*\*\*  
 INLET STATION (FT) 0.00  
 INLET ELEVATION (FT) 1319.60  
 OUTLET STATION (FT) 106.00  
 OUTLET ELEVATION (FT) 1319.30  
 NUMBER OF BARRELS 3.00  
 SLOPE (V-FT/H-FT) 0.0028  
 CULVERT LENGTH ALONG SLOPE (FT) 106.00

\*\*\*\*\* CULVERT DATA SUMMARY \*\*\*\*\*  
 BARREL SHAPE BOX  
 BARREL SPAN 10.00 FT  
 BARREL RISE 3.00 FT  
 BARREL MATERIAL CONCRETE  
 BARREL MANNING'S N 0.012  
 INLET TYPE CONVENTIONAL  
 INLET EDGE AND WALL SQUARE EDGE (0 DEG. FLARE)  
 INLET DEPRESSION NONE

CURRENT DATE: 01-30-1993  
CURRENT TIME: 00:31:43

FILE DATE: 01-30-1993  
FILE NAME: RIDG3BBL

-----  
TAILWATER  
-----

CONSTANT WATER SURFACE ELEVATION  
1318.50

-----  
ROADWAY OVERTOPPING DATA  
-----

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH (FT)	30.00
CREST LENGTH (FT)	1000.00
OVERTOPPING CREST ELEVATION (FT)	1327.00

-----

CURRENT DATE: 01-30-1993  
 CURRENT TIME: 00:30:39

FILE DATE: 01-30-1993  
 FILE NAME: RIDG4BBL

-----  
 FHWA CULVERT ANALYSIS  
 HY-8, VERSION 3.2  
 -----

C	SITE DATA			CULVERT SHAPE, MATERIAL, INLET					
L	INLET	OUTLET	CULVERT	BARRELS	SHAPE	SPAN	RISE	MANNING	INLET
V	ELEV.	ELEV.	LENGTH	MATERIAL	(FT)	(FT)	(FT)	n	TYPE
	(FT)	(FT)	(FT)						
1	1319.60	1319.30	106.00	4 RCB	10.00	3.00	.012		CONVENTIONAL
2									
3									
4									
5									
6									

-----  
 SUMMARY OF CULVERT FLOWS (CFS)      FILE: RIDG4BBL      DATE: 01-30-1993  
 -----

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
1319.60	0	0	0	0	0	0	0	0	1
1321.23	150	150	0	0	0	0	0	0	1
1321.61	300	300	0	0	0	0	0	0	1
1322.25	450	450	0	0	0	0	0	0	1
1322.90	600	600	0	0	0	0	0	0	1
1323.61	750	750	0	0	0	0	0	0	1
1324.43	900	900	0	0	0	0	0	0	1
1325.39	1050	1050	0	0	0	0	0	0	1
1326.49	1200	1200	0	0	0	0	0	0	1
1327.08	1350	1272	0	0	0	0	0	68	11
1327.17	1500	1283	0	0	0	0	0	207	5
1327.00	1262	1262	0	0	0	0	0	0	OVERTOPPING

-----  
 SUMMARY OF ITERATIVE SOLUTION ERRORS      FILE: RIDG4BBL      DATE: 01-30-1993  
 -----

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
1319.60	0.00	0	0	0.00
1321.23	0.00	150	0	0.00
1321.61	0.00	300	0	0.00
1322.25	0.00	450	0	0.00
1322.90	0.00	600	0	0.00
1323.61	0.00	750	0	0.00
1324.43	0.00	900	0	0.00
1325.39	0.00	1050	0	0.00
1326.49	0.00	1200	0	0.00
1327.08	-0.01	1350	10	0.75
1327.17	-0.01	1500	10	0.67

<1> TOLERANCE (FT) = 0.010      <2> TOLERANCE (%) = 1.000  
 -----

CURRENT DATE: 01-30-1993  
 CURRENT TIME: 00:30:39

FILE DATE: 01-30-1993  
 FILE NAME: RIDG4BBL

-----  
 CULVERT # 1  
 -----

PERFORMANCE CURVE FOR 4 BARREL(S)

Q (cfs)	HWE (ft)	TWE (ft)	ICH (ft)	OCH (ft)	FLOW TYPE	CCE (ft)	FCE (ft)	TCE (ft)	VO (fps)
0	1319.60	1318.50	0.00	-0.30	0-NF	0.00	1319.60	0.00	0.00
150	1321.23	1318.50	1.29	1.63	6-FF	0.00	0.00	0.00	4.93
300	1321.61	1318.50	2.01	2.00	6-FF	0.00	0.00	0.00	6.39
450	1322.25	1318.50	2.65	2.44	6-FF	0.00	0.00	0.00	7.35
600	1322.90	1318.50	3.30	2.96	6-FF	0.00	0.00	0.00	8.04
750	1323.61	1318.50	4.01	3.56	6-FF	0.00	0.00	0.00	8.72
900	1324.43	1318.50	4.83	4.26	6-FF	0.00	0.00	0.00	9.21
1050	1325.39	1318.50	5.79	5.13	2-M2	0.00	0.00	0.00	9.43
1200	1326.49	1318.50	6.89	5.91	4-FF	0.00	0.00	0.00	10.00
1272	1327.08	1318.50	7.48	6.31	4-FF	0.00	0.00	0.00	10.60
1283	1327.17	1318.50	7.57	6.37	4-FF	0.00	0.00	0.00	10.69

El. inlet face invert 1319.60 ft El. outlet invert 1319.30 ft  
 El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

\*\*\*\*\* SITE DATA \*\*\*\*\* CULVERT INVERT \*\*\*\*\*  
 INLET STATION (FT) 0.00  
 INLET ELEVATION (FT) 1319.60  
 OUTLET STATION (FT) 106.00  
 OUTLET ELEVATION (FT) 1319.30  
 NUMBER OF BARRELS 4.00  
 SLOPE (V-FT/H-FT) 0.0028  
 CULVERT LENGTH ALONG SLOPE (FT) 106.00

\*\*\*\*\* CULVERT DATA SUMMARY \*\*\*\*\*  
 BARREL SHAPE BOX  
 BARREL SPAN 10.00 FT  
 BARREL RISE 3.00 FT  
 BARREL MATERIAL CONCRETE  
 BARREL MANNING'S N 0.012  
 INLET TYPE CONVENTIONAL  
 INLET EDGE AND WALL SQUARE EDGE (0 DEG. FLARE)  
 INLET DEPRESSION NONE

CURRENT DATE: 01-30-1993  
CURRENT TIME: 00:30:39

FILE DATE: 01-30-1993  
FILE NAME: RIDG4BBL

-----  
TAILWATER  
-----

CONSTANT WATER SURFACE ELEVATION  
1318.50

-----  
ROADWAY OVERTOPPING DATA  
-----

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH (FT)	30.00
CREST LENGTH (FT)	1000.00
OVERTOPPING CREST ELEVATION (FT)	1327.00

-----

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*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* FEBRUARY 1981 *
* REVISED 02 AUG 88 *
*
* RUN DATE 02/06/1993 TIME 14:16:00 *
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* THE HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *
*
*****

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X X XXXXXX XXXX X
X X X X X XX
X X X X X
XXXXXX XXXX X XXXX X
X X X X X
X X X X X
X X XXXXXX XXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1 ID FOREST LAKES & REFLECTION RIDGE 6TH, 7TH & 8TH  
 2 ID PROJ NO 36-92431-2273  
 3 ID ANALYSIS OF POND AT SW COR 29TH & RIDGE  
 4 ID MODEL SOUTH FOREST LAKES POND & RR6 POND AS ONE BASIN  
 5 ID 100-YR 24-HR STORMS  
 6 ID FOUR OPTIONAL OUTLETS AT RIDGE ROAD  
 7 ID PROFESSIONAL ENGINEERING CONSULTANTS, P.A.  
 8 ID WICHITA, KANSAS  
 9 ID MWB 02/06/93  
 10 ID FILE:FORLKS\QREVEND.HEC

\*\*\* LIST \*\*\*  
 \*\*\* FREE \*\*\*

\*DIAGRAM

11 IT 6 01FEB93 0600 0 02FEB93 1154  
 12 IN 30 01FEB93 0600  
 13 IO 3 0  
 14 JP 4  
 \* JR PREC 0.5938 0.6875 0.9063 1.0000  
 \*  
 \* NO FOR LKS DRAIN BASIN - UNDEV., CULT.  
 \*  
 15 KK FL1  
 16 BA 0.122  
 17 PB 7.8  
 18 PC 0.08 0.09 0.10 0.11 0.12 0.133 0.147 0.163 0.181 0.204  
 19 PC 0.235 0.283 0.663 0.735 0.772 0.799 0.820 0.835 0.850 0.865  
 20 PC 0.880 0.890 0.900 0.910 0.916 0.925 0.934 0.943 0.952 0.958  
 21 PC 0.964 0.970 0.976 0.982 0.988 0.994 1.000  
 22 LS 0 80 0  
 23 UD 0.55

\*  
 \* NO FOR LKS DET POND - BANK EL=1332, STATIC POOL = 1328  
 \* 2-7'X4' RCB USED FOR FLOOD ROUTING  
 \*

24 KK FLPND1  
 25 RS 1 ELEV 1328.0  
 26 SA 1.80 2.40  
 27 SE 1328.0 1332.0  
 \* 2-8X4 DATA 64.0 96.0 137.6 176.0 224.0 272.0 320.0 368.0  
 28 SQ 0 56 84 120 154 196 238 280 322  
 29 SE 1328.0 1329.2 1329.6 1330.0 1330.4 1330.8 1331.2 1331.6 1332.0  
 \*  
 \* MID FOR LKS BASIN - 1/4 AC RES, 38% IMP  
 \*

30 KK FL2  
 31 BA .0902  
 32 PB 7.8  
 33 PC 0.08 0.09 0.10 0.11 0.12 0.133 0.147 0.163 0.181 0.204  
 34 PC 0.235 0.283 0.663 0.735 0.772 0.799 0.820 0.835 0.850 0.865  
 35 PC 0.880 0.890 0.900 0.910 0.916 0.925 0.934 0.943 0.952 0.958  
 36 PC 0.964 0.970 0.976 0.982 0.988 0.994 1.000  
 37 LS 0 76 38

HEC-1 INPUT

PAGE 2

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
38        UD      0.21
*
*          ADD HYDROGRAPHS FOR MID FOR LKS DET POND
*
39        KK      FL12
40        HC      2      0
*
*          MID FOR LKS DET PND  BANK EL 1329, STATIC POOL = 1325
*          15 FT WEIR  USED FOR FLOOD ROUTING
*
41        KK      FLPND2
42        RS      1      ELEV 1325.0
43        SA      6.8    8.7
44        SE      1325.0 1329.0
45        SS      1325.0 15.0    3.0    1.5
* SQ/SE CARDS NOT USED IN THIS RUN
* SQ  0  84.0 126.0 180.6 231.0 294.0 357.0 420.0 483.0
* SE1325.0 1326.2 1326.6 1327.0 1327.4 1327.8 1328.2 1328.6 1329.0
*
*          SO FOR LKS BASIN - 1/4 AC RES 38 % IMP
*
46        KK      FL3
47        BA      .0922
48        PB      7.8
49        PC      0.08    0.09    0.10    0.11    0.12    0.133  0.147  0.163  0.181  0.204
50        PC      0.235  0.283  0.663  0.735  0.772  0.799  0.820  0.835  0.850  0.865
51        PC      0.880  0.890  0.900  0.910  0.916  0.925  0.934  0.943  0.952  0.958
52        PC      0.964  0.970  0.976  0.982  0.988  0.994  1.000
53        LS      0      68      38
54        UD      0.27
*
*          ADD HYDROGRAPHS FROM 3 FOR LKS BASINS FOR FLOOD ROUTING
*
55        KK      FL123
56        HC      2      0
*
* *****
*          SO FOR LKS POND NOT USED THIS RUN
*          ITS STORAGE ADDED TO POND AT 29TH & RIDGE IN RR6
* *****
*          SO FOR LKS DET POND - BANK EL=1326  STATIC POOL =1322
*          2-8'X4' RCB USED FOR FLOOD ROUTING
* KK FLPND3
* KP      3
* KO      1      0
* RS      1      ELEV 1322.0
* SA      5.4    6.2
* SE1322.0 1326.0
* 3-8X4DATA 96    144    206.4 264.0 336.0 408.0 480.0 552.0
* SQ      0      64     84     120    154    196    272    320    368
* SE1322.0 1323.2 1323.6 1324.0 1324.4 1324.8 1325.2 1325.6 1326.0
*

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REC-1 INPUT

PAGE 3

LINE	ID	1	2	3	4	5	6	7	8	9	10
57	KK WRR7\$8	AREA WEST OF RR 7TH & 8TH									
58	BA	0.1094									
59	PB	7.8									
60	PC	0.08	0.09	0.10	0.11	0.12	0.133	0.147	0.163	0.181	0.204
61	PC	0.235	0.283	0.663	0.735	0.772	0.799	0.820	0.835	0.850	0.865
62	PC	0.880	0.890	0.900	0.910	0.916	0.925	0.934	0.943	0.952	0.958
63	PC	0.964	0.970	0.976	0.982	0.988	0.994	1.000			
64	LS	0	72	0							
65	UD	0.15									
	*										
	*	AREA NO OF 29TH & WEST OF FOREST LAKES									
66	KK WFORLKS	AREA WEST OF FOREST LAKES									
67	BA	.3831									
68	PB	7.8									
69	PC	0.08	0.09	0.10	0.11	0.12	0.133	0.147	0.163	0.181	0.204
70	PC	0.235	0.283	0.663	0.735	0.772	0.799	0.820	0.835	0.850	0.865
71	PC	0.880	0.890	0.900	0.910	0.916	0.925	0.934	0.943	0.952	0.958
72	PC	0.964	0.970	0.976	0.982	0.988	0.994	1.000			
73	LS	0	74	0							
74	UD	0.97									
75	KK WTTIME	COMB FLOW IN S DT 29TH W OF TEE TIME									
76	RC	2	0								
77	KK RR7\$8	AREA OF RR 7TH & 8TH									
78	BA	0.078									
79	PB	7.8									
80	PC	0.08	0.09	0.10	0.11	0.12	0.133	0.147	0.163	0.181	0.204
81	PC	0.235	0.283	0.663	0.735	0.772	0.799	0.820	0.835	0.850	0.865
82	PC	0.880	0.890	0.900	0.910	0.916	0.925	0.934	0.943	0.952	0.958
83	PC	0.964	0.970	0.976	0.982	0.988	0.994	1.000			
84	LS	0	72	0							
85	UD	0.15									
	*										
	*	COMB FLOW IN SOUTH DITCH OF 29TH									
	*										
86	KK DITCH										
87	RC	2	0								
	*										
	*										
88	KK WW	BASIN WW -- RESERVE AROUND POND #4									
89	BA	.0094									
90	PB	7.8									
91	PC	0.08	0.09	0.10	0.11	0.12	0.133	0.147	0.163	0.181	0.204
92	PC	0.235	0.283	0.663	0.735	0.772	0.799	0.820	0.835	0.850	0.865
93	PC	0.880	0.890	0.900	0.910	0.916	0.925	0.934	0.943	0.952	0.958
94	PC	0.964	0.970	0.976	0.982	0.988	0.994	1.000			
95	LS	0	98	0							
96	UD	0.10									

HEC-1 INPUT

PAGE 4

LINE	ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10
97	KK	INPND4									
98	HC	3	0								
99	KK	POND4	STAGE-STORAGE THRU POND #4 AT 29TH & RIDGE								
100	KP	1									
101	RS	1	ELEV	1319.6							
		* SA/ SE CARDS NOT USED---DATA FOR RR6 POND #4									
		* SA	2.5	3.8	6.1						
		* SE	1319.6	1325.7	1328.0						
		* SV/SE DATA FOR COMBINED PONDS									
102	SV	0	5.4	6.6	20.5	27.8	37.5	43.5	50.0	60.0	
103	SE	1319.6	1321.6	1322	1323.6	1324.4	1325.4	1326.0	1327	1328	
104	SQ	0	150	300	315	600	900	1000	1200	1350	1500
105	SE	1319.6	1322.9	1326.5	1327.0	1327.2	1327.33	1327.37	1327.44	1327.48	1327.53
106	KP	2									
		* PLAN 2 IS 2-10X3 RCBB AT RIDGE ROAD									
107	RS	1	ELEV	1319.6							
		* SA/ SE CARDS NOT USED---DATA FOR RR6 POND #4									
		* SA	2.5	3.8	6.1						
		* SE	1319.6	1325.7	1328.0						
		* SV/SE DATA FOR COMBINED PONDS									
108	SV	0	5.4	6.6	20.5	27.8	37.5	43.5	50.0	60.0	
109	SE	1319.6	1321.6	1322	1323.6	1324.4	1325.4	1326.0	1327	1328	
110	SQ	0	150	300	450	600	631	750	900	1200	1400
111	SE	1319.6	1321.6	1322.9	1324.4	1326.5	1327.0	1327.1	1327.2	1327.3	1327.4
112	KP	3									
113	KO	1	0								
		* PLAN 3 IS 3-10X3 RCBB AT RIDGE ROAD									
114	RS	1	ELEV	1319.6							
		* SA/ SE CARDS NOT USED---DATA FOR RR6 POND #4									
		* SA	2.5	3.8	6.1						
		* SE	1319.6	1325.7	1328.0						
		* SV/SE DATA FOR COMBINED PONDS									
115	SV	0	5.4	6.6	20.5	27.8	37.5	43.5	50.0	60.0	
116	SE	1319.6	1321.6	1322	1323.6	1324.4	1325.4	1326.0	1327	1328	
117	SQ	0	300	450	600	750	900	947	1050	1200	1500
118	SE	1319.6	1322.0	1322.9	1323.9	1325.1	1326.5	1327.0	1327.1	1327.2	1327.3
119	KP	4									
		* PLAN 4 IS 4-10X3 RCBB AT RIDGE ROAD									
120	RS	1	ELEV	1319.6							
		* SA/ SE CARDS NOT USED---DATA FOR RR6 POND #4									
		* SA	2.5	3.8	6.1						
		* SE	1319.6	1325.7	1328.0						
		* SV/SE DATA FOR COMBINED PONDS									
121	SV	0	5.4	6.6	20.5	27.8	37.5	43.5	50.0	60.0	
122	SE	1319.6	1321.6	1322	1323.6	1324.4	1325.4	1326.0	1327	1328	
123	SQ	0	300	450	600	750	900	1050	1200	1262	1500
124	SE	1319.6	1321.6	1322.2	1322.9	1323.6	1324.4	1325.4	1326.5	1327.0	1327.2
125	ZZ										

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
15	FL1	
	V	
	V	
24	FLPND1	
	.	
30		FL2
	.	
39	FL12.....	
	V	
	V	
41	FLPND2	
	.	
46		FL3
	.	
55	FL123.....	
	.	
57		WRR7\$8
	.	
66		WFORLKS
	.	
75	WTIME.....	
	.	
77		RR7\$8
	.	
86	DITCH.....	
	.	
88		WW
	.	
97	INPND4.....	
	V	
	V	
99	POND4	

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION





PLAN 3 INPUT DATA FOR STATION FLI ARE SAME AS FOR PLAN 1

\*\*\* \*\*

PLAN 4 INPUT DATA FOR STATION FLI ARE SAME AS FOR PLAN 1

\*\*\* \*\*

\*\*\*\*\*  
 \* \*  
 24 KK \* FLPND1 \*  
 \* \*  
 \*\*\*\*\*

HYDROGRAPH ROUTING DATA

25 RS	STORAGE ROUTING									
	NSTPS	1	NUMBER OF SUBREACHES							
	ITYP		ELEV TYPE OF INITIAL CONDITION							
	RSVRIC	1328.00	INITIAL CONDITION							
	X	.00	WORKING R AND D COEFFICIENT							
26 SA	AREA	1.8	2.4							
27 SE	ELEVATION	1328.00	1332.00							
28 SQ	DISCHARGE	0.	56.	84.	120.	154.	196.	238.	280.	322.
29 SE	ELEVATION	1328.00	1329.20	1329.60	1330.00	1330.40	1330.80	1331.20	1331.60	1332.00

\*\*\*

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	8.37
ELEVATION	1328.00	1332.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	2.26	3.06	3.89	4.73	5.61	6.50	7.42	8.37
OUTFLOW	.00	56.00	84.00	120.00	154.00	196.00	238.00	280.00	322.00
ELEVATION	1328.00	1329.20	1329.60	1330.00	1330.40	1330.80	1331.20	1331.60	1332.00

\*\*\* \*\*

HYDROGRAPH AT STATION FLPND1  
 FOR PLAN 1, RATIO = 1.00

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)	(CFS)				
+ 198.	6.60	58.	18.	14.	14.	
		(INCHES)	4.431	5.438	5.438	5.438
		(AC-FT)	29.	35.	35.	35.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)					
+ 6.	6.60	2.	1.	1.	1.	
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)					
+ 1330.82	6.60	1329.03	1328.33	1328.26	1328.26	

CUMULATIVE AREA = .12 SQ MI

\*\*\* \*\*

PLAN 2 INPUT DATA FOR STATION FLPND1 ARE SAME AS FOR PLAN 1

\*\*\* \*\*

HYDROGRAPH AT STATION FLPND1  
FOR PLAN 2, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
198.	6.60	(CFS)	58.	18.	14.	14.
		(INCHES)	4.431	5.438	5.438	5.438
		(AC-FT)	29.	35.	35.	35.
PEAK STORAGE + (AC-FT)	TIME (HR)		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	29.90-HR
6.	6.60		2.	1.	1.	1.
PEAK STAGE + (FEET)	TIME (HR)		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	29.90-HR
1330.82	6.60		1329.03	1328.33	1328.26	1328.26

CUMULATIVE AREA = .12 SQ MI

\*\*\* \*\*

PLAN 3 INPUT DATA FOR STATION FLPND1 ARE SAME AS FOR PLAN 1

\*\*\* \*\*

HYDROGRAPH AT STATION FLPND1  
FOR PLAN 3, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
198.	6.60	(CFS)	58.	18.	14.	14.
		(INCHES)	4.431	5.438	5.438	5.438
		(AC-FT)	29.	35.	35.	35.
PEAK STORAGE + (AC-FT)	TIME (HR)		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	29.90-HR
6.	6.60		2.	1.	1.	1.
PEAK STAGE + (FEET)	TIME (HR)		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	29.90-HR
1330.82	6.60		1329.03	1328.33	1328.26	1328.26

CUMULATIVE AREA = .12 SQ MI

\*\*\* \*\*

PLAN 4 INPUT DATA FOR STATION FLPND1 ARE SAME AS FOR PLAN 1

\*\*\* \*\*

HYDROGRAPH AT STATION FLPND1  
FOR PLAN 4, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
198.	6.60	(CFS)	58.	18.	14.	14.
		(INCHES)	4.431	5.438	5.438	5.438
		(AC-FT)	29.	35.	35.	35.
PEAK STORAGE + (AC-FT)	TIME (HR)		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	29.90-HR
6.	6.60		2.	1.	1.	1.
PEAK STAGE + (FEET)	TIME (HR)		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	29.90-HR
1330.82	6.60		1329.03	1328.33	1328.26	1328.26



(AC-FT) 23. 29. 29. 29.

CUMULATIVE AREA = .09 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION FL2  
FOR PLAN 1, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+ 277.	6.10	(CFS)	46.	15.	12.	12.
		(INCHES)	4.755	6.049	6.049	6.049
		(AC-FT)	23.	29.	29.	29.

CUMULATIVE AREA = .09 SQ MI

\*\*\* \*\*

PLAN 2 INPUT DATA FOR STATION FL2 ARE SAME AS FOR PLAN 1

\*\*\* \*\*

PLAN 3 INPUT DATA FOR STATION FL2 ARE SAME AS FOR PLAN 1

\*\*\* \*\*

PLAN 4 INPUT DATA FOR STATION FL2 ARE SAME AS FOR PLAN 1

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
39 KK \* FL12 \*  
\* \*  
\*\*\*\*\*

40 HC HYDROGRAPH COMBINATION  
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

\*\*\*

\*\*\* \*\*

HYDROGRAPH AT STATION FL12  
FOR PLAN 1, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+ 345.	6.10	(CFS)	103.	33.	26.	26.
		(INCHES)	4.529	5.698	5.698	5.698
		(AC-FT)	51.	64.	64.	64.

CUMULATIVE AREA = .21 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION FL12  
FOR PLAN 2, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+ 345.	6.10	(CFS)	103.	33.	26.	26.
		(INCHES)	4.529	5.698	5.698	5.698
		(AC-FT)	51.	64.	64.	64.

CUMULATIVE AREA = .21 SQ MI

\*\*\*            \*\*\*            \*\*\*            \*\*\*            \*\*\*

HYDROGRAPH AT STATION FL12  
FOR PLAN 3, RATIO = 1.00

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
345.	6.10	(CFS)	103.	33.	26.	26.
		(INCHES)	4.529	5.698	5.698	5.698
		(AC-FT)	51.	64.	64.	64.

CUMULATIVE AREA = .21 SQ MI

\*\*\*            \*\*\*            \*\*\*            \*\*\*            \*\*\*

HYDROGRAPH AT STATION FL12  
FOR PLAN 4, RATIO = 1.00

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
345.	6.10	(CFS)	103.	33.	26.	26.
		(INCHES)	4.529	5.698	5.698	5.698
		(AC-FT)	51.	64.	64.	64.

CUMULATIVE AREA = .21 SQ MI

\*\*\* \*\*

\*\*\*\*\*  
\*            \*  
41 KK    \*    FLPND2   \*  
\*            \*  
\*\*\*\*\*

HYDROGRAPH ROUTING DATA

42 RS	STORAGE ROUTING		
	NSTPS	1	NUMBER OF SUBREACHES
	ITYP		ELEV TYPE OF INITIAL CONDITION
	RSVRC	1325.00	INITIAL CONDITION
	X	.00	WORKING R AND D COEFFICIENT
43 SA	AREA	6.8	8.7
44 SE	ELEVATION	1325.00	1329.00
45 SS	SPILLWAY		
	CREL	1325.00	SPILLWAY CREST ELEVATION
	SPWID	15.00	SPILLWAY WIDTH
	COCW	3.00	WEIR COEFFICIENT
	EXPW	1.50	EXPONENT OF HEAD

\*\*\*

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	30.92
ELEVATION	1325.00	1329.00

COMPUTED OUTFLOW-ELEVATION DATA

OUTFLOW	.00	.00	.06	.49	1.67	3.95	7.71	13.33	21.18	31.61
ELEVATION	1325.00	1325.00	1325.01	1325.05	1325.11	1325.20	1325.31	1325.44	1325.60	1325.79
OUTFLOW	45.00	61.73	82.16	106.67	135.62	169.39	208.34	252.84	303.27	360.00
ELEVATION	1326.00	1326.23	1326.49	1326.78	1327.09	1327.42	1327.78	1328.16	1328.57	1329.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	.08	.34	.76	1.35	2.12	3.07	4.20	5.51	7.03
OUTFLOW	.00	.06	.49	1.67	3.95	7.71	13.33	21.18	31.61	45.00
ELEVATION	1325.00	1325.01	1325.05	1325.11	1325.20	1325.31	1325.44	1325.60	1325.79	1326.00
STORAGE	8.74	10.66	12.81	15.18	17.79	20.66	23.79	27.21	30.92	
OUTFLOW	61.73	82.16	106.67	135.62	169.39	208.34	252.84	303.27	360.00	
ELEVATION	1326.23	1326.49	1326.78	1327.09	1327.42	1327.78	1328.16	1328.57	1329.00	

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HYDROGRAPH AT STATION FLPND2  
FOR PLAN 1, RATIO = 1.00

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)				
+ 192.	7.00	(CFS)			
		(INCHES)			
		(AC-FT)			
		97.	32.	26.	26.
		4.261	5.642	5.668	5.668
		48.	64.	64.	64.
PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
+ (AC-FT)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+ 19.	7.00	12.	5.	4.	4.
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
+ (FEET)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+ 1327.62	7.00	1326.61	1325.66	1325.54	1325.54

CUMULATIVE AREA = .21 SQ MI

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PLAN 2 INPUT DATA FOR STATION FLPND2 ARE SAME AS FOR PLAN 1

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HYDROGRAPH AT STATION FLPND2  
FOR PLAN 2, RATIO = 1.00

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)				
+ 192.	7.00	(CFS)			
		(INCHES)			
		(AC-FT)			
		97.	32.	26.	26.
		4.261	5.642	5.668	5.668
		48.	64.	64.	64.
PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
+ (AC-FT)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+ 19.	7.00	12.	5.	4.	4.
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
+ (FEET)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+ 1327.62	7.00	1326.61	1325.66	1325.54	1325.54

CUMULATIVE AREA = .21 SQ MI

\*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*

PLAN 3 INPUT DATA FOR STATION FLPND2 ARE SAME AS FOR PLAN 1

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION FLPND2  
FOR PLAN 3, RATIO = 1.00

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR

+ (CFS)	(HR)	(CFS)				
+ 192.	7.00	97.	32.	26.	26.	
		(INCHES)	4.261	5.642	5.668	5.668
		(AC-FT)	48.	64.	64.	64.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	29.90-HR	
+ (AC-FT)	(HR)					
+ 19.	7.00	12.	5.	4.	4.	
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR	
+ (FEET)	(HR)					
+ 1327.62	7.00	1326.61	1325.66	1325.54	1325.54	

CUMULATIVE AREA = .21 SQ MI

\*\*\* \*\*

PLAN 4 INPUT DATA FOR STATION FLND2 ARE SAME AS FOR PLAN 1

\*\*\* \*\*

HYDROGRAPH AT STATION FLND2  
FOR PLAN 4, RATIO = 1.00

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR	
+ (CFS)	(HR)					
+ 192.	7.00	97.	32.	26.	26.	
		(INCHES)	4.261	5.642	5.668	5.668
		(AC-FT)	48.	64.	64.	64.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	29.90-HR	
+ (AC-FT)	(HR)					
+ 19.	7.00	12.	5.	4.	4.	
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR	
+ (FEET)	(HR)					
+ 1327.62	7.00	1326.61	1325.66	1325.54	1325.54	

CUMULATIVE AREA = .21 SQ MI

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\* \*  
46 KK \* FL3 \*  
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12 IN TIME DATA FOR INPUT TIME SERIES  
JXMIN 30 TIME INTERVAL IN MINUTES  
JXDATE 1FEB93 STARTING DATE  
JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

47 BA SUBBASIN CHARACTERISTICS  
TAREA .09 SUBBASIN AREA

PRECIPITATION DATA

48 PB STORM 7.80 BASIN TOTAL PRECIPITATION

49 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00



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 \* \*  
 55 KK \* FL123 \*  
 \* \*  
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56 HC HYDROGRAPH COMBINATION  
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION FL123  
 FOR PLAN 1, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			29.90-HR
			6-HR	24-HR	72-HR	
+ 327.	6.20	138.	46.	37.	37.	
		(INCHES) 4.210	5.584	5.613	5.613	
		(AC-FT) 68.	91.	91.	91.	

CUMULATIVE AREA = .30 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION FL123  
 FOR PLAN 2, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			29.90-HR
			6-HR	24-HR	72-HR	
+ 327.	6.20	138.	46.	37.	37.	
		(INCHES) 4.210	5.584	5.613	5.613	
		(AC-FT) 68.	91.	91.	91.	

CUMULATIVE AREA = .30 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION FL123  
 FOR PLAN 3, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			29.90-HR
			6-HR	24-HR	72-HR	
+ 327.	6.20	138.	46.	37.	37.	
		(INCHES) 4.210	5.584	5.613	5.613	
		(AC-FT) 68.	91.	91.	91.	

CUMULATIVE AREA = .30 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION FL123  
 FOR PLAN 4, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			29.90-HR
			6-HR	24-HR	72-HR	
+ 327.	6.20	138.	46.	37.	37.	
		(INCHES) 4.210	5.584	5.613	5.613	
		(AC-FT) 68.	91.	91.	91.	

CUMULATIVE AREA = .30 SQ MI





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UNIT HYDROGRAPH  
50 END-OF-PERIOD ORDINATES

5.	18.	34.	55.	82.	116.	145.	166.	178.	181.
180.	171.	159.	146.	129.	108.	90.	75.	64.	54.
47.	40.	35.	29.	25.	21.	18.	15.	13.	11.
9.	8.	7.	6.	5.	4.	4.	3.	3.	2.
2.	2.	2.	1.	1.	1.	1.	1.	0.	0.

\*\*\*      \*\*\*      \*\*\*      \*\*\*      \*\*\*

HYDROGRAPH AT STATION WFORLKS  
FOR PLAN 1, RATIO = 1.00

TOTAL RAINFALL = 7.80, TOTAL LOSS = 3.05, TOTAL EXCESS = 4.75

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	444.	6.90			
		(CFS)	159.	49.	39.
		(INCHES)	3.853	4.747	4.747
		(AC-FT)	79.	97.	97.

CUMULATIVE AREA = .38 SQ MI

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HYDROGRAPH AT STATION WFORLKS  
FOR PLAN 1, RATIO = 1.00

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	444.	6.90			
		(CFS)	159.	49.	39.
		(INCHES)	3.853	4.747	4.747
		(AC-FT)	79.	97.	97.

CUMULATIVE AREA = .38 SQ MI

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PLAN 2 INPUT DATA FOR STATION WFORLKS ARE SAME AS FOR PLAN 1

\*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*

PLAN 3 INPUT DATA FOR STATION WFORLKS ARE SAME AS FOR PLAN 1

\*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*

PLAN 4 INPUT DATA FOR STATION WFORLKS ARE SAME AS FOR PLAN 1

\*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*    \*\*\*

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75 KK      \*      \*      \*      \*      \*      \*      \*      \*      \*      \*      \*      \*      \*      \*      \*      \*  
          \*      WTIME    \*      COMB FLOW IN S DT 29TH W OF TEE TIME  
          \*      \*      \*      \*      \*      \*      \*      \*      \*      \*      \*      \*      \*      \*      \*  
\*\*\*\*\*

76 HC      HYDROGRAPH COMBINATION  
          ICOMP            2    NUMBER OF HYDROGRAPHS TO COMBINE

\*\*\*

\*\*\*      \*\*\*      \*\*\*      \*\*\*      \*\*\*

HYDROGRAPH AT STATION WTIME  
FOR PLAN 1, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
486.	6.80	(CFS) 202.	62.	50.	50.
		(INCHES) 3.809	4.697	4.697	4.697
		(AC-FT) 100.	123.	123.	123.

CUMULATIVE AREA = .49 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION WTTIME  
FOR PLAN 2, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
486.	6.80	(CFS) 202.	62.	50.	50.
		(INCHES) 3.809	4.697	4.697	4.697
		(AC-FT) 100.	123.	123.	123.

CUMULATIVE AREA = .49 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION WTTIME  
FOR PLAN 3, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
486.	6.80	(CFS) 202.	62.	50.	50.
		(INCHES) 3.809	4.697	4.697	4.697
		(AC-FT) 100.	123.	123.	123.

CUMULATIVE AREA = .49 SQ MI

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HYDROGRAPH AT STATION WTTIME  
FOR PLAN 4, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
486.	6.80	(CFS) 202.	62.	50.	50.
		(INCHES) 3.809	4.697	4.697	4.697
		(AC-FT) 100.	123.	123.	123.

CUMULATIVE AREA = .49 SQ MI

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77 KK RR7&8 AREA OF RR 7TH & 8TH

12 IN TIME DATA FOR INPUT TIME SERIES  
JXMIN 30 TIME INTERVAL IN MINUTES  
JXDATE 1FEB93 STARTING DATE  
JXTIME 600 STARTING TIME

SUBBASIN RUNOFF DATA

78 BA SUBBASIN CHARACTERISTICS  
TAREA .08 SUBBASIN AREA



PLAN 3 INPUT DATA FOR STATION RR7\$8 ARE SAME AS FOR PLAN 1

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PLAN 4 INPUT DATA FOR STATION RR7\$8 ARE SAME AS FOR PLAN 1

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 \* \*  
 86 KK \* DITCH \*  
 \* \*  
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87 HC HYDROGRAPH COMBINATION  
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION DITCH  
 FOR PLAN 1, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			29.90-HR
			6-HR	24-HR	72-HR	
+ 608.	6.10	233.	72.	58.	58.	
		(INCHES) 3.794	4.672	4.672	4.672	
		(AC-FT) 115.	142.	142.	142.	

CUMULATIVE AREA = .57 SQ MI

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HYDROGRAPH AT STATION DITCH  
 FOR PLAN 2, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			29.90-HR
			6-HR	24-HR	72-HR	
+ 608.	6.10	233.	72.	58.	58.	
		(INCHES) 3.794	4.672	4.672	4.672	
		(AC-FT) 115.	142.	142.	142.	

CUMULATIVE AREA = .57 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION DITCH  
 FOR PLAN 3, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			29.90-HR
			6-HR	24-HR	72-HR	
+ 608.	6.10	233.	72.	58.	58.	
		(INCHES) 3.794	4.672	4.672	4.672	
		(AC-FT) 115.	142.	142.	142.	

CUMULATIVE AREA = .57 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION DITCH  
 FOR PLAN 4, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			29.90-HR
			6-HR	24-HR	72-HR	





CUMULATIVE AREA = .88 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION INPND4  
FOR PLAN 3, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+ 958.	6.10	376.	119.	96.	96.	
		(INCHES) 3.954	5.017	5.027	5.027	
		(AC-FT) 186.	237.	237.	237.	

CUMULATIVE AREA = .88 SQ MI

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HYDROGRAPH AT STATION INPND4  
FOR PLAN 4, RATIO = 1.00

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+ 958.	6.10	376.	119.	96.	96.	
		(INCHES) 3.954	5.017	5.027	5.027	
		(AC-FT) 186.	237.	237.	237.	

CUMULATIVE AREA = .88 SQ MI

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\* \*  
99 KK \* POND4 \*  
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STAGE-STORAGE THRU POND #4 AT 29TH & RIDGE

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100 KP PLAN 1 FOR STATION POND4 STAGE-STORAGE THRU POND #4 AT 29TH & RIDGE

HYDROGRAPH ROUTING DATA

101 RS	STORAGE ROUTING										
	NSTPS	1	NUMBER OF SUBREACHES								
	ITYP	ELEV	TYPE OF INITIAL CONDITION								
	RSVVIC	1319.60	INITIAL CONDITION								
	X	.00	WORKING R AND D COEFFICIENT								
102 SV	STORAGE	.0	5.4	6.6	20.5	27.8	37.5	43.5	50.0	60.0	
103 SE	ELEVATION	1319.60	1321.60	1322.00	1323.60	1324.40	1325.40	1326.00	1327.00	1328.00	
104 SQ	DISCHARGE	0.	150.	300.	315.	600.	900.	1000.	1200.	1350.	1500.
105 SE	ELEVATION	1319.60	1322.90	1326.50	1327.00	1327.20	1327.33	1327.37	1327.44	1327.48	1327.53

\*\*\*

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	5.40	6.60	14.42	20.50	27.80	37.50	43.50	46.75	50.00
OUTFLOW	.00	90.91	109.09	150.00	179.16	212.50	254.17	279.17	300.00	315.00
ELEVATION	1319.60	1321.60	1322.00	1322.90	1323.60	1324.40	1325.40	1326.00	1326.50	1327.00
STORAGE	52.00	53.30	53.70	54.40	54.80	55.30	60.00			
OUTFLOW	600.00	900.00	1000.00	1200.00	1350.00	1500.00	2908.54			
ELEVATION	1327.20	1327.33	1327.37	1327.44	1327.48	1327.53	1328.00			

\*\*\* WARNING \*\*\* MODIFIED PULS ROUTING MAY BE NUMERICALLY UNSTABLE FOR OUTFLOWS BETWEEN 900. TO 2909.  
 THE ROUTED HYDROGRAPH SHOULD BE EXAMINED FOR OSCILLATIONS OR OUTFLOWS GREATER THAN PEAK INFLOWS.  
 THIS CAN BE CORRECTED BY DECREASING THE TIME INTERVAL OR INCREASING STORAGE (USE A LONGER REACH.)

PEAK FLOW		TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	(CFS)	6-HR	24-HR	72-HR	29.90-HR
+	756.	6.90	337.	119.	96.	96.
		(INCHES)	3.540	5.015	5.026	5.026
		(AC-FT)	167.	237.	237.	237.

PEAK STORAGE		TIME	MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)	(AC-FT)	6-HR	24-HR	72-HR	29.90-HR
+	53.	6.90	41.	13.	10.	10.

PEAK STAGE		TIME	MAXIMUM AVERAGE STAGE			
(FEET)	(HR)	(FEET)	6-HR	24-HR	72-HR	29.90-HR
+	1327.27	6.90	1325.89	1321.95	1321.49	1321.49

CUMULATIVE AREA = .88 SQ MI

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106 KP PLAN 2 FOR STATION POND4 STAGE-STORAGE THRU POND #4 AT 29TH & RIDGE

HYDROGRAPH ROUTING DATA

107 RS	STORAGE ROUTING										
	NSTPS	1	NUMBER OF SUBREACHES								
	ITYP	ELEV	TYPE OF INITIAL CONDITION								
	RSVRIC	1319.60	INITIAL CONDITION								
	X	.00	WORKING R AND D COEFFICIENT								
108 SV	STORAGE	.0	5.4	6.6	20.5	27.8	37.5	43.5	50.0	60.0	
109 SE	ELEVATION	1319.60	1321.60	1322.00	1323.60	1324.40	1325.40	1326.00	1327.00	1328.00	
110 SQ	DISCHARGE	0.	150.	300.	450.	600.	631.	750.	900.	1200.	1400.
111 SE	ELEVATION	1319.60	1321.60	1322.90	1324.40	1326.50	1327.00	1327.10	1327.20	1327.30	1327.40

\*\*\*

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	5.40	6.60	14.42	20.50	27.80	37.50	43.50	46.75	50.00
OUTFLOW	.00	150.00	196.15	300.00	370.00	450.00	521.43	564.29	600.00	631.00
ELEVATION	1319.60	1321.60	1322.00	1322.90	1323.60	1324.40	1325.40	1326.00	1326.50	1327.00
STORAGE	51.00	52.00	53.00	54.00	60.00					
OUTFLOW	750.00	900.00	1200.00	1400.00	2600.24					
ELEVATION	1327.10	1327.20	1327.30	1327.40	1328.00					

\*\*\* WARNING \*\*\* MODIFIED PULS ROUTING MAY BE NUMERICALLY UNSTABLE FOR OUTFLOWS BETWEEN 900. TO 1200.  
 THE ROUTED HYDROGRAPH SHOULD BE EXAMINED FOR OSCILLATIONS OR OUTFLOWS GREATER THAN PEAK INFLOWS.  
 THIS CAN BE CORRECTED BY DECREASING THE TIME INTERVAL OR INCREASING STORAGE (USE A LONGER REACH.)

PEAK FLOW		TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	(CFS)	6-HR	24-HR	72-HR	29.90-HR
+	584.	7.40	373.	119.	96.	96.

	(INCHES)	3.916	5.016	5.027	5.027
	(AC-FT)	185.	237.	237.	237.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE		
		6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)				
45.	7.40	23.	7.	5.	5.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE		
		6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)				
1326.28	7.40	1323.80	1321.00	1320.73	1320.73
CUMULATIVE AREA =		.88 SQ MI			

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112 KP PLAN 3 FOR STATION POND4 STAGE-STORAGE THRU POND #4 AT 29TH & RIDGE

113 KO OUTPUT CONTROL VARIABLES  
 IPRNT 1 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

HYDROGRAPH ROUTING DATA

114 RS STORAGE ROUTING  
 NSTPS 1 NUMBER OF SUBREACHES  
 ITYP ELEV TYPE OF INITIAL CONDITION  
 RSVRIC 1319.60 INITIAL CONDITION  
 X .00 WORKING R AND D COEFFICIENT

115 SV	STORAGE	.0	5.4	6.6	20.5	27.8	37.5	43.5	50.0	60.0	
116 SE	ELEVATION	1319.60	1321.60	1322.00	1323.60	1324.40	1325.40	1326.00	1327.00	1328.00	
117 SQ	DISCHARGE	0.	300.	450.	600.	750.	900.	947.	1050.	1200.	1500.
118 SE	ELEVATION	1319.60	1322.00	1322.90	1323.90	1325.10	1326.50	1327.00	1327.10	1327.20	1327.30

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COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	5.40	6.60	14.42	20.50	23.24	27.80	34.59	37.50	43.50
OUTFLOW	.00	250.00	300.00	450.00	554.99	600.00	662.50	750.00	782.15	846.43
ELEVATION	1319.60	1321.60	1322.00	1322.90	1323.60	1323.90	1324.40	1325.10	1325.40	1326.00
STORAGE	46.75	50.00	51.00	52.00	53.00	60.00				
OUTFLOW	900.00	947.00	1050.00	1200.00	1500.00	3597.80				
ELEVATION	1326.50	1327.00	1327.10	1327.20	1327.30	1328.00				

\*\*\* WARNING \*\*\* MODIFIED PULS ROUTING MAY BE NUMERICALLY UNSTABLE FOR OUTFLOWS BETWEEN 1200. TO 3598.  
 THE ROUTED HYDROGRAPH SHOULD BE EXAMINED FOR OSCILLATIONS OR OUTFLOWS GREATER THAN PEAK INFLOWS.  
 THIS CAN BE CORRECTED BY DECREASING THE TIME INTERVAL OR INCREASING STORAGE (USE A LONGER REACH.)

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HYDROGRAPH AT STATION POND4  
 PLAN 3, RATIO = 1.00

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DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE		
1	FEB	0600	1	0.	.0	1319.6	*	1	FEB	1600	101	175.	3.8	1321.0	*	2	FEB	0200	201	14.	.3	1319.7
1	FEB	0606	2	0.	.0	1319.6	*	1	FEB	1606	102	169.	3.7	1321.0	*	2	FEB	0206	202	13.	.3	1319.7
1	FEB	0612	3	0.	.0	1319.6	*	1	FEB	1612	103	164.	3.5	1320.9	*	2	FEB	0212	203	12.	.3	1319.7
1	FEB	0618	4	1.	.0	1319.6	*	1	FEB	1618	104	158.	3.4	1320.9	*	2	FEB	0218	204	11.	.2	1319.7
1	FEB	0624	5	1.	.0	1319.6	*	1	FEB	1624	105	152.	3.3	1320.8	*	2	FEB	0224	205	10.	.2	1319.7
1	FEB	0630	6	2.	.0	1319.6	*	1	FEB	1630	106	146.	3.2	1320.8	*	2	FEB	0230	206	9.	.2	1319.7
1	FEB	0636	7	2.	.0	1319.6	*	1	FEB	1636	107	141.	3.1	1320.7	*	2	FEB	0236	207	9.	.2	1319.7
1	FEB	0642	8	3.	.1	1319.6	*	1	FEB	1642	108	137.	3.0	1320.7	*	2	FEB	0242	208	8.	.2	1319.7
1	FEB	0648	9	3.	.1	1319.6	*	1	FEB	1648	109	133.	2.9	1320.7	*	2	FEB	0248	209	8.	.2	1319.7
1	FEB	0654	10	4.	.1	1319.6	*	1	FEB	1654	110	129.	2.8	1320.6	*	2	FEB	0254	210	7.	.2	1319.7
1	FEB	0700	11	4.	.1	1319.6	*	1	FEB	1700	111	126.	2.7	1320.6	*	2	FEB	0300	211	7.	.2	1319.7

1 FEB 0706	12	4.	.1	1319.6 *	1 FEB 1706	112	122.	2.6	1320.6 *	2 FEB 0306	212	7.	.1	1319.7
1 FEB 0712	13	4.	.1	1319.6 *	1 FEB 1712	113	119.	2.6	1320.6 *	2 FEB 0312	213	6.	.1	1319.7
1 FEB 0718	14	5.	.1	1319.6 *	1 FEB 1718	114	117.	2.5	1320.5 *	2 FEB 0318	214	6.	.1	1319.6
1 FEB 0724	15	5.	.1	1319.6 *	1 FEB 1724	115	114.	2.5	1320.5 *	2 FEB 0324	215	6.	.1	1319.6
1 FEB 0730	16	5.	.1	1319.6 *	1 FEB 1730	116	111.	2.4	1320.5 *	2 FEB 0330	216	5.	.1	1319.6
1 FEB 0736	17	5.	.1	1319.6 *	1 FEB 1736	117	109.	2.4	1320.5 *	2 FEB 0336	217	5.	.1	1319.6
1 FEB 0742	18	5.	.1	1319.6 *	1 FEB 1742	118	106.	2.3	1320.4 *	2 FEB 0342	218	5.	.1	1319.6
1 FEB 0748	19	5.	.1	1319.6 *	1 FEB 1748	119	102.	2.2	1320.4 *	2 FEB 0348	219	5.	.1	1319.6
1 FEB 0754	20	5.	.1	1319.6 *	1 FEB 1754	120	99.	2.1	1320.4 *	2 FEB 0354	220	4.	.1	1319.6
1 FEB 0800	21	5.	.1	1319.6 *	1 FEB 1800	121	95.	2.1	1320.4 *	2 FEB 0400	221	4.	.1	1319.6
1 FEB 0806	22	5.	.1	1319.6 *	1 FEB 1806	122	92.	2.0	1320.3 *	2 FEB 0406	222	4.	.1	1319.6
1 FEB 0812	23	6.	.1	1319.6 *	1 FEB 1812	123	90.	1.9	1320.3 *	2 FEB 0412	223	4.	.1	1319.6
1 FEB 0818	24	6.	.1	1319.6 *	1 FEB 1818	124	89.	1.9	1320.3 *	2 FEB 0418	224	4.	.1	1319.6
1 FEB 0824	25	6.	.1	1319.6 *	1 FEB 1824	125	88.	1.9	1320.3 *	2 FEB 0424	225	4.	.1	1319.6
1 FEB 0830	26	6.	.1	1319.7 *	1 FEB 1830	126	87.	1.9	1320.3 *	2 FEB 0430	226	3.	.1	1319.6
1 FEB 0836	27	7.	.1	1319.7 *	1 FEB 1836	127	86.	1.9	1320.3 *	2 FEB 0436	227	3.	.1	1319.6
1 FEB 0842	28	7.	.2	1319.7 *	1 FEB 1842	128	85.	1.8	1320.3 *	2 FEB 0442	228	3.	.1	1319.6
1 FEB 0848	29	7.	.2	1319.7 *	1 FEB 1848	129	84.	1.8	1320.3 *	2 FEB 0448	229	3.	.1	1319.6
1 FEB 0854	30	7.	.2	1319.7 *	1 FEB 1854	130	83.	1.8	1320.3 *	2 FEB 0454	230	3.	.1	1319.6
1 FEB 0900	31	8.	.2	1319.7 *	1 FEB 1900	131	83.	1.8	1320.3 *	2 FEB 0500	231	3.	.1	1319.6
1 FEB 0906	32	8.	.2	1319.7 *	1 FEB 1906	132	82.	1.8	1320.3 *	2 FEB 0506	232	3.	.1	1319.6
1 FEB 0912	33	8.	.2	1319.7 *	1 FEB 1912	133	82.	1.8	1320.3 *	2 FEB 0512	233	3.	.1	1319.6
1 FEB 0918	34	8.	.2	1319.7 *	1 FEB 1918	134	81.	1.8	1320.2 *	2 FEB 0518	234	3.	.1	1319.6
1 FEB 0924	35	9.	.2	1319.7 *	1 FEB 1924	135	81.	1.7	1320.2 *	2 FEB 0524	235	3.	.1	1319.6
1 FEB 0930	36	9.	.2	1319.7 *	1 FEB 1930	136	81.	1.7	1320.2 *	2 FEB 0530	236	2.	.1	1319.6
1 FEB 0936	37	9.	.2	1319.7 *	1 FEB 1936	137	81.	1.7	1320.2 *	2 FEB 0536	237	2.	.1	1319.6
1 FEB 0942	38	10.	.2	1319.7 *	1 FEB 1942	138	80.	1.7	1320.2 *	2 FEB 0542	238	2.	.1	1319.6
1 FEB 0948	39	10.	.2	1319.7 *	1 FEB 1948	139	80.	1.7	1320.2 *	2 FEB 0548	239	2.	.0	1319.6
1 FEB 0954	40	10.	.2	1319.7 *	1 FEB 1954	140	80.	1.7	1320.2 *	2 FEB 0554	240	2.	.0	1319.6
1 FEB 1000	41	11.	.2	1319.7 *	1 FEB 2000	141	80.	1.7	1320.2 *	2 FEB 0600	241	2.	.0	1319.6
1 FEB 1006	42	11.	.2	1319.7 *	1 FEB 2006	142	80.	1.7	1320.2 *	2 FEB 0606	242	2.	.0	1319.6
1 FEB 1012	43	12.	.3	1319.7 *	1 FEB 2012	143	79.	1.7	1320.2 *	2 FEB 0612	243	2.	.0	1319.6
1 FEB 1018	44	14.	.3	1319.7 *	1 FEB 2018	144	77.	1.7	1320.2 *	2 FEB 0618	244	2.	.0	1319.6
1 FEB 1024	45	15.	.3	1319.7 *	1 FEB 2024	145	76.	1.6	1320.2 *	2 FEB 0624	245	2.	.0	1319.6
1 FEB 1030	46	17.	.4	1319.7 *	1 FEB 2030	146	74.	1.6	1320.2 *	2 FEB 0630	246	2.	.0	1319.6
1 FEB 1036	47	19.	.4	1319.7 *	1 FEB 2036	147	73.	1.6	1320.2 *	2 FEB 0636	247	2.	.0	1319.6
1 FEB 1042	48	21.	.5	1319.8 *	1 FEB 2042	148	72.	1.5	1320.2 *	2 FEB 0642	248	2.	.0	1319.6
1 FEB 1048	49	24.	.5	1319.8 *	1 FEB 2048	149	70.	1.5	1320.2 *	2 FEB 0648	249	2.	.0	1319.6
1 FEB 1054	50	28.	.6	1319.8 *	1 FEB 2054	150	69.	1.5	1320.2 *	2 FEB 0654	250	2.	.0	1319.6
1 FEB 1100	51	31.	.7	1319.9 *	1 FEB 2100	151	68.	1.5	1320.1 *	2 FEB 0700	251	2.	.0	1319.6
1 FEB 1106	52	36.	.8	1319.9 *	1 FEB 2106	152	67.	1.4	1320.1 *	2 FEB 0706	252	2.	.0	1319.6
1 FEB 1112	53	41.	.9	1319.9 *	1 FEB 2112	153	66.	1.4	1320.1 *	2 FEB 0712	253	2.	.0	1319.6
1 FEB 1118	54	49.	1.0	1320.0 *	1 FEB 2118	154	65.	1.4	1320.1 *	2 FEB 0718	254	1.	.0	1319.6
1 FEB 1124	55	57.	1.2	1320.1 *	1 FEB 2124	155	64.	1.4	1320.1 *	2 FEB 0724	255	1.	.0	1319.6
1 FEB 1130	56	65.	1.4	1320.1 *	1 FEB 2130	156	63.	1.4	1320.1 *	2 FEB 0730	256	1.	.0	1319.6
1 FEB 1136	57	86.	1.9	1320.3 *	1 FEB 2136	157	62.	1.3	1320.1 *	2 FEB 0736	257	1.	.0	1319.6
1 FEB 1142	58	145.	3.1	1320.8 *	1 FEB 2142	158	61.	1.3	1320.1 *	2 FEB 0742	258	1.	.0	1319.6
1 FEB 1148	59	250.	5.4	1321.6 *	1 FEB 2148	159	60.	1.3	1320.1 *	2 FEB 0748	259	1.	.0	1319.6
1 FEB 1154	60	336.	8.5	1322.2 *	1 FEB 2154	160	60.	1.3	1320.1 *	2 FEB 0754	260	1.	.0	1319.6
1 FEB 1200	61	410.	12.3	1322.7 *	1 FEB 2200	161	59.	1.3	1320.1 *	2 FEB 0800	261	1.	.0	1319.6
1 FEB 1206	62	484.	16.4	1323.1 *	1 FEB 2206	162	59.	1.3	1320.1 *	2 FEB 0806	262	1.	.0	1319.6
1 FEB 1212	63	540.	19.6	1323.5 *	1 FEB 2212	163	58.	1.3	1320.1 *	2 FEB 0812	263	1.	.0	1319.6
1 FEB 1218	64	575.	21.7	1323.7 *	1 FEB 2218	164	58.	1.2	1320.1 *	2 FEB 0818	264	1.	.0	1319.6
1 FEB 1224	65	598.	23.1	1323.9 *	1 FEB 2224	165	57.	1.2	1320.1 *	2 FEB 0824	265	1.	.0	1319.6
1 FEB 1230	66	616.	24.4	1324.0 *	1 FEB 2230	166	57.	1.2	1320.1 *	2 FEB 0830	266	1.	.0	1319.6
1 FEB 1236	67	633.	25.6	1324.2 *	1 FEB 2236	167	56.	1.2	1320.1 *	2 FEB 0836	267	1.	.0	1319.6
1 FEB 1242	68	648.	26.7	1324.3 *	1 FEB 2242	168	56.	1.2	1320.0 *	2 FEB 0842	268	1.	.0	1319.6
1 FEB 1248	69	661.	27.7	1324.4 *	1 FEB 2248	169	56.	1.2	1320.0 *	2 FEB 0848	269	1.	.0	1319.6
1 FEB 1254	70	671.	28.4	1324.5 *	1 FEB 2254	170	56.	1.2	1320.0 *	2 FEB 0854	270	1.	.0	1319.6
1 FEB 1300	71	678.	29.0	1324.5 *	1 FEB 2300	171	55.	1.2	1320.0 *	2 FEB 0900	271	1.	.0	1319.6
1 FEB 1306	72	682.	29.3	1324.6 *	1 FEB 2306	172	55.	1.2	1320.0 *	2 FEB 0906	272	1.	.0	1319.6
1 FEB 1312	73	683.	29.4	1324.6 *	1 FEB 2312	173	55.	1.2	1320.0 *	2 FEB 0912	273	1.	.0	1319.6
1 FEB 1318	74	680.	29.1	1324.5 *	1 FEB 2318	174	55.	1.2	1320.0 *	2 FEB 0918	274	1.	.0	1319.6
1 FEB 1324	75	672.	28.6	1324.5 *	1 FEB 2324	175	55.	1.2	1320.0 *	2 FEB 0924	275	1.	.0	1319.6
1 FEB 1330	76	662.	27.8	1324.4 *	1 FEB 2330	176	54.	1.2	1320.0 *	2 FEB 0930	276	1.	.0	1319.6
1 FEB 1336	77	648.	26.7	1324.3 *	1 FEB 2336	177	54.	1.2	1320.0 *	2 FEB 0936	277	1.	.0	1319.6
1 FEB 1342	78	631.	25.5	1324.2 *	1 FEB 2342	178	54.	1.2	1320.0 *	2 FEB 0942	278	1.	.0	1319.6
1 FEB 1348	79	613.	24.2	1324.0 *	1 FEB 2348	179	54.	1.2	1320.0 *	2 FEB 0948	279	1.	.0	1319.6
1 FEB 1354	80	592.	22.8	1323.8 *	1 FEB 2354	180	54.	1.2	1320.0 *	2 FEB 0954	280	1.	.0	1319.6
1 FEB 1400	81	568.	21.3	1323.7 *	2 FEB 0000	181	54.	1.2	1320.0 *	2 FEB 1000	281	1.	.0	1319.6
1 FEB 1406	82	544.	19.8	1323.5 *	2 FEB 0006	182	53.	1.2	1320.0 *	2 FEB 1006	282	1.	.0	1319.6
1 FEB 1412	83	518.	18.4	1323.4 *	2 FEB 0012	183	52.	1.1	1320.0 *	2 FEB 1012	283	1.	.0	1319.6
1 FEB 1418	84	493.	16.9	1323.2 *	2 FEB 0018	184	49.	1.1	1320.0 *	2 FEB 1018	284	1.	.0	1319.6
1 FEB 1424	85	469.	15.5	1323.0 *	2 FEB 0024	185	46.	1.0	1320.0 *	2 FEB 1024	285	1.	.0	1319.6
1 FEB 1430	86	444.	14.1	1322.9 *	2 FEB 0030	186	43.	.9	1319.9 *	2 FEB 1030	286	1.	.0	1319.6
1 FEB 1436	87	419.	12.8	1322.7 *	2 FEB 0036	187	40.	.9	1319.9 *	2 FEB 1036	287	1.	.0	1319.6
1 FEB 1442	88	396.	11.6	1322.6 *	2 FEB 0042	188	38.	.8	1319.9 *	2 FEB 1042	288	1.	.0	1319.6
1 FEB 1448	89	374.	10.5	1322.4 *	2 FEB 0048	189	35.	.8	1319.9 *	2 FEB 1048	289	1.	.0	1319.6
1 FEB 1454	90	354.	9.4	1322.3 *	2 FEB 0054	190	33.	.7	1319.9 *	2 FEB 1054	290	1.	.0	1319.6
1 FEB 1500	91	335.	8.4	1322.2 *	2 FEB 0100	191	31.	.7	1319.8 *	2 FEB 1100	291	1.	.0	1319.6

1 FEB 1506	92	317.	7.5	1322.1	*	2 FEB 0106	192	29.	.6	1319.8	*	2 FEB 1106	292	1.	.0	1319.6
1 FEB 1512	93	300.	6.6	1322.0	*	2 FEB 0112	193	27.	.6	1319.8	*	2 FEB 1112	293	1.	.0	1319.6
1 FEB 1518	94	271.	5.9	1321.8	*	2 FEB 0118	194	25.	.5	1319.8	*	2 FEB 1118	294	1.	.0	1319.6
1 FEB 1524	95	247.	5.3	1321.6	*	2 FEB 0124	195	23.	.5	1319.8	*	2 FEB 1124	295	1.	.0	1319.6
1 FEB 1530	96	227.	4.9	1321.4	*	2 FEB 0130	196	21.	.5	1319.8	*	2 FEB 1130	296	1.	.0	1319.6
1 FEB 1536	97	211.	4.6	1321.3	*	2 FEB 0136	197	19.	.4	1319.8	*	2 FEB 1136	297	1.	.0	1319.6
1 FEB 1542	98	199.	4.3	1321.2	*	2 FEB 0142	198	18.	.4	1319.7	*	2 FEB 1142	298	1.	.0	1319.6
1 FEB 1548	99	189.	4.1	1321.1	*	2 FEB 0148	199	16.	.3	1319.7	*	2 FEB 1148	299	1.	.0	1319.6
1 FEB 1554	100	181.	3.9	1321.1	*	2 FEB 0154	200	15.	.3	1319.7	*	2 FEB 1154	300	1.	.0	1319.6

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PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
683.	7.20		375.	119.	96.	96.
		(INCHES)	3.938	5.017	5.027	5.027
		(AC-FT)	186.	237.	237.	237.

PEAK STORAGE + (AC-FT)	TIME (HR)	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	29.90-HR
29.	7.20	13.	4.	3.	3.

PEAK STAGE + (FEET)	TIME (HR)	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR
1324.56	7.20	1322.39	1320.50	1320.33	1320.33

CUMULATIVE AREA = .88 SQ MI

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119 KP PLAN 4 FOR STATION POND4 STAGE-STORAGE THRU POND #4 AT 29TH & RIDGE  
HYDROGRAPH ROUTING DATA

120 RS STORAGE ROUTING  
NSTPS 1 NUMBER OF SUBREACHES  
ITYP ELEV TYPE OF INITIAL CONDITION  
RSVRIC 1319.60 INITIAL CONDITION  
X .00 WORKING R AND D COEFFICIENT

121 SV	STORAGE	.0	5.4	6.6	20.5	27.8	37.5	43.5	50.0	60.0
122 SE	ELEVATION	1319.60	1321.60	1322.00	1323.60	1324.40	1325.40	1326.00	1327.00	1328.00
123 SQ	DISCHARGE	0.	300.	450.	600.	750.	900.	1050.	1200.	1262.
124 SE	ELEVATION	1319.60	1321.60	1322.20	1322.90	1323.60	1324.40	1325.40	1326.50	1327.00

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COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	5.40	6.60	8.34	14.42	20.50	27.80	37.50	43.50	46.75
OUTFLOW	.00	300.00	400.01	450.00	600.00	750.00	900.00	1050.00	1131.82	1200.00
ELEVATION	1319.60	1321.60	1322.00	1322.20	1322.90	1323.60	1324.40	1325.40	1326.00	1326.50
STORAGE	50.00	52.00	60.00							
OUTFLOW	1262.00	1500.00	2452.29							
ELEVATION	1327.00	1327.20	1328.00							

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HYDROGRAPH AT STATION POND4  
PLAN 4, RATIO = 1.00

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DA	MON	HR	MIN	ORD	OUTFLOW	STORAGE	STAGE	*	DA	MON	HR	MIN	ORD	OUTFLOW	STORAGE	STAGE	*	DA	MON	HR	MIN	ORD	OUTFLOW	STORAGE	STAGE
1	FEB	0600	1	0.	.0	1319.6	*	1	FEB	1600	101	169.	3.0	1320.7	*	2	FEB	0200	201	13.	.2	1319.7			
1	FEB	0606	2	0.	.0	1319.6	*	1	FEB	1606	102	165.	3.0	1320.7	*	2	FEB	0206	202	12.	.2	1319.7			
1	FEB	0612	3	0.	.0	1319.6	*	1	FEB	1612	103	160.	2.9	1320.7	*	2	FEB	0212	203	11.	.2	1319.7			

1 FEB 0618	4	1.	.0	1319.6 *	1 FEB 1618	104	154.	2.8	1320.6 *	2 FEB 0218	204	10.	.2	1319.7
1 FEB 0624	5	1.	.0	1319.6 *	1 FEB 1624	105	149.	2.7	1320.6 *	2 FEB 0224	205	10.	.2	1319.7
1 FEB 0630	6	2.	.0	1319.6 *	1 FEB 1630	106	143.	2.6	1320.6 *	2 FEB 0230	206	9.	.2	1319.7
1 FEB 0636	7	2.	.0	1319.6 *	1 FEB 1636	107	139.	2.5	1320.5 *	2 FEB 0236	207	9.	.2	1319.7
1 FEB 0642	8	3.	.1	1319.6 *	1 FEB 1642	108	135.	2.4	1320.5 *	2 FEB 0242	208	8.	.1	1319.7
1 FEB 0648	9	3.	.1	1319.6 *	1 FEB 1648	109	131.	2.4	1320.5 *	2 FEB 0248	209	8.	.1	1319.7
1 FEB 0654	10	4.	.1	1319.6 *	1 FEB 1654	110	127.	2.3	1320.4 *	2 FEB 0254	210	7.	.1	1319.6
1 FEB 0700	11	4.	.1	1319.6 *	1 FEB 1700	111	124.	2.2	1320.4 *	2 FEB 0300	211	7.	.1	1319.6
1 FEB 0706	12	4.	.1	1319.6 *	1 FEB 1706	112	121.	2.2	1320.4 *	2 FEB 0306	212	6.	.1	1319.6
1 FEB 0712	13	4.	.1	1319.6 *	1 FEB 1712	113	118.	2.1	1320.4 *	2 FEB 0312	213	6.	.1	1319.6
1 FEB 0718	14	5.	.1	1319.6 *	1 FEB 1718	114	115.	2.1	1320.4 *	2 FEB 0318	214	6.	.1	1319.6
1 FEB 0724	15	5.	.1	1319.6 *	1 FEB 1724	115	113.	2.0	1320.4 *	2 FEB 0324	215	5.	.1	1319.6
1 FEB 0730	16	5.	.1	1319.6 *	1 FEB 1730	116	110.	2.0	1320.3 *	2 FEB 0330	216	5.	.1	1319.6
1 FEB 0736	17	5.	.1	1319.6 *	1 FEB 1736	117	108.	1.9	1320.3 *	2 FEB 0336	217	5.	.1	1319.6
1 FEB 0742	18	5.	.1	1319.6 *	1 FEB 1742	118	105.	1.9	1320.3 *	2 FEB 0342	218	5.	.1	1319.6
1 FEB 0748	19	5.	.1	1319.6 *	1 FEB 1748	119	101.	1.8	1320.3 *	2 FEB 0348	219	5.	.1	1319.6
1 FEB 0754	20	5.	.1	1319.6 *	1 FEB 1754	120	97.	1.7	1320.2 *	2 FEB 0354	220	4.	.1	1319.6
1 FEB 0800	21	5.	.1	1319.6 *	1 FEB 1800	121	94.	1.7	1320.2 *	2 FEB 0400	221	4.	.1	1319.6
1 FEB 0806	22	5.	.1	1319.6 *	1 FEB 1806	122	91.	1.6	1320.2 *	2 FEB 0406	222	4.	.1	1319.6
1 FEB 0812	23	6.	.1	1319.6 *	1 FEB 1812	123	89.	1.6	1320.2 *	2 FEB 0412	223	4.	.1	1319.6
1 FEB 0818	24	6.	.1	1319.6 *	1 FEB 1818	124	88.	1.6	1320.2 *	2 FEB 0418	224	4.	.1	1319.6
1 FEB 0824	25	6.	.1	1319.6 *	1 FEB 1824	125	87.	1.6	1320.2 *	2 FEB 0424	225	4.	.1	1319.6
1 FEB 0830	26	7.	.1	1319.6 *	1 FEB 1830	126	86.	1.6	1320.2 *	2 FEB 0430	226	3.	.1	1319.6
1 FEB 0836	27	7.	.1	1319.6 *	1 FEB 1836	127	85.	1.5	1320.2 *	2 FEB 0436	227	3.	.1	1319.6
1 FEB 0842	28	7.	.1	1319.6 *	1 FEB 1842	128	85.	1.5	1320.2 *	2 FEB 0442	228	3.	.1	1319.6
1 FEB 0848	29	7.	.1	1319.6 *	1 FEB 1848	129	84.	1.5	1320.2 *	2 FEB 0448	229	3.	.1	1319.6
1 FEB 0854	30	8.	.1	1319.7 *	1 FEB 1854	130	83.	1.5	1320.2 *	2 FEB 0454	230	3.	.1	1319.6
1 FEB 0900	31	8.	.1	1319.7 *	1 FEB 1900	131	82.	1.5	1320.1 *	2 FEB 0500	231	3.	.1	1319.6
1 FEB 0906	32	8.	.1	1319.7 *	1 FEB 1906	132	82.	1.5	1320.1 *	2 FEB 0506	232	3.	.1	1319.6
1 FEB 0912	33	8.	.1	1319.7 *	1 FEB 1912	133	81.	1.5	1320.1 *	2 FEB 0512	233	3.	.0	1319.6
1 FEB 0918	34	9.	.2	1319.7 *	1 FEB 1918	134	81.	1.5	1320.1 *	2 FEB 0518	234	3.	.0	1319.6
1 FEB 0924	35	9.	.2	1319.7 *	1 FEB 1924	135	81.	1.5	1320.1 *	2 FEB 0524	235	3.	.0	1319.6
1 FEB 0930	36	9.	.2	1319.7 *	1 FEB 1930	136	81.	1.5	1320.1 *	2 FEB 0530	236	2.	.0	1319.6
1 FEB 0936	37	9.	.2	1319.7 *	1 FEB 1936	137	80.	1.4	1320.1 *	2 FEB 0536	237	2.	.0	1319.6
1 FEB 0942	38	10.	.2	1319.7 *	1 FEB 1942	138	80.	1.4	1320.1 *	2 FEB 0542	238	2.	.0	1319.6
1 FEB 0948	39	10.	.2	1319.7 *	1 FEB 1948	139	80.	1.4	1320.1 *	2 FEB 0548	239	2.	.0	1319.6
1 FEB 0954	40	11.	.2	1319.7 *	1 FEB 1954	140	80.	1.4	1320.1 *	2 FEB 0554	240	2.	.0	1319.6
1 FEB 1000	41	11.	.2	1319.7 *	1 FEB 2000	141	80.	1.4	1320.1 *	2 FEB 0600	241	2.	.0	1319.6
1 FEB 1006	42	12.	.2	1319.7 *	1 FEB 2006	142	80.	1.4	1320.1 *	2 FEB 0606	242	2.	.0	1319.6
1 FEB 1012	43	13.	.2	1319.7 *	1 FEB 2012	143	79.	1.4	1320.1 *	2 FEB 0612	243	2.	.0	1319.6
1 FEB 1018	44	14.	.3	1319.7 *	1 FEB 2018	144	77.	1.4	1320.1 *	2 FEB 0618	244	2.	.0	1319.6
1 FEB 1024	45	15.	.3	1319.7 *	1 FEB 2024	145	75.	1.4	1320.1 *	2 FEB 0624	245	2.	.0	1319.6
1 FEB 1030	46	17.	.3	1319.7 *	1 FEB 2030	146	74.	1.3	1320.1 *	2 FEB 0630	246	2.	.0	1319.6
1 FEB 1036	47	19.	.3	1319.7 *	1 FEB 2036	147	72.	1.3	1320.1 *	2 FEB 0636	247	2.	.0	1319.6
1 FEB 1042	48	22.	.4	1319.7 *	1 FEB 2042	148	71.	1.3	1320.1 *	2 FEB 0642	248	2.	.0	1319.6
1 FEB 1048	49	25.	.5	1319.8 *	1 FEB 2048	149	70.	1.3	1320.1 *	2 FEB 0648	249	2.	.0	1319.6
1 FEB 1054	50	29.	.5	1319.8 *	1 FEB 2054	150	69.	1.2	1320.1 *	2 FEB 0654	250	2.	.0	1319.6
1 FEB 1100	51	33.	.6	1319.8 *	1 FEB 2100	151	68.	1.2	1320.1 *	2 FEB 0700	251	2.	.0	1319.6
1 FEB 1106	52	37.	.7	1319.8 *	1 FEB 2106	152	66.	1.2	1320.0 *	2 FEB 0706	252	2.	.0	1319.6
1 FEB 1112	53	43.	.8	1319.9 *	1 FEB 2112	153	65.	1.2	1320.0 *	2 FEB 0712	253	1.	.0	1319.6
1 FEB 1118	54	51.	.9	1319.9 *	1 FEB 2118	154	64.	1.2	1320.0 *	2 FEB 0718	254	1.	.0	1319.6
1 FEB 1124	55	59.	1.1	1320.0 *	1 FEB 2124	155	63.	1.1	1320.0 *	2 FEB 0724	255	1.	.0	1319.6
1 FEB 1130	56	68.	1.2	1320.1 *	1 FEB 2130	156	62.	1.1	1320.0 *	2 FEB 0730	256	1.	.0	1319.6
1 FEB 1136	57	91.	1.6	1320.2 *	1 FEB 2136	157	62.	1.1	1320.0 *	2 FEB 0736	257	1.	.0	1319.6
1 FEB 1142	58	158.	2.8	1320.7 *	1 FEB 2142	158	61.	1.1	1320.0 *	2 FEB 0742	258	1.	.0	1319.6
1 FEB 1148	59	275.	4.9	1321.4 *	1 FEB 2148	159	60.	1.1	1320.0 *	2 FEB 0748	259	1.	.0	1319.6
1 FEB 1154	60	427.	7.5	1322.1 *	1 FEB 2154	160	59.	1.1	1320.0 *	2 FEB 0754	260	1.	.0	1319.6
1 FEB 1200	61	506.	10.6	1322.5 *	1 FEB 2200	161	59.	1.1	1320.0 *	2 FEB 0800	261	1.	.0	1319.6
1 FEB 1206	62	586.	13.9	1322.8 *	1 FEB 2206	162	58.	1.0	1320.0 *	2 FEB 0806	262	1.	.0	1319.6
1 FEB 1212	63	645.	16.2	1323.1 *	1 FEB 2212	163	58.	1.0	1320.0 *	2 FEB 0812	263	1.	.0	1319.6
1 FEB 1218	64	675.	17.5	1323.3 *	1 FEB 2218	164	57.	1.0	1320.0 *	2 FEB 0818	264	1.	.0	1319.6
1 FEB 1224	65	691.	18.1	1323.3 *	1 FEB 2224	165	57.	1.0	1320.0 *	2 FEB 0824	265	1.	.0	1319.6
1 FEB 1230	66	704.	18.6	1323.4 *	1 FEB 2230	166	57.	1.0	1320.0 *	2 FEB 0830	266	1.	.0	1319.6
1 FEB 1236	67	716.	19.1	1323.4 *	1 FEB 2236	167	56.	1.0	1320.0 *	2 FEB 0836	267	1.	.0	1319.6
1 FEB 1242	68	727.	19.6	1323.5 *	1 FEB 2242	168	56.	1.0	1320.0 *	2 FEB 0842	268	1.	.0	1319.6
1 FEB 1248	69	735.	19.9	1323.5 *	1 FEB 2248	169	56.	1.0	1320.0 *	2 FEB 0848	269	1.	.0	1319.6
1 FEB 1254	70	739.	20.1	1323.5 *	1 FEB 2254	170	55.	1.0	1320.0 *	2 FEB 0854	270	1.	.0	1319.6
1 FEB 1300	71	740.	20.1	1323.6 *	1 FEB 2300	171	55.	1.0	1320.0 *	2 FEB 0900	271	1.	.0	1319.6
1 FEB 1306	72	736.	19.9	1323.5 *	1 FEB 2306	172	55.	1.0	1320.0 *	2 FEB 0906	272	1.	.0	1319.6
1 FEB 1312	73	728.	19.6	1323.5 *	1 FEB 2312	173	55.	1.0	1320.0 *	2 FEB 0912	273	1.	.0	1319.6
1 FEB 1318	74	713.	19.0	1323.4 *	1 FEB 2318	174	55.	1.0	1320.0 *	2 FEB 0918	274	1.	.0	1319.6
1 FEB 1324	75	694.	18.2	1323.3 *	1 FEB 2324	175	54.	1.0	1320.0 *	2 FEB 0924	275	1.	.0	1319.6
1 FEB 1330	76	671.	17.3	1323.2 *	1 FEB 2330	176	54.	1.0	1320.0 *	2 FEB 0930	276	1.	.0	1319.6
1 FEB 1336	77	645.	16.2	1323.1 *	1 FEB 2336	177	54.	1.0	1320.0 *	2 FEB 0936	277	1.	.0	1319.6
1 FEB 1342	78	617.	15.1	1323.0 *	1 FEB 2342	178	54.	1.0	1320.0 *	2 FEB 0942	278	1.	.0	1319.6
1 FEB 1348	79	588.	13.9	1322.8 *	1 FEB 2348	179	54.	1.0	1320.0 *	2 FEB 0948	279	1.	.0	1319.6
1 FEB 1354	80	559.	12.8	1322.7 *	1 FEB 2354	180	54.	1.0	1320.0 *	2 FEB 0954	280	1.	.0	1319.6
1 FEB 1400	81	530.	11.6	1322.6 *	2 FEB 0000	181	54.	1.0	1320.0 *	2 FEB 1000	281	1.	.0	1319.6
1 FEB 1406	82	502.	10.5	1322.4 *	2 FEB 0006	182	53.	1.0	1320.0 *	2 FEB 1006	282	1.	.0	1319.6
1 FEB 1412	83	475.	9.3	1322.3 *	2 FEB 0012	183	51.	.9	1319.9 *	2 FEB 1012	283	1.	.0	1319.6

1 FEB 1418	84	448.	8.3	1322.2 *	2 FEB 0018	184	48.	.9	1319.9 *	2 FEB 1018	284	1.	.0	1319.6
1 FEB 1424	85	418.	7.2	1322.1 *	2 FEB 0024	185	45.	.8	1319.9 *	2 FEB 1024	285	1.	.0	1319.6
1 FEB 1430	86	378.	6.3	1321.9 *	2 FEB 0030	186	42.	.8	1319.9 *	2 FEB 1030	286	1.	.0	1319.6
1 FEB 1436	87	325.	5.7	1321.7 *	2 FEB 0036	187	39.	.7	1319.9 *	2 FEB 1036	287	1.	.0	1319.6
1 FEB 1442	88	294.	5.3	1321.6 *	2 FEB 0042	188	37.	.7	1319.8 *	2 FEB 1042	288	1.	.0	1319.6
1 FEB 1448	89	276.	5.0	1321.4 *	2 FEB 0048	189	34.	.6	1319.8 *	2 FEB 1048	289	1.	.0	1319.6
1 FEB 1454	90	261.	4.7	1321.3 *	2 FEB 0054	190	32.	.6	1319.8 *	2 FEB 1054	290	1.	.0	1319.6
1 FEB 1500	91	247.	4.4	1321.2 *	2 FEB 0100	191	30.	.5	1319.8 *	2 FEB 1100	291	1.	.0	1319.6
1 FEB 1506	92	235.	4.2	1321.2 *	2 FEB 0106	192	28.	.5	1319.8 *	2 FEB 1106	292	1.	.0	1319.6
1 FEB 1512	93	224.	4.0	1321.1 *	2 FEB 0112	193	26.	.5	1319.8 *	2 FEB 1112	293	1.	.0	1319.6
1 FEB 1518	94	214.	3.9	1321.0 *	2 FEB 0118	194	24.	.4	1319.8 *	2 FEB 1118	294	1.	.0	1319.6
1 FEB 1524	95	205.	3.7	1321.0 *	2 FEB 0124	195	22.	.4	1319.7 *	2 FEB 1124	295	1.	.0	1319.6
1 FEB 1530	96	197.	3.5	1320.9 *	2 FEB 0130	196	20.	.4	1319.7 *	2 FEB 1130	296	1.	.0	1319.6
1 FEB 1536	97	190.	3.4	1320.9 *	2 FEB 0136	197	18.	.3	1319.7 *	2 FEB 1136	297	1.	.0	1319.6
1 FEB 1542	98	184.	3.3	1320.8 *	2 FEB 0142	198	17.	.3	1319.7 *	2 FEB 1142	298	1.	.0	1319.6
1 FEB 1548	99	178.	3.2	1320.8 *	2 FEB 0148	199	15.	.3	1319.7 *	2 FEB 1148	299	1.	.0	1319.6
1 FEB 1554	100	173.	3.1	1320.8 *	2 FEB 0154	200	14.	.3	1319.7 *	2 FEB 1154	300	1.	.0	1319.6

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PEAK FLOW		TIME	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	740.	7.00	375.	119.	96.	96.
		(INCHES)	3.943	5.017	5.027	5.027
		(AC-FT)	186.	237.	237.	237.
PEAK STORAGE		TIME	MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	29.90-HR
+	(AC-FT)	(HR)				
+	20.	7.00	9.	3.	2.	2.
PEAK STAGE		TIME	MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	29.90-HR
+	(FEET)	(HR)				
+	1323.55	7.00	1321.77	1320.31	1320.17	1320.17
CUMULATIVE AREA =			.88 SQ MI			

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIO 1	RATIOS APPLIED TO FLOWS
				1.00	
HYDROGRAPH AT					
+ FL1	.12	1	FLOW	238.	
			TIME	6.40	
		2	FLOW	238.	
			TIME	6.40	
		3	FLOW	238.	
			TIME	6.40	
		4	FLOW	238.	
			TIME	6.40	
ROUTED TO					
+ FLPND1	.12	1	FLOW	198.	
			TIME	6.60	
		2	FLOW	198.	
			TIME	6.60	
		3	FLOW	198.	
			TIME	6.60	
		4	FLOW	198.	
			TIME	6.60	
			** PEAK STAGES IN FEET **		
		1	STAGE	1330.82	
			TIME	6.60	
		2	STAGE	1330.82	
			TIME	6.60	
		3	STAGE	1330.82	
			TIME	6.60	
		4	STAGE	1330.82	
			TIME	6.60	
HYDROGRAPH AT					
+ FL2	.09	1	FLOW	277.	
			TIME	6.10	
		2	FLOW	277.	
			TIME	6.10	
		3	FLOW	277.	
			TIME	6.10	
		4	FLOW	277.	
			TIME	6.10	
2 COMBINED AT					
+ FL12	.21	1	FLOW	345.	
			TIME	6.10	
		2	FLOW	345.	
			TIME	6.10	
		3	FLOW	345.	
			TIME	6.10	
		4	FLOW	345.	
			TIME	6.10	
ROUTED TO					
+ FLPND2	.21	1	FLOW	192.	
			TIME	7.00	
		2	FLOW	192.	
			TIME	7.00	
		3	FLOW	192.	
			TIME	7.00	
		4	FLOW	192.	
			TIME	7.00	
			** PEAK STAGES IN FEET **		
		1	STAGE	1327.62	
			TIME	7.00	
		2	STAGE	1327.62	
			TIME	7.00	
		3	STAGE	1327.62	
			TIME	7.00	
		4	STAGE	1327.62	
			TIME	7.00	

HYDROGRAPH AT				
+	FL3	.09	1	FLOW 238. TIME 6.10
			2	FLOW 238. TIME 6.10
			3	FLOW 238. TIME 6.10
			4	FLOW 238. TIME 6.10
2 COMBINED AT				
+	FL123	.30	1	FLOW 327. TIME 6.20
			2	FLOW 327. TIME 6.20
			3	FLOW 327. TIME 6.20
			4	FLOW 327. TIME 6.20
HYDROGRAPH AT				
+	WRR7\$8	.11	1	FLOW 290. TIME 6.00
			2	FLOW 290. TIME 6.00
			3	FLOW 290. TIME 6.00
			4	FLOW 290. TIME 6.00
HYDROGRAPH AT				
+	WFORLKS	.38	1	FLOW 444. TIME 6.90
			2	FLOW 444. TIME 6.90
			3	FLOW 444. TIME 6.90
			4	FLOW 444. TIME 6.90
2 COMBINED AT				
+	WTIME	.49	1	FLOW 486. TIME 6.80
			2	FLOW 486. TIME 6.80
			3	FLOW 486. TIME 6.80
			4	FLOW 486. TIME 6.80
HYDROGRAPH AT				
+	RR7\$8	.08	1	FLOW 207. TIME 6.00
			2	FLOW 207. TIME 6.00
			3	FLOW 207. TIME 6.00
			4	FLOW 207. TIME 6.00
2 COMBINED AT				
+	DITCH	.57	1	FLOW 608. TIME 6.10
			2	FLOW 608. TIME 6.10
			3	FLOW 608. TIME 6.10
			4	FLOW 608. TIME 6.10
HYDROGRAPH AT				
+	WW	.01	1	FLOW 39. TIME 6.00
			2	FLOW 39. TIME 6.00
			3	FLOW 39. TIME 6.00
			4	FLOW 39. TIME 6.00

3 COMBINED AT

+	INPND4	.88	1	FLOW	958.
				TIME	6.10
			2	FLOW	958.
				TIME	6.10
			3	FLOW	958.
				TIME	6.10
			4	FLOW	958.
				TIME	6.10

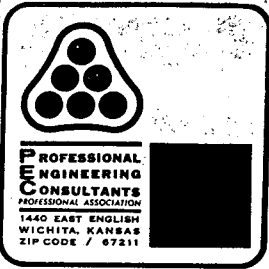
ROUTED TO

+	POND4	.88	1	FLOW	756.
				TIME	6.90
			2	FLOW	584.
				TIME	7.40
			3	FLOW	683.
				TIME	7.20
			4	FLOW	740.
				TIME	7.00

\*\* PEAK STAGES IN FEET \*\*

1	STAGE	1327.27
	TIME	6.90
2	STAGE	1326.28
	TIME	7.40
3	STAGE	1324.56
	TIME	7.20
4	STAGE	1323.55
	TIME	7.00

\*\*\* NORMAL END OF HEC-1 \*\*\*



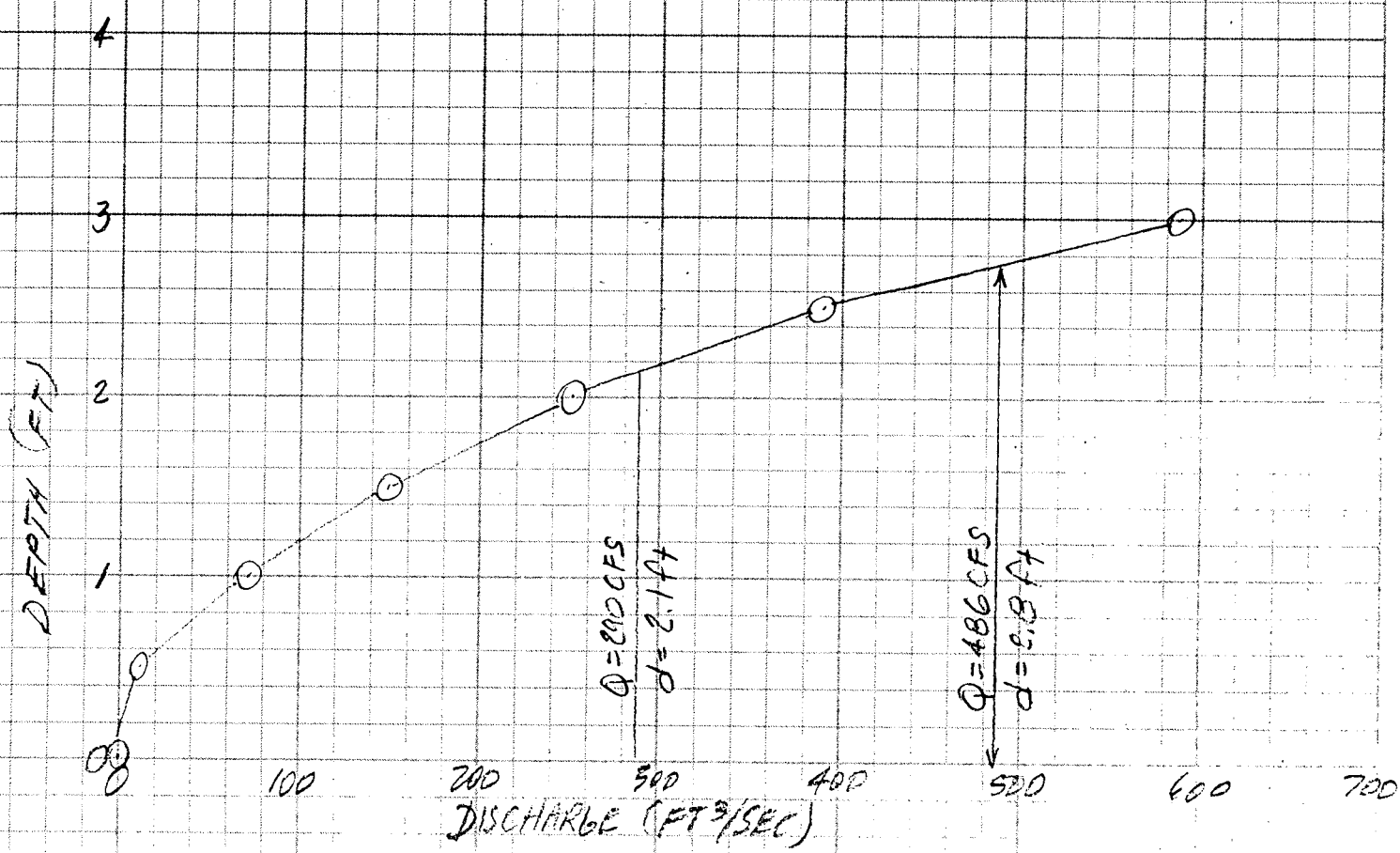
Date 2/8/93 MMB Page \_\_\_\_\_ of \_\_\_\_\_

Project FOREST LALES

Item 29TH ST DITCH CAPACITY

SLOPE = 1%  
 B = 10' Z = 4:1:1 RETARDANCE CLASS E

FLOW DEPTH	AREA	HYD. R.	VEL.	DISCHARGE
0.5	6	0.4	2.0	12
1.0	15	0.8	4.7	71
1.5	24	1.1	6.2	149
2.0	36	1.35	7.0	252
2.5	50	1.65	7.8	390
3.0	66	1.9	8.4	587
3.5	84	2.15	9.1	764
4.0	110	2.45		
4.5	125	2.7		
5.0	150	2.92		





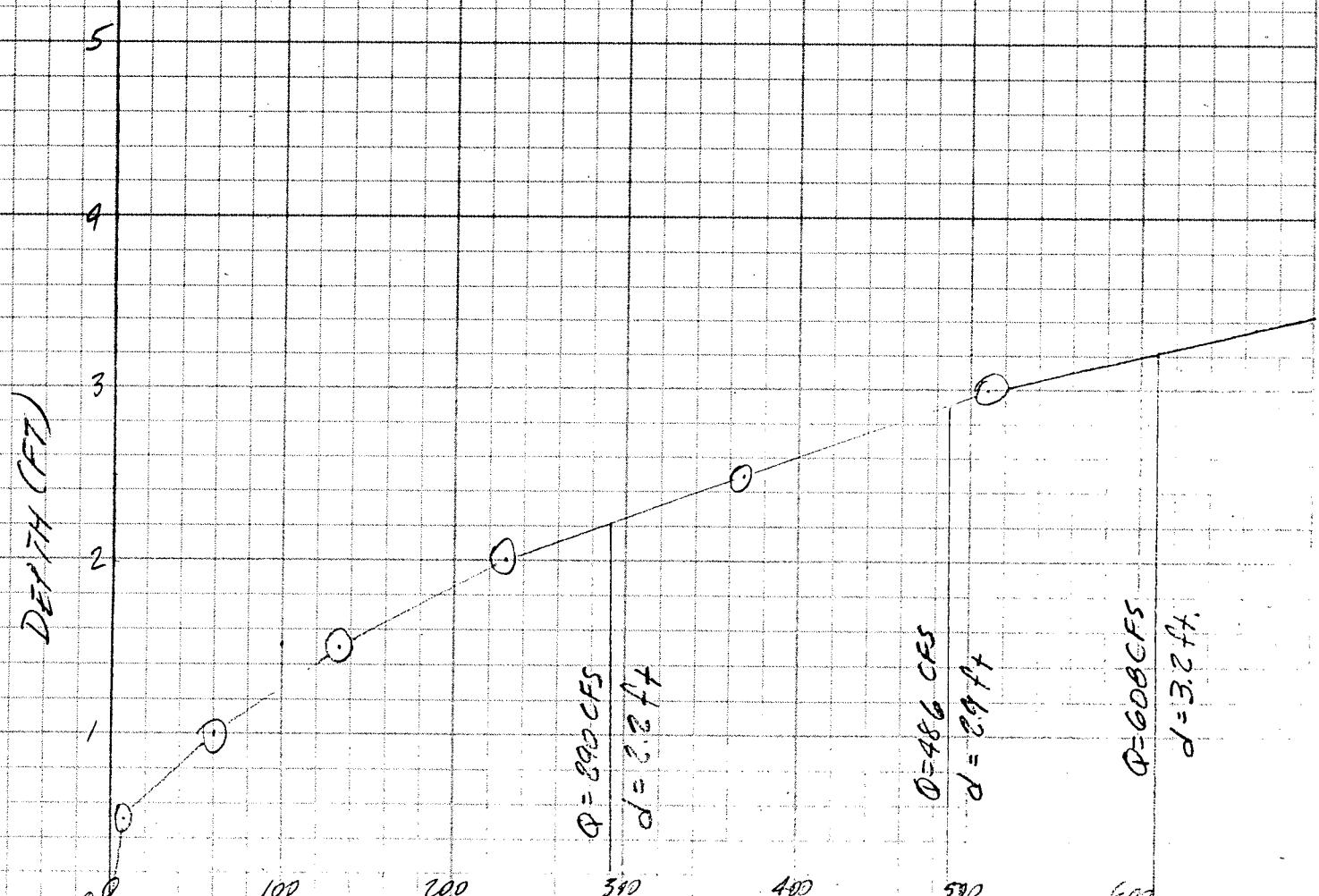
Date 2/8/93 MWB Page \_\_\_\_\_ of \_\_\_\_\_

Project FOREST LAKES

Item 29TH ST DITCH CAPACITY

SLOPE = 0.8%  
 B = 10' Z = 4:1 RETARDANCE CLASS E

FLOW DEPTH ft	AREA ft <sup>2</sup>	HYDR. RAD ft	VEL. ft/sec	Q ft <sup>3</sup> /sec
0.5	6	0.4	1.8	11
1.0	15	0.8	4.0	60
1.5	24	1.1	5.6	134
2.0	36	1.35	6.4	230
2.5	50	1.65	7.4	370
3.0	66	1.9	7.7	508
3.5	84	2.15	8.6	722
4.0	110	2.45	9.2	





Date 10/24/92 MWB Page        of       

Project FOREST LAKES

Item DITCH CAPACITY

SLOPE = 0.2%

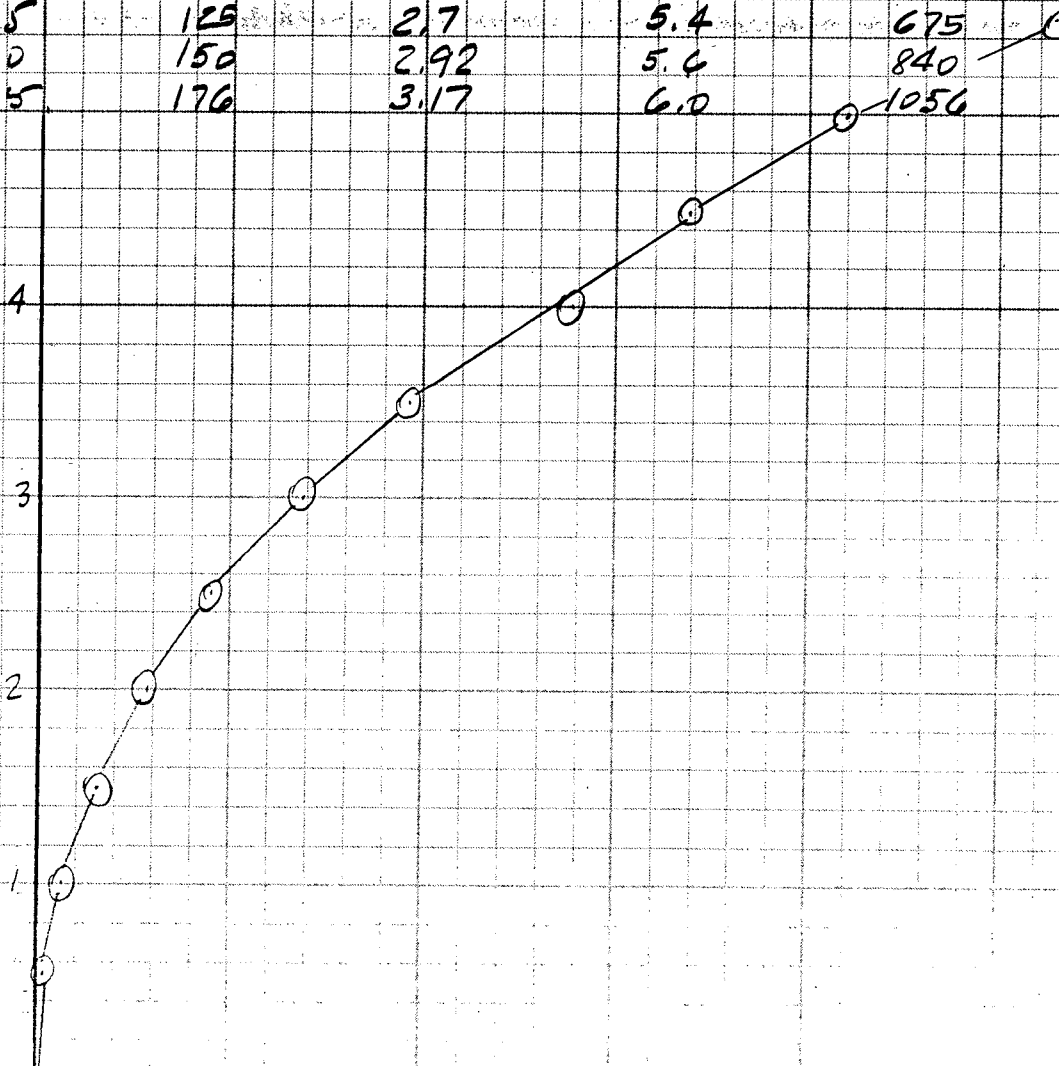
B = 10'

Z = 4:1

RETARDANCE CLASS E

FLOW DEPTH ft	AREA ft <sup>2</sup>	HYDRAULIC RADIUS ft	VELOCITY ft/sec	DISCHARGE ft <sup>3</sup> /sec
0.5	0	0.4	0.58	3.5
1.0	15	0.8	1.7	25.5
1.5	24	1.1	2.4	57.6
2.0	36	1.35	3.2	115.2
2.5	50	1.65	4.7	185.0
3.0	66	1.9	4.2	277
3.5	84	2.15	4.6	386
4.0	110	2.45	5.0	550
4.5	125	2.7	5.4	675
5.0	150	2.92	5.6	840
5.5	176	3.17	6.0	1056

DEPTH OF FLOW (FT)



# RETARDANCE CLASS E

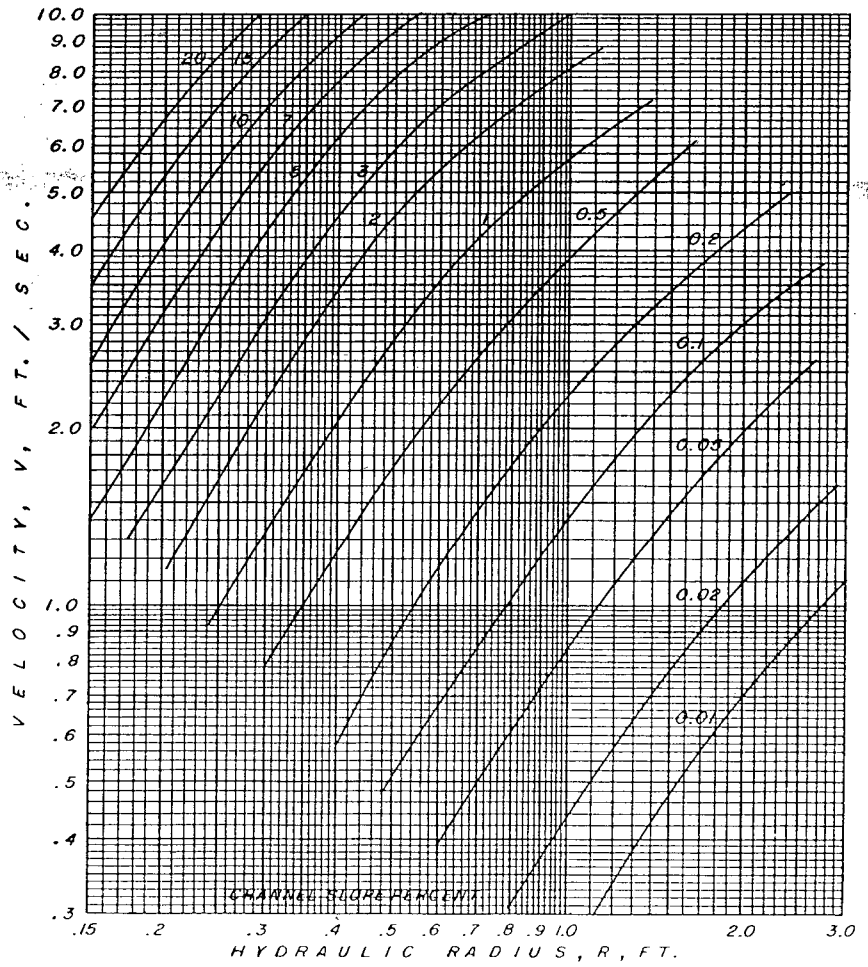
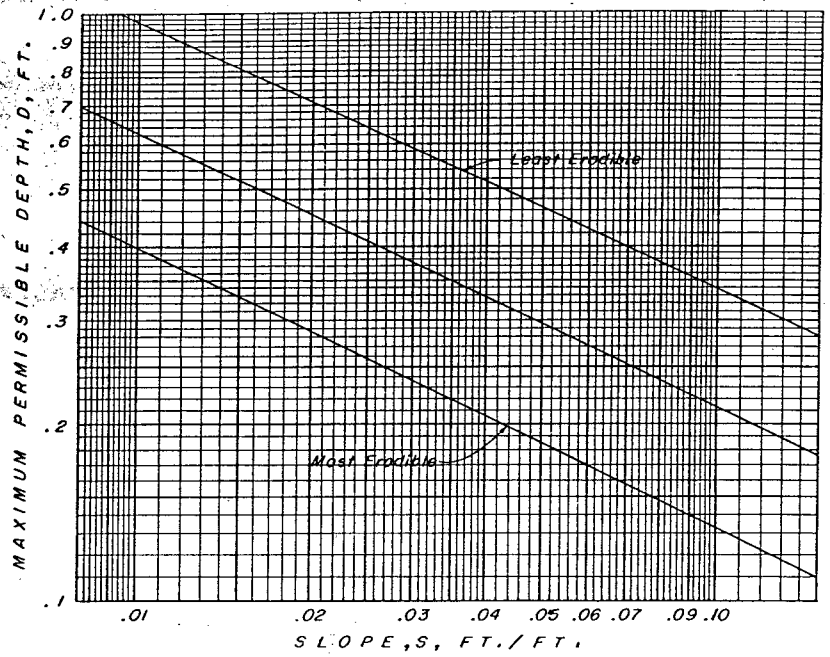


Figure 3D-4-1-1-E

# HYDRAULIC PROPERTIES OF TRAPEZOIDAL CHANNELS (AREA OF FLOW)

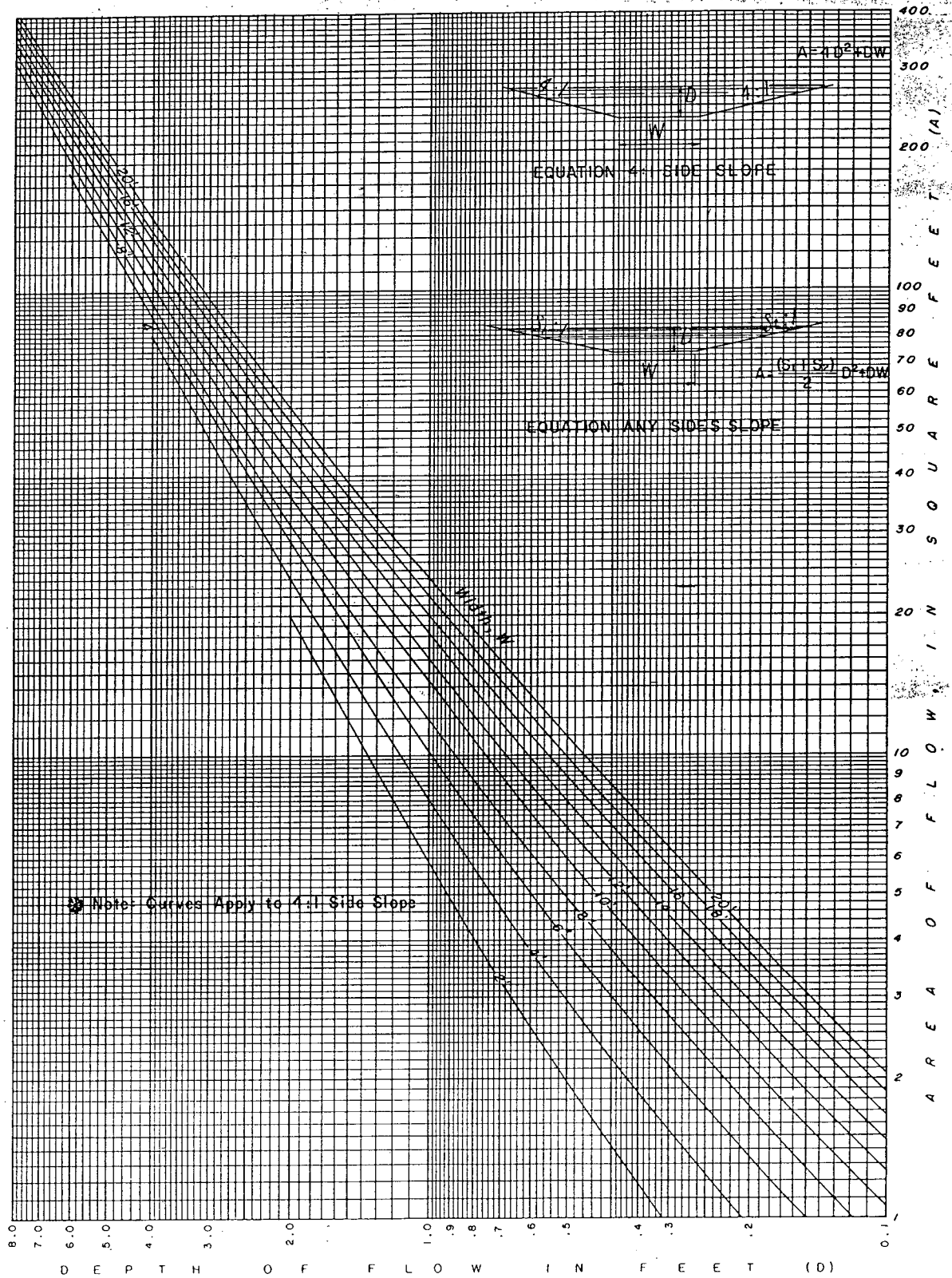


Figure 3D-4-1-1-3-A

# HYDRAULIC PROPERTIES OF TRAPEZOIDAL CHANNELS (HYDRAULIC RADIUS)

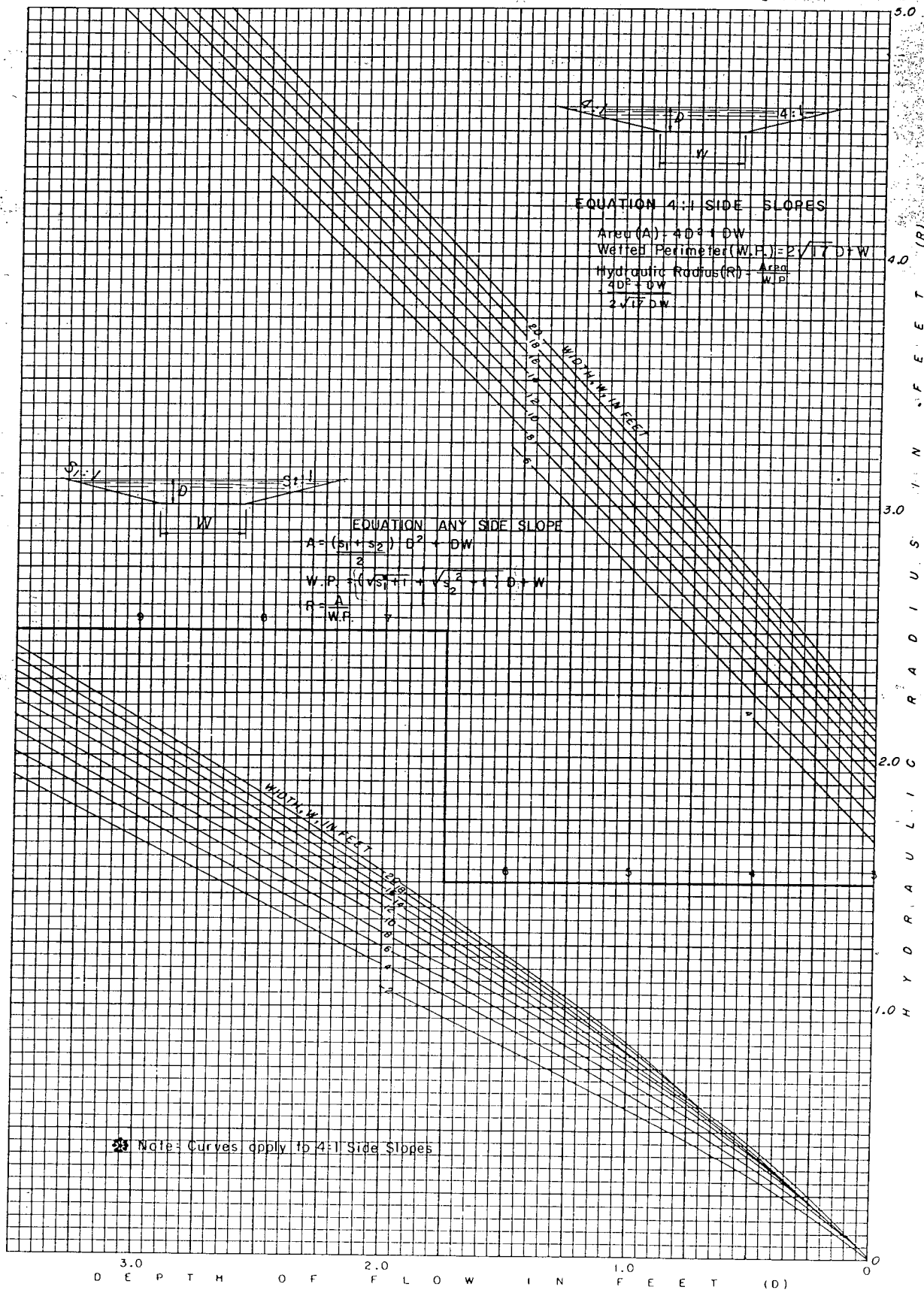


Figure 3D-4-1-1-3-B

NW CORNER  
NW 1/4-4-27-1W

29TH

70 AC ±

NE COR.  
NW 1/4 4-27-1W

1"=100'

TILER

ASSUMED  
DA BOUNDARY (TYP.)

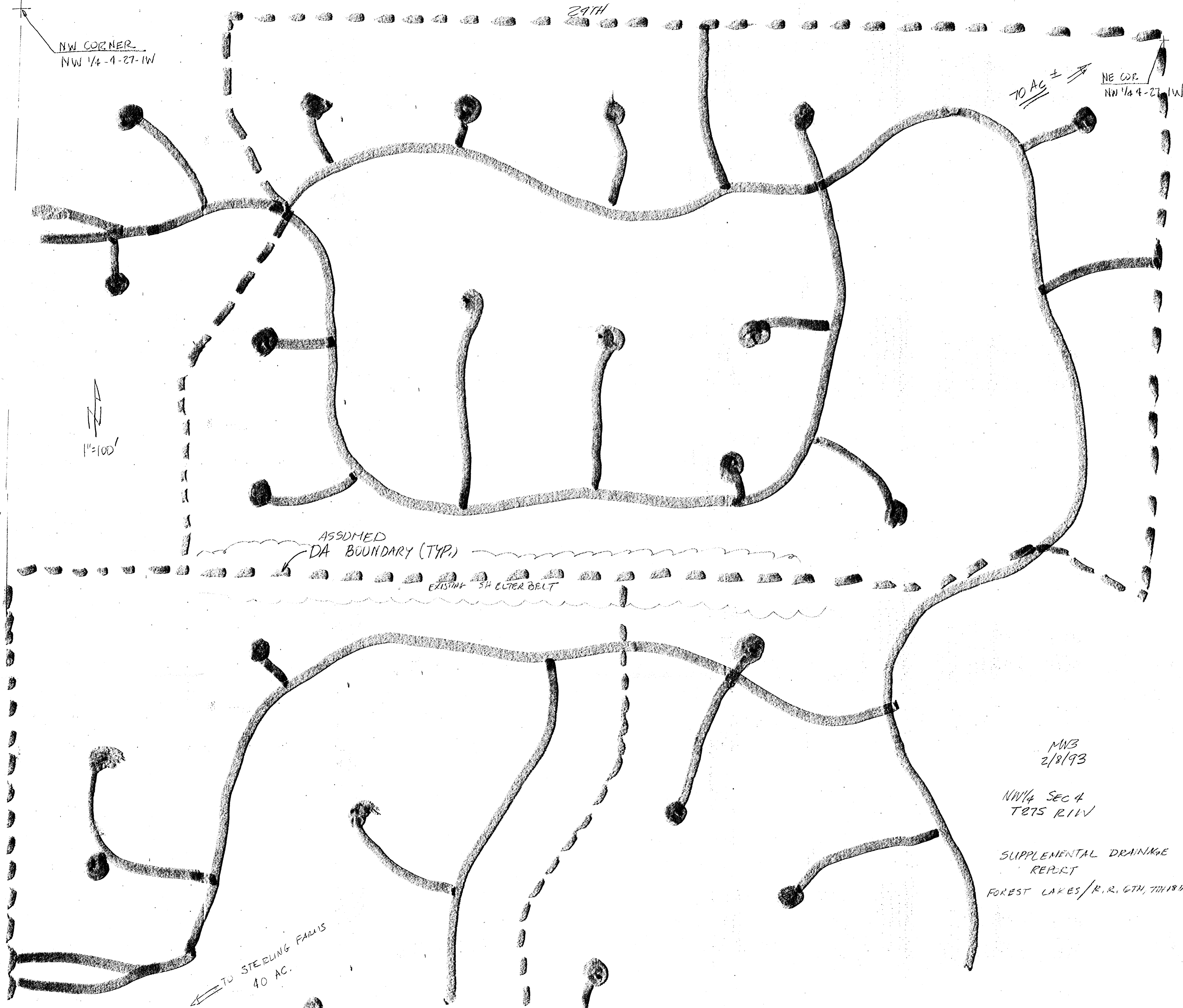
EXISTING SH OUTER BELT

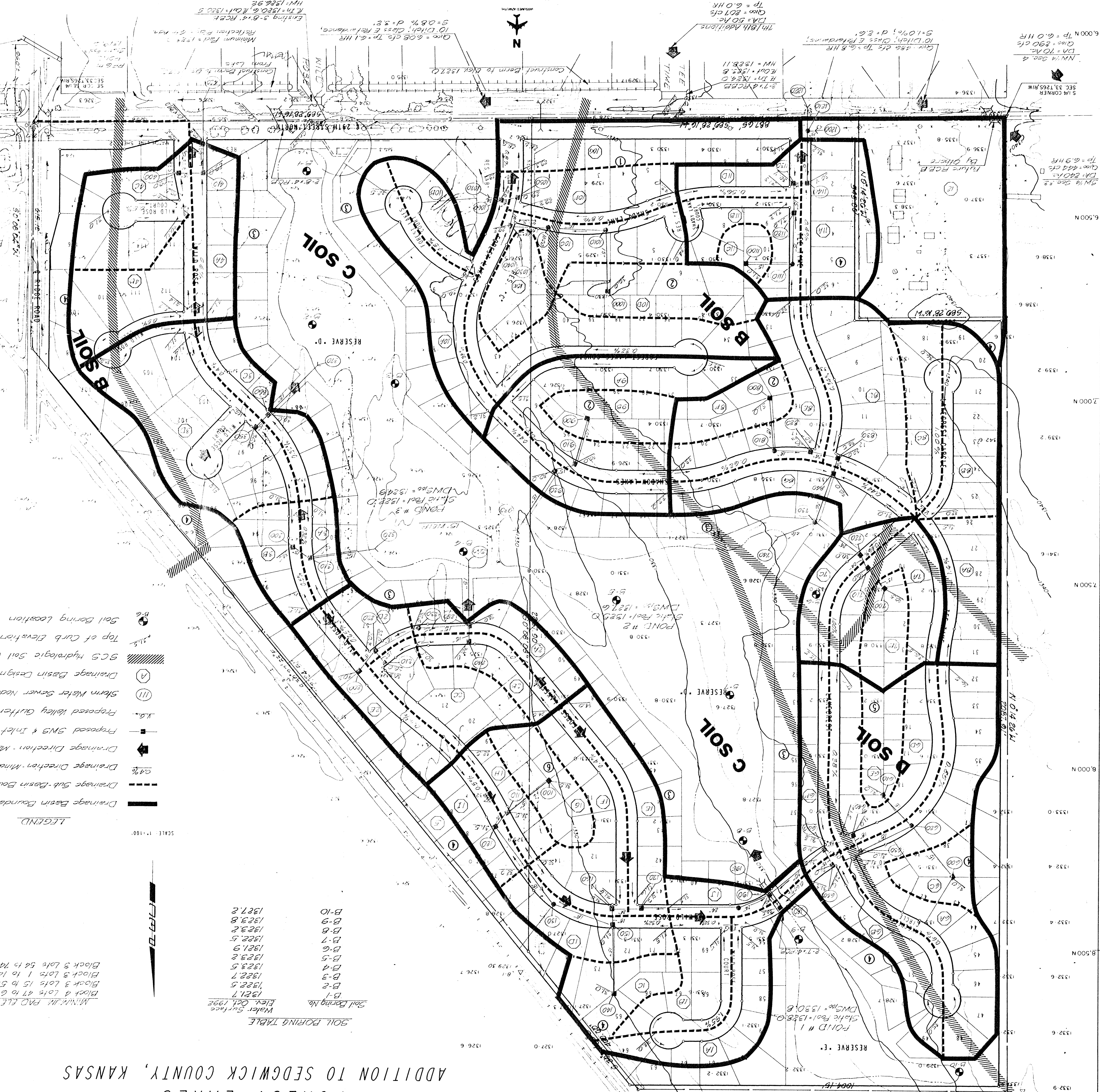
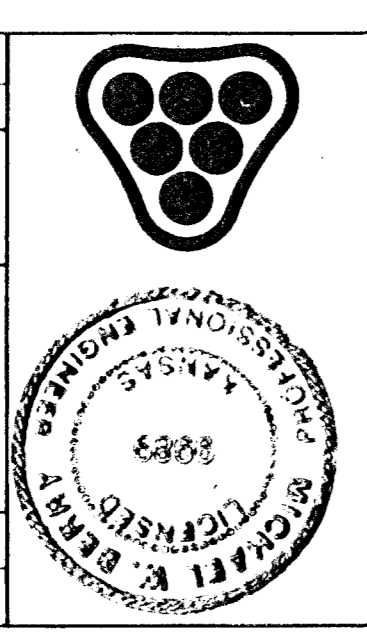
MWB  
2/8/93

NW 1/4 SEC 4  
T875 R11W

SUPPLEMENTAL DRAINAGE  
REPORT  
FOREST LAKES/R.R. GTR, THRU 1994

TO STERLING FARMS  
40 AC.





- LEGEND**
- Drainage Basin Boundary
  - - - Drainage Sub-Basin Boundary
  - Drainage Direction - Minor Storm & St. Grnd.
  - Drainage Direction - Major Storm
  - Proposed SWS & Inlet
  - Proposed Valley Gutter
  - Storm Water Sewer Node Designation
  - Drainage Basin Designation
  - SCS Hydrologic Soil Group
  - Top of Curb Elevation
  - Soil Boring Location

**WATER SURFACE ELEVATIONS**

Block 4 Lots 47 to 60	1327.0
Block 3 Lots 15 to 53	1327.0
Block 3 Lots 1 to 14	1327.0
Block 3 Lots 54 to 74	1327.0
Block 2 Lots 1 to 10	1327.2
Block 1 Lots 1 to 10	1327.2
Block 1 Lots 11 to 20	1327.2
Block 1 Lots 21 to 30	1327.2
Block 1 Lots 31 to 40	1327.2
Block 1 Lots 41 to 50	1327.2
Block 1 Lots 51 to 60	1327.2
Block 1 Lots 61 to 70	1327.2
Block 1 Lots 71 to 80	1327.2
Block 1 Lots 81 to 90	1327.2
Block 1 Lots 91 to 100	1327.2

**SOIL BORING TABLE**

Soil Boring No.	Water Surface Elev. Oct. 1992
B-1	1327.7
B-2	1327.5
B-3	1327.5
B-4	1327.5
B-5	1327.5
B-6	1327.5
B-7	1327.5
B-8	1327.5
B-9	1327.8
B-10	1327.2

**FOREST LAKES**  
ADDITION TO SEDGWICK COUNTY, KANSAS

9.000 N  
 8.500 N  
 8.000 N  
 7.500 N  
 7.000 N  
 6.500 N  
 6.000 N  
 5.500 N  
 5.000 N  
 4.500 N  
 4.000 N  
 3.500 N  
 3.000 N  
 2.500 N  
 2.000 N  
 1.500 N  
 1.000 N  
 0.500 N  
 0.000 N

7.500 E  
 7.000 E  
 6.500 E  
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