



Drainage Plan for
Casa Bella Addition
Wichita, Sedgwick County, Kansas
July 1, 2005

Ruggles & Bohm P.A.

Engineering, Surveying, Land Planning

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Wichita, Kansas 67203

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July 1, 2005

Vicky Huang, P.E.
Subdivision Engineer
City of Wichita – 7th Floor
455 N. Main
Wichita, KS 67202

Re: Final Drainage Plan for Casa Bella Addition

Dear Ms. Huang,

Attached with this letter are the drainage calculations and supporting information for Casa Bella Addition. The report consists of the pond routing calculations with detailed output from HEC-1, followed by interior pipe and structure analysis and sizing. All of the storm water sewer system designs will be validated by the use of Hasted Methods StormCAD program at the time of final design. Similarly, all pond design (both storage and outlet capabilities) will be re-routed at the time of final design.

Also included with this report is a four-corner lot grading plan for Casa Bella Addition, and a drainage plan map.

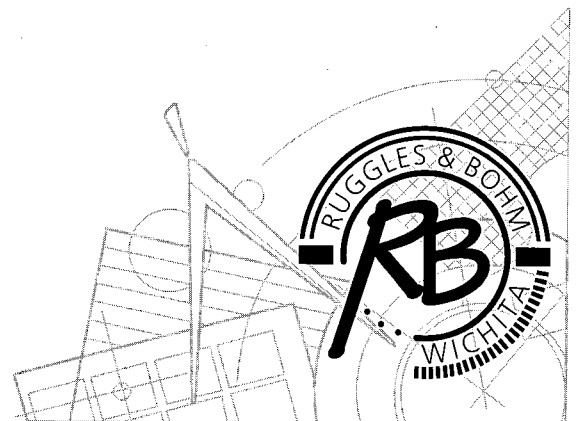
Please review this information and advise me of any questions or comments you may have.

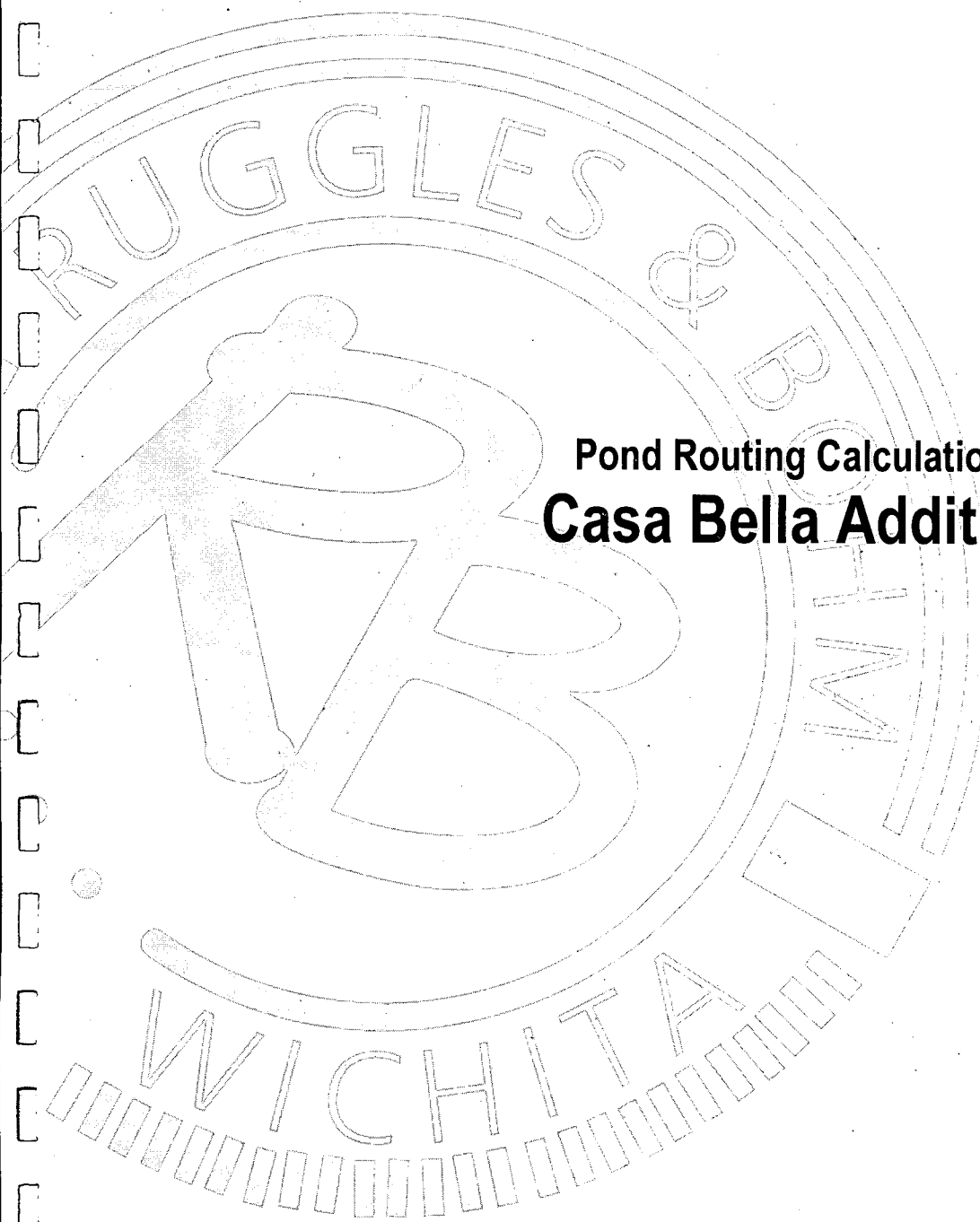
Regards,



Christopher M. Bohm, P.E.

Encl.





Pond Routing Calculations
Casa Bella Addition

Ruggles & Bohm P.A.

Engineering, Surveying, Land Planning

Cass Bella Addition:
Drainage Calcs.

4/6/05
CMB
1/6

Total Orig. Area to North Line of
Cass Bella = 196 Acres = 0.306 sq. mi.

Tc, velocity method: D = 3900 feet

First 400' sheet flow, $V_1 = 0.28$ f/sec
(Pasture @ 1.0%)

Next 400' Grassed Waterway @ 1.0%
 $V_2 = 1.12$ f/sec

Next 300' Channel, Assume $V = 2.0$ f/sec

Balance of Distance = 2300 feet, Assume
Channel Velocity = 2.5 f/sec

$$T_c = 400' / (0.28)(60) + 400' / (1.12)(60) + 300' / (2.0)(60) + 2300' / (2.5)(60) = 52 \text{ minutes (seems reasonable).}$$

$$S_C L_{eq} = 0.16 T_c; S_b L_{eq} = 0.52 \text{ hours}$$

Hydrological Soil Group "D" (Clay Soil)

2/00

Current Land Use = Crops, Small grain,
good condition; CN = 87

There is a small amount of existing residential
property in the basin, however, this is
a very small percentage, so ignore.

Determine the existing peak flow from
the watershed using HEC-1.

File = CASA.hcl CASA.out

Results: $Q_{100} = \underline{436}$ cfs natural
from Basin.

Developed Basin: of the 196 Acres in
the basin, new development = 133 Acres

$$\text{Find New } \overline{CN} = \frac{((196 \text{ Ac} - 133 \text{ Ac}) 87 + 133(91))}{196 \text{ Ac}}$$

$\overline{CN} = 89.7$ OR use 90 developed CN.

Time of concentration offsite will not
be affected, however local, onsite travel

3/4

times will be reduced (somewhat).
Assume T_c will be reduced by 20%
due to development,

$$\text{or } T_{cD} = 0.8 (T_c) = 0.8 (52 \text{ min})$$

$$T_{cD} = 42 \text{ minutes,}$$

SCS Lag = $0.16 T_c$, so \rightarrow SCS Lag = 0.42 hrs
for developed condition.

Detention Requirements, CASA BELLA
Addition, target Q max out developed
condition = 436 cfs.

Pond System Design:

Pond A (South Pond)

Pond B (South Res C Pond)

Pond C (North Res C Pond)

Pond D (Future Pond on Unplatted Tract).

Route such that Pond A, B, C provide
All of the Detention Required. Pond D
is future, so ignore storage in this pond.

So, Q_{100} from Pond C + Developed flow
@ Pond D site total discharge ≤ 436 cfs.

Developed Condition Pond Routing: 4/6

Pond A: $D_A = 81$ Acres, $T_c = 30$ min

(From V_1, V_2 , original T_c Run)

$$\overline{CN} = \frac{(53 \text{ Ac (Und)}) (87) + (28 \text{ Ac (Dev)}) (91)}{81}$$

$\overline{CN} = 88$ Developed Pond A.

$T_c = V_1 + V_2$ from previous calculation = 30 min
SCS lag = $0.6 T_c = 0.30$ Hours

Q_{100} Pond A = 198 cfs

USE Single 5' x 4' RCBC outlet

w/ Soil Saver US @ 1344.0

(See Box 1 output for P Curve)

Pond A:	<u>Elev</u>	<u>Ac</u>
	1344	1.35 Ac
	1348	1.76 Ac

Route w/ Basin A; $Q_{out} = 160$ cfs
@ Elev = 1347.0

OK For Now

Pond E (Far West Side, Reserve J) $\frac{5}{6}$

BA = 11.0 AC

$T_c = 20$ min, Lag = 0.20 hrs

CN = 88 (Developed)

Pond E Data

1346 0.8

1349 1.0

Q_{100} in = 28 cfs

Try 24" RCP

		<u>H_w/D</u>	<u>Q</u>
1346	-	-	0.5
46 ^s	0.5	0.125	1
47	1	0.15	4.5
47 ^s	1.5	0.175	9
48 ^o	2	1	14
48 ^s	2.5	1.25	18

OK - Q out = 16 cfs @ 1348.3 Elev

POND B: (Developed)

6/6

$B_A = 37$ Acres (All on site)

$CN = 91$

$T_c = 30 \text{ min} = \text{SCS Lag} = 0.30 \text{ hours}$

Add Hydro Pond A and Pond E to
Pond B Hydro for total Q_{in}

Pond Data: Pond B

@ 1339.5 = 2.2 AC 12.5' weir wall

@ 1343 = 2.7 AC

$Q_{out} = 242 \text{ cfs}$, Stage = 1342.96 (1343) OK

Pond Data, Pond C

$B_A = 51$ Acres; Assume that all will
be developed = $CN = 91$

$T_c = 30 \text{ min}$, SCS Lag = 0.30 hours

Add to Pond B out-flow = peak $I_n = 352 \text{ cfs}$.

SINGLE 5' x 4' REBC 10' TAILWATER / MITERED E.S.

tmp#1.txt

N = 0.013

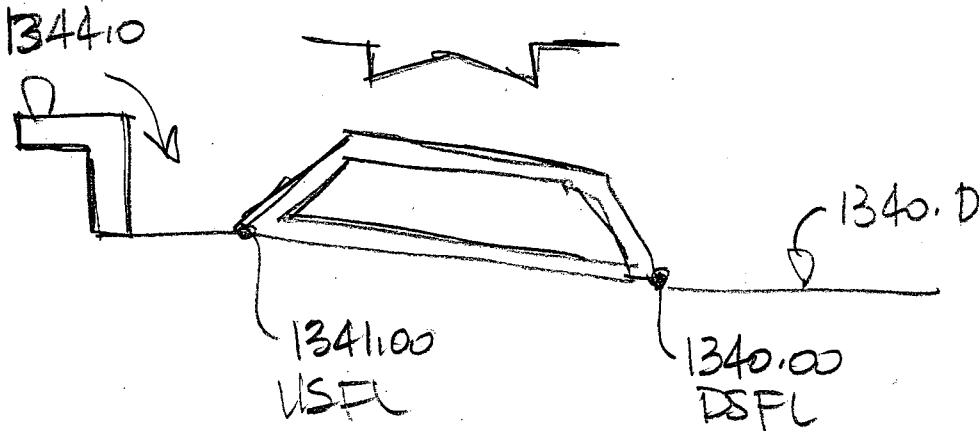
#Units=Flowrate,cfs,Elevation,ft,Elevation,ft,Elevation,ft
Flowrate Outlet Elev Inlet Elev Cntrl Elev
#-----

10.0000,	0.0000,	1341.8041,	1341.8041
20.0000,	0.0000,	1342.3027,	1342.3027
30.0000,	0.0000,	1342.7231,	1342.7231
40.0000,	0.0000,	1343.0997,	1343.0997
50.0000,	0.0000,	1343.4467,	1343.4467
60.0000,	0.0000,	1343.7719,	1343.7719
70.0000,	0.0000,	1344.0800,	1344.0800
80.0000,	0.0000,	1344.3741,	1344.3741
90.0000,	0.0000,	1344.6567,	1344.6567
100.0000,	0.0000,	1344.9292,	1344.9292
110.0000,	0.0000,	1345.1931,	1345.1931
120.0000,	0.0000,	1345.4494,	1345.4494
130.0000,	0.0000,	1345.6989,	1345.6989
140.0000,	0.0000,	1345.9423,	1345.9423
150.0000,	0.0000,	1346.5517,	1346.5517
160.0000,	0.0000,	1346.9564,	1346.9564
170.0000,	0.0000,	1347.3054,	1347.3054
180.0000,	0.0000,	1347.6755,	1347.6755
190.0000,	0.0000,	1348.0668,	1348.0668
200.0000,	0.0000,	1348.4792,	1348.4792

USFL 1341.0

DSFL 1340.0

US SOIL SAVER ELEV = 1344.0



POND A OUTLET STRUCTURE

HEC1 S/N: 1343000364 HMVersion: 6.33 Data File: casa.hcl

```
*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
ENGINEERS *
* MAY 1991 *
CENTER *
* VERSION 4.0.1E *
*
*
95616 *
* RUN DATE 04/19/2005 TIME 10:09:05 *
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*
* U.S. ARMY CORPS OF
* HYDROLOGIC ENGINEERING
*
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA
*
* (916) 756-1104
*
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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX
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::::::::::::::::::::::::::::::::::::
::::::::::::::::::::::::::::::::::::
::: Full Microcomputer Implementation :::
::: by :::
::: Haestad Methods, Inc. :::
::: :::
::::::::::::::::::::::::::::::::::::
::::::::::::::::::::::::::::::::::::
```

37 Brookside Road * Waterbury, Connecticut 06708 * (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.
THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT
STRUCTURE.
THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77
VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

```

LINE          ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*** FREE ***
1             *DIAGRAM
2             ID      CASA BELLA ADDITION POND ROUTING CALCULATIONS
3             ID      24-HOUR STORM W/15 MINUTE DISTRIBUTION AND SCS UNIT HYDROGRAPH AND LAG METHO
4             ID      NATURAL DRAINAGE AREA TO POND SITE
5             IT      5
6             IN      30
7             IO      4
8             KK      UNDEV
9             * TOTAL DRAINAGE AREA TO 2-36" RCP PIPES UNDER MT. VERNON
10            * USED TO DETERMINE MAXIMUM OUTFLOW FROM SITE
11            PB      7.8
12            PC      0      2      4      6      9      12      15      19      27      46
13            PC      62     68     72     76     79     82     85     87     90     92
14            PC      94     96     98     99     100
15            BA      0.306
16            UD      0.52
17            LS      0      87
18            KK      ADEV
19            * BASIN A (SOUTH POND) IN DEVELOPED CONDITION
20            BA      0.127
21            UD      0.30
22            LS      0      88
23            KK      PONDA
24            * POND DATA FOR SOUTH POND, DEVELOPED BASIN A WILL BE ROUTED THROUGH THIS POND
25            * OUTLET STRUCTURE A SINGLE 5'x4' RCBC
26            RS      1      ELEV 1344.0
27            SA      1.35   1.76
28            SE      1344   1348
29            SQ      0      10     50     90     130    160    180
30            * NOTE ELEVATIONS ARE LOWER ON OUTFLOW - SOIL SAVER UPSTREAM CONTROLS STORAGE
31            SE      1341   1341.8 1343.4 1344.65 1345.69 1346.95 1347.67
32            KO      0      0      0      0      21
33            KK      EDEV
34            * AREA FOR POND E IN DEVELOPED CONDITION
35            BA      0.017
36            UD      0.30
37            LS      0      88
38            KK      PONDE
39            * STAGE STORAGE DATA FOR POND E
40            * OUTLET STRUCTURE IS 24 INCH RCP (INLET CONTROLLED)
41            RS      1      ELEV 1347
42            SA      0.8    1.0
43            SE      1346   1349
44            SQ      0      1      4.5    9      14     18
45            SE      1346   1346.5 1347   1347.5 1348   1348.5
    
```

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

36      KK  BDEV
          * DATA FOR DEVELOPED AREA B
37      BA  0.058
38      UD  .30
39      LS  0      91

40      KK  ABACK
41      BI  PONDA 21
          * NOTE - THE BI CARD BRINGS FORWARD THE DATA FROM PONDA SO HYDROGRAPHS PONDA
          * POND E AND BASIN B CAN BE COMBINED INTO ONE INPUT HYDROGRAPH FOR POND B

42      KK  COMB
43      HC  3
          * THIS HAS CALCULATED THE INFLOW HYDROGRAPH INTO POND B

44      KK  PONDB
          * STAGE STORAGE DATA FOR POND B
          * OUTLET STRUCTURE IS 12.5 FOOT WEIR WALL
45      RS  1      ELEV 1339.50
46      SA  2.2    2.7    2.8
47      SE  1339.5  1343   1344
48      SQ  0      13.3   37.5   68.9   106.1  148.2  194.9  245.5  300
49      SE  1339.5  1340   1340.5  1341   1341.5  1342   1342.5  1343   1343.5

50      KK  CDEV
          * DATA FOR DEVELOPED AREA C
51      BA  0.080
52      UD  0.30
53      LS  0      91

54      KK  COMB2
          * COMBINE AREA C HYDROGRAPH WITH OUTLET HYDROGRAPH FROM POND B
          * THIS WILL GENERATE THE INFLOW HYDROGRAPH FOR POND C
55      HC  2

56      KK  PONDC
          * STAGE STORAGE DATA FOR POND C
          * OUTLET STRUCTURE IS A 20 FOOT WEIR WALL
57      RS  1      ELEV 1334
58      SA  2.3    3.0
59      SE  1334   1337
60      SQ  0      21      60      110     169     237     312     392
61      SE  1334   1334.5  1335   1335.5  1336   1336.5  1337   1337.5
62      ZZ
    
```

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
7	UNDEV	
15	.	ADEV
	.	V
	.	V
19	.	PONDA
26	.	EDEV
	.	V
	.	V
30	.	PONDE
36	.	.
	.	BDEV
40	.	.
	.	ABACK
42	.	COMB.....
	.	V
	.	V
44	.	PONDB
50	.	.
	.	CDEV
54	.	COMB2.....
	.	V
	.	V
56	.	PONDC

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
ENGINEERS *
* MAY 1991 *
CENTER *
* VERSION 4.0.1E *
*
*
95616 *
* RUN DATE 04/19/2005 TIME 10:09:05 *
*
*
*****
*****
    
```

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 609 SECOND STREET
 DAVIS, CALIFORNIA
 (916) 756-1104

CASA BELLA ADDITION POND ROUTING CALCULATIONS
 24-HOUR STORM W/15 MINUTE DISTRIBUTION AND SCS UNIT HYDROGRAPH AND LAG METHO
 NATURAL DRAINAGE AREA TO POND SITE

```

6 IO      OUTPUT CONTROL VARIABLES
          IPRNT      4  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL      0.  HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA
          NMIN       5  MINUTES IN COMPUTATION INTERVAL
          IDATE      1  0  STARTING DATE
          ITIME      0000 STARTING TIME
          NQ         289 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE     2  0  ENDING DATE
          NDTIME     0000 ENDING TIME
          ICENT      19  CENTURY MARK

          COMPUTATION INTERVAL 0.08 HOURS
          TOTAL TIME BASE      24.00 HOURS
    
```

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-Feet
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

```

*****
*
* UNDEV *
*
*****
    
```

```

5 IN      TIME DATA FOR INPUT TIME SERIES
          JXMIN      30  TIME INTERVAL IN MINUTES
          JXDATE     1  0  STARTING DATE
          JXTIME     0  0  STARTING TIME
    
```

SUBBASIN RUNOFF DATA

```

12 BA     SUBBASIN CHARACTERISTICS
          TAREA      0.31 SUBBASIN AREA
    
```

PRECIPITATION DATA

```

8 PB      STORM      7.80 BASIN TOTAL PRECIPITATION
    
```

```

9 PI      INCREMENTAL PRECIPITATION PATTERN
          0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.33
          0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.50 0.50
          0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50
          0.50 0.50 0.50 0.50 0.50 0.50 0.67 0.67 0.67 0.67
          0.67 0.67 1.33 1.33 1.33 1.33 1.33 1.33 1.33 1.33
          1.00 1.00 3.17 3.17 3.17 2.67 2.67 2.67 2.67 2.67
          1.00 1.00 1.00 1.00 1.00 1.00 1.00 0.67 0.67 0.67
          0.67 0.67 0.67 0.67 0.67 0.67 0.67 0.67 0.50 0.50
          0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50
          0.50 0.50 0.50 0.50 0.50 0.50 0.33 0.33 0.33 0.33
          0.33 0.33 0.50 0.50 0.50 0.50 0.50 0.50 0.33 0.33
          0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.33
          0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.33
          0.17 0.17 0.17 0.17 0.17 0.17 0.17 0.17 0.17 0.17
    
```

```

14 LS     SCS LOSS RATE
          SIRTLE     0.30 INITIAL ABSTRACTION
    
```

CRVNBR 87.00 CURVE NUMBER
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

13 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 0.52 LAG

UNIT HYDROGRAPH
 33 END-OF-PERIOD ORDINATES

17.	49.	101.	170.	228.	259.	262.	247.	219.	183.
139.	106.	83.	66.	52.	41.	32.	25.	20.	15.
12.	10.	8.	6.	5.	4.	3.	2.	2.	1.
1.	1.	0.							

 * ADEV *

SUBBASIN RUNOFF DATA

16 BA SUBBASIN CHARACTERISTICS
 TAREA 0.13 SUBBASIN AREA

PRECIPITATION DATA

8 PB STORM 7.80 BASIN TOTAL PRECIPITATION

9 PI INCREMENTAL PRECIPITATION PATTERN

0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.67	0.67	0.67	0.67
0.67	0.67	1.33	1.33	1.33	1.33	1.33	1.33	1.33	3.17	3.17
3.17	3.17	3.17	3.17	3.17	2.67	2.67	2.67	2.67	2.67	2.67
1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.67	0.67	0.67	0.67
0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.33	0.33	0.33	0.33
0.33	0.33	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.33	0.33
0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
0.33	0.33	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17
0.17	0.17	0.17	0.17	0.17						

18 LS SCS LOSS RATE
 STRTL 0.27 INITIAL ABSTRACTION
 CRVNBR 88.00 CURVE NUMBER
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

17 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 0.30 LAG

UNIT HYDROGRAPH
 20 END-OF-PERIOD ORDINATES

25.	81.	154.	180.	165.	129.	82.	55.	38.	25.
17.	11.	8.	5.	3.	2.	2.	1.	1.	0.

 * PONDA *

25 KO OUTPUT CONTROL VARIABLES

IPRNT	4	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	289	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.083	TIME INTERVAL IN HOURS

HYDROGRAPH ROUTING DATA

20 RS STORAGE ROUTING

NSTPS	1	NUMBER OF SUBREACHES
ITYP	ELEV	TYPE OF INITIAL CONDITION
RSVRC	1344.00	INITIAL CONDITION
X	0.00	WORKING R AND D COEFFICIENT

21 SA AREA 1.4 1.8

22 SE ELEVATION 1344.00 1348.00
 23 SQ DISCHARGE 0. 10. 50. 90. 130. 160. 180.
 24 SE ELEVATION 1341.00 1341.80 1343.40 1344.65 1345.69 1346.95 1347.67

COMPUTED STORAGE-ELEVATION DATA

STORAGE 0.00 6.20
 ELEVATION 1344.00 1348.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE 0.00 0.00 0.00 0.00 0.90 2.42 4.41 5.63 6.20
 OUTFLOW 0.00 10.00 50.00 69.20 90.00 130.00 160.00 180.00 189.16
 ELEVATION 1341.00 1341.80 1343.40 1344.00 1344.65 1345.69 1346.95 1347.67 1348.00

 * EDEV *

SUBBASIN RUNOFF DATA

27 BA SUBBASIN CHARACTERISTICS
 TAREA 0.02 SUBBASIN AREA

PRECIPITATION DATA

8 PB STORM 7.80 BASIN TOTAL PRECIPITATION

9 PI INCREMENTAL PRECIPITATION PATTERN

0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.67	0.67	0.67	0.67
0.67	0.67	1.33	1.33	1.33	1.33	1.33	1.33	1.33	3.17	3.17
3.17	3.17	3.17	3.17	2.67	2.67	2.67	2.67	2.67	2.67	2.67
1.00	1.00	1.00	1.00	1.00	1.00	0.67	0.67	0.67	0.67	0.67
0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.33	0.33	0.33	0.33	0.33
0.33	0.33	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.33	0.33
0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
0.33	0.33	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17
0.17	0.17	0.17	0.17							

29 LS SCS LOSS RATE
 STRTL 0.27 INITIAL ABSTRACTION
 CRVNBR 88.00 CURVE NUMBER
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

28 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 0.30 LAG

UNIT HYDROGRAPH
 20 END-OF-PERIOD ORDINATES

3.	11.	21.	24.	22.	17.	11.	7.	5.	3.
2.	2.	1.	1.	0.	0.	0.	0.	0.	0.

 * PONDE *

HYDROGRAPH ROUTING DATA

31 RS STORAGE ROUTING
 NSTPS 1 NUMBER OF SUBREACHES
 ITYP ELEV TYPE OF INITIAL CONDITION
 RSVRIC 1347.00 INITIAL CONDITION
 X 0.00 WORKING R AND D COEFFICIENT

32 SA AREA 0.8 1.0

33 SE ELEVATION 1346.00 1349.00

34 SQ DISCHARGE 0. 1. 5. 9. 14. 18.

35 SE ELEVATION 1346.00 1346.50 1347.00 1347.50 1348.00 1348.50

COMPUTED STORAGE-ELEVATION DATA

STORAGE 0.00 2.69
ELEVATION 1346.00 1349.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE 0.00 0.41 0.83 1.27 1.73 2.20 2.69
OUTFLOW 0.00 1.00 4.50 9.00 14.00 18.00 22.00
ELEVATION 1346.00 1346.50 1347.00 1347.50 1348.00 1348.50 1349.00

* *
* BDEV *
* *

SUBBASIN RUNOFF DATA

37 BA SUBBASIN CHARACTERISTICS
TAREA 0.06 SUBBASIN AREA

PRECIPITATION DATA

8 PB STORM 7.80 BASIN TOTAL PRECIPITATION

9 PI INCREMENTAL PRECIPITATION PATTERN

0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.67	0.67	0.67	0.67	0.67
0.67	0.67	1.33	1.33	1.33	1.33	1.33	1.33	1.33	3.17	3.17
3.17	3.17	3.17	3.17	2.67	2.67	2.67	2.67	2.67	2.67	2.67
1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.67	0.67	0.67	0.67
0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.33	0.33	0.33	0.33
0.33	0.33	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.33	0.33
0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
0.33	0.33	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17
0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17

39 LS SCS LOSS RATE
STRTL 0.20 INITIAL ABSTRACTION
CRVNR 91.00 CURVE NUMBER
RTIMP 0.00 PERCENT IMPERVIOUS AREA

38 UD SCS DIMENSIONLESS UNITGRAPH
TLAG 0.30 LAG

UNIT HYDROGRAPH
20 END-OF-PERIOD ORDINATES

11.	37.	70.	82.	75.	59.	37.	25.	17.	11.
8.	5.	3.	2.	2.	1.	1.	1.	0.	0.

* *
* ABACK *
* *

41 BI READ STATION PONDA HYDROGRAPH FROM UNIT 21

* *
* COMB *
* *

43 HC HYDROGRAPH COMBINATION
ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

* *
* PONDB *
* *

HYDROGRAPH ROUTING DATA

45 RS STORAGE ROUTING
 NSTPS 1 NUMBER OF SUBREACHES
 ITYP ELEV TYPE OF INITIAL CONDITION
 RSVRIC 1339.50 INITIAL CONDITION
 X 0.00 WORKING R AND D COEFFICIENT

46 SA AREA 2.2 2.7 2.8

47 SE ELEVATION 1339.50 1343.00 1344.00

48 SQ DISCHARGE 0. 13. 38. 69. 106. 148. 195. 246. 300.

49 SE ELEVATION 1339.50 1340.00 1340.50 1341.00 1341.50 1342.00 1342.50 1343.00 1343.50

COMPUTED STORAGE-ELEVATION DATA

STORAGE	0.00	8.56	11.31
ELEVATION	1339.50	1343.00	1344.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	0.00	1.12	2.27	3.45	4.68	5.93	7.23	8.56	9.92	11.31
OUTFLOW	0.00	13.30	37.50	68.90	106.10	148.20	194.90	245.50	300.00	354.50
ELEVATION	1339.50	1340.00	1340.50	1341.00	1341.50	1342.00	1342.50	1343.00	1343.50	1344.00

* *
* CDEV *
* *

SUBBASIN RUNOFF DATA

51 BA SUBBASIN CHARACTERISTICS
 TAREA 0.08 SUBBASIN AREA

PRECIPITATION DATA

8 PB STORM 7.80 BASIN TOTAL PRECIPITATION

9 PI INCREMENTAL PRECIPITATION PATTERN

0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.67	0.67	0.67	0.67
0.67	0.67	1.33	1.33	1.33	1.33	1.33	1.33	1.33	3.17	3.17
3.17	3.17	3.17	3.17	2.67	2.67	2.67	2.67	2.67	2.67	2.67
1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.67	0.67	0.67	0.67
0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.50	0.50
0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
0.33	0.33	0.50	0.50	0.50	0.50	0.50	0.33	0.33	0.33	0.33
0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
0.33	0.33	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17
0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17

53 LS SCS LOSS RATE
 STRTL 0.20 INITIAL ABSTRACTION
 CRVNR 91.00 CURVE NUMBER
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

52 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 0.30 LAG

UNIT HYDROGRAPH
20 END-OF-PERIOD ORDINATES

16.	51.	97.	113.	104.	81.	52.	35.	24.	16.
11.	7.	5.	3.	2.	1.	1.	1.	0.	0.

* *
* COMB2 *
* *

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*
*****
55 HC      HYDROGRAPH COMBINATION
           ICOMP      2  NUMBER OF HYDROGRAPHS TO COMBINE
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*****

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*****
*
*   PONDC   *
*
*****

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HYDROGRAPH ROUTING DATA

```

57 RS      STORAGE ROUTING
           NSTPS      1  NUMBER OF SUBREACHES
           ITYP      ELEV  TYPE OF INITIAL CONDITION
           RSVRIC    1334.00  INITIAL CONDITION
           X          0.00  WORKING R AND D COEFFICIENT

58 SA      AREA      2.3      3.0

59 SE      ELEVATION 1334.00 1337.00

60 SQ      DISCHARGE  0.      21.      60.      110.      169.      237.      312.      392.

61 SE      ELEVATION 1334.00 1334.50 1335.00 1335.50 1336.00 1336.50 1337.00 1337.50

```

COMPUTED STORAGE-ELEVATION DATA

```

STORAGE      0.00      7.93
ELEVATION    1334.00 1337.00

```

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

```

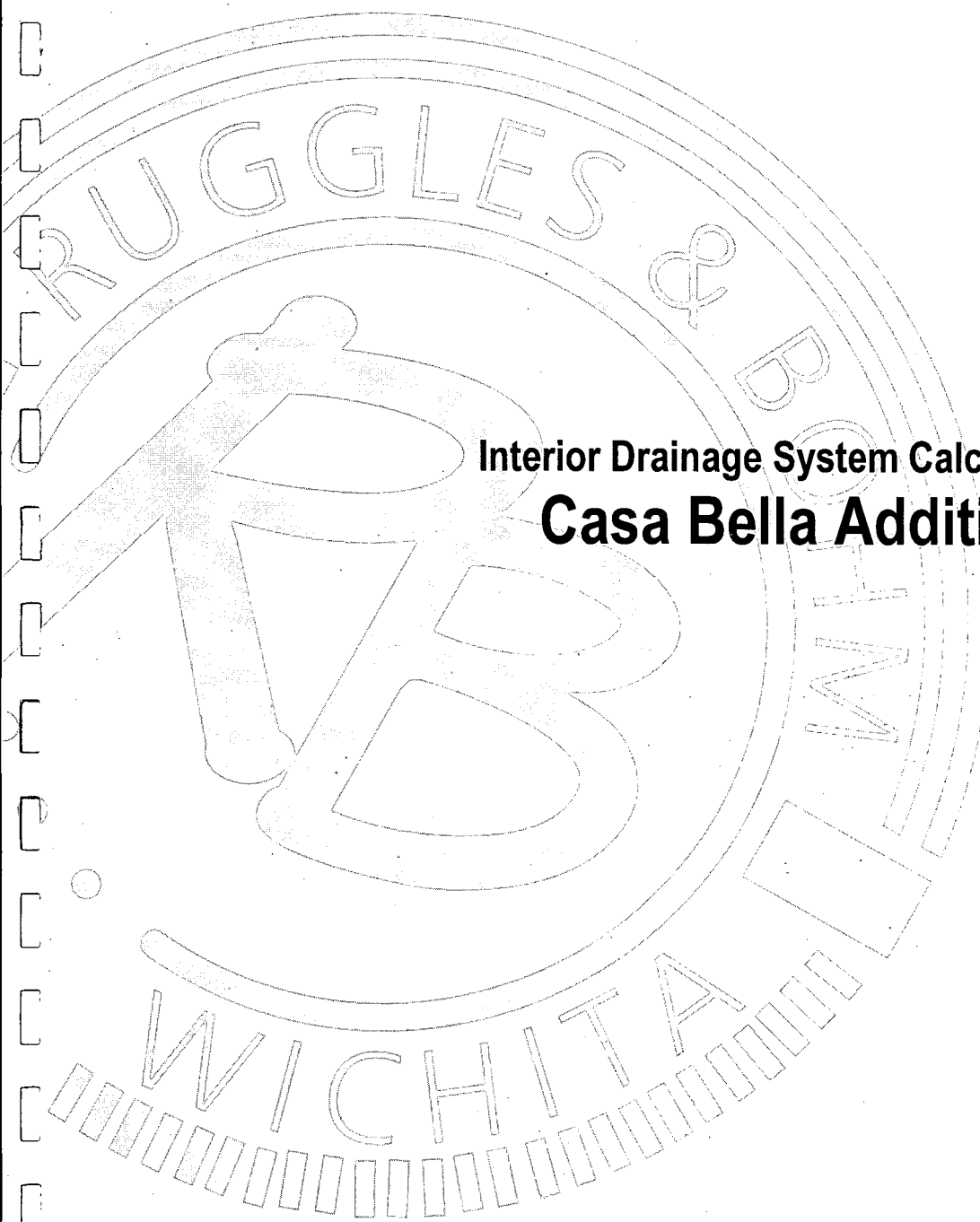
STORAGE      0.00      1.18      2.41      3.70      5.05      6.46      7.93      9.46
OUTFLOW      0.00      21.00     60.00     110.00    169.00    237.00    312.00    392.00
ELEVATION    1334.00 1334.50 1335.00 1335.50 1336.00 1336.50 1337.00 1337.50

```

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

OF STAGE	OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME MAX
					6-HOUR	24-HOUR	72-HOUR			
5.25	HYDROGRAPH AT	UNDEV	436.	5.08	169.	51.	51.	0.31	1346.97	
	HYDROGRAPH AT	ADEV	198.	4.75	71.	22.	22.	0.13		
	ROUTED TO	PONDA	160.	5.25	71.	22.	22.	0.13		
5.42	HYDROGRAPH AT	EDEV	27.	4.75	10.	3.	3.	0.02	1348.27	
	ROUTED TO	PONDE	16.	5.42	9.	3.	3.	0.02		
	HYDROGRAPH AT	BDEV	95.	4.75	34.	10.	10.	0.06		
5.33	HYDROGRAPH AT	ABACK	160.	5.25	71.	22.	22.	0.13	1342.96	
	3 COMBINED AT	COMB	261.	5.08	114.	36.	36.	0.20		
	ROUTED TO	PONDB	242.	5.33	113.	36.	36.	0.20		
	HYDROGRAPH AT	CDEV	130.	4.75	47.	14.	14.	0.08		
	2 COMBINED AT	COMB2	352.	5.17	160.	50.	50.	0.28		
5.33	ROUTED TO	PONDC	335.	5.33	159.	50.	50.	0.28	1337.14	

*** NORMAL END OF HEC-1 ***



Interior Drainage System Calculations
Casa Bella Addition

Ruggles & Bohm P.A.

Engineering, Surveying, Land Planning

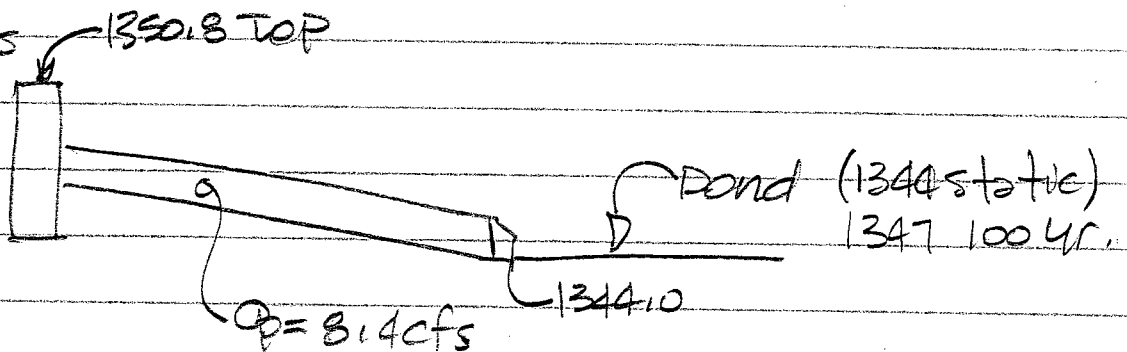
CMB
6/30/05
1/8

Casa Bella Addr
Interior Drainage Calcs.

See Drainage Map for Areas and
Calculated Flows.

Pipe 100 (Area A)
100 yr design

$$Q_{100} = 8.4 \text{ cfs}$$



$$L = 250' ; \text{ HGL} = 1350 - 1347 = \frac{3'}{250} = 1.2\% \text{ HGL}$$

"
From Design Data 4; 18" RCP C 0.64 O.K.
Inlet to be sized w/ SWD project.
100 yr. overspill O.K. (to road)

Pipe 200 (B, C, and D).

Area C, rear yard drainage.
100 year pipe required.

CMB

4-30-05

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$$Q_{100} (\text{Area C}) = 17.4 \text{ cfs}$$

Check Inlet Capacity:
Beehive Inlet; Orifice Flow;

$$Q = 0.6 A \sqrt{2gh} \quad \text{where max } h = 1.0 \text{ feet}$$

$$g = 32.2 \text{ f/s}^2$$

$$\text{Area Beehive top} = 1.8 \text{ sq. ft.}$$

$$Q = 0.6 (1.8) \sqrt{(2)(32.2)(1.0)}$$

$$Q = 8.7 \text{ cfs}$$

Need @ least 2 beehive inlets in this basin, both in sump conditions.

$$Q_p = 17.4 \text{ cfs}$$

$$\text{Area B} = Q_{100} = 17.4 \text{ cfs}$$

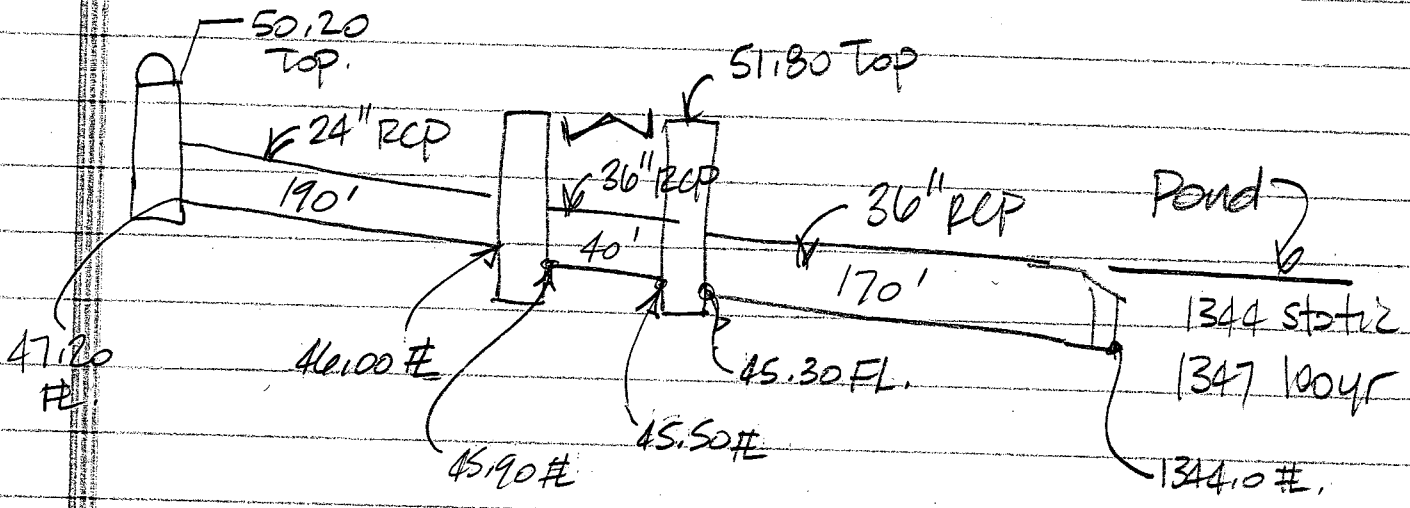
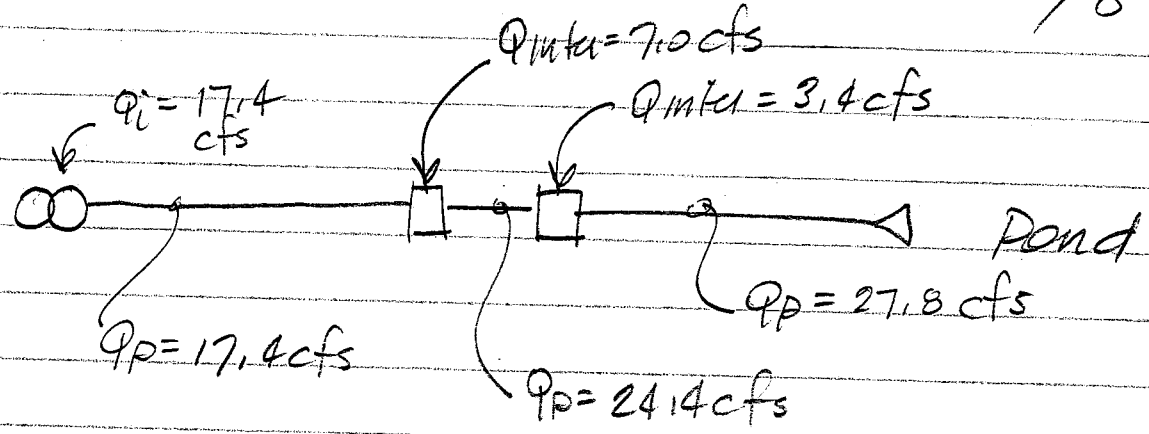
To bypass Inlet.

From Inlet program, $s = 0.5\%$;
Inlet can intercept 7.0 cfs, bypasses the balance. $L = 10'$ for the Inlet.

Area D; $Q_{100} = 3.4 \text{ cfs}$, should be intercepted in whole by Inlet.

CMB
 6-30-05
 3/8

System 200



System Max HGL = $\frac{50.20 - 1347}{400} = 0.80\%$

From Design Data 4:

Q = 17.4 ; 24" @ 0.60 ; OK

Q = 24.4 ; 24" @ 1.16 - No
 36" @ 0.13% - O.K.

Q = 27.8 ; 36" @ 0.17% - O.K.

Storm-CAD final system @ design.

CMB
6-30-05
4/8

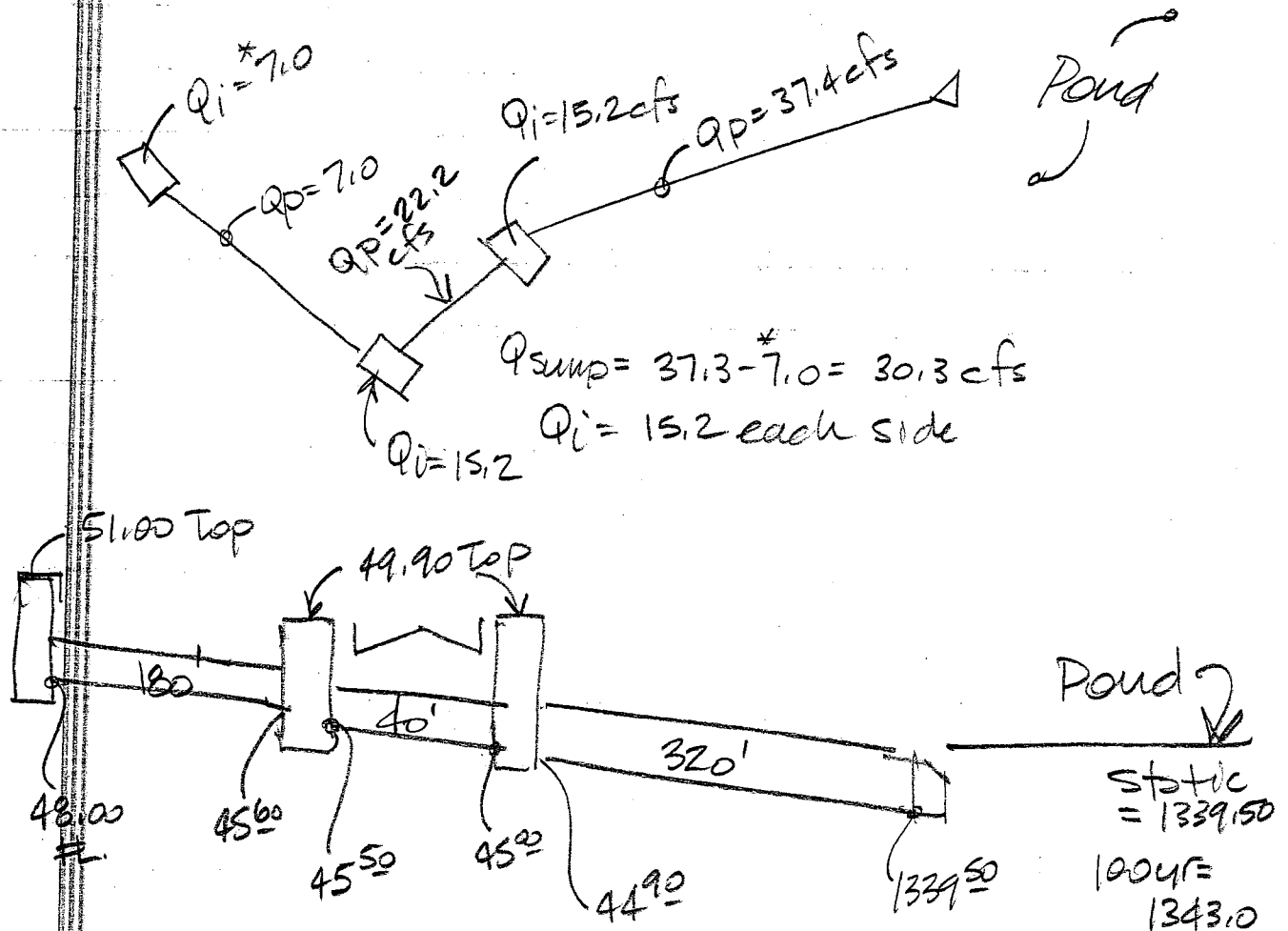
System 300 (Area B, E)

Total Flow to Sump = Area E = 26.9 cfs
 + Bypass B = 17.4 cfs - 7.0 cfs = 10.4 cfs

Total Flow = 37.3 cfs @ Sump

Note: Bypass Inlet @ NW Cor. Michelle Cir and Tara Falls.

This Inlet will Intercept 7.0 cfs @ L=10'



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 5-29-05
 S/B

Available HGL (System 400)
 $= \frac{48.90 - 43.0}{(320 + 40)} = 1.64\%$

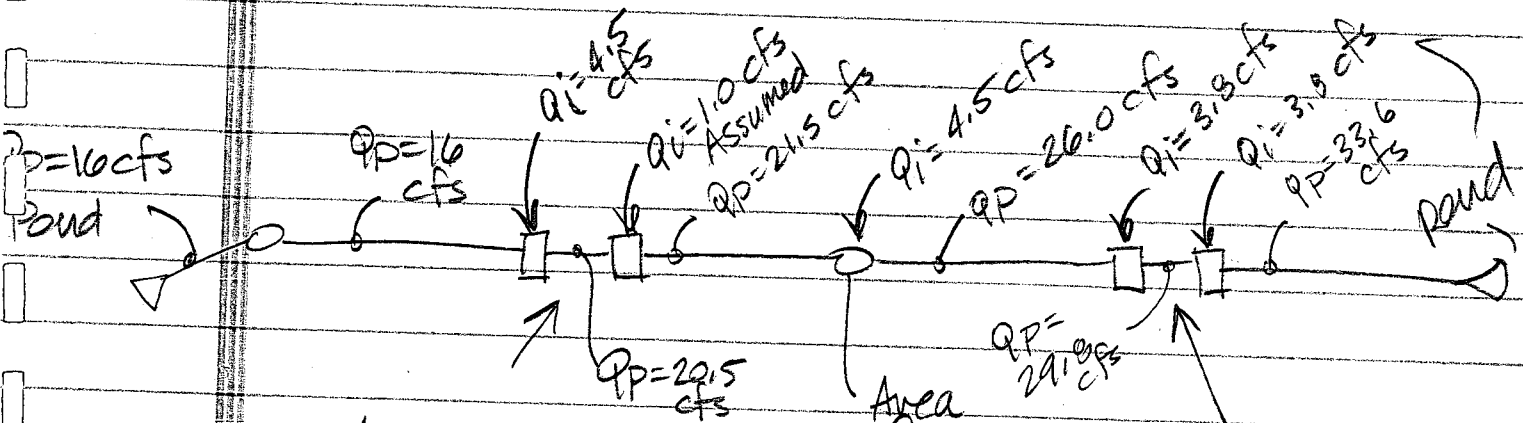
Top pipe; $Q = 7.0$ cfs; 15" RCP 1.173 - O.K.

$Q_p = 22.2$ cfs (street xing); 24" RCP 0.96 - O.K.

Q_p (last pipe) = 34.7 cfs; 36" RCP 0.30 - O.K.

System 400 (Areas F, G, H)

This system also includes the outflow from to Pond in Reserve I. This pond can discharge 16.0 cfs in the 100yr event.



Area F
 $Q_{100} = 11.3$ cfs approach
 From Inlet program
 Q_i (west) = 4.5 cfs
 slope = 1.5%

Area G
 $Q_{100} = 4.5$ cfs

Area H
 $Q_{100} = 11.3$ cfs
 Bypass
 $= 5.9$ cfs / side
 slope = 0.5%
 $Q = 3.8$ cfs per inlet

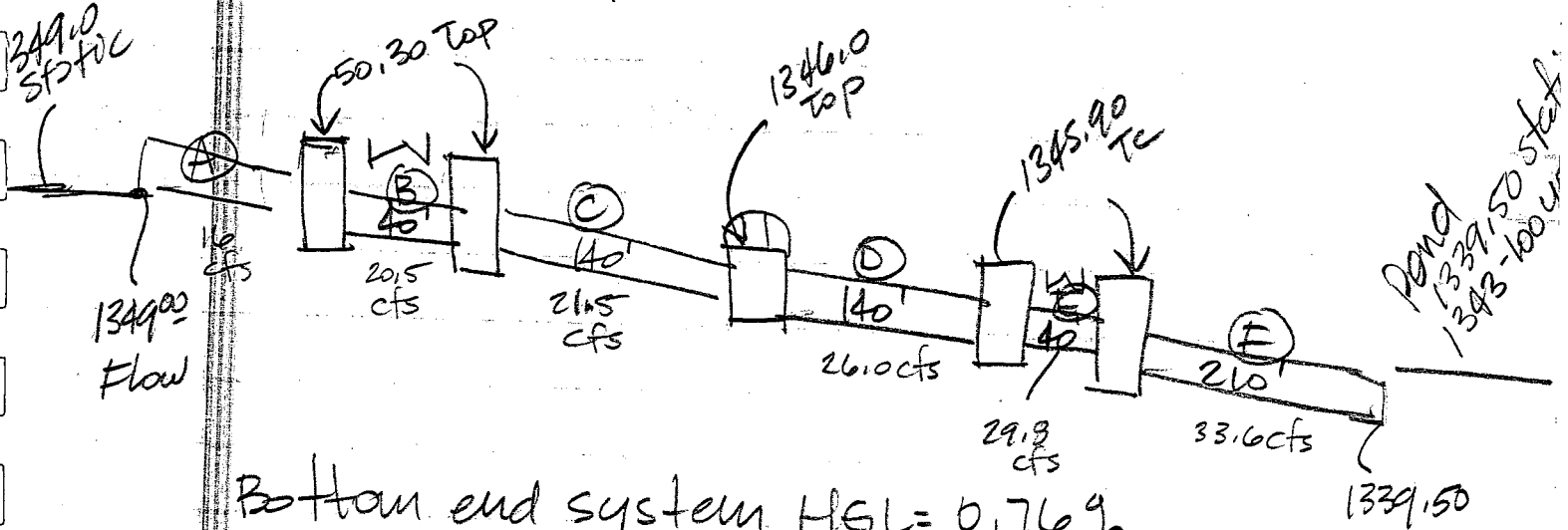
AMB
5-30-05
6/8

System 400

$$\frac{44.90 - 43.0}{250} = 0.76\%$$

HGL

Available HGL =



Bottom end system HGL = 0.76%

Upper reaches may be better, keep, check for design w/ storm-CAD.

Pipe A: $Q_p = 16 \text{ cfs}$; 24" @ 1.02% (Margin 21)

Pipe F; $Q_p = 33.6 \text{ cfs}$; 36" @ 0.25% - OK

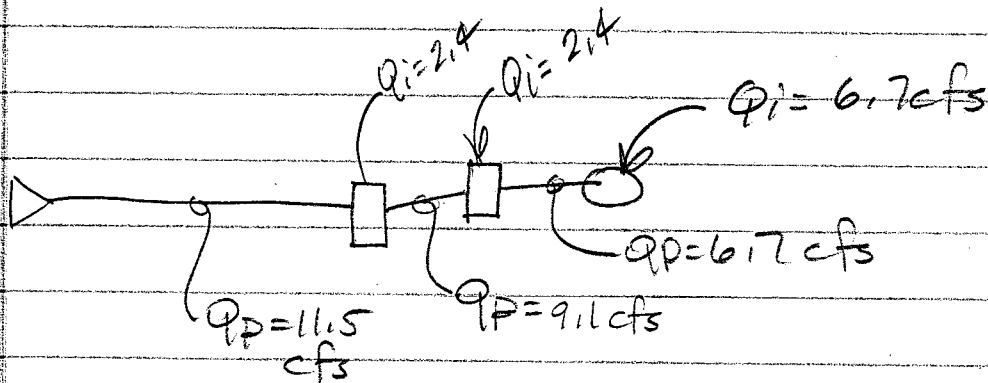
Balance of System = 36"

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 6-30-05
 7/8

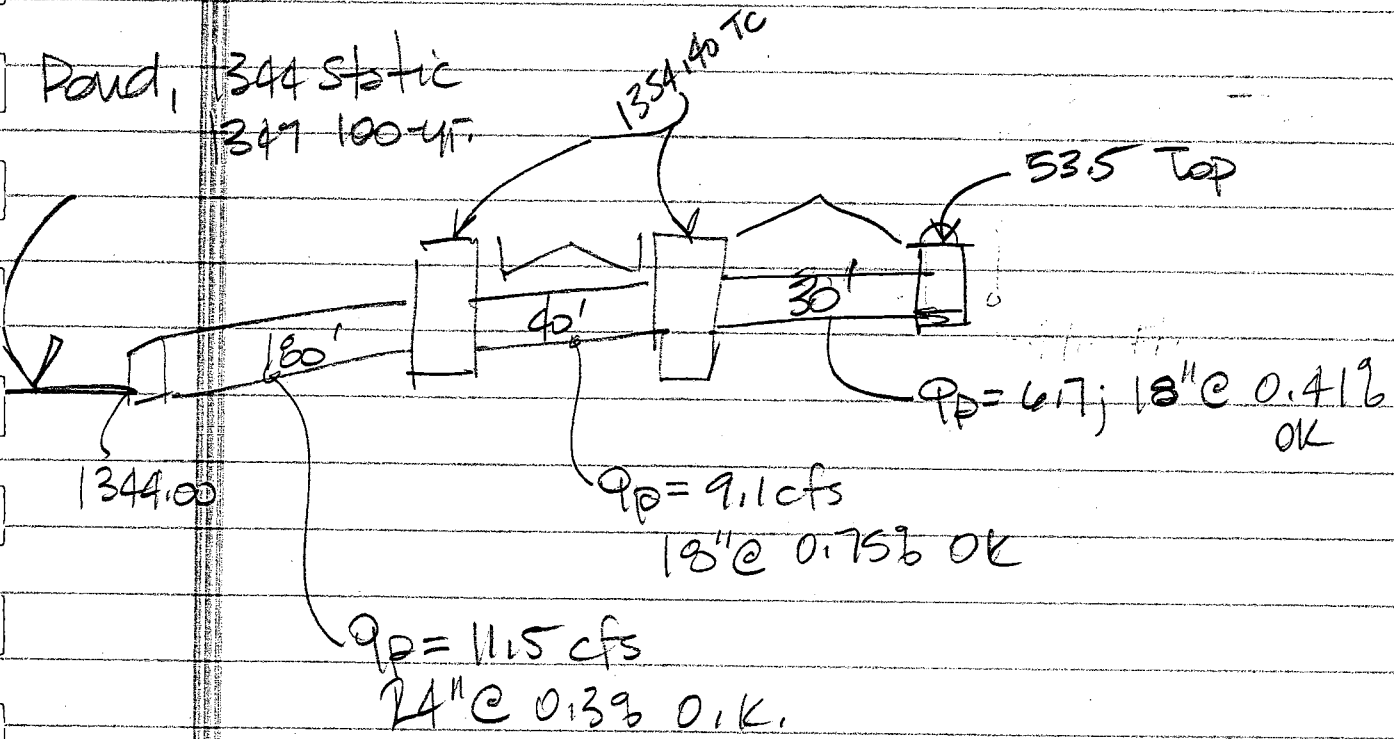
System 500 (Areas I : J)

Area I; $Q_{100} = 8.4 \text{ cfs}$
 $= 4.2/\text{side} @ 1.3\% \text{ Slope}$
 $10' \text{ Inlets Collect} = 2.4 \text{ cfs/side}$

Area J (rear Yard - Cam bypass)
 $Q_{100} = 6.7 \text{ cfs}$



Pond, 344 static
 347 100-yr



CMB
6-30-05
3/8

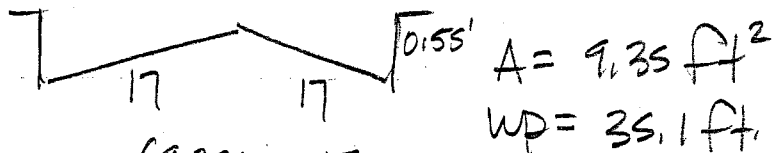
Area J Drains to Box Culvert Inlet
Openings @ Willowgreen.

$$Q_{100} = 31.4 \text{ cfs} + \text{Bypass from I} = 3.6 \text{ cfs}$$
$$\text{totaling} = 35 \text{ cfs (100 yr).}$$

For 2 year Storm = 10.7 cfs.

Check Street Capacity:

Full Curb Across Box Area to Willowgreen Ct.



$$V = \frac{1.49}{0.02} \left(\frac{9.35}{35.1} \right)^{0.167} (1.13\%)^{1/2}$$

$$V = 3.5 \text{ f/sec} \quad Q = V \cdot A$$

$$Q = (9.35)(3.5) = 32 \text{ cfs}$$

O.K! - 2 yr storm in curb - No problem
w/ 100 year storm.

