

PLAT NO. 404



303 S. TOPEKA • WICHITA, KANSAS 67202

Professional Engineering Consultants, P.A.

RETURN POSTAGE GUARANTEED

To: DRAINAGE PLAN AND SUPPORTING CALCULATIONS
FOR

NEWMARKET OFFICE TO WICHITA,
SEDGWICK COUNTY, KANSAS

PEC PROJECT NO. 36-06138-0161

SCANNED

NEWMARKET SQUARE
Wichita, Sedgwick County, Kansas
04/10/06

NewMarket Square is a 40.0 acre, commercial office development located in the northwest part of Wichita in Sedgwick County, Kansas. The future 40 acre development will consist of parking lots, buildings, storm sewer and detention ponds. This report contains a drawing of the drainage plan, supporting calculations and data for the NewMarket Square Drainage Plan.

Hydrology

The proposed plat lies in the SE 1/4, Section 31, T26S, R1W. The soil on-site is comprised of Shellabarger sandy loam (Sa), Vanoss silt loam (Va) and Waurika silt loam (Wb), which are classified in hydrologic groups B, B and D, respectively. The land is currently used for agricultural purposes and has short grass and bare ground throughout. The site is bordered to the north and east by residential properties, to the south by 29th Street North, and to the west currently by agriculture land. The area to the west of the proposed NewMarket Development will be a developed 137.5 acre residential development consisting of 233 lots, streets, and detention ponds. A natural drainage channel cuts through this site from the west property line (Fontana Development) to the east property line and then flowing to the south to 29th street where it passes through a 24" culvert. Existing site drains to the channel that runs through the property with an additional 267 cfs being contributed from the Fontana property. The proposed Basin A drains to the same outfall as the pre-developed flow. This post-development flow will flow through the series of ponds, with structures, and eventually to the natural drainage channel on the south side of 29th street. It was assumed in the design of this drainage plan that the culvert underneath 29th street would be improved along with the 29th street in the future and the flowline elevation set at 159.00.

The Rational Method was used to calculate runoff quantities. Runoff coefficients were estimated based on tables presented in the Design Aids section of this report using fully

developed conditions. Time of concentration was based on slope, flow velocity and length of flow through each basin and was not allowed to be less than 20 minutes. It was assumed in the post-development calculations that the proposed office park would be 50% impervious. The HEC-1 computer program was used to route the runoff through the ponds and determine the post-development conditions leaving the site.

The analysis was made based on the available site data which includes the following: 1" = 100' topographic map with 1' contours of the site, a Sedgwick County Soil Survey Map and noted references.

Design Aids

This section includes material used to assist in designing the drainage system. A 1" = 100' scale Drainage Plan map (Attachment A) and a 1" = 100' scale Four-Corner Plan map (Attachment B) are enclosed in the pockets.

References

Design of Urban Highway Drainage – The State of the Art, by Reitz & Jens, Inc., April 1980.

Drainage of Highway Pavements, Hydraulic Engineering Circular #12, by Tye Engineering, Inc., March 1984.

Interim Drainage and Storm Sewer Policy for Design Criteria and Documentation, City of Wichita, Kansas, 1985.

Soil Survey of Sedgwick County, Kansas, US Department of Agriculture, Soil Conservation Service, 1979.

Time of concentration (Tc) or travel time (Tt)

Project : NEWMARKET OFFICE
 Location : Wichita, Kansas

By: SB Date: 4/10/2006
 Checked: _____ Date: _____

Circle One Present Developed

Circle One Tc Tt through subarea

NOTES: Space for as many as two segments per flow type can be used for each worksheet.
 Include map, schematic, or description of flow segments.

Sheet flow (Applicable to Tc only)

1. Surface description (Table 3-1)
2. Mannings roughness coeff., n (Table 3-1)
3. Flow length, L (total L < 300 ft.)
4. Two-yr 24-hr rainfall, P2
5. Calculated Land slope, s
- 5a. Land Elevation For Upper End Of Flow Path
- 5b. Land Elevation For Lower End Of Flow Path
6. Compute Tt

Segment ID

| | |
|-------|-------|
| AB | |
| Grass | |
| 0.08 | |
| ft | 300 |
| in | 3.60 |
| ft/ft | 0.022 |
| 171.5 | |
| 165.0 | |
| hr | 0.22 |
| = | |
| 0.22 | |

Shallow concentrated flow

7. Surface description (Paved or Unpaved)
8. Flow length, L
9. Calculated Watercourse slope, s
- 9a. Land Elevation For Upper End Of Flow Path
- 9b. Land Elevation For Lower End Of Flow Path
10. Average velocity, V (Figure 3-1)
11. Tt = L/3600V Compute Tt

Segment ID

| | |
|---------|-------|
| BC | |
| Unpaved | |
| 900 | |
| ft | 900 |
| ft/ft | 0.001 |
| 165.0 | |
| 163.7 | |
| ft/s | 0.61 |
| hr | 0.41 |
| = | |
| 0.41 | |

Channel Flow

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a/Pw Compute r
15. Channel slope, s
16. Manning's roughness coeff., n
17. $V = 1.49(r^{0.667})(s^{0.50})/n$ Compute V
18. Flow length, L
19. Tt = L/3600V Compute Tt
20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19)

Segment ID

| | |
|-------|--------|
| CD | |
| sf | 100.00 |
| ft | 60 |
| ft | 1.667 |
| ft/ft | 0.001 |
| 0.011 | |
| ft/s | 6.3 |
| ft | 1050 |
| hr | 0.046 |
| = | |
| 0.05 | |
| hr | |
| 0.67 | |

Reference Urban Hydrology for Small Watersheds
 Technical Release 55, Soil Conservation Service
 U.S. Department of Agriculture, June 1986

Use Time Of Concentration =

40 Minutes

NEWMARKET OFFICE

Project: 4/10/2006

Date: SRB

Manual Input

EXISTING

Total Area 50.00 Acres

| Soil Group | A (% of Total Area) | B (% of Total Area) | C (% of Total Area) | D (% of Total Area) | Total |
|------------|------------------------|------------------------|------------------------|------------------------|-------|
| | 0% | 60% | 0% | 40% | 100% |
| Acres | 0.00 | 24.00 | 0.00 | 16.00 | 40.00 |

| Land Use | Commercial (% of Total Area) | Industrial (% of Total Area) | Multi-Family (% of Total Area) | Public (% of Total Area) | Single Family (% of Total Area) | Vacant/Agriculture (% of Total Area) |
|----------|---------------------------------|---------------------------------|-----------------------------------|-----------------------------|------------------------------------|---|
| Existing | 0% | 0% | 0% | 0% | 20% | 80% |
| Acres | 0.00 | 0.00 | 0.00 | 0.00 | 10.00 | 40.00 |

Existing
 Length of Flow 1900 ft
 Slope 0:01 %
 Waterflow Desc Bare Ground/Ag.
 Avg Velocity 0.63 ft/sec
 Tc 0.84 hours

15 min <= Tc <= 24 hrs

Runoff Coefficients * Used Soil Group C

| Return Period (Years) | Commercial | Industrial | Multi-Family | Public | Single Family | Vacant/Agriculture |
|-----------------------|------------|------------|--------------|--------|---------------|--------------------|
| 2 | 0.68 | 0.68 | 0.63 | 0.49 | 0.48 | 0.24 |
| 5 | 0.69 | 0.69 | 0.66 | 0.51 | 0.51 | 0.27 |
| 10 | 0.73 | 0.73 | 0.71 | 0.56 | 0.57 | 0.35 |
| 25 | 0.75 | 0.75 | 0.73 | 0.59 | 0.60 | 0.40 |
| 50 | 0.77 | 0.77 | 0.76 | 0.62 | 0.64 | 0.45 |
| 100 | 0.80 | 0.80 | 0.79 | 0.66 | 0.68 | 0.51 |

Existing Conditions

| Return Period (Years) | Runoff Coefficient * | Rainfall Intensity (in/hr) | Area (Acres) | Runoff (cfs) |
|-----------------------|----------------------|----------------------------|--------------|--------------|
| 2 | 0.29 | 2.24 | 50.00 | 32.26 |
| 5 | 0.32 | 2.76 | 50.00 | 43.88 |
| 10 | 0.39 | 3.22 | 50.00 | 63.43 |
| 25 | 0.44 | 3.76 | 50.00 | 82.72 |
| 50 | 0.49 | 4.25 | 50.00 | 103.70 |
| 100 | 0.54 | 4.66 | 50.00 | 126.75 |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

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*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   FEBRUARY 1981                   *
*   REVISED 02 AUG 88               *
*
* RUN DATE 04/10/2006 TIME 15:18:09 *
*
*****
    
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*****
*
* U.S. ARMY CORPS OF ENGINEERS      *
* THE HYDROLOGIC ENGINEERING CENTER *
*   609 SECOND STREET               *
*   DAVIS, CALIFORNIA 95616        *
*   (916) 551-1748                 *
*
*****
    
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X   X  XXXXXX  XXXX      X
X   X  X      X   X     XX
X   X  X      X           X
XXXXXX XXXX  X      XXXX  X
X   X  X      X           X
X   X  X      X   X     X
X   X  XXXXXX  XXXX      XXX
    
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

HRC-1 INPUT

PAGE 1

| LINE | ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|--------------|----|--|---------|--------|--------|--------|---------|--------|--------|--------|--------|
| 1 | ID | MODIFIED FONTANA DRAINAGE PLAN (40-AC UNDEVELOPED TRACT D/S ADDED) | | | | | | | | | |
| 2 | ID | 40- ACRE NEW MARKET OFFICE TRACT (PRE-PROJECT CONDITIONS) | | | | | | | | | |
| 3 | ID | BY BLB DATE 03-13-04, MODIFIED BY PDF 4/10/06 | | | | | | | | | |
| *** LIST *** | | | | | | | | | | | |
| *** FREE *** | | | | | | | | | | | |
| *DIAGRAM | | | | | | | | | | | |
| 4 | IT | 15 | 01JAN04 | 1200 | | 0 | 02JAN04 | 2000 | | | |
| 5 | IN | 15 | 01JAN04 | 1200 | | | | | | | |
| 6 | IO | 0 | 5 | | | | | | | | |
| 7 | JR | PREC | 7.8 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 8 | KK | BSN5 | | | | | | | | | |
| 9 | KO | 5 | | | | | | | | | |
| 10 | BA | 0.023 | | | | | | | | | |
| 11 | PB | 1.00 | | | | | | | | | |
| 12 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 13 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 14 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 15 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 16 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 17 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 18 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 19 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 20 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 21 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 22 | LS | 0 | 68 | 10 | | | | | | | |
| 23 | UD | 0.600 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 24 | KK | POND7 | | | | | | | | | |
| 25 | KO | 5 | | | | | | | | | |
| 26 | RS | 1 | ELEV | 162.0 | | | | | | | |
| 27 | SA | 2.55 | 2.71 | 2.88 | 3.06 | | | | | | |
| 28 | SE | 171.0 | 172.0 | 173.0 | 174.0 | | | | | | |
| 29 | SQ | 0 | 3.2 | 6.4 | 9.6 | 12.8 | 16.0 | 19.2 | 22.4 | 25.6 | 28.8 |
| 30 | SQ | 32.0 | | | | | | | | | |
| 31 | SE | 171.0 | 171.35 | 171.56 | 171.73 | 171.88 | 172.02 | 172.16 | 172.28 | 172.40 | 172.52 |
| 32 | SE | 172.6 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 33 | KK | BSN4 | | | | | | | | | |
| 34 | KO | 5 | | | | | | | | | |
| 35 | BA | 0.020 | | | | | | | | | |
| 36 | PB | 1.00 | | | | | | | | | |
| 37 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 38 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 39 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 40 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 41 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 42 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

HEC-1 INPUT

PAGE 2

| LINE | ID |1 |2 |3 |4 |5 |6 |7 |8 |9 |10 |
|------|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|
| 43 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 44 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 45 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 46 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 47 | LS | 0 | 68 | 10 | | | | | | | |
| 48 | UD | 0.850 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 49 | KK | PD7&4 | | | | | | | | | |
| 50 | KO | 5 | | | | | | | | | |
| 51 | HC | 2 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 52 | KK | POND6 | | | | | | | | | |
| 53 | KO | 5 | | | | | | | | | |
| 54 | RS | 1 | ELEV | 162.0 | | | | | | | |
| 55 | SA | 1.85 | 1.99 | 2.14 | 2.29 | | | | | | |
| 56 | SE | 170.0 | 171.0 | 172.0 | 173.0 | | | | | | |
| 57 | SQ | 0 | 2.2 | 4.4 | 6.6 | 8.8 | 11.0 | 13.2 | 15.4 | 17.6 | 19.8 |
| 58 | SQ | 22.0 | | | | | | | | | |
| 59 | SE | 170.0 | 170.72 | 171.11 | 171.42 | 171.77 | 172.21 | 172.75 | 173.40 | 174.14 | 174.98 |
| 60 | SE | 175.9 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 61 | KK | BSN7 | | | | | | | | | |
| 62 | KO | 5 | | | | | | | | | |
| 63 | BA | 0.055 | | | | | | | | | |
| 64 | PB | 1.00 | | | | | | | | | |
| 65 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 66 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 67 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 68 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 69 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.307 | 0.331 | 0.355 |
| 70 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 71 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 72 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 73 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 74 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 75 | LS | 0 | 68 | 10 | | | | | | | |
| 76 | UD | 0.840 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 77 | KK | 7PD6 | | | | | | | | | |
| 78 | KO | 5 | | | | | | | | | |
| 79 | HC | 2 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

HEC-1 INPUT

PAGE 3

| LINE | ID..... | 1..... | 2..... | 3..... | 4..... | 5..... | 6..... | 7..... | 8..... | 9..... | 10 | |
|------|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--|
| 80 | KK | POND5 | | | | | | | | | | |
| 81 | KO | 5 | | | | | | | | | | |
| 82 | RS | 1 | ELEV | 159.0 | | | | | | | | |
| 83 | SA | 2.67 | 2.84 | 3.01 | 3.19 | | | | | | | |
| 84 | SE | 167.0 | 168.0 | 169.0 | 170.0 | | | | | | | |
| 85 | SQ | 0 | 6.3 | 12.6 | 18.9 | 25.2 | 31.5 | 37.8 | 44.1 | 50.4 | 56.7 | |
| 86 | SQ | 63.0 | | | | | | | | | | |
| 87 | SE | 167.0 | 167.55 | 167.87 | 168.14 | 168.39 | 168.61 | 168.82 | 169.01 | 169.20 | 169.38 | |
| 88 | SE | 169.6 | | | | | | | | | | |
| | * | | | | | | | | | | | |
| | * | | | | | | | | | | | |
| 89 | KK | BSN6 | | | | | | | | | | |
| 90 | KO | 5 | | | | | | | | | | |
| 91 | BA | 0.008 | | | | | | | | | | |
| 92 | PB | 1.00 | | | | | | | | | | |
| 93 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 | |
| 94 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 | |
| 95 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 | |
| 96 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 | |
| 97 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 | |
| 98 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 | |
| 99 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 | |
| 100 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 | |
| 101 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 | |
| 102 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | | |
| 103 | LS | 0 | 68 | 10 | | | | | | | | |
| 104 | UD | 0.530 | | | | | | | | | | |
| | * | | | | | | | | | | | |
| | * | | | | | | | | | | | |
| 105 | KK | RTE6 | | | | | | | | | | |
| 106 | KO | 5 | 5 | | | | | | | | | |
| 107 | RT | 0 | 0 | 3 | | | | | | | | |
| | * | | | | | | | | | | | |
| | * | | | | | | | | | | | |
| 108 | KK | OFFST | | | | | | | | | | |
| 109 | BA | 0.359 | | | | | | | | | | |
| 110 | PB | 1.00 | | | | | | | | | | |
| 111 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 | |
| 112 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 | |
| 113 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 | |
| 114 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 | |
| 115 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 | |
| 116 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 | |
| 117 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 | |
| 118 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 | |
| 119 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 | |
| 120 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | | |
| 121 | LS | 0 | 70 | 10 | | | | | | | | |
| 122 | UD | 1.575 | | | | | | | | | | |
| | * | | | | | | | | | | | |
| | * | | | | | | | | | | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

HEC-1 INPUT

PAGE 4

| LINE | ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|------|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 123 | KK | BSNB | | | | | | | | | |
| 124 | KO | 5 | | | | | | | | | |
| 125 | BA | 0.027 | | | | | | | | | |
| 126 | PB | 1.00 | | | | | | | | | |
| 127 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 128 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 129 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 130 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 131 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 132 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 133 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 134 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 135 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 136 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 137 | LS | 0 | 68 | 10 | | | | | | | |
| 138 | UD | 0.490 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 139 | KK | 606P5 | | | | | | | | | |
| 140 | KO | 5 | | | | | | | | | |
| 141 | EC | 4 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 142 | KK | POND4 | | | | | | | | | |
| 143 | KO | 5 | | | | | | | | | |
| 144 | RS | 1 | ELEV | 158.0 | | | | | | | |
| 145 | SA | 3.06 | 3.24 | 3.42 | 3.61 | | | | | | |
| 146 | SE | 166.0 | 167.0 | 168.0 | 169.0 | | | | | | |
| 147 | SL | 158.0 | 14.73 | 0.6 | 0.5 | | | | | | |
| 148 | SS | 167.0 | 0.00 | 3.0 | 1.5 | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 149 | KK | BSN10 | | | | | | | | | |
| 150 | KO | 5 | | | | | | | | | |
| 151 | BA | 0.021 | | | | | | | | | |
| 152 | PB | 1.00 | | | | | | | | | |
| 153 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 154 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 155 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 156 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 157 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 158 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 159 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 160 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 161 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 162 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 163 | LS | 0 | 68 | 10 | | | | | | | |
| 164 | UD | 0.670 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

HBC-1 INPUT

PAGE 5

| LINE | ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|------|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 165 | KK | 10PDA | | | | | | | | | |
| 166 | KO | 5 | | | | | | | | | |
| 167 | HC | 2 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 168 | KK | POND3 | | | | | | | | | |
| 169 | KO | 5 | | | | | | | | | |
| 170 | RS | 1 | ELEV | 162.0 | | | | | | | |
| 171 | SA | 1.70 | 1.83 | 1.98 | 2.12 | | | | | | |
| 172 | SE | 166.0 | 167.0 | 168.0 | 169.0 | | | | | | |
| 173 | SL | 158.5 | 14.73 | 0.6 | 0.5 | | | | | | |
| 174 | SS | 168.0 | 0.00 | 3.0 | 1.5 | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 175 | KK | BSN3 | | | | | | | | | |
| 176 | KO | 5 | | | | | | | | | |
| 177 | BA | 0.024 | | | | | | | | | |
| 178 | PB | 1.00 | | | | | | | | | |
| 179 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 180 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 181 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 182 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 183 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.307 | 0.663 | 0.699 |
| 184 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 185 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 186 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 187 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 188 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 189 | LS | 0 | 68 | 10 | | | | | | | |
| 190 | UD | 0.580 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 191 | KK | BSN2 | | | | | | | | | |
| 192 | KO | 5 | | | | | | | | | |
| 193 | BA | 0.025 | | | | | | | | | |
| 194 | PB | 1.00 | | | | | | | | | |
| 195 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 196 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 197 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 198 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 199 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.307 | 0.663 | 0.699 |
| 200 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 201 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 202 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 203 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 204 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 205 | LS | 0 | 68 | 10 | | | | | | | |
| 206 | UD | 0.670 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

HEC-1 INPUT

PAGE 6

| LINE | ID..... | 1..... | 2..... | 3..... | 4..... | 5..... | 6..... | 7..... | 8..... | 9..... | 10 |
|------|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 207 | KK | POND1 | | | | | | | | | |
| 208 | KO | 5 | | | | | | | | | |
| 209 | RS | 1 | ELEV | 162.0 | | | | | | | |
| 210 | SA | 0.36 | 0.43 | 0.49 | 0.57 | | | | | | |
| 211 | SE | 170.0 | 171.0 | 172.0 | 173.0 | | | | | | |
| 212 | SQ | 0 | 3.2 | 6.4 | 9.6 | 12.8 | 16.0 | 19.2 | 22.4 | 25.6 | 28.8 |
| 213 | SQ | 32.0 | | | | | | | | | |
| 214 | SE | 170.0 | 170.17 | 170.27 | 170.35 | 170.42 | 170.49 | 170.56 | 170.62 | 170.67 | 170.73 |
| 215 | SE | 170.8 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 216 | KK | 3PDI&3 | | | | | | | | | |
| 217 | KO | 5 | | | | | | | | | |
| 218 | HC | 3 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 219 | KK | POND2 | | | | | | | | | |
| 220 | KO | 5 | | | | | | | | | |
| 221 | RS | 1 | ELEV | 158.0 | | | | | | | |
| 222 | SA | 2.08 | 2.23 | 2.38 | 2.54 | | | | | | |
| 223 | SE | 166.0 | 167.0 | 168.0 | 169.0 | | | | | | |
| 224 | SQ | 0 | 26.9 | 53.8 | 80.7 | 107.6 | 134.5 | 161.4 | 188.3 | 215.2 | 242.1 |
| 225 | SQ | 269.0 | | | | | | | | | |
| 226 | SE | 166.0 | 166.50 | 166.79 | 167.03 | 167.25 | 167.45 | 167.63 | 167.81 | 167.98 | 168.14 |
| 227 | SE | 168.3 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 228 | KK | NORTH | | | | | | | | | |
| 229 | KO | 5 | | | | | | | | | |
| 230 | BA | 0.0156 | | | | | | | | | |
| 231 | PB | 1.00 | | | | | | | | | |
| 232 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 233 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 234 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 235 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 236 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 237 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 238 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 239 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 240 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 241 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 242 | LS | 0 | 70 | 0 | | | | | | | |
| 243 | UD | 0.40 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

HEC-1 INPUT

PAGE 7

| LINE | ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|------|----|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 244 | KK | OFFSTE | | | | | | | | | |
| 245 | KO | 5 | | | | | | | | | |
| 246 | HC | 2 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | ROUTE 267 CFS FROM FONTANA + 10 ACRES FROM THE NORTH TO 29TH STREET | | | | | | | | | |
| | * | | | | | | | | | | |
| 247 | KK | RTE6 | | | | | | | | | |
| 248 | KO | 5 | | | | | | | | | |
| 249 | RT | 0 | 0 | 2.0 | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 250 | KK | NM-UND | | | | | | | | | |
| 251 | KO | 5 | | | | | | | | | |
| 252 | BA | 0.0625 | | | | | | | | | |
| 253 | PB | 1.00 | | | | | | | | | |
| 254 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 255 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 256 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 257 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 258 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.307 | 0.331 | 0.355 |
| 259 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 260 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 261 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 262 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 263 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 264 | LS | 0 | 70 | 0 | | | | | | | |
| 265 | UD | 0.40 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 266 | KK | 29TH | | | | | | | | | |
| 267 | KO | 5 | | | | | | | | | |
| 268 | HC | 2 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 269 | ZZ | | | | | | | | | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

SCHEMATIC DIAGRAM OF STREAM NETWORK

| INPUT LINE NO. | (V) ROUTING | (--->) DIVERSION OR PUMP FLOW |
|----------------|---------------|--|
| | (.) CONNECTOR | (<---) RETURN OF DIVERTED OR PUMPED FLOW |
| 8 | BSN5 | |
| | V | |
| | V | |
| 24 | POND7 | |
| | . | |
| 33 | BSN4 | |
| | . | |
| 49 | PD7&4..... | |
| | V | |
| | V | |
| 52 | POND6 | |
| | . | |
| 61 | BSN7 | |
| | . | |
| 77 | 7PD6..... | |
| | V | |
| | V | |
| 80 | POND5 | |
| | . | |
| 89 | BSN6 | |
| | V | |
| | V | |
| 105 | RTE6 | |
| | . | |
| 108 | OFFST | |
| | . | |
| 123 | BSN8 | |
| | . | |
| 139 | 608P5..... | |
| | V | |
| | V | |
| 142 | POND4 | |
| | . | |
| 149 | BSN10 | |
| | . | |
| 165 | 10PD4..... | |
| | V | |
| | V | |
| 168 | POND3 | |
| | . | |
| 175 | BSN3 | |
| | . | |
| 191 | BSN2 | |
| | V | |
| | V | |
| 207 | POND1 | |
| | . | |
| 216 | 3PD1&3..... | |
| | V | |
| | V | |
| 219 | POND2 | |
| | . | |
| 228 | NORTH | |
| | . | |
| 244 | OFFSTE..... | |
| | V | |
| | V | |
| 247 | RTE6 | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

250

·
·
·

NM-UND

266

29TH.....

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

```
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* FEBRUARY 1981
* REVISED 02 AUG 88
*
* RUN DATE 04/10/2006 TIME 15:18:09
*
*****
```

```
*****
*
* U.S. ARMY CORPS OF ENGINEERS
* THE HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*
*****
```

MODIFIED FONTANA DRAINAGE PLAN (40-AC UNDEVELOPED TRACT D/S ADDED)
 40- ACRE NEW MARKET OFFICE TRACT (PRE-PROJECT CONDITIONS)
 BY BLB DATE 03-13-04, MODIFIED BY PDF 4/10/06

```
6 IO OUTPUT CONTROL VARIABLES
      IPRNT 0 PRINT CONTROL
      IPLOT 5 PLOT CONTROL
      QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
      NMIN 15 MINUTES IN COMPUTATION INTERVAL
      IDATE 1JAN 4 STARTING DATE
      ITIME 1200 STARTING TIME
      NQ 129 NUMBER OF HYDROGRAPH ORDINATES
      NDDATE 2JAN 4 ENDING DATE
      NDTIME 2000 ENDING TIME
      ICENT 19 CENTURY MARK

      COMPUTATION INTERVAL .25 HOURS
      TOTAL TIME BASE 32.00 HOURS
```

```
ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT
```

```
JP MULTI-PLAN OPTION
      NPLAN 1 NUMBER OF PLANS
```

```
JR MULTI-RATIO OPTION
      RATIOS OF PRECIPITATION
      7.80
```

*** ** ** ** **

```
*****
*
*
* 8 KK BSN5
*
*
*****
```

```
9 KO OUTPUT CONTROL VARIABLES
      IPRNT 5 PRINT CONTROL
      IPLOT 5 PLOT CONTROL
      QSCAL 0. HYDROGRAPH PLOT SCALE
```

*** ** ** **~

```
*****
*
*
* 24 KK POND7
*
*
*****
```

```
25 KO OUTPUT CONTROL VARIABLES
      IPRNT 5 PRINT CONTROL
```

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
33 KK * BSN4 *
* *

34 KO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPL0T 5 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
49 KK * PD7&4 *
* *

50 KO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPL0T 5 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
52 KK * POND6 *
* *

53 KO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPL0T 5 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
61 KK * BSN7 *
* *

62 KO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPL0T 5 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
77 KK * 7PD6 *
* *

78 KO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

IPL0T 5 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

```

*****
*           *
80 KK  *   POND5 *
*           *
*****
  
```

81 KO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPL0T 5 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

```

*****
*           *
89 KK  *   BSN6 *
*           *
*****
  
```

90 KO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPL0T 5 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

```

*****
*           *
105 KK *   RTE6 *
*           *
*****
  
```

106 KO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPL0T 5 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

```

*****
*           *
108 KK *   OFFST *
*           *
*****
  
```

5 IN TIME DATA FOR INPUT TIME SERIES
 JXMIN 15 TIME INTERVAL IN MINUTES
 JXDATE 1JAN 4 STARTING DATE
 JXTIME 1200 STARTING TIME

SUBBASIN RUNOFF DATA

109 BA SUBBASIN CHARACTERISTICS
 TAREA .36 SUBBASIN AREA

PRECIPITATION DATA

110 PB STORM 1.00 BASIN TOTAL PRECIPITATION

111 PI INCREMENTAL PRECIPITATION PATTERN

| | | | | | | | | | | |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |
| .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |
| .00 | .00 | .00 | .00 | .01 | .01 | .00 | .01 | .00 | .01 | .01 |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

| | | | | | | | | | | |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| .01 | .00 | .01 | .01 | .01 | .01 | .01 | .01 | .01 | .01 | .01 |
| .01 | .01 | .02 | .02 | .02 | .02 | .10 | .28 | .04 | .04 | .04 |
| .02 | .02 | .01 | .01 | .01 | .01 | .01 | .01 | .01 | .01 | .01 |
| .01 | .01 | .01 | .01 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |
| .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |
| .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |
| .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |

121 LS SCS LOSS RATE
 STRTL .86 INITIAL ABSTRACTION
 CRVNR 70.00 CURVE NUMBER
 RTIMP 10.00 PERCENT IMPERVIOUS AREA

122 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 1.58 LAG

UNIT HYDROGRAPH 34 END-OF-PERIOD ORDINATES

| | | | | | | | | | |
|-----|-----|-----|-----|-----|------|------|-----|-----|-----|
| 6. | 19. | 38. | 65. | 88. | 100. | 102. | 96. | 86. | 72. |
| 55. | 42. | 33. | 26. | 21. | 16. | 13. | 10. | 8. | 6. |
| 5. | 4. | 3. | 2. | 2. | 1. | 1. | 1. | 1. | 1. |
| 0. | 0. | 0. | 0. | | | | | | |

HYDROGRAPH AT STATION OFFST

| DA | MON | HRMN | ORD | RAIN | LOSS | EXCESS | COMP Q | * | DA | MON | HRMN | ORD | RAIN | LOSS | EXCESS | COMP Q |
|----|-----|------|-----|------|------|--------|--------|---|----|-----|------|-----|------|------|--------|--------|
| 1 | JAN | 1200 | 1 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0415 | 66 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1215 | 2 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0430 | 67 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1230 | 3 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0445 | 68 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1245 | 4 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0500 | 69 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1300 | 5 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0515 | 70 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1315 | 6 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0530 | 71 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1330 | 7 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0545 | 72 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1345 | 8 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0600 | 73 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1400 | 9 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0615 | 74 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1415 | 10 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0630 | 75 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1430 | 11 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0645 | 76 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1445 | 12 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0700 | 77 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1500 | 13 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0715 | 78 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1515 | 14 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0730 | 79 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1530 | 15 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0745 | 80 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1545 | 16 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0800 | 81 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1600 | 17 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0815 | 82 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1615 | 18 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0830 | 83 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1630 | 19 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0845 | 84 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1645 | 20 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0900 | 85 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1700 | 21 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0915 | 86 | .00 | .00 | .00 | 1. |
| 1 | JAN | 1715 | 22 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0930 | 87 | .00 | .00 | .00 | 0. |
| 1 | JAN | 1730 | 23 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0945 | 88 | .00 | .00 | .00 | 0. |
| 1 | JAN | 1745 | 24 | .00 | .00 | .00 | 0. | * | 2 | JAN | 1000 | 89 | .00 | .00 | .00 | 0. |
| 1 | JAN | 1800 | 25 | .00 | .00 | .00 | 0. | * | 2 | JAN | 1015 | 90 | .00 | .00 | .00 | 0. |
| 1 | JAN | 1815 | 26 | .01 | .00 | .00 | 0. | * | 2 | JAN | 1030 | 91 | .00 | .00 | .00 | 0. |
| 1 | JAN | 1830 | 27 | .01 | .00 | .00 | 0. | * | 2 | JAN | 1045 | 92 | .00 | .00 | .00 | 0. |
| 1 | JAN | 1845 | 28 | .00 | .00 | .00 | 0. | * | 2 | JAN | 1100 | 93 | .00 | .00 | .00 | 0. |
| 1 | JAN | 1900 | 29 | .01 | .00 | .00 | 0. | * | 2 | JAN | 1115 | 94 | .00 | .00 | .00 | 0. |
| 1 | JAN | 1915 | 30 | .00 | .00 | .00 | 0. | * | 2 | JAN | 1130 | 95 | .00 | .00 | .00 | 0. |
| 1 | JAN | 1930 | 31 | .01 | .00 | .00 | 0. | * | 2 | JAN | 1145 | 96 | .00 | .00 | .00 | 0. |
| 1 | JAN | 1945 | 32 | .01 | .00 | .00 | 0. | * | 2 | JAN | 1200 | 97 | .00 | .00 | .00 | 0. |
| 1 | JAN | 2000 | 33 | .00 | .00 | .00 | 0. | * | 2 | JAN | 1215 | 98 | .00 | .00 | .00 | 0. |
| 1 | JAN | 2015 | 34 | .01 | .01 | .00 | 0. | * | 2 | JAN | 1230 | 99 | .00 | .00 | .00 | 0. |
| 1 | JAN | 2030 | 35 | .01 | .01 | .00 | 0. | * | 2 | JAN | 1245 | 100 | .00 | .00 | .00 | 0. |
| 1 | JAN | 2045 | 36 | .01 | .01 | .00 | 0. | * | 2 | JAN | 1300 | 101 | .00 | .00 | .00 | 0. |
| 1 | JAN | 2100 | 37 | .01 | .01 | .00 | 0. | * | 2 | JAN | 1315 | 102 | .00 | .00 | .00 | 0. |
| 1 | JAN | 2115 | 38 | .01 | .01 | .00 | 0. | * | 2 | JAN | 1330 | 103 | .00 | .00 | .00 | 0. |
| 1 | JAN | 2130 | 39 | .01 | .01 | .00 | 1. | * | 2 | JAN | 1345 | 104 | .00 | .00 | .00 | 0. |
| 1 | JAN | 2145 | 40 | .01 | .01 | .00 | 1. | * | 2 | JAN | 1400 | 105 | .00 | .00 | .00 | 0. |
| 1 | JAN | 2200 | 41 | .01 | .01 | .00 | 1. | * | 2 | JAN | 1415 | 106 | .00 | .00 | .00 | 0. |
| 1 | JAN | 2215 | 42 | .01 | .01 | .00 | 1. | * | 2 | JAN | 1430 | 107 | .00 | .00 | .00 | 0. |
| 1 | JAN | 2230 | 43 | .01 | .01 | .00 | 1. | * | 2 | JAN | 1445 | 108 | .00 | .00 | .00 | 0. |
| 1 | JAN | 2245 | 44 | .02 | .01 | .00 | 1. | * | 2 | JAN | 1500 | 109 | .00 | .00 | .00 | 0. |
| 1 | JAN | 2300 | 45 | .02 | .01 | .00 | 1. | * | 2 | JAN | 1515 | 110 | .00 | .00 | .00 | 0. |
| 1 | JAN | 2315 | 46 | .02 | .02 | .00 | 1. | * | 2 | JAN | 1530 | 111 | .00 | .00 | .00 | 0. |
| 1 | JAN | 2330 | 47 | .02 | .02 | .00 | 1. | * | 2 | JAN | 1545 | 112 | .00 | .00 | .00 | 0. |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

| | | | | | | | | | | | | |
|------------|----|-----|-----|-----|----|---|------------|-----|-----|-----|-----|----|
| 1 JAN 2345 | 48 | .10 | .09 | .01 | 1. | * | 2 JAN 1600 | 113 | .00 | .00 | .00 | 0. |
| 2 JAN 0000 | 49 | .28 | .25 | .03 | 1. | * | 2 JAN 1615 | 114 | .00 | .00 | .00 | 0. |
| 2 JAN 0015 | 50 | .04 | .03 | .00 | 2. | * | 2 JAN 1630 | 115 | .00 | .00 | .00 | 0. |
| 2 JAN 0030 | 51 | .04 | .03 | .00 | 3. | * | 2 JAN 1645 | 116 | .00 | .00 | .00 | 0. |
| 2 JAN 0045 | 52 | .02 | .02 | .00 | 4. | * | 2 JAN 1700 | 117 | .00 | .00 | .00 | 0. |
| 2 JAN 0100 | 53 | .02 | .02 | .00 | 5. | * | 2 JAN 1715 | 118 | .00 | .00 | .00 | 0. |
| 2 JAN 0115 | 54 | .01 | .01 | .00 | 5. | * | 2 JAN 1730 | 119 | .00 | .00 | .00 | 0. |
| 2 JAN 0130 | 55 | .01 | .01 | .00 | 5. | * | 2 JAN 1745 | 120 | .00 | .00 | .00 | 0. |
| 2 JAN 0145 | 56 | .01 | .01 | .00 | 5. | * | 2 JAN 1800 | 121 | .00 | .00 | .00 | 0. |
| 2 JAN 0200 | 57 | .01 | .01 | .00 | 5. | * | 2 JAN 1815 | 122 | .00 | .00 | .00 | 0. |
| 2 JAN 0215 | 58 | .01 | .01 | .00 | 4. | * | 2 JAN 1830 | 123 | .00 | .00 | .00 | 0. |
| 2 JAN 0230 | 59 | .01 | .01 | .00 | 4. | * | 2 JAN 1845 | 124 | .00 | .00 | .00 | 0. |
| 2 JAN 0245 | 60 | .01 | .01 | .00 | 3. | * | 2 JAN 1900 | 125 | .00 | .00 | .00 | 0. |
| 2 JAN 0300 | 61 | .01 | .01 | .00 | 3. | * | 2 JAN 1915 | 126 | .00 | .00 | .00 | 0. |
| 2 JAN 0315 | 62 | .01 | .01 | .00 | 2. | * | 2 JAN 1930 | 127 | .00 | .00 | .00 | 0. |
| 2 JAN 0330 | 63 | .01 | .01 | .00 | 2. | * | 2 JAN 1945 | 128 | .00 | .00 | .00 | 0. |
| 2 JAN 0345 | 64 | .01 | .01 | .00 | 2. | * | 2 JAN 2000 | 129 | .00 | .00 | .00 | 0. |
| 2 JAN 0400 | 65 | .01 | .01 | .00 | 1. | * | | | | | | |

TOTAL RAINFALL = 1.00, TOTAL LOSS = .90, TOTAL EXCESS = .10

| PEAK FLOW (CFS) | TIME (HR) | MAXIMUM AVERAGE FLOW | | | |
|--------------------|--------------|----------------------|-------|-------|----------|
| | | 6-HR | 24-HR | 72-HR | 32.00-HR |
| 5. | 13.50 | 3. | 1. | 1. | 1. |
| | (INCHES) | .069 | .103 | .104 | .104 |
| | (AC-FT) | 1. | 2. | 2. | 2. |

CUMULATIVE AREA = .36 SQ MI

HYDROGRAPH AT STATION OFFST PLAN 1, RATIO = 7.80

| DA | MON | HRMN | ORD | RAIN | LOSS | EXCESS | COMP Q | | DA | MON | HRMN | ORD | RAIN | LOSS | EXCESS | COMP Q |
|----|-----|------|-----|------|------|--------|--------|---|----|-----|------|-----|------|------|--------|--------|
| 1 | JAN | 1200 | 1 | .00 | .00 | .00 | 0. | * | 2 | JAN | 0415 | 66 | .04 | .01 | .03 | 77. |
| 1 | JAN | 1215 | 2 | .02 | .02 | .00 | 0. | * | 2 | JAN | 0430 | 67 | .03 | .00 | .03 | 70. |
| 1 | JAN | 1230 | 3 | .02 | .02 | .00 | 0. | * | 2 | JAN | 0445 | 68 | .04 | .01 | .03 | 64. |
| 1 | JAN | 1245 | 4 | .02 | .01 | .00 | 0. | * | 2 | JAN | 0500 | 69 | .03 | .00 | .03 | 58. |
| 1 | JAN | 1300 | 5 | .02 | .02 | .00 | 0. | * | 2 | JAN | 0515 | 70 | .04 | .01 | .03 | 53. |
| 1 | JAN | 1315 | 6 | .02 | .02 | .00 | 0. | * | 2 | JAN | 0530 | 71 | .03 | .00 | .03 | 49. |
| 1 | JAN | 1330 | 7 | .02 | .02 | .00 | 1. | * | 2 | JAN | 0545 | 72 | .04 | .01 | .03 | 45. |
| 1 | JAN | 1345 | 8 | .02 | .01 | .00 | 1. | * | 2 | JAN | 0600 | 73 | .03 | .00 | .03 | 41. |
| 1 | JAN | 1400 | 9 | .02 | .02 | .00 | 1. | * | 2 | JAN | 0615 | 74 | .04 | .01 | .03 | 39. |
| 1 | JAN | 1415 | 10 | .02 | .02 | .00 | 1. | * | 2 | JAN | 0630 | 75 | .03 | .00 | .03 | 36. |
| 1 | JAN | 1430 | 11 | .03 | .03 | .00 | 1. | * | 2 | JAN | 0645 | 76 | .03 | .00 | .03 | 34. |
| 1 | JAN | 1445 | 12 | .02 | .02 | .00 | 2. | * | 2 | JAN | 0700 | 77 | .04 | .01 | .03 | 33. |
| 1 | JAN | 1500 | 13 | .02 | .02 | .00 | 2. | * | 2 | JAN | 0715 | 78 | .03 | .00 | .03 | 32. |
| 1 | JAN | 1515 | 14 | .02 | .02 | .00 | 2. | * | 2 | JAN | 0730 | 79 | .04 | .01 | .03 | 31. |
| 1 | JAN | 1530 | 15 | .03 | .03 | .00 | 2. | * | 2 | JAN | 0745 | 80 | .03 | .00 | .03 | 30. |
| 1 | JAN | 1545 | 16 | .02 | .02 | .00 | 2. | * | 2 | JAN | 0800 | 81 | .04 | .01 | .03 | 29. |
| 1 | JAN | 1600 | 17 | .02 | .02 | .00 | 2. | * | 2 | JAN | 0815 | 82 | .02 | .00 | .02 | 29. |
| 1 | JAN | 1615 | 18 | .03 | .03 | .00 | 2. | * | 2 | JAN | 0830 | 83 | .02 | .00 | .02 | 28. |
| 1 | JAN | 1630 | 19 | .03 | .03 | .00 | 2. | * | 2 | JAN | 0845 | 84 | .02 | .00 | .02 | 28. |
| 1 | JAN | 1645 | 20 | .03 | .03 | .00 | 2. | * | 2 | JAN | 0900 | 85 | .02 | .00 | .02 | 27. |
| 1 | JAN | 1700 | 21 | .03 | .03 | .00 | 2. | * | 2 | JAN | 0915 | 86 | .02 | .00 | .02 | 26. |
| 1 | JAN | 1715 | 22 | .03 | .03 | .00 | 2. | * | 2 | JAN | 0930 | 87 | .02 | .00 | .02 | 25. |
| 1 | JAN | 1730 | 23 | .03 | .03 | .00 | 2. | * | 2 | JAN | 0945 | 88 | .02 | .00 | .02 | 24. |
| 1 | JAN | 1745 | 24 | .03 | .03 | .00 | 3. | * | 2 | JAN | 1000 | 89 | .02 | .00 | .02 | 23. |
| 1 | JAN | 1800 | 25 | .03 | .03 | .00 | 3. | * | 2 | JAN | 1015 | 90 | .02 | .00 | .02 | 22. |
| 1 | JAN | 1815 | 26 | .04 | .04 | .00 | 3. | * | 2 | JAN | 1030 | 91 | .02 | .00 | .02 | 21. |
| 1 | JAN | 1830 | 27 | .04 | .04 | .00 | 3. | * | 2 | JAN | 1045 | 92 | .02 | .00 | .02 | 21. |
| 1 | JAN | 1845 | 28 | .04 | .04 | .00 | 3. | * | 2 | JAN | 1100 | 93 | .02 | .00 | .02 | 20. |
| 1 | JAN | 1900 | 29 | .04 | .04 | .00 | 3. | * | 2 | JAN | 1115 | 94 | .02 | .00 | .02 | 20. |
| 1 | JAN | 1915 | 30 | .04 | .04 | .00 | 3. | * | 2 | JAN | 1130 | 95 | .02 | .00 | .02 | 20. |
| 1 | JAN | 1930 | 31 | .04 | .04 | .00 | 3. | * | 2 | JAN | 1145 | 96 | .02 | .00 | .02 | 20. |
| 1 | JAN | 1945 | 32 | .04 | .03 | .00 | 3. | * | 2 | JAN | 1200 | 97 | .02 | .00 | .02 | 19. |
| 1 | JAN | 2000 | 33 | .04 | .03 | .00 | 3. | * | 2 | JAN | 1215 | 98 | .00 | .00 | .00 | 19. |
| 1 | JAN | 2015 | 34 | .05 | .05 | .01 | 3. | * | 2 | JAN | 1230 | 99 | .00 | .00 | .00 | 19. |
| 1 | JAN | 2030 | 35 | .05 | .05 | .01 | 4. | * | 2 | JAN | 1245 | 100 | .00 | .00 | .00 | 18. |
| 1 | JAN | 2045 | 36 | .05 | .04 | .01 | 4. | * | 2 | JAN | 1300 | 101 | .00 | .00 | .00 | 16. |
| 1 | JAN | 2100 | 37 | .05 | .04 | .01 | 4. | * | 2 | JAN | 1315 | 102 | .00 | .00 | .00 | 15. |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

| | | | | | | | | | | | | |
|------------|----|------|-----|------|------|---|------------|-----|-----|-----|-----|-----|
| 1 JAN 2115 | 38 | .06 | .05 | .01 | 5. | * | 2 JAN 1330 | 103 | .00 | .00 | .00 | 13. |
| 1 JAN 2130 | 39 | .06 | .05 | .02 | 5. | * | 2 JAN 1345 | 104 | .00 | .00 | .00 | 10. |
| 1 JAN 2145 | 40 | .07 | .05 | .02 | 6. | * | 2 JAN 1400 | 105 | .00 | .00 | .00 | 8. |
| 1 JAN 2200 | 41 | .07 | .05 | .02 | 7. | * | 2 JAN 1415 | 106 | .00 | .00 | .00 | 7. |
| 1 JAN 2215 | 42 | .09 | .06 | .03 | 8. | * | 2 JAN 1430 | 107 | .00 | .00 | .00 | 5. |
| 1 JAN 2230 | 43 | .09 | .06 | .03 | 10. | * | 2 JAN 1445 | 108 | .00 | .00 | .00 | 4. |
| 1 JAN 2245 | 44 | .12 | .08 | .04 | 11. | * | 2 JAN 1500 | 109 | .00 | .00 | .00 | 3. |
| 1 JAN 2300 | 45 | .12 | .07 | .05 | 14. | * | 2 JAN 1515 | 110 | .00 | .00 | .00 | 3. |
| 1 JAN 2315 | 46 | .19 | .11 | .08 | 16. | * | 2 JAN 1530 | 111 | .00 | .00 | .00 | 2. |
| 1 JAN 2330 | 47 | .19 | .10 | .09 | 20. | * | 2 JAN 1545 | 112 | .00 | .00 | .00 | 2. |
| 1 JAN 2345 | 48 | .81 | .37 | .44 | 27. | * | 2 JAN 1600 | 113 | .00 | .00 | .00 | 1. |
| 2 JAN 0000 | 49 | 2.15 | .64 | 1.51 | 46. | * | 2 JAN 1615 | 114 | .00 | .00 | .00 | 1. |
| 2 JAN 0015 | 50 | .28 | .06 | .22 | 78. | * | 2 JAN 1630 | 115 | .00 | .00 | .00 | 1. |
| 2 JAN 0030 | 51 | .28 | .06 | .22 | 125. | * | 2 JAN 1645 | 116 | .00 | .00 | .00 | 1. |
| 2 JAN 0045 | 52 | .15 | .03 | .12 | 182. | * | 2 JAN 1700 | 117 | .00 | .00 | .00 | 0. |
| 2 JAN 0100 | 53 | .14 | .03 | .11 | 231. | * | 2 JAN 1715 | 118 | .00 | .00 | .00 | 0. |
| 2 JAN 0115 | 54 | .11 | .02 | .09 | 262. | * | 2 JAN 1730 | 119 | .00 | .00 | .00 | 0. |
| 2 JAN 0130 | 55 | .10 | .02 | .08 | 273. | * | 2 JAN 1745 | 120 | .00 | .00 | .00 | 0. |
| 2 JAN 0145 | 56 | .09 | .02 | .07 | 268. | * | 2 JAN 1800 | 121 | .00 | .00 | .00 | 0. |
| 2 JAN 0200 | 57 | .08 | .01 | .06 | 251. | * | 2 JAN 1815 | 122 | .00 | .00 | .00 | 0. |
| 2 JAN 0215 | 58 | .06 | .01 | .05 | 225. | * | 2 JAN 1830 | 123 | .00 | .00 | .00 | 0. |
| 2 JAN 0230 | 59 | .05 | .01 | .05 | 193. | * | 2 JAN 1845 | 124 | .00 | .00 | .00 | 0. |
| 2 JAN 0245 | 60 | .06 | .01 | .05 | 165. | * | 2 JAN 1900 | 125 | .00 | .00 | .00 | 0. |
| 2 JAN 0300 | 61 | .05 | .01 | .05 | 143. | * | 2 JAN 1915 | 126 | .00 | .00 | .00 | 0. |
| 2 JAN 0315 | 62 | .06 | .01 | .05 | 125. | * | 2 JAN 1930 | 127 | .00 | .00 | .00 | 0. |
| 2 JAN 0330 | 63 | .05 | .01 | .05 | 109. | * | 2 JAN 1945 | 128 | .00 | .00 | .00 | 0. |
| 2 JAN 0345 | 64 | .06 | .01 | .05 | 96. | * | 2 JAN 2000 | 129 | .00 | .00 | .00 | 0. |
| 2 JAN 0400 | 65 | .05 | .01 | .05 | 85. | * | | | | | | |

TOTAL RAINFALL = 7.80, TOTAL LOSS = 3.16, TOTAL EXCESS = 4.64

| PEAK FLOW + (CFS) | TIME (HR) | MAXIMUM AVERAGE FLOW | | | | |
|----------------------|--------------|----------------------|-------|-------|----------|-------|
| | | 6-HR | 24-HR | 72-HR | 32.00-HR | |
| + 273. | 13.50 | 136. | 45. | 34. | 34. | |
| | | (INCHES) | 3.529 | 4.622 | 4.644 | 4.644 |
| | | (AC-FT) | 68. | 88. | 89. | 89. |

CUMULATIVE AREA = .36 SQ MI

*** **

* *
123 KK BSN8 *
* *

124 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
139 KK 608P5 *
* *

140 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

* *
142 KK * POND4 *
* *

143 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** ** **

* *
149 KK * BSN10 *
* *

150 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

* *
165 KK * 10PDA *
* *

166 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

* *
168 KK * POND3 *
* *

169 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

* *
175 KK * BSN3 *
* *

176 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

* *
191 KK * BSN2 *
* *

192 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** ** **

* *
207 KK * POND1 *
* *

208 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

* *
216 KK * 3PD1&3 *
* *

217 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

* *
219 KK * POND2 *
* *

220 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

* *
228 KK * NORTH *
* *

229 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

```
*****
*
244 KK * OFFSTE *
*
*****
```

```
245 KO OUTPUT CONTROL VARIABLES
      IPRNT      5 PRINT CONTROL
      IPLOT      5 PLOT CONTROL
      QSCAL      0. HYDROGRAPH PLOT SCALE
```

*** ** ** ** **

```
*****
*
247 KK * RTE6 *
*
*****
```

```
248 KO OUTPUT CONTROL VARIABLES
      IPRNT      5 PRINT CONTROL
      IPLOT      5 PLOT CONTROL
      QSCAL      0. HYDROGRAPH PLOT SCALE
```

*** ** ** **~

```
*****
*
250 KK * NM-UND *
*
*****
```

```
251 KO OUTPUT CONTROL VARIABLES
      IPRNT      5 PRINT CONTROL
      IPLOT      5 PLOT CONTROL
      QSCAL      0. HYDROGRAPH PLOT SCALE
```

*** ** ** **~

```
*****
*
266 KK * 29TH *
*
*****
```

```
267 KO OUTPUT CONTROL VARIABLES
      IPRNT      5 PRINT CONTROL
      IPLOT      5 PLOT CONTROL
      QSCAL      0. HYDROGRAPH PLOT SCALE
```

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

| OPERATION | STATION | AREA | PLAN | RATIOS APPLIED TO PRECIPITATION | |
|---------------|---------|------|------|---------------------------------|--------|
| | | | | RATIO 1 | |
| | | | | 7.80 | |
| HYDROGRAPH AT | | | | | |
| + | BSN5 | .02 | 1 | FLOW | 32. |
| | | | | TIME | 12.50 |
| ROUTED TO | | | | | |
| + | POND7 | .02 | 1 | FLOW | 12. |
| | | | | TIME | 13.50 |
| | | | | ** PEAK STAGES IN FEET ** | |
| | | | 1 | STAGE | 171.83 |
| | | | | TIME | 13.50 |
| HYDROGRAPH AT | | | | | |
| + | BSN4 | .02 | 1 | FLOW | 22. |
| | | | | TIME | 12.75 |
| 2 COMBINED AT | | | | | |
| + | PD7&4 | .04 | 1 | FLOW | 31. |
| | | | | TIME | 13.00 |
| ROUTED TO | | | | | |
| + | POND6 | .04 | 1 | FLOW | 10. |
| | | | | TIME | 15.50 |
| | | | | ** PEAK STAGES IN FEET ** | |
| | | | 1 | STAGE | 172.05 |
| | | | | TIME | 15.50 |
| HYDROGRAPH AT | | | | | |
| + | BSN7 | .05 | 1 | FLOW | 61. |
| | | | | TIME | 12.75 |
| 2 COMBINED AT | | | | | |
| + | 7PD6 | .10 | 1 | FLOW | 64. |
| | | | | TIME | 12.75 |
| ROUTED TO | | | | | |
| + | POND5 | .10 | 1 | FLOW | 35. |
| | | | | TIME | 13.75 |
| | | | | ** PEAK STAGES IN FEET ** | |
| | | | 1 | STAGE | 168.73 |
| | | | | TIME | 13.75 |
| HYDROGRAPH AT | | | | | |
| + | BSN6 | .01 | 1 | FLOW | 12. |
| | | | | TIME | 12.50 |
| ROUTED TO | | | | | |
| + | RTE6 | .01 | 1 | FLOW | 12. |
| | | | | TIME | 13.25 |
| HYDROGRAPH AT | | | | | |
| + | OFFST | .36 | 1 | FLOW | 273. |
| | | | | TIME | 13.50 |
| HYDROGRAPH AT | | | | | |
| + | BSN8 | .03 | 1 | FLOW | 40. |
| | | | | TIME | 12.25 |
| 4 COMBINED AT | | | | | |
| + | 608P5 | .49 | 1 | FLOW | 326. |
| | | | | TIME | 13.50 |
| ROUTED TO | | | | | |
| + | POND4 | .49 | 1 | FLOW | 232. |
| | | | | TIME | 14.50 |
| | | | | ** PEAK STAGES IN FEET ** | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. Existing Conditions

| | | | | | |
|---------------|--------|-----|---|---------------------------|--------|
| | | | 1 | STAGE | 168.71 |
| | | | | TIME | 14.50 |
| HYDROGRAPH AT | | | | | |
| + | BSN10 | .02 | 1 | FLOW | 27. |
| | | | | TIME | 12.50 |
| 2 COMBINED AT | | | | | |
| + | 10PD4 | .51 | 1 | FLOW | 236. |
| | | | | TIME | 14.50 |
| ROUTED TO | | | | | |
| + | POND3 | .51 | 1 | FLOW | 224. |
| | | | | TIME | 15.50 |
| | | | | ** PEAK STAGES IN FEET ** | |
| | | | 1 | STAGE | 168.52 |
| | | | | TIME | 15.50 |
| HYDROGRAPH AT | | | | | |
| + | BSN3 | .02 | 1 | FLOW | 33. |
| | | | | TIME | 12.50 |
| HYDROGRAPH AT | | | | | |
| + | BSN2 | .03 | 1 | FLOW | 32. |
| | | | | TIME | 12.50 |
| ROUTED TO | | | | | |
| + | POND1 | .03 | 1 | FLOW | 31. |
| | | | | TIME | 12.75 |
| | | | | ** PEAK STAGES IN FEET ** | |
| | | | 1 | STAGE | 170.78 |
| | | | | TIME | 12.75 |
| 3 COMBINED AT | | | | | |
| + | 3PD1&3 | .56 | 1 | FLOW | 270. |
| | | | | TIME | 12.50 |
| ROUTED TO | | | | | |
| + | POND2 | .56 | 1 | FLOW | 267. |
| | | | | TIME | 12.75 |
| | | | | ** PEAK STAGES IN FEET ** | |
| | | | 1 | STAGE | 168.29 |
| | | | | TIME | 12.75 |
| HYDROGRAPH AT | | | | | |
| + | NORTH | .02 | 1 | FLOW | 27. |
| | | | | TIME | 12.25 |
| 2 COMBINED AT | | | | | |
| + | OFFSTE | .58 | 1 | FLOW | 281. |
| | | | | TIME | 12.75 |
| ROUTED TO | | | | | |
| + | RTE6 | .58 | 1 | FLOW | 281. |
| | | | | TIME | 13.25 |
| HYDROGRAPH AT | | | | | |
| + | NM-UND | .06 | 1 | FLOW | 108. |
| | | | | TIME | 12.25 |
| 2 COMBINED AT | | | | | |
| + | 29TH | .64 | 1 | FLOW | 321. |
| | | | | TIME | 12.50 |

*** NORMAL END OF HEC-1 ***

Project: **NEWMARKET OFFICE**
 Date: **4/10/2006**
 Prep. By: **SRB**

Manual Input

POST-DEVELOPMENT

Total Area **50.00 Acres**

| Soil Group | A (% of Total Area) | B (% of Total Area) | C (% of Total Area) | D (% of Total Area) | Total |
|------------|------------------------|------------------------|------------------------|------------------------|-------|
| | 0% | 75% | 0% | 25% | 100% |
| Acres | 0.00 | 30.00 | 0.00 | 10.00 | 50.00 |

| Land Use | Commercial (% of Total Area) | Industrial (% of Total Area) | Multi-Family (% of Total Area) | Public (% of Total Area) | Single Family (% of Total Area) | Vacant/Agriculture (% of Total Area) |
|----------|---------------------------------|---------------------------------|-----------------------------------|-----------------------------|------------------------------------|---|
| Existing | 40% | 0% | 0% | 0% | 20% | 40% |
| Acres | 20.00 | 0.00 | 0.00 | 0.00 | 10.00 | 20.00 |

Length of Flow **1300 ft**
 Slope **1:00 %**
 Waterflow Desc **IMP AREA**
 Avg Velocity **1.08 ft/sec**
 Tc **0.33 hours**

15 min <= Tc <= 24 hrs

Runoff Coefficients * Used Soil Group B/D

| Return Period (Years) | Commercial | Industrial | Multi-Family | Public | Single Family | Vacant/Agriculture |
|-----------------------|------------|------------|--------------|--------|---------------|--------------------|
| 2 | 0.68 | 0.68 | 0.70 | 0.49 | 0.50 | 0.54 |
| 5 | 0.69 | 0.69 | 0.73 | 0.51 | 0.54 | 0.56 |
| 10 | 0.73 | 0.73 | 0.79 | 0.56 | 0.62 | 0.61 |
| 25 | 0.75 | 0.75 | 0.81 | 0.59 | 0.66 | 0.64 |
| 50 | 0.77 | 0.77 | 0.83 | 0.62 | 0.70 | 0.67 |
| 100 | 0.80 | 0.80 | 0.86 | 0.66 | 0.76 | 0.70 |

Existing Conditions

| Return Period (Years) | Runoff Coefficient * | Rainfall Intensity (in/hr) | Area (Acres) | Runoff (cfs) |
|-----------------------|----------------------|----------------------------|--------------|--------------|
| 2 | 0.68 | 3.33 | 50.00 | 113.22 |
| 5 | 0.69 | 4.00 | 50.00 | 138.00 |
| 10 | 0.73 | 4.60 | 50.00 | 167.90 |
| 25 | 0.75 | 5.35 | 50.00 | 200.63 |
| 50 | 0.77 | 6.00 | 50.00 | 231.00 |
| 100 | 0.80 | 6.53 | 50.00 | 261.20 |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

```
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* FEBRUARY 1981 *
* REVISED 02 AUG 88 *
*
* RUN DATE 04/10/2006 TIME 15:29:00 *
*
*****
```

```
*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* THE HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *
*
*****
```

```

X   X  XXXXXX  XXXX      X
X   X  X      I   X      XX
X   X  X      I           X
XXXXXX XXXX  I   XXXX  X
X   X  X      I           X
X   X  X      I   X      X
X   X  XXXXXX  XXXX      XX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
 THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 1

| LINE | ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|--------------|----|--|---------|--------|--------|--------|---------|--------|--------|--------|--------|
| 1 | ID | MODIFIED FONTANA DRAINAGE PLAN (40-AC NEW MARKET OFFICE SPACE TRACT ADDED) | | | | | | | | | |
| 2 | ID | DEVELOPED CONDITIONS | | | | | | | | | |
| 3 | ID | BY BLE DATE 03-13-04, MODIFIED BY PDF 4/10/06 | | | | | | | | | |
| *** LIST *** | | | | | | | | | | | |
| *** FREE *** | | | | | | | | | | | |
| *DIAGRAM | | | | | | | | | | | |
| 4 | IT | 15 | 01JAN04 | 1200 | | 0 | 02JAN04 | 2000 | | | |
| 5 | IN | 15 | 01JAN04 | 1200 | | | | | | | |
| 6 | IO | 0 | 5 | | | | | | | | |
| 7 | JR | PREC | 7.8 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 8 | KK | BSN5 | | | | | | | | | |
| 9 | KO | 5 | | | | | | | | | |
| 10 | BA | 0.023 | | | | | | | | | |
| 11 | PB | 1.00 | | | | | | | | | |
| 12 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 13 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 14 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 15 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 16 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 17 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 18 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 19 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 20 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 21 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 22 | LS | 0 | 68 | 10 | | | | | | | |
| 23 | UD | 0.600 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 24 | KK | POND7 | | | | | | | | | |
| 25 | KO | 5 | | | | | | | | | |
| 26 | RS | 1 | ELEV | 162.0 | | | | | | | |
| 27 | SA | 2.55 | 2.71 | 2.88 | 3.06 | | | | | | |
| 28 | SE | 171.0 | 172.0 | 173.0 | 174.0 | | | | | | |
| 29 | SQ | 0 | 3.2 | 6.4 | 9.6 | 12.8 | 16.0 | 19.2 | 22.4 | 25.6 | 28.8 |
| 30 | SQ | 32.0 | | | | | | | | | |
| 31 | SE | 171.0 | 171.35 | 171.56 | 171.73 | 171.88 | 172.02 | 172.16 | 172.28 | 172.40 | 172.52 |
| 32 | SE | 172.6 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 33 | KK | BSN4 | | | | | | | | | |
| 34 | KO | 5 | | | | | | | | | |
| 35 | BA | 0.020 | | | | | | | | | |
| 36 | PB | 1.00 | | | | | | | | | |
| 37 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 38 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 39 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 40 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 41 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 42 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 2

| LINE | ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|------|----|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 43 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 44 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 45 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 46 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 47 | LS | 0 | 68 | 10 | | | | | | | |
| 48 | UD | 0.850 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 49 | KK | PD7&4 | | | | | | | | | |
| 50 | KO | 5 | | | | | | | | | |
| 51 | HC | 2 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 52 | KK | POND6 | | | | | | | | | |
| 53 | KO | 5 | | | | | | | | | |
| 54 | RS | 1 | ELEV | 162.0 | | | | | | | |
| 55 | SA | 1.85 | 1.99 | 2.14 | 2.29 | | | | | | |
| 56 | SE | 170.0 | 171.0 | 172.0 | 173.0 | | | | | | |
| 57 | SQ | 0 | 2.2 | 4.4 | 6.6 | 8.8 | 11.0 | 13.2 | 15.4 | 17.6 | 19.8 |
| 58 | SQ | 22.0 | | | | | | | | | |
| 59 | SE | 170.0 | 170.72 | 171.11 | 171.42 | 171.77 | 172.21 | 172.75 | 173.40 | 174.14 | 174.98 |
| 60 | SE | 175.9 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 61 | KK | BSN7 | | | | | | | | | |
| 62 | KO | 5 | | | | | | | | | |
| 63 | BA | 0.055 | | | | | | | | | |
| 64 | PB | 1.00 | | | | | | | | | |
| 65 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 66 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 67 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 68 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 69 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 70 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 71 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 72 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 73 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 74 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 75 | LS | 0 | 68 | 10 | | | | | | | |
| 76 | UD | 0.840 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 77 | KK | 7PD6 | | | | | | | | | |
| 78 | KO | 5 | | | | | | | | | |
| 79 | HC | 2 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 3

| LINE | ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|------|----|-------|------------|--------|--------|--------|--------|--------|--------|--------|--------|
| 80 | KK | POND5 | | | | | | | | | |
| 81 | KO | 5 | | | | | | | | | |
| 82 | RS | 1 | ELEV 159.0 | | | | | | | | |
| 83 | SA | 2.67 | 2.84 | 3.01 | 3.19 | | | | | | |
| 84 | SE | 167.0 | 168.0 | 169.0 | 170.0 | | | | | | |
| 85 | SQ | 0 | 6.3 | 12.6 | 18.9 | 25.2 | 31.5 | 37.8 | 44.1 | 50.4 | 56.7 |
| 86 | SQ | 63.0 | | | | | | | | | |
| 87 | SE | 167.0 | 167.55 | 167.87 | 168.14 | 168.39 | 168.61 | 168.82 | 169.01 | 169.20 | 169.38 |
| 88 | SE | 169.6 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 89 | KK | BSN6 | | | | | | | | | |
| 90 | KO | 5 | | | | | | | | | |
| 91 | BA | 0.008 | | | | | | | | | |
| 92 | PB | 1.00 | | | | | | | | | |
| 93 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 94 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 95 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 96 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 97 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 98 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 99 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 100 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 101 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 102 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 103 | LS | 0 | 68 | 10 | | | | | | | |
| 104 | UD | 0.530 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 105 | KK | RTE6 | | | | | | | | | |
| 106 | KO | 5 | | | | | | | | | |
| 107 | RT | 0 | 0 | 3 | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 108 | KK | OFFST | | | | | | | | | |
| 109 | KO | 5 | | | | | | | | | |
| 110 | BA | 0.359 | | | | | | | | | |
| 111 | PB | 1.00 | | | | | | | | | |
| 112 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 113 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 114 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 115 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 116 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 117 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 118 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 119 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 120 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 121 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 122 | LS | 0 | 70 | 10 | | | | | | | |
| 123 | UD | 1.575 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 4

| LINE | ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|------|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 124 | KK | BSN8 | | | | | | | | | |
| 125 | KO | 5 | | | | | | | | | |
| 126 | BA | 0.027 | | | | | | | | | |
| 127 | PB | 1.00 | | | | | | | | | |
| 128 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 129 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 130 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 131 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 132 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 133 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 134 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 135 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 136 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 137 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 138 | LS | 0 | 68 | 10 | | | | | | | |
| 139 | UD | 0.490 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 140 | KK | 608P5 | | | | | | | | | |
| 141 | KO | 5 | | | | | | | | | |
| 142 | HC | 4 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 143 | KK | POND4 | | | | | | | | | |
| 144 | KO | 5 | | | | | | | | | |
| 145 | RS | 1 | ELEV | 158.0 | | | | | | | |
| 146 | SA | 3.06 | 3.24 | 3.42 | 3.61 | | | | | | |
| 147 | SE | 166.0 | 167.0 | 168.0 | 169.0 | | | | | | |
| 148 | SL | 158.0 | 14.73 | 0.6 | 0.5 | | | | | | |
| 149 | SS | 167.0 | 0.00 | 3.0 | 1.5 | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 150 | KK | BSN10 | | | | | | | | | |
| 151 | KO | 5 | | | | | | | | | |
| 152 | BA | 0.021 | | | | | | | | | |
| 153 | PB | 1.00 | | | | | | | | | |
| 154 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 155 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 156 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 157 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 158 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 159 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 160 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 161 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 162 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 163 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 164 | LS | 0 | 68 | 10 | | | | | | | |
| 165 | UD | 0.670 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 5

| LINE | ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|------|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 166 | KK | 10PDA | | | | | | | | | |
| 167 | KO | 5 | | | | | | | | | |
| 168 | HC | 2 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 169 | KK | POND3 | | | | | | | | | |
| 170 | KO | 5 | | | | | | | | | |
| 171 | RS | 1 | ELEV | 162.0 | | | | | | | |
| 172 | SA | 1.70 | 1.83 | 1.98 | 2.12 | | | | | | |
| 173 | SE | 166.0 | 167.0 | 168.0 | 169.0 | | | | | | |
| 174 | SL | 158.5 | 14.73 | 0.6 | 0.5 | | | | | | |
| 175 | SS | 168.0 | 0.00 | 3.0 | 1.5 | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 176 | KK | BSN3 | | | | | | | | | |
| 177 | KO | 5 | | | | | | | | | |
| 178 | BA | 0.024 | | | | | | | | | |
| 179 | PB | 1.00 | | | | | | | | | |
| 180 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 181 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 182 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 183 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 184 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 185 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 186 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 187 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 188 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 189 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 190 | LS | 0 | 68 | 10 | | | | | | | |
| 191 | UD | 0.580 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 192 | KK | BSN2 | | | | | | | | | |
| 193 | KO | 5 | | | | | | | | | |
| 194 | BA | 0.025 | | | | | | | | | |
| 195 | PB | 1.00 | | | | | | | | | |
| 196 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 197 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 198 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 199 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 200 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 201 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 202 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 203 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 204 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 205 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 206 | LS | 0 | 68 | 10 | | | | | | | |
| 207 | UD | 0.670 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 6

| LINE | ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|------|-----------|--|--------|---------------|--------|--------|--------|--------|--------|--------|--------|
| 208 | KK POND1 | | | | | | | | | | |
| 209 | KO | 5 | | | | | | | | | |
| 210 | RS | 1 | ELEV | 162.0 | | | | | | | |
| 211 | SA | 0.36 | 0.43 | 0.49 | 0.57 | | | | | | |
| 212 | SE | 170.0 | 171.0 | 172.0 | 173.0 | | | | | | |
| 213 | SQ | 0 | 3.2 | 6.4 | 9.6 | 12.8 | 16.0 | 19.2 | 22.4 | 25.6 | 28.8 |
| 214 | SQ | 32.0 | | | | | | | | | |
| 215 | SE | 170.0 | 170.17 | 170.27 | 170.35 | 170.42 | 170.49 | 170.56 | 170.62 | 170.67 | 170.73 |
| 216 | SE | 170.8 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 217 | KK 3PD1&3 | | | | | | | | | | |
| 218 | KO | 5 | | | | | | | | | |
| 219 | HC | 3 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 220 | KK POND2 | | | | | | | | | | |
| 221 | KO | 5 | | | | | | | | | |
| 222 | RS | 1 | ELEV | 158.0 | | | | | | | |
| 223 | SA | 2.08 | 2.23 | 2.38 | 2.54 | | | | | | |
| 224 | SE | 166.0 | 167.0 | 168.0 | 169.0 | | | | | | |
| 225 | SQ | 0 | 26.9 | 53.8 | 80.7 | 107.6 | 134.5 | 161.4 | 188.3 | 215.2 | 242.1 |
| 226 | SQ | 269.0 | | | | | | | | | |
| 227 | SE | 166.0 | 166.50 | 166.79 | 167.03 | 167.25 | 167.45 | 167.63 | 167.81 | 167.98 | 168.14 |
| 228 | SE | 168.3 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 229 | KK PONDA | | | | | | | | | | |
| 230 | KO | 5 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | ASSUMED OUTLET | 10 | WEIR AT ELEV. | 162.5 | | | | | | |
| | * | | | | | | | | | | |
| 231 | RS | 1 | ELEV | 162.5 | | | | | | | |
| 232 | SA | 1.30 | 1.30 | | | | | | | | |
| 233 | SE | 162.5 | 170.0 | | | | | | | | |
| 234 | SQ | 0 | 35 | 70 | 105 | 140 | 175 | 210 | 245 | 280 | 315 |
| 235 | SQ | 350.0 | | | | | | | | | |
| 236 | SE | 162.5 | 163.63 | 164.30 | 164.86 | 165.36 | 165.81 | 166.24 | 166.65 | 167.03 | 167.40 |
| 237 | SE | 167.8 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | 10 ACRES NORTH OF PROPOSED DEVELOPMENT | | | | | | | | | |
| | * | | | | | | | | | | |
| 238 | KK NORTH | | | | | | | | | | |
| 239 | KO | 5 | | | | | | | | | |
| 240 | BA | 0.0156 | | | | | | | | | |
| 241 | PB | 1.00 | | | | | | | | | |
| 242 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 243 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 244 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 7

| LINE | ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|------|----|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 245 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 246 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 247 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 248 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 249 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 250 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 251 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 252 | LS | 0 | 70 | 0 | | | | | | | |
| 253 | UD | 0.40 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 254 | KK | OFFSTE | | | | | | | | | |
| 255 | RO | 5 | | | | | | | | | |
| 256 | HC | 2 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | ADDED 40 ACRES DEVELOPED OFFICE PARK Tc=20 MINUTED, 50% IMPERVIOUS | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 257 | KK | DEV-1 | | | | | | | | | |
| 258 | RO | 5 | | | | | | | | | |
| 259 | BA | 0.0625 | | | | | | | | | |
| 260 | PB | 1.00 | | | | | | | | | |
| 261 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 262 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 263 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 264 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 265 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 266 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 267 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 268 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 269 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 270 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 271 | LS | 0 | 70 | 50 | | | | | | | |
| 272 | UD | 0.20 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 273 | KK | 29TH | | | | | | | | | |
| 274 | RO | 5 | | | | | | | | | |
| 275 | HC | 2 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 8

| LINE | ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10 |
|------|---|
| 276 | KK PONDB |
| 277 | KO 5 |
| | * * ASSUMED OUTLET 10 WEIR AT ELEV. 159.0 * |
| 278 | RS 1 ELEV 159.0 |
| 279 | SA 5.10 5.10 |
| 280 | SE 159.0 170.0 |
| 281 | SQ 0 35 70 105 140 175 210 245 280 315 |
| 282 | SQ 350.0 |
| 283 | SE 159.0 160.13 160.80 161.36 161.86 162.31 162.74 163.15 163.53 163.90 |
| 284 | SE 164.3 |
| | * * * |
| 285 | ZZ |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

SCHEMATIC DIAGRAM OF STREAM NETWORK

| INPUT LINE NO. | (V) ROUTING | (--->) DIVERSION OR PUMP FLOW |
|----------------|---------------|--|
| NO. | (.) CONNECTOR | (<---) RETURN OF DIVERTED OR PUMPED FLOW |
| 8 | BSN5 | |
| | V | |
| | V | |
| 24 | POND7 | |
| | . | |
| 33 | BSN4 | |
| | . | |
| | . | |
| 49 | PD7&4..... | |
| | V | |
| | V | |
| 52 | POND6 | |
| | . | |
| 61 | BSN7 | |
| | . | |
| | . | |
| 77 | 7PD6..... | |
| | V | |
| | V | |
| 80 | POND5 | |
| | . | |
| 89 | BSN6 | |
| | V | |
| | V | |
| 105 | RTE6 | |
| | . | |
| | . | |
| 108 | OFFST | |
| | . | |
| | . | |
| 124 | BSN8 | |
| | . | |
| | . | |
| 140 | 608P5..... | |
| | V | |
| | V | |
| 143 | POND4 | |
| | . | |
| 150 | BSN10 | |
| | . | |
| | . | |
| 166 | 10PD4..... | |
| | V | |
| | V | |
| 169 | POND3 | |
| | . | |
| 176 | BSN3 | |
| | . | |
| | . | |
| 192 | BSN2 | |
| | V | |
| | V | |
| 208 | POND1 | |
| | . | |
| | . | |
| 217 | 3PD1&3..... | |
| | V | |
| | V | |
| 220 | POND2 | |
| | V | |
| | V | |
| 229 | PONDA | |
| | . | |
| | . | |
| 238 | NORTH | |
| | . | |
| | . | |
| 254 | OFFSTE..... | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

257 DEV-1
273 29TH.....
V
V
276 PONDB

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

```
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* FEBRUARY 1981
* REVISED 02 AUG 88
*
* RUN DATE 04/10/2006 TIME 15:29:00
*
*****
```

```
*****
*
* U.S. ARMY CORPS OF ENGINEERS
* THE HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*
*****
```

MODIFIED FONTANA DRAINAGE PLAN (40-AC NEW MARKET OFFICE SPACE TRACT ADDED)
 DEVELOPED CONDITIONS
 BY BLB DATE 03-13-04, MODIFIED BY PDF 4/10/06

```
6 IO      OUTPUT CONTROL VARIABLES
          IPRNT      0  PRINT CONTROL
          IPLOT      5  PLOT CONTROL
          QSCAL      0.  HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA
          NMIN       15  MINUTES IN COMPUTATION INTERVAL
          IDATE      1JAN 4  STARTING DATE
          ITIME      1200  STARTING TIME
          NQ         129  NUMBER OF HYDROGRAPH ORDINATES
          NDDATE     2JAN 4  ENDING DATE
          NDTIME     2000  ENDING TIME
          ICENT      19  CENTURY MARK

          COMPUTATION INTERVAL .25 HOURS
          TOTAL TIME BASE 32.00 HOURS
```

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FARRENHEIT

```
JP        MULTI-PLAN OPTION
          NPLAN      1  NUMBER OF PLANS
```

```
JR        MULTI-RATIO OPTION
          RATIOS OF PRECIPITATION
          7.80
```

*** ** ** ** **

```
*****
*
*      BSN5
*
*****
```

```
9 KO      OUTPUT CONTROL VARIABLES
          IPRNT      5  PRINT CONTROL
          IPLOT      5  PLOT CONTROL
          QSCAL      0.  HYDROGRAPH PLOT SCALE
```

*** ** ** **~

```
*****
*
*      POND7
*
*****
```

```
25 KO     OUTPUT CONTROL VARIABLES
          IPRNT      5  PRINT CONTROL
```

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
33 KK * BSN4 *
* *

34 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
49 KK * PD7&4 *
* *

50 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
52 KK * POND6 *
* *

53 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
61 KK * BSN7 *
* *

62 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
77 KK * 7PD6 *
* *

78 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPLLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
80 KK * POND5 *
* *

81 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
89 KK * BSN6 *
* *

90 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
105 KK * RTE6 *
* *

106 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
108 KK * OFFST *
* *

109 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
124 KK * BSN8 *
* *

125 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
80 KK * PONDS *
* *

81 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
89 KK * BSN6 *
* *

90 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
105 KK * RTE6 *
* *

106 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
108 KK * OFFST *
* *

109 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
124 KK * BSN8 *
* *

125 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
140 KK * 608P5 *
* *

141 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
143 KK * POND4 *
* *

144 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
150 KK * BSN10 *
* *

151 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
166 KK * 10PD4 *
* *

167 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
169 KK * POND3 *
* *

170 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
176 KK * BSN3 *
* *

177 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
192 KK * BSN2 *
* *

193 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
208 KK * POND1 *
* *

209 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
217 KK * 3PD1&3 *
* *

218 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
220 KK * POND2 *
* *

221 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** ** **

* *
229 KK * PONDA *
* *

230 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** ** **

* *
238 KK * NORTH *
* *

239 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

* *
254 KK * OFFSTE *
* *

255 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

* *
257 KK * DEV-1 *
* *

258 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

* *
273 KK * 29TH *
* *

274 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** ** **

* *
276 KK * PONDE *
* *

277 KO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPL0T 5 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

| OPERATION | STATION | AREA | PLAN | RATIOS APPLIED TO PRECIPITATION | |
|---------------|---------|------|---------------------------|---------------------------------|------|
| | | | | RATIO 1 | 7.80 |
| HYDROGRAPH AT | | | | | |
| + BSN5 | .02 | 1 | FLOW | 32. | |
| | | | TIME | 12.50 | |
| ROUTED TO | | | | | |
| + POND7 | .02 | 1 | FLOW | 12. | |
| | | | TIME | 13.50 | |
| | | | ** PEAK STAGES IN FEET ** | | |
| | | 1 | STAGE | 171.83 | |
| | | | TIME | 13.50 | |
| HYDROGRAPH AT | | | | | |
| + BSN4 | .02 | 1 | FLOW | 22. | |
| | | | TIME | 12.75 | |
| 2 COMBINED AT | | | | | |
| + PD7&4 | .04 | 1 | FLOW | 31. | |
| | | | TIME | 13.00 | |
| ROUTED TO | | | | | |
| + POND6 | .04 | 1 | FLOW | 10. | |
| | | | TIME | 15.50 | |
| | | | ** PEAK STAGES IN FEET ** | | |
| | | 1 | STAGE | 172.05 | |
| | | | TIME | 15.50 | |
| HYDROGRAPH AT | | | | | |
| + BSN7 | .05 | 1 | FLOW | 61. | |
| | | | TIME | 12.75 | |
| 2 COMBINED AT | | | | | |
| + 7PD6 | .10 | 1 | FLOW | 64. | |
| | | | TIME | 12.75 | |
| ROUTED TO | | | | | |
| + POND5 | .10 | 1 | FLOW | 35. | |
| | | | TIME | 13.75 | |
| | | | ** PEAK STAGES IN FEET ** | | |
| | | 1 | STAGE | 168.73 | |
| | | | TIME | 13.75 | |
| HYDROGRAPH AT | | | | | |
| + BSN6 | .01 | 1 | FLOW | 12. | |
| | | | TIME | 12.50 | |
| ROUTED TO | | | | | |
| + RTE6 | .01 | 1 | FLOW | 12. | |
| | | | TIME | 13.25 | |
| HYDROGRAPH AT | | | | | |
| + OFFST | .36 | 1 | FLOW | 273. | |
| | | | TIME | 13.50 | |
| HYDROGRAPH AT | | | | | |
| + BSN8 | .03 | 1 | FLOW | 40. | |
| | | | TIME | 12.25 | |
| 4 COMBINED AT | | | | | |
| + 608P5 | .49 | 1 | FLOW | 326. | |
| | | | TIME | 13.50 | |
| ROUTED TO | | | | | |
| + POND4 | .49 | 1 | FLOW | 232. | |
| | | | TIME | 14.50 | |
| | | | ** PEAK STAGES IN FEET ** | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

| | | | | | |
|---------------|--------|-----|---|---------------------------|--------|
| | | | 1 | STAGE | 168.71 |
| | | | | TIME | 14.50 |
| HYDROGRAPH AT | | | | | |
| + | BSN10 | .02 | 1 | FLOW | 27. |
| | | | | TIME | 12.50 |
| 2 COMBINED AT | | | | | |
| + | 10PD4 | .51 | 1 | FLOW | 236. |
| | | | | TIME | 14.50 |
| ROUTED TO | | | | | |
| + | POND3 | .51 | 1 | FLOW | 224. |
| | | | | TIME | 15.50 |
| | | | | ** PEAK STAGES IN FEET ** | |
| | | | 1 | STAGE | 168.52 |
| | | | | TIME | 15.50 |
| HYDROGRAPH AT | | | | | |
| + | BSN3 | .02 | 1 | FLOW | 33. |
| | | | | TIME | 12.50 |
| HYDROGRAPH AT | | | | | |
| + | BSN2 | .03 | 1 | FLOW | 32. |
| | | | | TIME | 12.50 |
| ROUTED TO | | | | | |
| + | POND1 | .03 | 1 | FLOW | 31. |
| | | | | TIME | 12.75 |
| | | | | ** PEAK STAGES IN FEET ** | |
| | | | 1 | STAGE | 170.78 |
| | | | | TIME | 12.75 |
| 3 COMBINED AT | | | | | |
| + | 3PD1&3 | .56 | 1 | FLOW | 270. |
| | | | | TIME | 12.50 |
| ROUTED TO | | | | | |
| + | POND2 | .56 | 1 | FLOW | 267. |
| | | | | TIME | 12.75 |
| | | | | ** PEAK STAGES IN FEET ** | |
| | | | 1 | STAGE | 168.29 |
| | | | | TIME | 12.75 |
| ROUTED TO | | | | | |
| + | PONDA | .56 | 1 | FLOW | 264. |
| | | | | TIME | 13.00 |
| | | | | ** PEAK STAGES IN FEET ** | |
| | | | 1 | STAGE | 166.86 |
| | | | | TIME | 13.00 |
| HYDROGRAPH AT | | | | | |
| + | NORTH | .02 | 1 | FLOW | 27. |
| | | | | TIME | 12.25 |
| 2 COMBINED AT | | | | | |
| + | OFFSTE | .58 | 1 | FLOW | 274. |
| | | | | TIME | 13.00 |
| HYDROGRAPH AT | | | | | |
| + | DEV-1 | .06 | 1 | FLOW | 184. |
| | | | | TIME | 12.00 |
| 2 COMBINED AT | | | | | |
| + | 29TH | .64 | 1 | FLOW | 411. |
| | | | | TIME | 12.00 |
| ROUTED TO | | | | | |
| + | PONDB | .64 | 1 | FLOW | 321. |
| | | | | TIME | 12.50 |
| | | | | ** PEAK STAGES IN FEET ** | |
| | | | 1 | STAGE | 163.97 |
| | | | | TIME | 12.50 |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

*** NORMAL END OF REC-1 ***

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

```
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   FEBRUARY 1981                   *
*   REVISED 02 AUG 88               *
*
* RUN DATE 04/10/2006 TIME 15:29:00 *
*
*****
```

```
*****
*
* U.S. ARMY CORPS OF ENGINEERS      *
* THE HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET                 *
* DAVIS, CALIFORNIA 95616          *
* (916) 551-1748                   *
*
*****
```

```

X  X  XXXXXX  XXXX  X
X  X  X      X  X  XX
X  X  X      I    I
XXXXXX XXXX  I    XXXX  I
X  X  X      X    X  I
X  X  X      X    X  X
X  X  XXXXXX  XXXX  XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 1

| LINE | ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|--------------|----|--|---------|--------|--------|--------|---------|--------|--------|--------|--------|
| 1 | ID | MODIFIED FONTANA DRAINAGE PLAN (40-AC NEW MARKET OFFICE SPACE TRACT ADDED) | | | | | | | | | |
| 2 | ID | DEVELOPED CONDITIONS | | | | | | | | | |
| 3 | ID | BY BLB DATE 03-13-04, MODIFIED BY PDF 4/10/06 | | | | | | | | | |
| *** LIST *** | | | | | | | | | | | |
| *** FREE *** | | | | | | | | | | | |
| *DIAGRAM | | | | | | | | | | | |
| 4 | IT | 15 | 01JAN04 | 1200 | | 0 | 02JAN04 | 2000 | | | |
| 5 | IN | 15 | 01JAN04 | 1200 | | | | | | | |
| 6 | IO | 0 | 5 | | | | | | | | |
| 7 | JR | PREC | 7.8 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 8 | KK | BSN5 | | | | | | | | | |
| 9 | KO | 5 | | | | | | | | | |
| 10 | BA | 0.023 | | | | | | | | | |
| 11 | PB | 1.00 | | | | | | | | | |
| 12 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 13 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 14 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 15 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 16 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 17 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 18 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 19 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 20 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 21 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 22 | LS | 0 | 68 | 10 | | | | | | | |
| 23 | UD | 0.600 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 24 | KK | POND7 | | | | | | | | | |
| 25 | KO | 5 | | | | | | | | | |
| 26 | RS | 1 | ELEV | 162.0 | | | | | | | |
| 27 | SA | 2.55 | 2.71 | 2.88 | 3.06 | | | | | | |
| 28 | SE | 171.0 | 172.0 | 173.0 | 174.0 | | | | | | |
| 29 | SQ | 0 | 3.2 | 6.4 | 9.6 | 12.8 | 16.0 | 19.2 | 22.4 | 25.6 | 28.8 |
| 30 | SQ | 32.0 | | | | | | | | | |
| 31 | SE | 171.0 | 171.35 | 171.56 | 171.73 | 171.88 | 172.02 | 172.16 | 172.28 | 172.40 | 172.52 |
| 32 | SE | 172.6 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 33 | KK | BSN4 | | | | | | | | | |
| 34 | KO | 5 | | | | | | | | | |
| 35 | BA | 0.020 | | | | | | | | | |
| 36 | PB | 1.00 | | | | | | | | | |
| 37 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 38 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 39 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 40 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 41 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 42 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 2

| LINE | ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|------|----|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 43 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 44 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 45 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 46 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 47 | LS | 0 | 68 | 10 | | | | | | | |
| 48 | UD | 0.850 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 49 | KK | PD7&4 | | | | | | | | | |
| 50 | KO | 5 | | | | | | | | | |
| 51 | HC | 2 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 52 | KK | POND6 | | | | | | | | | |
| 53 | KO | 5 | | | | | | | | | |
| 54 | RS | 1 | ELEV | 162.0 | | | | | | | |
| 55 | SA | 1.85 | 1.99 | 2.14 | 2.29 | | | | | | |
| 56 | SE | 170.0 | 171.0 | 172.0 | 173.0 | | | | | | |
| 57 | SQ | 0 | 2.2 | 4.4 | 6.6 | 8.8 | 11.0 | 13.2 | 15.4 | 17.6 | 19.8 |
| 58 | SQ | 22.0 | | | | | | | | | |
| 59 | SE | 170.0 | 170.72 | 171.11 | 171.42 | 171.77 | 172.21 | 172.75 | 173.40 | 174.14 | 174.98 |
| 60 | SE | 175.9 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 61 | KK | BSN7 | | | | | | | | | |
| 62 | KO | 5 | | | | | | | | | |
| 63 | BA | 0.055 | | | | | | | | | |
| 64 | PB | 1.00 | | | | | | | | | |
| 65 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 66 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 67 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 68 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 69 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 70 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 71 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 72 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 73 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 74 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 75 | LS | 0 | 68 | 10 | | | | | | | |
| 76 | UD | 0.840 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 77 | KK | 7PD6 | | | | | | | | | |
| 78 | KO | 5 | | | | | | | | | |
| 79 | HC | 2 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 3

| LINE | ID..... | 1..... | 2..... | 3..... | 4..... | 5..... | 6..... | 7..... | 8..... | 9..... | 10 | |
|------|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--|
| 80 | KK | POND5 | | | | | | | | | | |
| 81 | KO | 5 | | | | | | | | | | |
| 82 | RS | 1 | ELEV | 159.0 | | | | | | | | |
| 83 | SA | 2.67 | 2.84 | 3.01 | 3.19 | | | | | | | |
| 84 | SE | 167.0 | 168.0 | 169.0 | 170.0 | | | | | | | |
| 85 | SQ | 0 | 6.3 | 12.6 | 18.9 | 25.2 | 31.5 | 37.8 | 44.1 | 50.4 | 56.7 | |
| 86 | SQ | 63.0 | | | | | | | | | | |
| 87 | SE | 167.0 | 167.55 | 167.87 | 168.14 | 168.39 | 168.61 | 168.82 | 169.01 | 169.20 | 169.38 | |
| 88 | SE | 169.6 | | | | | | | | | | |
| | * | | | | | | | | | | | |
| 89 | KK | BSN6 | | | | | | | | | | |
| 90 | KO | 5 | | | | | | | | | | |
| 91 | BA | 0.008 | | | | | | | | | | |
| 92 | PB | 1.00 | | | | | | | | | | |
| 93 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 | |
| 94 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 | |
| 95 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 | |
| 96 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 | |
| 97 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 | |
| 98 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 | |
| 99 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 | |
| 100 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 | |
| 101 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 | |
| 102 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | | |
| 103 | LS | 0 | 68 | 10 | | | | | | | | |
| 104 | UD | 0.530 | | | | | | | | | | |
| | * | | | | | | | | | | | |
| 105 | KK | RTE6 | | | | | | | | | | |
| 106 | KO | 5 | | | | | | | | | | |
| 107 | RT | 0 | 0 | 3 | | | | | | | | |
| | * | | | | | | | | | | | |
| 108 | KK | OFFST | | | | | | | | | | |
| 109 | KO | 5 | | | | | | | | | | |
| 110 | BA | 0.359 | | | | | | | | | | |
| 111 | PB | 1.00 | | | | | | | | | | |
| 112 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 | |
| 113 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 | |
| 114 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 | |
| 115 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 | |
| 116 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 | |
| 117 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 | |
| 118 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 | |
| 119 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 | |
| 120 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 | |
| 121 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | | |
| 122 | LS | 0 | 70 | 10 | | | | | | | | |
| 123 | UD | 1.575 | | | | | | | | | | |
| | * | | | | | | | | | | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 4

| LINE | ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|------|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 124 | KK | BSN8 | | | | | | | | | |
| 125 | KO | 5 | | | | | | | | | |
| 126 | BA | 0.027 | | | | | | | | | |
| 127 | PB | 1.00 | | | | | | | | | |
| 128 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 129 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 130 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 131 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 132 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 133 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 134 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 135 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 136 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 137 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 138 | LS | 0 | 68 | 10 | | | | | | | |
| 139 | UD | 0.490 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 140 | KK | 608P5 | | | | | | | | | |
| 141 | KO | 5 | | | | | | | | | |
| 142 | HC | 4 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 143 | KK | POND4 | | | | | | | | | |
| 144 | KO | 5 | | | | | | | | | |
| 145 | RS | 1 | ELEV | 158.0 | | | | | | | |
| 146 | SA | 3.06 | 3.24 | 3.42 | 3.61 | | | | | | |
| 147 | SE | 166.0 | 167.0 | 168.0 | 169.0 | | | | | | |
| 148 | SL | 158.0 | 14.73 | 0.6 | 0.5 | | | | | | |
| 149 | SS | 167.0 | 0.00 | 3.0 | 1.5 | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 150 | KK | BSN10 | | | | | | | | | |
| 151 | KO | 5 | | | | | | | | | |
| 152 | BA | 0.021 | | | | | | | | | |
| 153 | PB | 1.00 | | | | | | | | | |
| 154 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 155 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 156 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 157 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 158 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 159 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 160 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 161 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 162 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 163 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 164 | LS | 0 | 68 | 10 | | | | | | | |
| 165 | UD | 0.670 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 5

| LINE | ID..... | 1..... | 2..... | 3..... | 4..... | 5..... | 6..... | 7..... | 8..... | 9..... | 10..... |
|------|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|
| 166 | KK | 10PD4 | | | | | | | | | |
| 167 | KO | 5 | | | | | | | | | |
| 168 | HC | 2 | 0 | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 169 | KK | POND3 | | | | | | | | | |
| 170 | KO | 5 | | | | | | | | | |
| 171 | RS | 1 | ELEV | 162.0 | | | | | | | |
| 172 | SA | 1.70 | 1.83 | 1.98 | 2.12 | | | | | | |
| 173 | SE | 166.0 | 167.0 | 168.0 | 169.0 | | | | | | |
| 174 | SL | 158.5 | 14.73 | 0.6 | 0.5 | | | | | | |
| 175 | SS | 168.0 | 0.00 | 3.0 | 1.5 | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 176 | KK | BSN3 | | | | | | | | | |
| 177 | KO | 5 | | | | | | | | | |
| 178 | BA | 0.024 | | | | | | | | | |
| 179 | PB | 1.00 | | | | | | | | | |
| 180 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 181 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 182 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 183 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 184 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 185 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 186 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 187 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 188 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 189 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 190 | LS | 0 | 68 | 10 | | | | | | | |
| 191 | UD | 0.580 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |
| 192 | KK | BSN2 | | | | | | | | | |
| 193 | KO | 5 | | | | | | | | | |
| 194 | BA | 0.025 | | | | | | | | | |
| 195 | PB | 1.00 | | | | | | | | | |
| 196 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 |
| 197 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 |
| 198 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 |
| 199 | PC | 0.110 | 0.115 | 0.120 | 0.127 | 0.134 | 0.140 | 0.147 | 0.155 | 0.163 | 0.172 |
| 200 | PC | 0.181 | 0.193 | 0.204 | 0.220 | 0.235 | 0.259 | 0.283 | 0.387 | 0.663 | 0.699 |
| 201 | PC | 0.735 | 0.754 | 0.772 | 0.786 | 0.799 | 0.810 | 0.820 | 0.828 | 0.835 | 0.843 |
| 202 | PC | 0.850 | 0.858 | 0.865 | 0.873 | 0.880 | 0.885 | 0.889 | 0.894 | 0.898 | 0.903 |
| 203 | PC | 0.907 | 0.912 | 0.916 | 0.921 | 0.925 | 0.929 | 0.934 | 0.938 | 0.943 | 0.947 |
| 204 | PC | 0.952 | 0.955 | 0.958 | 0.961 | 0.964 | 0.967 | 0.970 | 0.973 | 0.976 | 0.979 |
| 205 | PC | 0.982 | 0.985 | 0.988 | 0.991 | 0.994 | 0.997 | 1.000 | | | |
| 206 | LS | 0 | 68 | 10 | | | | | | | |
| 207 | UD | 0.670 | | | | | | | | | |
| | * | | | | | | | | | | |
| | * | | | | | | | | | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 6

| LINE | ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | |
|------|----|--|------------|--------|--------|--------|--------|--------|--------|--------|--------|--|
| 208 | KK | POND1 | | | | | | | | | | |
| 209 | KO | 5 | | | | | | | | | | |
| 210 | RS | 1 | ELEV 162.0 | | | | | | | | | |
| 211 | SA | 0.36 | 0.43 | 0.49 | 0.57 | | | | | | | |
| 212 | SE | 170.0 | 171.0 | 172.0 | 173.0 | | | | | | | |
| 213 | SQ | 0 | 3.2 | 6.4 | 9.6 | 12.8 | 16.0 | 19.2 | 22.4 | 25.6 | 28.8 | |
| 214 | SQ | 32.0 | | | | | | | | | | |
| 215 | SE | 170.0 | 170.17 | 170.27 | 170.35 | 170.42 | 170.49 | 170.56 | 170.62 | 170.67 | 170.73 | |
| 216 | SE | 170.8 | | | | | | | | | | |
| | * | | | | | | | | | | | |
| | * | | | | | | | | | | | |
| 217 | KK | 3PD1&3 | | | | | | | | | | |
| 218 | KO | 5 | | | | | | | | | | |
| 219 | HC | 3 | 0 | | | | | | | | | |
| | * | | | | | | | | | | | |
| | * | | | | | | | | | | | |
| 220 | KK | POND2 | | | | | | | | | | |
| 221 | KO | 5 | | | | | | | | | | |
| 222 | RS | 1 | ELEV 158.0 | | | | | | | | | |
| 223 | SA | 2.08 | 2.23 | 2.38 | 2.54 | | | | | | | |
| 224 | SE | 166.0 | 167.0 | 168.0 | 169.0 | | | | | | | |
| 225 | SQ | 0 | 26.9 | 53.8 | 80.7 | 107.6 | 134.5 | 161.4 | 188.3 | 215.2 | 242.1 | |
| 226 | SQ | 269.0 | | | | | | | | | | |
| 227 | SE | 166.0 | 166.50 | 166.79 | 167.03 | 167.25 | 167.45 | 167.63 | 167.81 | 167.98 | 168.14 | |
| 228 | SE | 168.3 | | | | | | | | | | |
| | * | | | | | | | | | | | |
| | * | | | | | | | | | | | |
| | * | | | | | | | | | | | |
| 229 | KK | PONDA | | | | | | | | | | |
| 230 | KO | 5 | | | | | | | | | | |
| | * | | | | | | | | | | | |
| | * | ASSUMED OUTLET 10 WEIR AT ELEV. 162.5 | | | | | | | | | | |
| | * | | | | | | | | | | | |
| 231 | RS | 1 | ELEV 162.5 | | | | | | | | | |
| 232 | SA | 1.30 | 1.30 | | | | | | | | | |
| 233 | SE | 162.5 | 170.0 | | | | | | | | | |
| 234 | SQ | 0 | 35 | 70 | 105 | 140 | 175 | 210 | 245 | 280 | 315 | |
| 235 | SQ | 350.0 | | | | | | | | | | |
| 236 | SE | 162.5 | 163.63 | 164.30 | 164.86 | 165.36 | 165.81 | 166.24 | 166.65 | 167.03 | 167.40 | |
| 237 | SE | 167.8 | | | | | | | | | | |
| | * | | | | | | | | | | | |
| | * | 10 ACRES NORTH OF PROPOSED DEVELOPMENT | | | | | | | | | | |
| | * | | | | | | | | | | | |
| 238 | KK | NORTH | | | | | | | | | | |
| 239 | KO | 5 | | | | | | | | | | |
| 240 | BA | 0.0156 | | | | | | | | | | |
| 241 | PB | 1.00 | | | | | | | | | | |
| 242 | PC | 0.000 | 0.003 | 0.006 | 0.008 | 0.011 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 | |
| 243 | PC | 0.029 | 0.032 | 0.035 | 0.038 | 0.042 | 0.045 | 0.048 | 0.052 | 0.056 | 0.060 | |
| 244 | PC | 0.064 | 0.068 | 0.072 | 0.076 | 0.080 | 0.085 | 0.090 | 0.095 | 0.100 | 0.105 | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 8

| | |
|------|---|
| LINE | ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10 |
| 276 | KK PONDB |
| 277 | KO 5 |
| | * * ASSUMED OUTLET 10 WEIR AT ELEV. 159.0 * |
| 278 | RS 1 ELEV 159.0 |
| 279 | SA 5.10 5.10 |
| 280 | SE 159.0 170.0 |
| 281 | SQ 0 35 70 105 140 175 210 245 280 315 |
| 282 | SQ 350.0 |
| 283 | SE 159.0 160.13 160.80 161.36 161.86 162.31 162.74 163.15 163.53 163.90 |
| 284 | SE 164.3 * * * |
| 285 | ZZ |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

SCHEMATIC DIAGRAM OF STREAM NETWORK

| INPUT LINE NO. | (V) ROUTING | (--->) DIVERSION OR PUMP FLOW |
|----------------|---------------|--|
| | (.) CONNECTOR | (<---) RETURN OF DIVERTED OR PUMPED FLOW |
| 8 | BSN5 | |
| | V | |
| | V | |
| 24 | POND7 | |
| | . | |
| 33 | BSN4 | |
| | . | |
| 49 | PD7&4..... | |
| | V | |
| | V | |
| 52 | POND6 | |
| | . | |
| 61 | BSN7 | |
| | . | |
| 77 | 7PD6..... | |
| | V | |
| | V | |
| 80 | POND5 | |
| | . | |
| 89 | BSN6 | |
| | V | |
| | V | |
| 105 | RTE6 | |
| | . | |
| 108 | | OFFST |
| | . | . |
| | . | . |
| 124 | | BSN8 |
| | . | . |
| | . | . |
| 140 | 608P5..... | |
| | V | |
| | V | |
| 143 | POND4 | |
| | . | |
| 150 | BSN10 | |
| | . | |
| 166 | 10PD4..... | |
| | V | |
| | V | |
| 169 | POND3 | |
| | . | |
| 176 | BSN3 | |
| | . | |
| 192 | | BSN2 |
| | . | V |
| | . | V |
| 208 | | POND1 |
| | . | . |
| | . | . |
| 217 | 3PD1&3..... | |
| | V | |
| | V | |
| 220 | POND2 | |
| | V | |
| | V | |
| 229 | PONDA | |
| | . | |
| 238 | | NORTH |
| | . | . |
| 254 | OFFSTE..... | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

257 DEV-1
273 29TH.....
V
V
276 PONDB

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

```
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* FEBRUARY 1981
* REVISED 02 AUG 88
*
* RUN DATE 04/10/2006 TIME 15:29:00
*
*****
```

```
*****
*
* U.S. ARMY CORPS OF ENGINEERS
* THE HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*
*****
```

MODIFIED FONTANA DRAINAGE PLAN (40-AC NEW MARKET OFFICE SPACE TRACT ADDED)
 DEVELOPED CONDITIONS
 BY BLB DATE 03-13-04, MODIFIED BY PDF 4/10/06

```
6 IO OUTPUT CONTROL VARIABLES
    IPRNT 0 PRINT CONTROL
    IPLOT 5 PLOT CONTROL
    QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
    NMIN 15 MINUTES IN COMPUTATION INTERVAL
    IDATE 1JAN 4 STARTING DATE
    ITIME 1200 STARTING TIME
    NQ 129 NUMBER OF HYDROGRAPH ORDINATES
    NDDATE 2JAN 4 ENDING DATE
    NDTIME 2000 ENDING TIME
    ICENT 19 CENTURY MARK

    COMPUTATION INTERVAL .25 HOURS
    TOTAL TIME BASE 32.00 HOURS
```

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

```
JP MULTI-PLAN OPTION
    NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
    RATIOS OF PRECIPITATION
    7.80
```

*** ** ** ** **

```
*****
*
* BSN5
*
*****
```

```
9 KO OUTPUT CONTROL VARIABLES
    IPRINT 5 PRINT CONTROL
    IPLOT 5 PLOT CONTROL
    QSCAL 0. HYDROGRAPH PLOT SCALE
```

*** ** ** **~

```
*****
*
* POND7
*
*****
```

```
25 KO OUTPUT CONTROL VARIABLES
    IPRINT 5 PRINT CONTROL
```

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPLLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** ** **

* *
33 KK * BSN4 *
* *

34 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** ** **

* *
49 KK * PD7&4 *
* *

50 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

* *
52 KK * POND6 *
* *

53 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

* *
61 KK * BSN7 *
* *

62 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

* *
77 KK * 7PD6 *
* *

78 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
80 KK * POND5 *
* *

81 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
89 KK * BSN6 *
* *

90 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
105 KK * RTE6 *
* *

106 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
108 KK * OFFST *
* *

109 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
124 KK * BSN8 *
* *

125 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
80 KK * POND5 *
* *

81 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
89 KK * BSN6 *
* *

90 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
105 KK * RTE6 *
* *

106 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
108 KK * OFFST *
* *

109 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
124 KK * BSN8 *
* *

125 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
140 KK * 608P5 *
* *

141 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
143 KK * POND4 *
* *

144 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
150 KK * BSN10 *
* *

151 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
166 KK * 10PD4 *
* *

167 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
169 KK * POND3 *
* *

170 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** ** **

* *
176 KK * BSN3 *
* *

177 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** ** **

* *
192 KK * BSN2 *
* *

193 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

* *
208 KK * POND1 *
* *

209 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

* *
217 KK * 3PD1&3 *
* *

218 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
I PLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** ** ** **~

* *
220 KK * POND2 *
* *

221 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
229 KK * PONDA *
* *

230 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
238 KK * NORTH *
* *

239 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
254 KK * OFFSTE *
* *

255 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
257 KK * DEV-1 *
* *

258 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
273 KK * 29TH *
* *

274 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPL0T 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

*** **

* *
276 KK * PONDB *
* *

277 KO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPL0T 5 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES TIME TO PEAK IN HOURS

| OPERATION | STATION | AREA | PLAN | RATIOS APPLIED TO PRECIPITATION | |
|---------------|---------|------|---------------------------|---------------------------------|--|
| | | | | RATIO 1 | |
| | | | | 7.80 | |
| HYDROGRAPH AT | | | | | |
| + BSN5 | .02 | 1 | FLOW | 32. | |
| | | | TIME | 12.50 | |
| ROUTED TO | | | | | |
| + POND7 | .02 | 1 | FLOW | 12. | |
| | | | TIME | 13.50 | |
| | | | ** PEAK STAGES IN FEET ** | | |
| | | 1 | STAGE | 171.83 | |
| | | | TIME | 13.50 | |
| HYDROGRAPH AT | | | | | |
| + BSN4 | .02 | 1 | FLOW | 22. | |
| | | | TIME | 12.75 | |
| 2 COMBINED AT | | | | | |
| + PD7&4 | .04 | 1 | FLOW | 31. | |
| | | | TIME | 13.00 | |
| ROUTED TO | | | | | |
| + POND6 | .04 | 1 | FLOW | 10. | |
| | | | TIME | 15.50 | |
| | | | ** PEAK STAGES IN FEET ** | | |
| | | 1 | STAGE | 172.05 | |
| | | | TIME | 15.50 | |
| HYDROGRAPH AT | | | | | |
| + BSN7 | .05 | 1 | FLOW | 61. | |
| | | | TIME | 12.75 | |
| 2 COMBINED AT | | | | | |
| + 7PD6 | .10 | 1 | FLOW | 64. | |
| | | | TIME | 12.75 | |
| ROUTED TO | | | | | |
| + POND5 | .10 | 1 | FLOW | 35. | |
| | | | TIME | 13.75 | |
| | | | ** PEAK STAGES IN FEET ** | | |
| | | 1 | STAGE | 168.73 | |
| | | | TIME | 13.75 | |
| HYDROGRAPH AT | | | | | |
| + BSN6 | .01 | 1 | FLOW | 12. | |
| | | | TIME | 12.50 | |
| ROUTED TO | | | | | |
| + RTE6 | .01 | 1 | FLOW | 12. | |
| | | | TIME | 13.25 | |
| HYDROGRAPH AT | | | | | |
| + OFFST | .36 | 1 | FLOW | 273. | |
| | | | TIME | 13.50 | |
| HYDROGRAPH AT | | | | | |
| + BSN8 | .03 | 1 | FLOW | 40. | |
| | | | TIME | 12.25 | |
| 4 COMBINED AT | | | | | |
| + 608P5 | .49 | 1 | FLOW | 326. | |
| | | | TIME | 13.50 | |
| ROUTED TO | | | | | |
| + POND4 | .49 | 1 | FLOW | 232. | |
| | | | TIME | 14.50 | |
| | | | ** PEAK STAGES IN FEET ** | | |

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

1 STAGE 168.71
TIME 14.50

HYDROGRAPH AT
+ BSN10 .02 1 FLOW 27.
TIME 12.50

2 COMBINED AT
+ 10PDA .51 1 FLOW 236.
TIME 14.50

ROUTED TO
+ POND3 .51 1 FLOW 224.
TIME 15.50

** PEAK STAGES IN FEET **
1 STAGE 168.52
TIME 15.50

HYDROGRAPH AT
+ BSN3 .02 1 FLOW 33.
TIME 12.50

HYDROGRAPH AT
+ BSN2 .03 1 FLOW 32.
TIME 12.50

ROUTED TO
+ POND1 .03 1 FLOW 31.
TIME 12.75

** PEAK STAGES IN FEET **
1 STAGE 170.78
TIME 12.75

3 COMBINED AT
+ 3PD1&3 .56 1 FLOW 270.
TIME 12.50

ROUTED TO
+ POND2 .56 1 FLOW 267.
TIME 12.75

** PEAK STAGES IN FEET **
1 STAGE 168.29
TIME 12.75

ROUTED TO
+ PONDA .56 1 FLOW 264.
TIME 13.00

** PEAK STAGES IN FEET **
1 STAGE 166.86
TIME 13.00

HYDROGRAPH AT
+ NORTH .02 1 FLOW 27.
TIME 12.25

2 COMBINED AT
+ OFFSTE .58 1 FLOW 274.
TIME 13.00

HYDROGRAPH AT
+ DEV-1 .06 1 FLOW 184.
TIME 12.00

2 COMBINED AT
+ 29TH .64 1 FLOW 411.
TIME 12.00

ROUTED TO
+ PONDB .64 1 FLOW 321.
TIME 12.50

** PEAK STAGES IN FEET **
1 STAGE 163.97
TIME 12.50

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

*** NORMAL END OF HEC-1 ***

KS-2-5

| County | Expected 24-hour Storm Rainfall in Inches | | | | | | Normal Annual Precipitation Inches |
|--------------|---|-----|-----|-----|-----|-----|------------------------------------|
| | Storm Frequency in Years | | | | | | |
| | 100 | 50 | 25 | 10 | 5 | 2 | |
| Pawnee | 6.6 | 6.0 | 5.2 | 4.5 | 3.7 | 2.8 | 23.3 |
| Phillips | 6.0 | 5.5 | 4.8 | 4.1 | 3.4 | 2.5 | 23.6 |
| Pottawatomie | 7.5 | 6.6 | 5.9 | 5.1 | 4.3 | 3.4 | 33.6 |
| Pratt | 7.2 | 6.4 | 5.6 | 4.8 | 4.1 | 3.0 | 24.6 |
| Rawlins | 5.5 | 5.0 | 4.3 | 3.6 | 3.1 | 2.3 | 21.0 |
| Reno | 7.4 | 6.6 | 5.8 | 5.0 | 4.2 | 3.2 | 27.7 |
| Republic | 6.8 | 6.0 | 5.4 | 4.6 | 3.9 | 2.9 | 28.6 |
| Rice | 7.3 | 6.4 | 5.6 | 4.8 | 4.1 | 3.0 | 26.6 |
| Riley | 7.4 | 6.5 | 5.8 | 5.1 | 4.3 | 3.3 | 33.5 |
| Rooks | 6.1 | 5.7 | 4.9 | 4.1 | 3.4 | 2.5 | 23.9 |
| Rush | 6.5 | 5.9 | 5.0 | 4.3 | 3.6 | 2.7 | 23.3 |
| Russell | 6.7 | 5.9 | 5.2 | 4.4 | 3.7 | 2.8 | 26.8 |
| Saline | 7.3 | 6.4 | 5.7 | 4.9 | 4.1 | 3.1 | 28.4 |
| Scott | 5.7 | 5.3 | 4.5 | 3.8 | 3.2 | 2.4 | 20.2 |
| Sedgwick | 7.8 | 7.0 | 6.1 | 5.3 | 4.5 | 3.5 | 30.6 |
| Seward | 6.0 | 5.7 | 4.8 | 4.2 | 3.5 | 2.6 | 19.8 |
| Shawnee | 7.8 | 6.8 | 6.1 | 5.3 | 4.5 | 3.5 | 34.7 |
| Sheridan | 5.7 | 5.3 | 4.5 | 3.8 | 3.2 | 2.4 | 21.3 |
| Sherman | 5.3 | 4.8 | 4.2 | 3.5 | 3.0 | 2.2 | 16.7 |
| Smith | 6.3 | 5.7 | 5.0 | 4.2 | 3.5 | 2.6 | 24.4 |
| Stafford | 7.1 | 6.2 | 5.5 | 4.7 | 4.0 | 2.9 | 25.1 |
| Stanton | 5.6 | 5.2 | 4.5 | 3.8 | 3.2 | 2.4 | 15.8 |
| Stevens | 5.9 | 5.5 | 4.7 | 4.1 | 3.4 | 2.5 | 19.7 |
| Sumner | 8.0 | 7.1 | 6.2 | 5.4 | 4.6 | 3.6 | 34.0 |

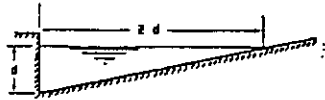
$x\text{-slope} = \frac{3}{8} \sqrt{1} = 0.03125\%$

$z = \frac{1}{x\text{-slope}} = \frac{1}{0.03125} = 32$

$n = 0.016$

$\frac{z}{n} = \frac{32}{0.016} = 2000$

always



EQUATION: $Q = 0.56 \left(\frac{z}{n}\right) S^{1/2} d^{2.48}$

n IS ROUGHNESS COEFFICIENT IN MANNING'S

FORMULA APPROPRIATE TO MATERIAL IN

BOTTOM OF CHANNEL

z IS RECIPROCAL OF CROSS SLOPE

REFERENCE: H. R. B. PROCEEDINGS 1948,

PAGE 150, EQUATION (14)

EXAMPLE (SEE INSTRUCTION 1)

GIVEN: $S = 0.03$

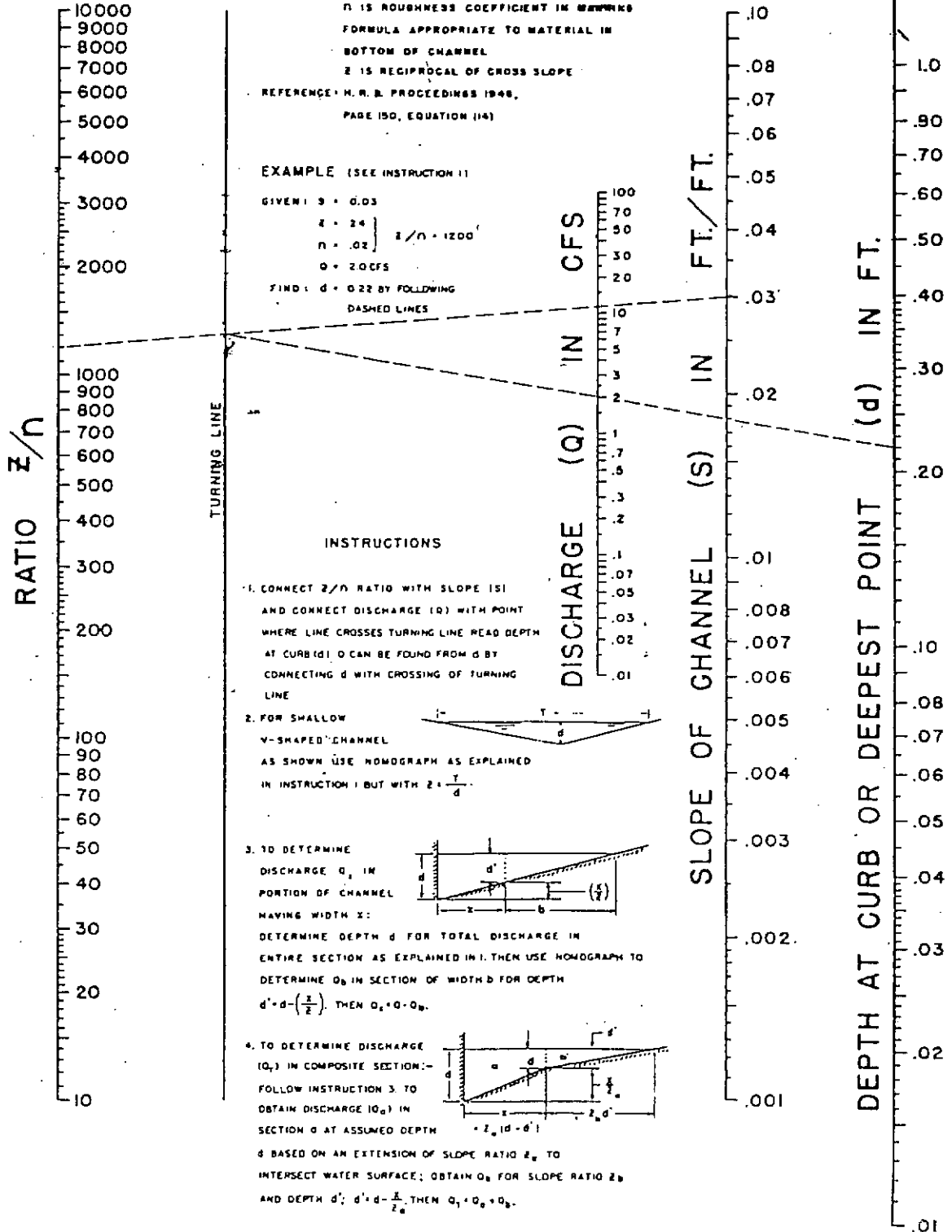
$z = 24$

$n = .02$

$Q = 20 \text{ CFS}$

$z/n = 1200$

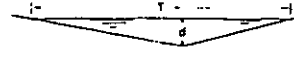
FIND: $d = 0.22$ BY FOLLOWING
DASHED LINES



INSTRUCTIONS

1. CONNECT z/n RATIO WITH SLOPE (S) AND CONNECT DISCHARGE (Q) WITH POINT WHERE LINE CROSSES TURNING LINE READ DEPTH AT CURB (d). d CAN BE FOUND FROM d BY CONNECTING d WITH CROSSING OF TURNING LINE

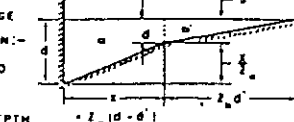
2. FOR SHALLOW V-SHAPED CHANNEL AS SHOWN USE NOMOGRAPH AS EXPLAINED IN INSTRUCTION 1 BUT WITH $z = \frac{1}{d}$



3. TO DETERMINE DISCHARGE Q_1 IN PORTION OF CHANNEL HAVING WIDTH z : DETERMINE DEPTH d FOR TOTAL DISCHARGE IN ENTIRE SECTION AS EXPLAINED IN 1. THEN USE NOMOGRAPH TO DETERMINE Q_2 IN SECTION OF WIDTH b FOR DEPTH $d' = d - \left(\frac{z}{2}\right)$. THEN $Q_1 = Q - Q_2$



4. TO DETERMINE DISCHARGE (Q_1) IN COMPOSITE SECTION: FOLLOW INSTRUCTION 3. TO OBTAIN DISCHARGE (Q_2) IN SECTION b AT ASSUMED DEPTH d BASED ON AN EXTENSION OF SLOPE RATIO z_2 TO INTERSECT WATER SURFACE; OBTAIN Q_3 FOR SLOPE RATIO z_1 AND DEPTH d' : $d' = d - \frac{z_1}{z_2}$. THEN $Q_1 = Q_2 + Q_3$



- ATTACHMENT A
DRAINAGE CRITERIA MANUAL

RAINFALL INTENSITY TABLE FOR SEDGWICK COUNTY, KANSAS

The following tabulation contains rainfall intensity in inches per hour as derived from ESSA Weather Bureau Technical Paper 40 Modified to NWS Hydro-35, 1977 During First Hour

| $(\frac{1}{T_c})$ DURATION IN MINUTES | RETURN PERIODS OF | | | | | | |
|---|-------------------|------|------|-------|-------|-------|--------|
| | 1-YR | 2-YR | 5-YR | 10-YR | 25-YR | 50-YR | 100-YR |
| 5 | $i = 4.18$ | 5.57 | 6.53 | 7.41 | 8.52 | 9.48 | 10.32 |
| 6 | 3.99 | 5.32 | 6.25 | 7.09 | 8.16 | 9.09 | 9.89 |
| 7 | 3.81 | 5.09 | 5.99 | 6.81 | 7.84 | 8.74 | 9.50 |
| 8 | 3.66 | 4.89 | 5.75 | 6.55 | 7.55 | 8.42 | 9.15 |
| 9 | 3.52 | 4.70 | 5.54 | 6.31 | 7.28 | 8.13 | 8.83 |
| 10 | 3.39 | 4.52 | 5.34 | 6.09 | 7.04 | 7.86 | 8.54 |
| 11 | 3.27 | 4.36 | 5.16 | 5.89 | 6.81 | 7.61 | 8.27 |
| 12 | 3.18 | 4.21 | 4.99 | 5.71 | 6.60 | 7.38 | 8.02 |
| 13 | 3.05 | 4.08 | 4.84 | 5.53 | 6.41 | 7.17 | 7.79 |
| 14 | 2.96 | 3.95 | 4.69 | 5.37 | 6.23 | 6.97 | 7.57 |
| 15 | 2.87 | 3.83 | 4.56 | 5.22 | 6.06 | 6.78 | 7.37 |
| 16 | 2.78 | 3.72 | 4.43 | 5.08 | 5.90 | 6.60 | 7.18 |
| 17 | 2.71 | 3.61 | 4.31 | 4.95 | 5.75 | 6.44 | 7.00 |
| 18 | 2.63 | 3.51 | 4.20 | 4.83 | 5.61 | 6.29 | 6.84 |
| 19 | 2.56 | 3.42 | 4.10 | 4.71 | 5.47 | 6.14 | 6.68 |
| 20 | 2.50 | 3.33 | 4.00 | 4.60 | 5.35 | 6.00 | 6.53 |
| 21 | 2.44 | 3.25 | 3.90 | 4.50 | 5.23 | 5.87 | 6.39 |
| 22 | 2.38 | 3.17 | 3.81 | 4.40 | 5.12 | 5.75 | 6.26 |
| 23 | 2.32 | 3.10 | 3.73 | 4.31 | 5.01 | 5.63 | 6.13 |
| 24 | 2.27 | 3.03 | 3.65 | 4.22 | 4.91 | 5.52 | 6.01 |
| 25 | 2.22 | 2.96 | 3.57 | 4.13 | 4.81 | 5.41 | 5.90 |
| 26 | 2.20 | 2.90 | 3.50 | 4.05 | 4.72 | 5.31 | 5.79 |
| 27 | 2.16 | 2.84 | 3.43 | 3.98 | 4.63 | 5.21 | 5.69 |
| 28 | 2.14 | 2.78 | 3.37 | 3.90 | 4.55 | 5.12 | 5.59 |
| 29 | 2.11 | 2.72 | 3.30 | 3.83 | 4.47 | 5.03 | 5.49 |
| 30 | 2.08 | 2.67 | 3.24 | 3.76 | 4.39 | 4.94 | 5.40 |
| 31 | 2.05 | 2.62 | 3.19 | 3.70 | 4.32 | 4.86 | 5.32 |
| 32 | 2.02 | 2.57 | 3.10 | 3.63 | 4.25 | 4.79 | 5.22 |
| 33 | 1.99 | 2.52 | 3.05 | 3.57 | 4.18 | 4.71 | 5.14 |
| 34 | 1.96 | 2.48 | 3.01 | 3.51 | 4.11 | 4.63 | 5.07 |
| 35 | 1.93 | 2.44 | 2.98 | 3.46 | 4.05 | 4.56 | 5.00 |
| 36 | 1.91 | 2.39 | 2.93 | 3.41 | 3.99 | 4.50 | 4.93 |
| 37 | 1.89 | 2.35 | 2.88 | 3.36 | 3.93 | 4.43 | 4.86 |
| 38 | 1.87 | 2.32 | 2.84 | 3.31 | 3.87 | 4.37 | 4.79 |
| 39 | 1.85 | 2.28 | 2.80 | 3.26 | 3.82 | 4.31 | 4.73 |
| 40 | 1.83 | 2.24 | 2.76 | 3.22 | 3.76 | 4.25 | 4.66 |
| 41 | 1.81 | 2.21 | 2.72 | 3.17 | 3.71 | 4.19 | 4.60 |
| 42 | 1.79 | 2.18 | 2.68 | 3.13 | 3.66 | 4.13 | 4.54 |
| 43 | 1.77 | 2.14 | 2.64 | 3.09 | 3.61 | 4.08 | 4.49 |
| 44 | 1.75 | 2.11 | 2.61 | 3.05 | 3.57 | 4.03 | 4.43 |
| 45 | 1.73 | 2.08 | 2.57 | 3.01 | 3.52 | 3.98 | 4.38 |

| <u>DURATION IN MINUTES</u> | <u>RETURN PERIODS OF</u> | | | | | | |
|--------------------------------|--------------------------|-------------|--------------|--------------|--------------|--------------|---------------|
| | <u>1-YR</u> | <u>2-YR</u> | <u>.5-YR</u> | <u>10-YR</u> | <u>25-YR</u> | <u>50-YR</u> | <u>100-YR</u> |
| 46 | 1.70 | 2.05 | 2.54 | 2.97 | 3.48 | 3.93 | 4.33 |
| 47 | 1.67 | 2.02 | 2.50 | 2.93 | 3.44 | 3.88 | 4.28 |
| 48 | 1.66 | 2.00 | 2.47 | 2.90 | 3.39 | 3.84 | 4.23 |
| 49 | 1.64 | 1.97 | 2.44 | 2.86 | 3.35 | 3.79 | 4.18 |
| 50 | 1.61 | 1.95 | 2.41 | 2.83 | 3.32 | 3.75 | 4.13 |
| 51 | 1.59 | 1.92 | 2.38 | 2.79 | 3.28 | 3.71 | 4.09 |
| 52 | 1.56 | 1.89 | 2.35 | 2.76 | 3.24 | 3.67 | 4.05 |
| 53 | 1.54 | 1.86 | 2.33 | 2.73 | 3.20 | 3.63 | 4.00 |
| 54 | 1.52 | 1.84 | 2.30 | 2.70 | 3.17 | 3.59 | 3.96 |
| 55 | 1.50 | 1.81 | 2.27 | 2.67 | 3.14 | 3.55 | 3.92 |
| 56 | 1.47 | 1.79 | 2.25 | 2.64 | 3.10 | 3.51 | 3.88 |
| 57 | 1.45 | 1.76 | 2.22 | 2.61 | 3.07 | 3.48 | 3.84 |
| 58 | 1.43 | 1.74 | 2.20 | 2.59 | 3.04 | 3.44 | 3.81 |
| 59 | 1.42 | 1.72 | 2.18 | 2.56 | 3.01 | 3.41 | 3.77 |
| 60 | 1.40 | 1.69 | 2.15 | 2.53 | 2.98 | 3.37 | 3.73 |
| 61 | 1.38 | 1.67 | 2.13 | 2.51 | 2.95 | 3.34 | 3.70 |
| 62 | 1.36 | 1.65 | 2.11 | 2.48 | 2.92 | 3.31 | 3.67 |
| 63 | 1.34 | 1.63 | 2.09 | 2.46 | 2.89 | 3.28 | 3.63 |
| 64 | 1.33 | 1.61 | 2.07 | 2.44 | 2.86 | 3.25 | 3.60 |
| 65 | 1.31 | 1.59 | 2.05 | 2.41 | 2.84 | 3.22 | 3.57 |
| 66 | 1.30 | 1.57 | 2.03 | 2.39 | 2.81 | 3.19 | 3.54 |
| 67 | 1.28 | 1.56 | 2.01 | 2.37 | 2.79 | 3.16 | 3.51 |
| 68 | 1.26 | 1.54 | 1.99 | 2.35 | 2.76 | 3.13 | 3.48 |
| 69 | 1.25 | 1.52 | 1.97 | 2.33 | 2.74 | 3.10 | 3.45 |
| 70 | 1.24 | 1.50 | 1.95 | 2.31 | 2.71 | 3.08 | 3.42 |
| 71 | 1.22 | 1.49 | 1.93 | 2.28 | 2.69 | 3.05 | 3.39 |
| 72 | 1.21 | 1.47 | 1.92 | 2.26 | 2.67 | 3.02 | 3.36 |
| 73 | 1.20 | 1.46 | 1.90 | 2.25 | 2.64 | 3.00 | 3.34 |
| 74 | 1.18 | 1.44 | 1.88 | 2.23 | 2.63 | 2.98 | 3.31 |
| 75 | 1.17 | 1.43 | 1.86 | 2.21 | 2.61 | 2.95 | 3.29 |
| 76 | 1.16 | 1.41 | 1.85 | 2.19 | 2.58 | 2.93 | 3.26 |
| 77 | 1.15 | 1.40 | 1.83 | 2.17 | 2.55 | 2.90 | 3.24 |
| 78 | 1.13 | 1.38 | 1.82 | 2.15 | 2.53 | 2.88 | 3.22 |
| 79 | 1.12 | 1.37 | 1.80 | 2.14 | 2.50 | 2.86 | 3.19 |
| 80 | 1.11 | 1.36 | 1.79 | 2.12 | 2.48 | 2.84 | 3.16 |
| 81 | 1.10 | 1.34 | 1.77 | 2.10 | 2.46 | 2.82 | 3.13 |
| 82 | 1.09 | 1.33 | 1.76 | 2.08 | 2.43 | 2.79 | 3.10 |
| 83 | 1.08 | 1.32 | 1.74 | 2.06 | 2.41 | 2.76 | 3.07 |
| 84 | 1.07 | 1.31 | 1.73 | 2.04 | 2.39 | 2.74 | 3.04 |
| 85 | 1.06 | 1.30 | 1.72 | 2.02 | 2.37 | 2.71 | 3.01 |
| 86 | 1.05 | 1.28 | 1.70 | 2.00 | 2.34 | 2.69 | 2.99 |
| 87 | 1.04 | 1.27 | 1.69 | 1.99 | 2.32 | 2.66 | 2.96 |
| 88 | 1.03 | 1.26 | 1.68 | 1.97 | 2.30 | 2.64 | 2.93 |
| 89 | 1.02 | 1.25 | 1.68 | 1.95 | 2.28 | 2.62 | 2.91 |
| 90 | 1.01 | 1.24 | 1.66 | 1.93 | 2.26 | 2.59 | 2.88 |

ATTACHMENT A CONTINUED
Page 3

| <u>DURATION IN MINUTES</u> | <u>RETURN PERIODS OF</u> | | | | | | |
|--------------------------------|--------------------------|-------------|-------------|--------------|--------------|--------------|---------------|
| | <u>1-YR</u> | <u>2-YR</u> | <u>5-YR</u> | <u>10-YR</u> | <u>25-YR</u> | <u>50-YR</u> | <u>100-YR</u> |
| 91 | 1.00 | 1.23 | 1.65 | 1.92 | 2.24 | 2.57 | 2.86 |
| 92 | 1.00 | 1.22 | 1.63 | 1.90 | 2.22 | 2.55 | 2.83 |
| 93 | 0.99 | 1.21 | 1.62 | 1.89 | 2.20 | 2.53 | 2.81 |
| 94 | 0.98 | 1.20 | 1.61 | 1.87 | 2.19 | 2.51 | 2.79 |
| 95 | 0.97 | 1.19 | 1.59 | 1.85 | 2.17 | 2.49 | 2.76 |
| 96 | 0.96 | 1.18 | 1.58 | 1.84 | 2.15 | 2.46 | 2.74 |
| 97 | 0.96 | 1.17 | 1.57 | 1.82 | 2.13 | 2.44 | 2.72 |
| 98 | 0.95 | 1.16 | 1.56 | 1.81 | 2.12 | 2.42 | 2.70 |
| 99 | 0.94 | 1.15 | 1.54 | 1.80 | 2.10 | 2.41 | 2.67 |
| 100 | 0.93 | 1.14 | 1.53 | 1.78 | 2.08 | 2.39 | 2.65 |
| 101 | 0.93 | 1.13 | 1.52 | 1.77 | 2.07 | 2.39 | 2.65 |
| 102 | 0.92 | 1.13 | 1.51 | 1.75 | 2.05 | 2.35 | 2.61 |
| 103 | 0.91 | 1.12 | 1.50 | 1.74 | 2.04 | 2.33 | 2.59 |
| 104 | 0.90 | 1.11 | 1.49 | 1.73 | 2.02 | 2.31 | 2.57 |
| 105 | 0.90 | 1.10 | 1.47 | 1.72 | 2.01 | 2.30 | 2.55 |
| 106 | 0.89 | 1.09 | 1.46 | 1.70 | 1.99 | 2.28 | 2.54 |
| 107 | 0.88 | 1.09 | 1.45 | 1.69 | 1.98 | 2.26 | 2.52 |
| 108 | 0.88 | 1.08 | 1.44 | 1.68 | 1.96 | 2.25 | 2.50 |
| 109 | 0.87 | 1.07 | 1.43 | 1.67 | 1.95 | 2.23 | 2.48 |
| 110 | 0.87 | 1.06 | 1.42 | 1.65 | 1.93 | 2.21 | 2.46 |
| 111 | 0.86 | 1.06 | 1.41 | 1.64 | 1.92 | 2.20 | 2.45 |
| 112 | 0.85 | 1.05 | 1.40 | 1.63 | 1.91 | 2.18 | 2.43 |
| 113 | 0.85 | 1.04 | 1.39 | 1.62 | 1.89 | 2.17 | 2.41 |
| 114 | 0.84 | 1.03 | 1.38 | 1.61 | 1.88 | 2.15 | 2.40 |
| 115 | 0.84 | 1.03 | 1.37 | 1.60 | 1.87 | 2.14 | 2.38 |
| 116 | 0.83 | 1.02 | 1.36 | 1.59 | 1.86 | 2.12 | 2.36 |
| 117 | 0.82 | 1.01 | 1.36 | 1.58 | 1.84 | 2.11 | 2.35 |
| 118 | 0.82 | 1.01 | 1.35 | 1.57 | 1.83 | 2.09 | 2.33 |
| 119 | 0.81 | 1.00 | 1.34 | 1.56 | 1.82 | 2.08 | 2.32 |
| 120 | 0.81 | 0.99 | 1.33 | 1.55 | 1.81 | 2.07 | 2.30 |

| <u>DURATION IN HOURS</u> | <u>RETURN PERIODS OF</u> | | | | | | |
|------------------------------|--------------------------|-------------|-------------|--------------|--------------|--------------|---------------|
| | <u>1-YR</u> | <u>2-YR</u> | <u>5-YR</u> | <u>10-YR</u> | <u>25-YR</u> | <u>50-YR</u> | <u>100-YR</u> |
| 2 | 0.81 | 0.99 | 1.33 | 1.55 | 1.81 | 2.07 | 2.30 |
| 3 | 0.59 | 0.72 | 0.97 | 1.13 | 1.32 | 1.51 | 1.68 |
| 4 | 0.47 | 0.58 | 0.78 | 0.91 | 1.06 | 1.21 | 1.35 |
| 5 | 0.40 | 0.49 | 0.66 | 0.77 | 0.89 | 1.02 | 1.14 |
| 6 | 0.35 | 0.42 | 0.57 | 0.67 | 0.78 | 0.89 | 0.99 |
| 8 | 0.28 | 0.34 | 0.46 | 0.53 | 0.62 | 0.71 | 0.79 |
| 10 | 0.23 | 0.29 | 0.39 | 0.45 | 0.52 | 0.60 | 0.67 |
| 12 | 0.20 | 0.25 | 0.33 | 0.39 | 0.45 | 0.52 | 0.58 |
| 18 | 0.15 | 0.18 | 0.24 | 0.28 | 0.33 | 0.38 | 0.42 |
| 24 | 0.12 | 0.15 | 0.20 | 0.23 | 0.27 | 0.31 | 0.34 |

ATTACHMENT B
DRAINAGE CRITERIA MANUAL

INCREMENTAL INFILTRATION VALUES IN INCHES

| Time Minutes** | SCS Hydrologic Soil Group | | | |
|-------------------|---------------------------|-----|-----|-----|
| | A | B | C | D |
| 5 | .33 | .26 | .19 | .12 |
| 10 | .25 | .17 | .09 | .04 |
| 15 | .18 | .11 | .05 | .02 |
| 20 | .13 | .07 | .03 | .02 |
| 25 | .10 | .05 | .03 | .02 |
| 30 | .08 | .05 | .03 | .02 |
| 35 | .08 | .05 | .03 | .02 |
| 40 | .08 | .05 | .03 | .02 |
| 45 | .08 | .05 | .03 | .02 |
| 50 | .08 | .05 | .03 | .02 |
| 55 | .08 | .05 | .03 | .02 |
| 60 | .08 | .05 | .03 | .02 |
| 65 | .08 | .05 | .03 | .02 |
| 70 | .08 | .05 | .03 | .02 |
| 75 | .08 | .05 | .03 | .02 |
| 80 | .08 | .05 | .03 | .02 |
| 85 | .08 | .05 | .03 | .02 |
| 90 | .08 | .05 | .03 | .02 |
| 95 | .08 | .05 | .03 | .02 |
| 100 | .08 | .05 | .03 | .02 |
| 105 | .08 | .05 | .03 | .02 |
| 110 | .08 | .05 | .03 | .02 |
| 115 | .08 | .05 | .03 | .02 |
| 120 | .08 | .05 | .03 | .02 |

**Time at end of the time increment

NOTE: Values for 125 minutes and additional 5 minute increments shall be the same as those shown for 120 minutes.

ATTACHMENT C

DRAINAGE CRITERIA MANUAL

DEPRESSION STORAGE LOSSES

| <u>Surface Type</u> | <u>Total Loss (Inches)</u> |
|------------------------------|--------------------------------|
| Impervious: | |
| Paved Areas | 0.1 |
| Flat Roofs | 0.1 |
| Sloped Roofs | 0.05 |
| Pervious: | |
| Lawns and Grass | 0.3 |
| Wooded Areas and Open Fields | 0.4 |

ATTACHMENT F

DETERMINATION OF DIMENSIONLESS
WATERSHED CONVEYANCE FACTOR (\emptyset)

$$\emptyset = \emptyset_1 + \emptyset_2$$

| \emptyset_1 | Classification |
|---------------|---|
| 0.6 | Extensive channel improvement and storm sewer system, closed conduit channel system |
| 0.7 | Moderate channel improvement and storm sewer system. |
| 0.8 | Some channel improvement and storm sewers, mainly cleaning and enlargement of existing channel. |
| 0.9 | Little channel improvement and storm sewers. |
| 1.0 | Natural channel conditions. |
| | |
| \emptyset_2 | Classification |
| 0.0 | No channel vegetation. |
| 0.1 | Light channel vegetation. |
| 0.2 | Moderate channel vegetation. |
| 0.3 | Heavy channel vegetation. |

EXHIBIT NO. 1

SOIL LEGEND

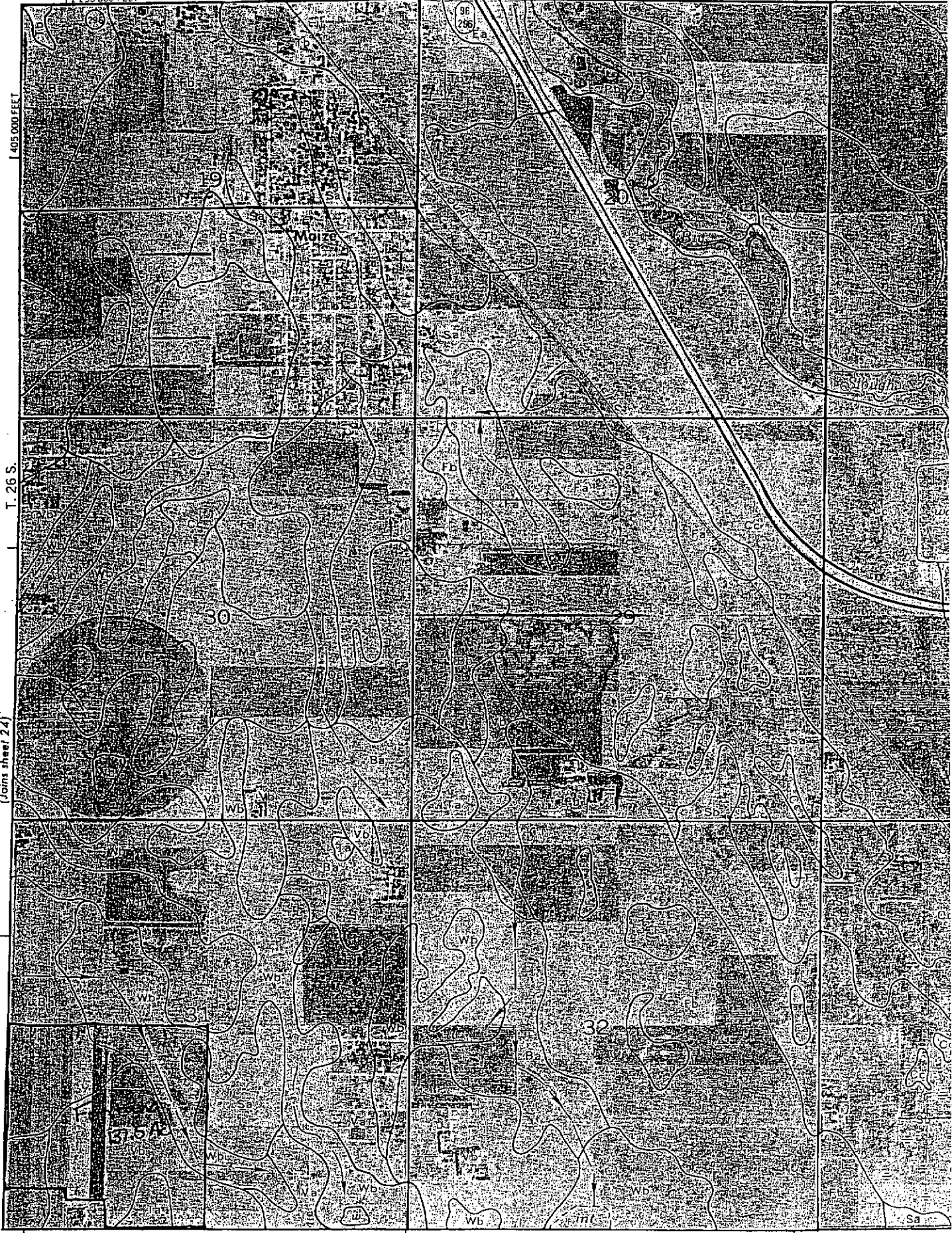
| <u>SYMBOL</u> | <u>HYDROLOGIC GROUP</u> | <u>NAME</u> |
|---------------|-------------------------|---|
| Aa | B | Albion-Shellabarger sandy loams, 1 to 4 percent slopes |
| Ab | B | Albion and Shellabarger sandy loams, 7 to 15 percent slopes |
| Ba | C | Blanket silt loam, 0 to 1 percent slopes |
| Bb | C | Blanket silt loam, 1 to 3 percent slopes |
| Ca | B | Canadian fine sandy loam |
| Cb | B | Canadian-Waldeck fine sandy loams |
| Cc | D | Carwile fine sandy loam |
| Cd | B | Clark-Ost clay loams, 1 to 4 percent slopes |
| Ce | C | Clime silty clay, 3 to 6 percent slopes |
| Ea | B | Elandco silt loam |
| Eb | B | Elandco silt loam, occasionally flooded |
| Ec | B | Elandco silt loam, frequently flooded |
| Fa | B | Farnum loam, 0 to 1 percent slopes |
| Fb | B | Farnum loam, 1 to 3 percent slopes |
| Fc | B | Farnum loam, sandy substratum, 0 to 1 percent slopes |
| Ga | D | Goessel silty clay, 0 to 1 percent slopes |
| Gb | D | Goessel silty clay, 1 to 2 percent slopes |
| Ia | D | Irwin silty clay loam, 1 to 3 percent slopes |
| Ib | D | Irwin silty clay loam, 3 to 6 percent slopes |
| Ic | D | Irwin silty clay loam, 2 to 6 percent slopes, eroded |
| La | C | Lesho loam |
| Lb | A | Lincoln soils |
| Ma | B | Milan loam, 1 to 3 percent slopes |
| Mb | B | Milan form, 3 to 6 percent slopes |
| Mc | B | Milan clay loam, 2 to 6 percent slopes, eroded |
| Na | B | Naron fine sandy loam |
| Oc | D | Owens clay loam, 1 to 3 percent slopes |
| Od | D | Owens-Rock outcrop complex, 3 to 10 percent slopes |
| Pa | | Pits |
| Pb | D | Plevna fine sandy loam |
| Pc | A | Pratt loamy fine sand, undulating |
| Pd | A | Pratt-Tivoli complex, rolling |
| Ra | D | Renfrow silty clay loam, 1 to 3 percent slopes |
| Rb | D | Renfrow silty clay loam, 3 to 6 percent slopes |
| Rc | D | Renfrow-Owens clay loams, 1 to 4 percent slopes |
| Rd | D | Rosehill silty clay, 1 to 3 percent slopes |
| Sa | B | Shellabarger sandy loam, 1 to 3 percent slopes |
| Sb | B | Shellabarger sandy loam, 3 to 6 percent slopes |
| Sc | B | Shellabarger sandy loam, 3 to 6 percent slopes, eroded |
| Ta | D | Tabler silty clay loam |
| Tb | D | Tabler-Drummond complex |
| Ua | B | Urban land-Canadian complex |
| Ub | B | Urban land-Elandco complex |
| Uc | B | Urban land-Farnum complex, 0 to 3 percent slopes |
| Ud | D | Urban land-Irwin complex, 1 to 3 percent slopes |
| Ue | D | Urban land-Tabler complex |
| Va | B | Vanoss silt loam, 0 to 1 percent slopes |
| Vb | B | Vanoss silt loam, 1 to 3 percent slopes |
| Vc | B | Vanoss silt loam, 3 to 6 percent slopes |
| Vd | B | Vanoss silt loam, 3 to 6 percent slopes, eroded |
| Ve | D | Vernon sandy loam, 1 to 3 percent slopes |
| Vf | D | Vernon sandy loam, 3 to 6 percent slopes |
| Wa | C | Waldeck sandy loam |
| Wb | D | Waurika silt loam |

2295 000 FEET

405 000 FEET

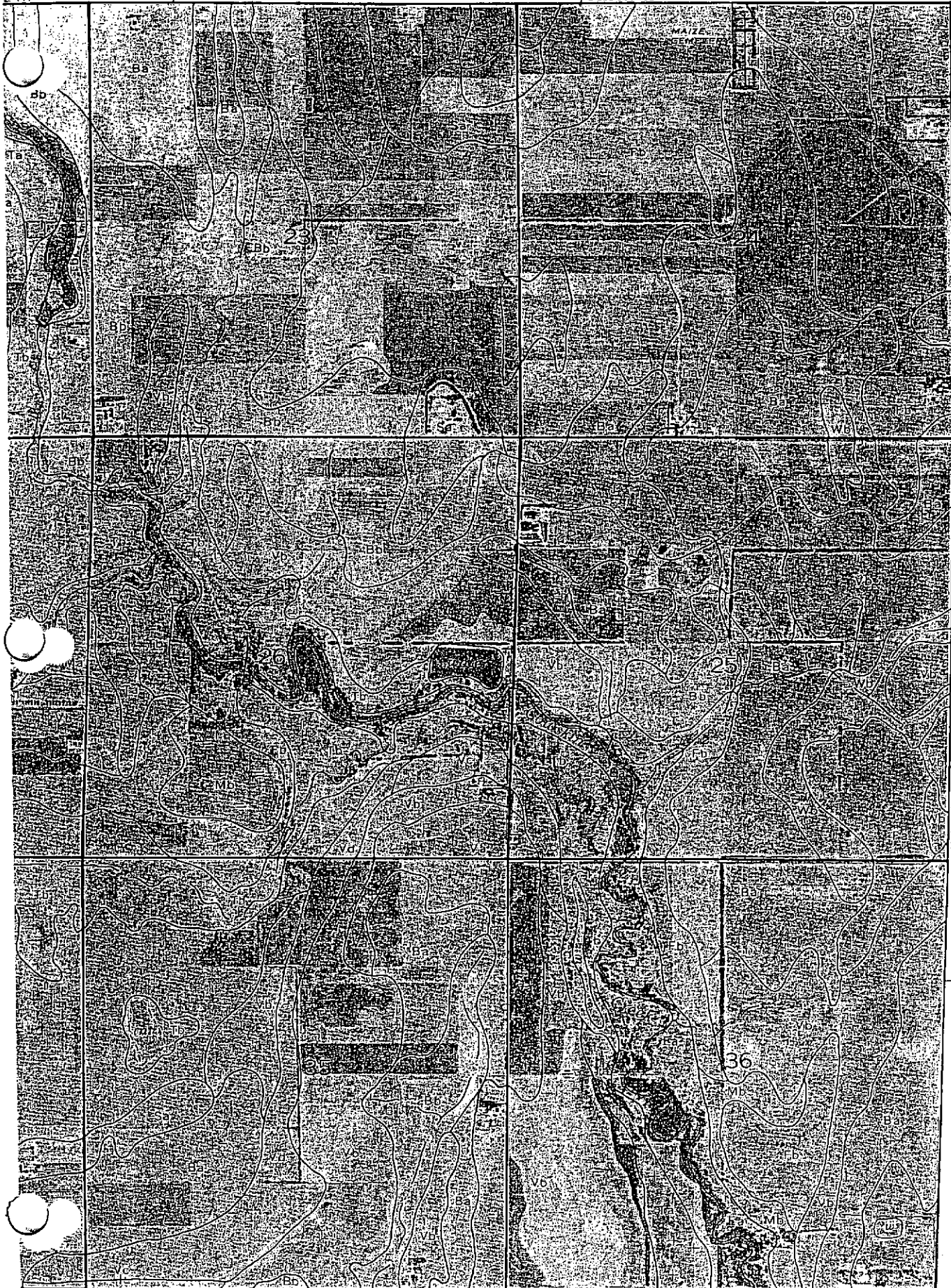
T. 26 S.

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2 W.

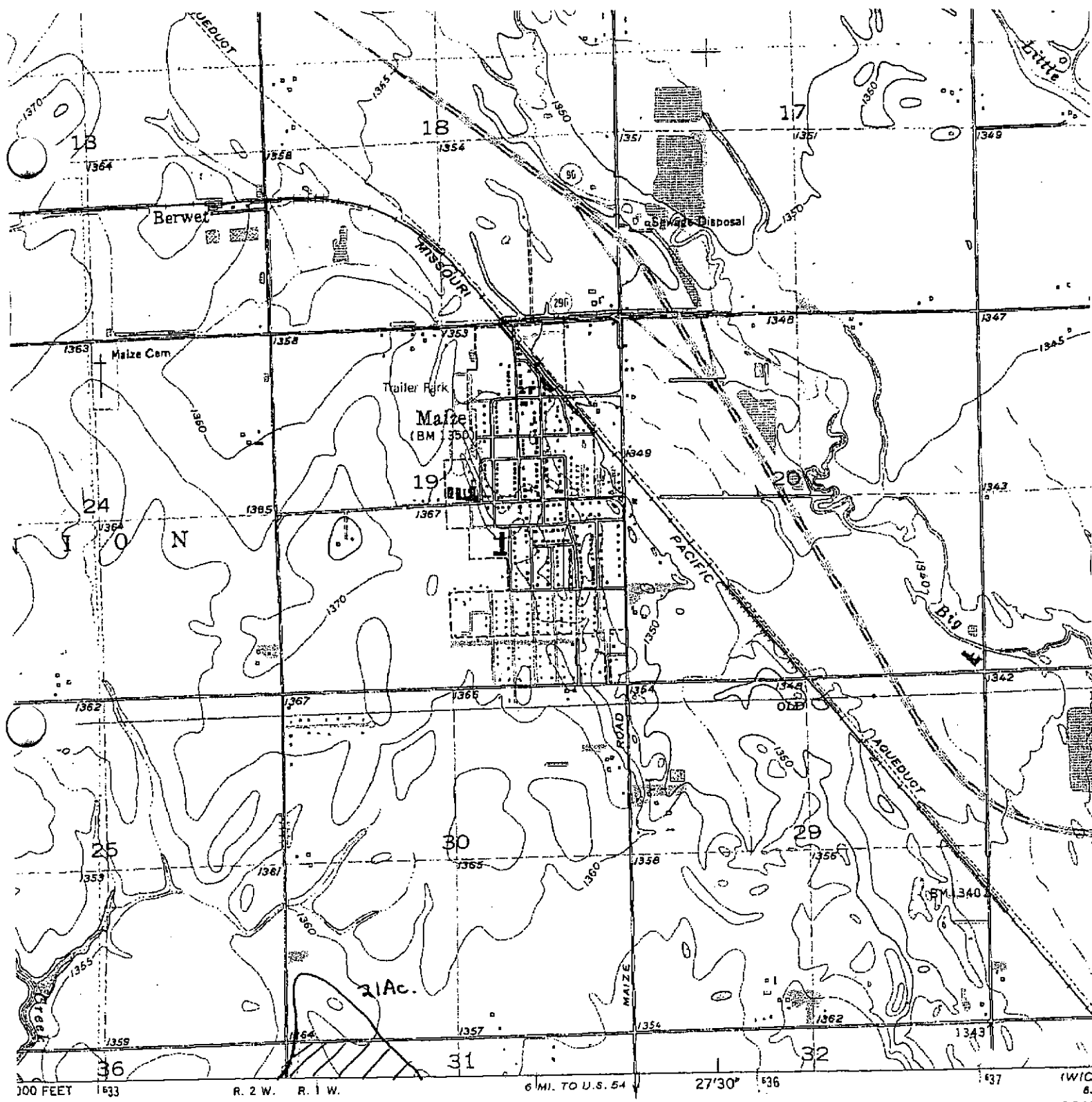
2 290 000 FEET



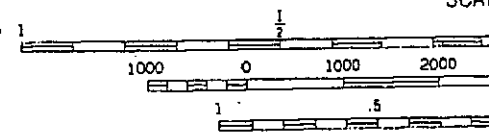
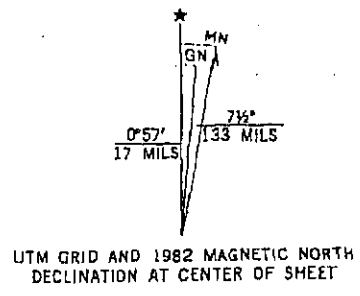
405 000 FEET

T. 26 S.

(Joins sheet 25)



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 in with State of Kansas agencies
 S and USC&GS
 Image in part compiled from aerial photographs
 55. Topography by planetable surveys 1939
 tion. 1927 North American datum
 based on Kansas coordinate system, south zone
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 on aerial photographs. This information is unchecked
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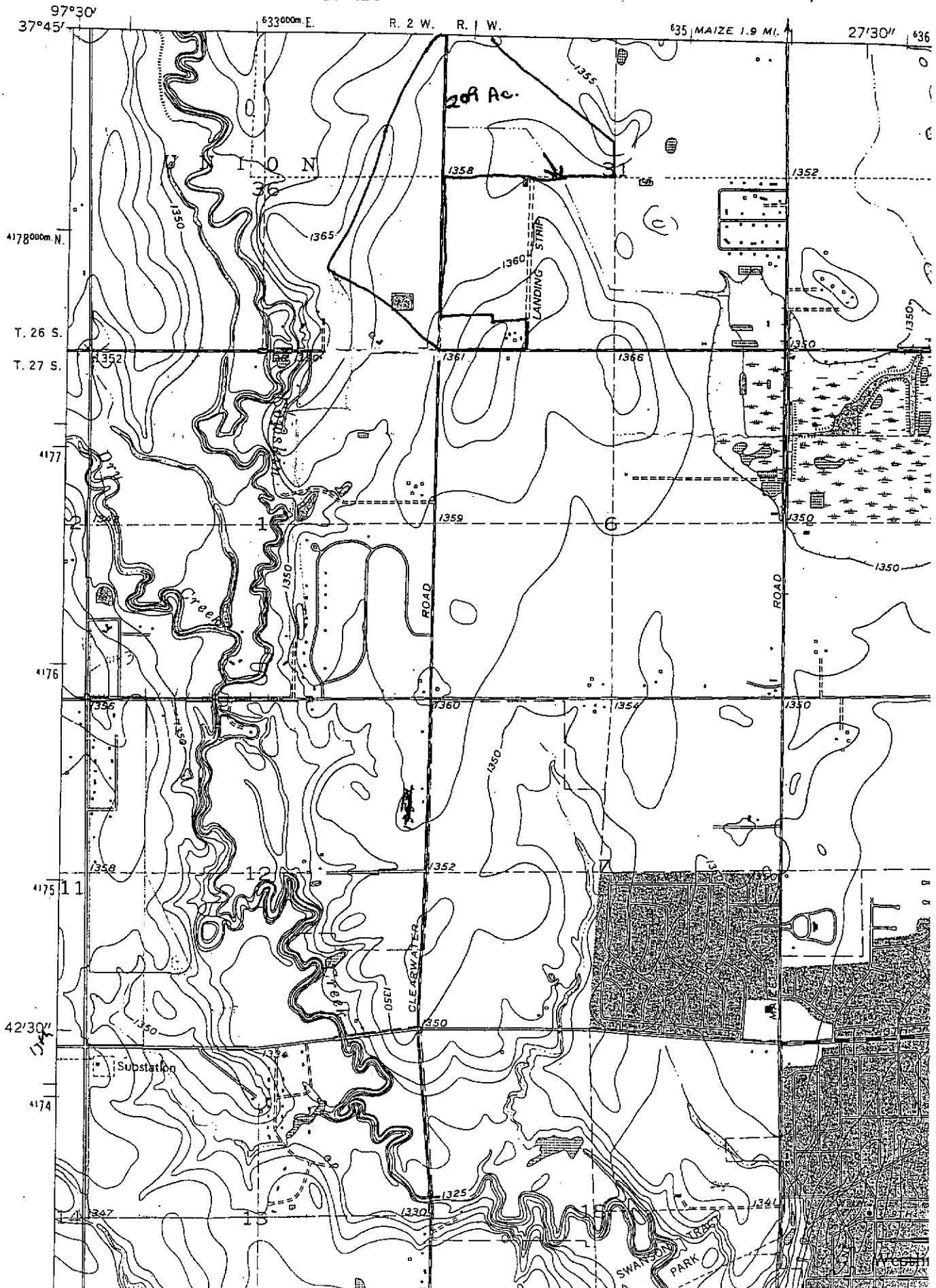
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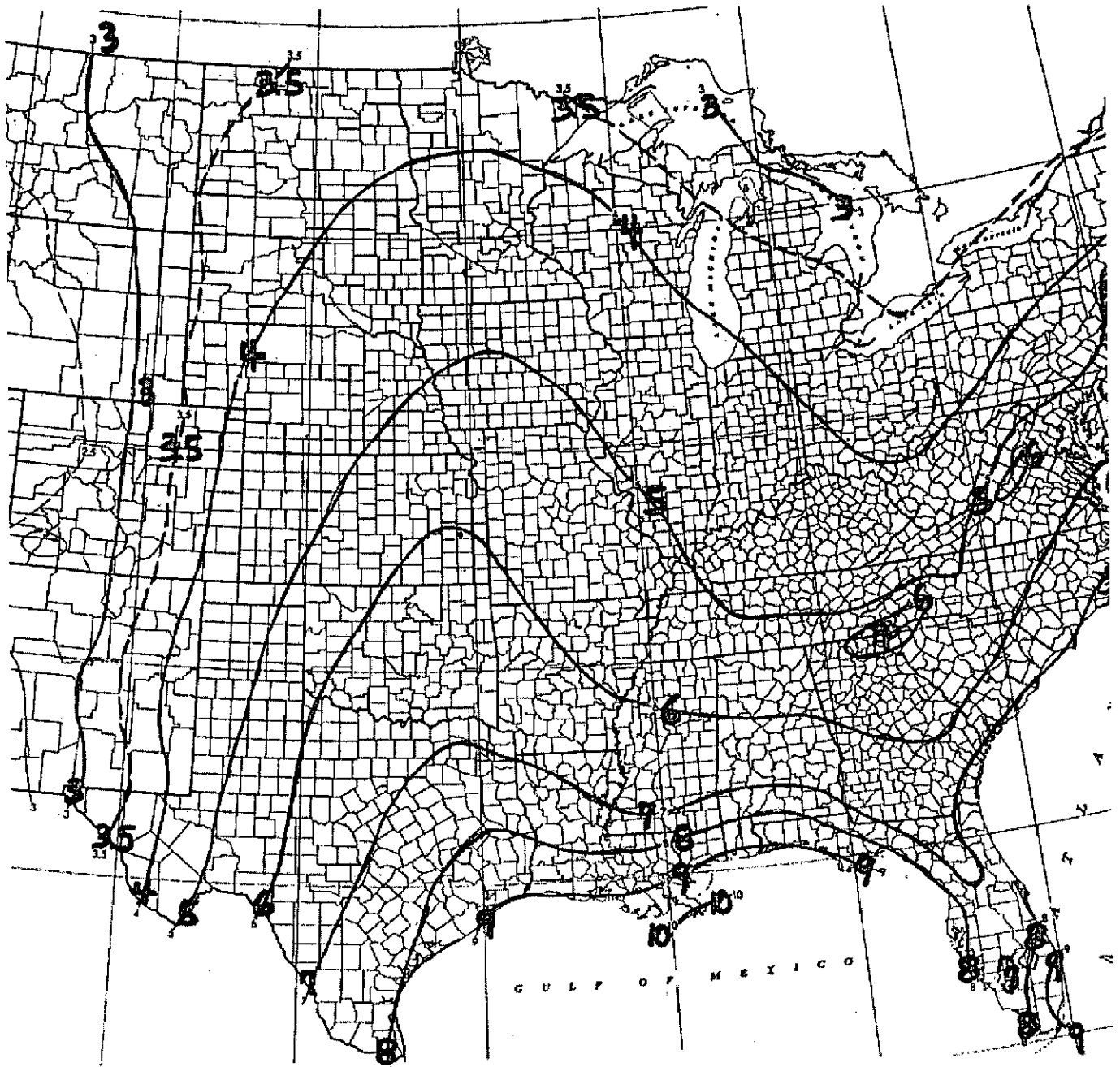
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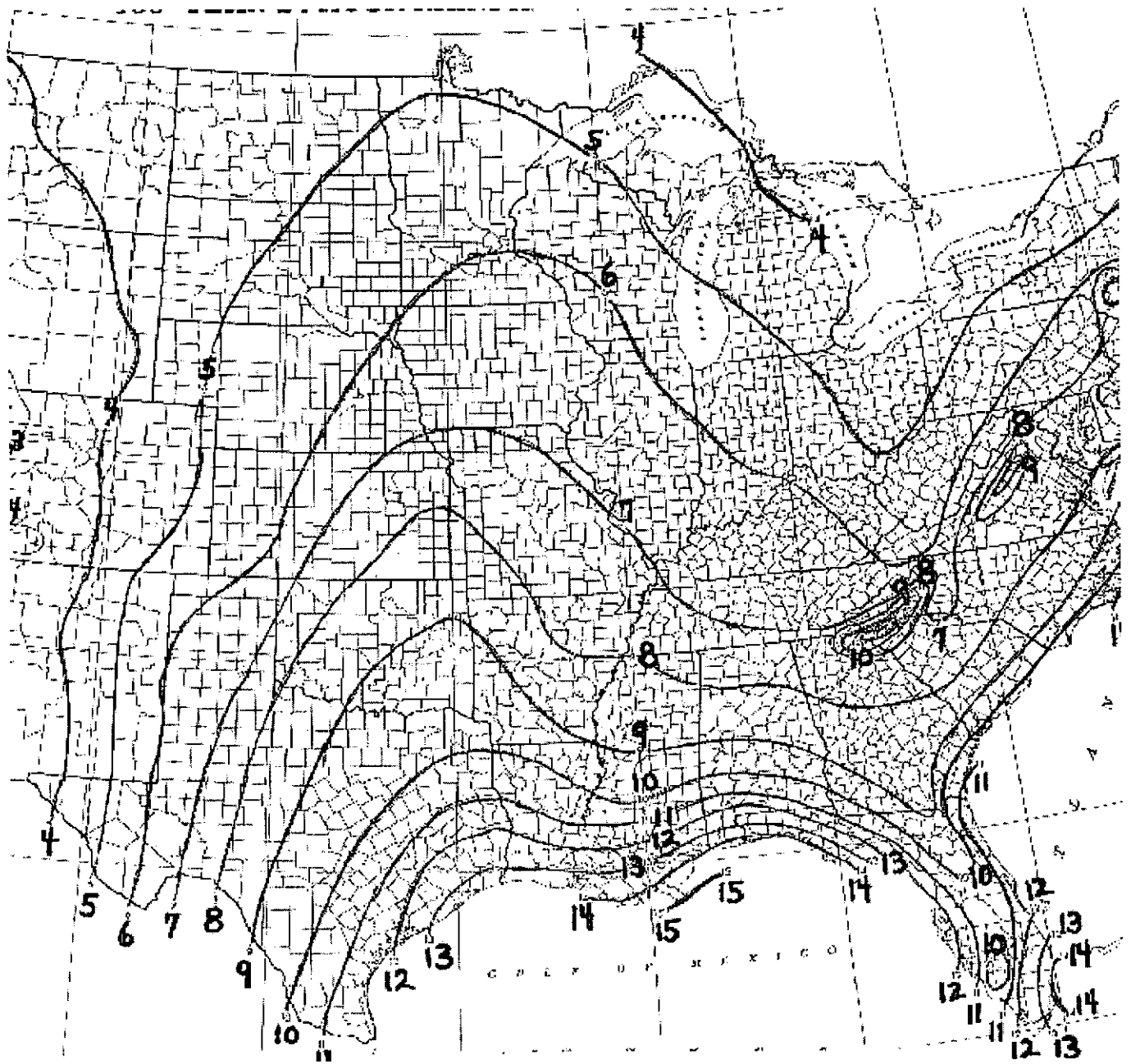
UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY



100 YEAR 6 HOUR RAINFALL (INCHES)



100 YEAR 24 HOUR RAINFALL (INCHES)



ATTACHMENT D

DRAINAGE CRITERIA

RECOMMENDED RUNOFF COEFFICIENTS FOR RATIONAL METHOD
AND PERCENT IMPERVIOUS FOR UNIT HYDROGRAPH METHOD

| Land Use or Surface Characteristics | Percent Impervious | Frequency | | | |
|--|-----------------------|-----------|------|------|------|
| | | 2 | 5 | 10 | 100 |
| 1. Business: | | | | | |
| Downtown Areas | 95 | 0.84 | 0.85 | 0.87 | 0.91 |
| Neighborhood Areas | 70 | 0.68 | 0.69 | 0.73 | 0.80 |
| 2. Residential: | | | | | |
| <u>Single Family (Soil Group D)</u> | | | | | |
| 1/8 Acre | 50 | 0.57 | 0.61 | 0.66 | 0.79 |
| 1/4 Acre | 38 | 0.50 | 0.54 | 0.62 | 0.76 |
| 1/3 Acre | 30 | 0.46 | 0.50 | 0.59 | 0.73 |
| 1/2 Acre | 25 | 0.42 | 0.48 | 0.56 | 0.72 |
| 3/4 Acre | 22 | 0.42 | 0.46 | 0.55 | 0.71 |
| 1 Acre | 20 | 0.41 | 0.45 | 0.54 | 0.71 |
| <u>Multi-Family (Soil Group D)</u> | | | | | |
| Multi-Unit (detached) | 60 | 0.62 | 0.66 | 0.72 | 0.82 |
| Multi-Unit (attached) | 65 | 0.64 | 0.68 | 0.73 | 0.83 |
| Apartments | 75 | 0.70 | 0.73 | 0.79 | 0.86 |
| <u>Single Family (Soil Group C)</u> | | | | | |
| 1/8 Acre | 50 | 0.55 | 0.58 | 0.64 | 0.73 |
| 1/4 Acre | 38 | 0.48 | 0.51 | 0.57 | 0.68 |
| 1/3 Acre | 30 | 0.43 | 0.46 | 0.53 | 0.65 |
| 1/2 Acre | 25 | 0.40 | 0.43 | 0.50 | 0.63 |
| 3/4 Acre | 22 | 0.39 | 0.42 | 0.49 | 0.62 |
| 1 Acre | 20 | 0.37 | 0.40 | 0.48 | 0.61 |
| <u>Multi-Family (Soil Group C)</u> | | | | | |
| Multi-Unit (detached) | 60 | 0.60 | 0.63 | 0.69 | 0.77 |
| Multi-Unit (attached) | 65 | 0.63 | 0.66 | 0.71 | 0.79 |
| Apartments | 75 | 0.68 | 0.72 | 0.77 | 0.83 |
| <u>Single-Family (Soil Group B)</u> | | | | | |
| 1/8 Acre | 50 | 0.52 | 0.54 | 0.59 | 0.67 |
| 1/4 Acre | 38 | 0.44 | 0.46 | 0.52 | 0.61 |
| 1/3 Acre | 30 | 0.39 | 0.41 | 0.47 | 0.57 |
| 1/2 Acre | 25 | 0.36 | 0.38 | 0.44 | 0.54 |
| 3/4 Acre | 22 | 0.34 | 0.36 | 0.42 | 0.52 |
| 1 Acre | 20 | 0.33 | 0.35 | 0.40 | 0.51 |
| <u>Multi-Family (Soil Group B)</u> | | | | | |
| Multi-Unit (detached) | 60 | 0.58 | 0.60 | 0.65 | 0.72 |
| Multi-Unit (attached) | 65 | 0.61 | 0.64 | 0.68 | 0.75 |
| Apartments | 75 | 0.67 | 0.70 | 0.74 | 0.80 |

| Land Use or Area Characteristics | Percent Impervious | Frequency | | | |
|--|-----------------------|-----------|------|------|------|
| | | 2 | 5 | 10 | 100 |
| <u>Single Family (Soil Group A)</u> | | | | | |
| 1/8 Acre | 50 | 0.47 | 0.50 | 0.54 | 0.60 |
| 1/4 Acre | 38 | 0.39 | 0.41 | 0.45 | 0.52 |
| 1/3 Acre | 30 | 0.33 | 0.35 | 0.39 | 0.47 |
| 1/2 Acre | 25 | 0.30 | 0.31 | 0.35 | 0.44 |
| 3/4 Acre | 22 | 0.28 | 0.29 | 0.33 | 0.42 |
| 1 Acre | 20 | 0.26 | 0.28 | 0.32 | 0.40 |
| <u>Multi-Family (Soil Group A)</u> | | | | | |
| Multi-Unit (detached) | 60 | 0.55 | 0.57 | 0.61 | 0.67 |
| Multi-Unit (attached) | 65 | 0.58 | 0.60 | 0.64 | 0.70 |
| Apartments | 75 | 0.65 | 0.68 | 0.72 | 0.77 |
| 3. Industrial: | | | | | |
| Light Areas | 70 | 0.68 | 0.69 | 0.73 | 0.80 |
| Heavy Areas | 80 | 0.74 | 0.76 | 0.79 | 0.84 |
| 4. Playgrounds: | 15 | 0.33 | 0.35 | 0.42 | 0.55 |
| 5. Schools: | 40 | 0.49 | 0.51 | 0.56 | 0.66 |
| 6. Railroad Yard Areas: | 30 | 0.43 | 0.45 | 0.50 | 0.62 |
| Undeveloped Urban Areas: | | | | | |
| Offsite Flow Analysis (when land use not defined) | 45 | 0.52 | 0.54 | 0.59 | 0.68 |
| 8. Streets: | | | | | |
| Paved | 99 | 0.87 | 0.88 | 0.90 | 0.93 |
| Gravel | 00 | 0.24 | 0.26 | 0.33 | 0.48 |
| 9. Drive, Parking Lots and Walks: | 96 | 0.87 | 0.87 | 0.88 | 0.89 |
| 10. Roofs: | 90 | 0.80 | 0.85 | 0.90 | 0.93 |
| 11. Urban Lawn Areas (See Note No. 1 below): | | | | | |
| <u>Soil Group A</u> | | | | | |
| Slope less than 1% | 00 | 0.08 | 0.09 | 0.13 | 0.23 |
| Slope 1% to 4% | 00 | 0.12 | 0.13 | 0.17 | 0.27 |
| Slope more than 4% | 00 | 0.16 | 0.17 | 0.21 | 0.31 |
| <u>Soil Group B</u> | | | | | |
| Slope less than 1% | 00 | 0.16 | 0.18 | 0.24 | 0.37 |
| Slope 1% to 4% | 00 | 0.20 | 0.22 | 0.28 | 0.41 |
| Slope more than 4% | 00 | 0.24 | 0.26 | 0.32 | 0.45 |
| <u>Soil Group C</u> | | | | | |
| Slope less than 1% | 00 | 0.24 | 0.27 | 0.35 | 0.51 |
| Slope 1% to 4% | 00 | 0.26 | 0.29 | 0.37 | 0.53 |
| Slope more than 4% | 00 | 0.28 | 0.31 | 0.39 | 0.55 |

| <u>Land Use or ace Characteristics</u> | <u>Percent Impervious</u> | <u>Frequency</u> | | | |
|--|-------------------------------|------------------|----------|-----------|------------|
| | | <u>2</u> | <u>5</u> | <u>10</u> | <u>100</u> |
| <u>Soil Group D</u> | | | | | |
| Slope less than 1% | 00 | 0.28 | 0.33 | 0.43 | 0.63 |
| Slope 1% to 4% | 00 | 0.30 | 0.35 | 0.45 | 0.65 |
| Slope more than 4% | 00 | 0.32 | 0.37 | 0.47 | 0.67 |

Note No. 1: Coefficients shown in the above table are for pervious open space areas with thick turf which includes pervious areas in parks and cemeteries. Coefficients shown above must be increased 0.02 for use with agricultural pasture areas. Coefficients shown above must be reduced by 0.04 for use with agricultural cultivated areas. Group A soils are well-drained, coarse textured sands with high infiltration rates. Group B soils are moderately well-drained, moderately coarse textured soils with moderate infiltration rates. Group C soils are moderately poor-drained, moderately fine textured soils with slow infiltration rates. Group D soils are poor-drained, fine textured soils with very slow infiltration rates.

GENERAL NOTE: These Rational Formula Coefficients may not be valid for basins 320 acres or larger.

ATTACHMENT E

DRAINAGE CRITERIA

AVERAGE OVERLAND FLOW VELOCITY FOR USE WITH URBANIZED AREAS

| Surface Type | VELOCITY IN FEET/SECOND FOR SLOPES IN PERCENT SHOWN | | | | | | | | | | | | | | | | | | | |
|---|---|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1.0 | 2.0 | 3.0 | 4.0 | 5.0 | 6.0 | 7.0 | 8.0 | 9.0 | 10.0 | 20.0 |
| Forest with Heavy Ground Litter or Meadow | 0.03 | 0.04 | 0.06 | 0.07 | 0.08 | 0.09 | 0.10 | 0.11 | 0.12 | 0.13 | 0.16 | 0.21 | 0.28 | 0.33 | 0.39 | 0.46 | 0.53 | 0.60 | 0.72 | 1.10 |
| Fallow or Minimum Tillage Cultivation | 0.06 | 0.08 | 0.10 | 0.12 | 0.13 | 0.14 | 0.16 | 0.17 | 0.18 | 0.19 | 0.29 | 0.40 | 0.51 | 0.66 | 0.78 | 0.91 | 1.05 | 1.20 | 1.44 | 2.10 |
| Short Grass Pasture or Lawns | 0.09 | 0.13 | 0.15 | 0.18 | 0.20 | 0.21 | 0.23 | 0.25 | 0.26 | 0.28 | 0.45 | 0.60 | 0.77 | 0.96 | 1.17 | 1.33 | 1.50 | 1.68 | 1.98 | 3.20 |
| Almost Bare Ground | 0.16 | 0.22 | 0.28 | 0.31 | 0.35 | 0.38 | 0.41 | 0.44 | 0.46 | 0.49 | 0.70 | 0.85 | 1.05 | 1.26 | 1.50 | 1.75 | 2.03 | 2.32 | 2.79 | 4.40 |
| Grassed Waterway | 0.35 | 0.48 | 0.58 | 0.67 | 0.77 | 0.84 | 0.91 | 0.98 | 1.05 | 1.12 | 1.54 | 1.82 | 2.10 | 2.38 | 2.78 | 3.20 | 3.66 | 4.14 | 4.56 | 7.00 |
| Paved Areas (Sheet Flow) or Shallow Gutter Flow | 0.44 | 0.62 | 0.77 | 0.91 | 1.05 | 1.12 | 1.19 | 1.26 | 1.33 | 1.40 | 2.00 | 2.55 | 3.20 | 3.83 | 4.41 | 5.04 | 5.70 | 6.00 | 6.20 | 9.00 |