



# LETTER OF TRANSMITTAL

**Professional Engineering Consultants, P.A.**

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TO: City of Wichita  
Storm Water Management  
7<sup>th</sup> Floor - City Hall  
455 N. Main  
Wichita, KS 67202

DATE: May 24, 2007

PROJECT NO.: 36-07290-5526

PROJECT: Oak Creek 4th Addition

ATTENTION: Vicki Huang

REFERENCE: Storm Water Drainage Report

FROM: Shawn Bryan

WE ARE SENDING YOU:  Attached  Under separate cover via \_\_\_\_\_ the following items:  
 Shop drawings  Prints  Plans  Samples  Specifications  
 Copy of letter  Change order  \_\_\_\_\_

COPIES	DATE	NO.	DESCRIPTION
1	05/24/2007	1	Storm Water Drainage Plan & Calculations for Oak Creek 4th Addition

**THESE ARE TRANSMITTED as checked below:**

For approval  Approved as submitted  Resubmit 1 copies for approval  
 For your use  Approved as noted  Submit \_\_\_\_\_ copies for distribution  
 As requested  Returned for corrections  Return \_\_\_\_\_ corrected prints  
 For review and comment  \_\_\_\_\_  
 FOR BIDS DUE \_\_\_\_\_  PRINTS RETURNED AFTER LOAN TO US

REMARKS: Vicki,  
Here is the storm water drainage report for Oak Creek 4th Addition that you requested from Rob Hartman with our office. Most of the data is dealing with the whole property (155 ac.) and Oak Creek 3<sup>rd</sup> Addition since this information was previously submitted with the Oak Creek 3<sup>rd</sup> Drainage Report. If you have any questions please feel free to contact me.

Thanks.

COPIES TO: File

By: Shawn R. Bryan



**Public Works, Engineering Division  
Final Drainage Plan Submittal Checklist**

Reviewer: <u>VICKI HUANG</u>	Date: <u>05-24-07</u>
Subdivision Name: <u>OAK CREEK 4TH ADDITION</u>	Location: <u>SW CORNER 21ST &amp; GREENWICH</u>
Total Land Area Of Ownership: <u>154.5</u> Acres	
Type: <input checked="" type="checkbox"/> Residential <input type="checkbox"/> Commercial <input type="checkbox"/> Industrial <input type="checkbox"/> Recreation <input type="checkbox"/> Municipal <input type="checkbox"/> Other	
Applicant: <u>SLAWSON COMMERCIAL PROPERTIES</u>	Contact: <u>MR. GEORGE SHERMAN</u> Phone #: <u>316-263-3201</u>
Engineer: <u>PEC</u>	Contact: <u>SHAWN BRYAN</u> Phone #: <u>316-206-1316</u>

Please check the appropriate box:

I = Included; NA = Non-Applicable; R= Required prior to development  
(If "NA" is checked, an explanation must be entered)

Tab 1. Project Narrative	Applicant			Engr	
	I	NA	Explanation / Location in Plan	I	NA
A. Site Location Map, using USGS Map			LOOK AT FIS MAP OR 4-CORNER PLAN		
B. Discussion of development, existing conditions, and proposed impacts on stormwater, wetland, riparian, and flood plain	X				
C. Discussion of offsite conditions	X				
D. Summary of runoff calculations (pre/post development) No increase in peak discharge for all storm series	X				
E. Narrative description of the type and function of the permanent best management practices that are incorporated into the site design		X			
F. Copy of the plat	X				
G. Preliminary grading plan (The final grading plan shall be sealed, signed and dated prior to Engineering receiving the final sanitary sewer plans. One plan sheet and PDF shall be submitted to the Subdivision Engineer.)		X			
H. Professional Engineer seal, signature and date on cover of report	X				
I. CD of drainage plan in PDF format (one file) and one paper copy bound with this checklist included behind the cover		X	WILL SUBMIT ONCE IT IS APPROVED		

Tab 2. Existing Conditions Runoff Calculations	Applicant			Engr	
	I	NA	Explanation / Location in Plan	I	NA
A. Copy of applicable orthophoto showing proposed project boundaries (preferable in color)					
B. Runoff Method (Rational, Hydrograph Method, or other approved methods by Engineering)	X		HEC-1 & HEC-RAS		
C. Existing topography (no greater than 2-foot contours, 1-foot recommend)	X				
D. Total Site Area and Total Impervious Area (acres)	X				
E. Benchmarks used for site control	X				
F. Streams, creeks, and waterway labeled	X				
G. Predominant soils from USDA soil surveys, and/or on site soil borings	X				
H. Location and boundaries of natural features such as wetlands, lakes, and ponds with the normal water elevation noted		X			
I. Location of existing roads, buildings, parking lots and other impervious areas.	X				



J. Location of existing utilities (e.g., water, sewer, gas, electric) and easements	X		ON PLAT		
K. Location of existing conveyance systems such as storm drains, inlets, catch basins, channels, swales, and areas of overland flow	X				
L. Flow paths	X				
M. Location and dimensions of existing channels, bridges or culvert crossings		X			
N. Existing conditions hydrologic analysis for runoff rates, volumes and velocities showing methodologies used and supporting calculations (2, 5, 10, 25 & 100 year, 24-hour storm events) or Critical Duration	X				
O. Assumed pre-developed runoff curve numbers					
P. Existing time of concentrations used in calculations	X				
Q. Evaluate immediate downstream drainage capacity, not to exceed more than 0.25 miles downstream of site		X	MEET PRE VS. POST RATE WILL NOT HAVE AN IMPACT ON DOWNSTREAM		
R. Existing structural elevations (e.g., invert of pipes, manholes, etc.)		X			
S. Cross-section data for open channels		X			
T. Ground water elevations, if applicable		X			

Tab 3. Post-Development Hydrologic Analysis	Applicant			Engr	
	I	NA	Explanation / Location in Plan	I	NA
A. Proposed (post-development) conditions hydrologic and hydraulic analysis for runoff rates, volumes, HGL, and velocities showing the methodologies used and supporting calculations for all applicable design storms (2, 5, 10, 25 & 100 year, 24-hour storm events)	X				
B. Proposed time of concentrations used in calculations		X			
C. Assumed post-developed runoff curve numbers	X				
D. Proposed contours for detention facilities (to equal area used in outlet rating curves)		X	ARE IN HEC1 MODEL		
E. Preliminary sizing calculations for stormwater controls including contributing drainage area, storage, and outlet configuration		X			
F. Stage-storage-discharge or outlet rating curves and inflow and outflow hydrographs for storage facilities		X			
G. Final analysis of potential upstream/downstream impact/effects of project, where necessary		X			
H. Existing and proposed structural elevations (e.g., invert of pipes, manholes, etc.)		X			
I. Design water surface elevations and normal pool elevation for ponds.		X			
J. Typical detail for outlet structures, embankments, spillways, grade control structures, conveyance channels, etc. To include height, width, elevation, and/or diameter.		X			
K. Proposed limits of clearing and grading		X			
L. Location of existing and proposed roads, buildings, parking lots and other impervious areas.	X				
M. Location of existing and proposed utilities (e.g., water, sewer) and easements	X				
N. Location of existing and proposed conveyance systems such as storm drains, inlets, catch basins, channels, swales, and areas of overland flow	X				
O. Preliminary location and dimensions of proposed channel modifications, such as bridge or culvert crossings		X			

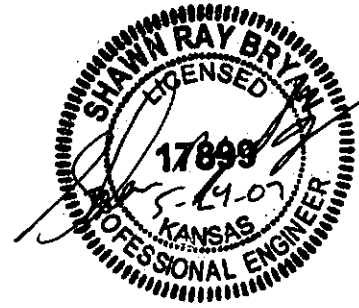


P. Preliminary selection and location of stormwater controls		X		
Q. Emergency overflow structure's flow path		X		
R. Detention facility provides one-foot of freeboard above the HWL and emergency outfall shown (top of berm elevation shown)		X		
S. The 100-year 24-hour HWL delineated on the plan for detention pond		X		
T. Lowest opening elevations table on the plat for structures located adjacent to channels or ponds			LOCATED ON 4-CORNER & DRAINAGE PLAN	
U. Stormwater Management Facilities located within a Reserve	X			
V. Maintenance responsibility of stormwater management facility shall be specified in the plat text (e.g. HOA, Lot Owners Association, or lot)		X		
W. Off-site drainage easements or agreements required, where necessary		X		

Tab 4. Floodplain Submittal	Applicant			Engr	
	I	NA	Explanation / Location in Plan	I	NA
A. Provide source of flood profile	X				
B. Nearest base flood elevations	X				
C. Delineation of pre-developed regulatory floodplain/floodway limits		X			
D. Delineation of post-developed regulatory floodplain and floodway limits		X			
E. Floodplain boundary determination per elevation (project limits shown)	X		MAP INCLUDED		
F. Provide source of floodway data table and discharges		X			
G. Provide all hydrologic and hydraulic study information for site-specific floodplain studies, unnumbered Zone A area elevation determinations and flood plain map revisions or required permits	X				
H. Provide regulatory floodway and four natural profile models (10,50,100, and 500-yr) for existing and future watershed conditions		X			
I. Location of floodplain/floodway limits and relationship of site to upstream/downstream properties (floodplain limits to be per elevation and scaled location)		X			
J. Flood plains and floodways located within a Reserve, where necessary	X				

Tab 5. Federal, State and Local Permits (to be provided prior to construction unless otherwise specified)	Applicant			Engr	
	I/R	NA	Explanation / Location in Plan	I/R	NA
A. US Army Corps of Engineers - Regulatory program permits (404 water quality certification)		X			
B. Kansas Department of Agriculture - Division of Water Resources Permits (Stream Obstruction, Channel Change, Flood Plain Fill, Levee, Water Appropriations, Dam safety permit, etc.)		X			
C. Federal Emergency Management Agency (FEMA) Letter of Map Changes (LOMA, LOMR, LOMR-f, CLOMR, etc.) Shall be included and approved when project modifies the limits of the floodway.		X	WILL SUBMIT COLMR FOR DEVELOPMENT AT LATER DATE		
D. Kansas Department of Transportation		X			
E. Sedgwick County Right-of-way Permit		X			

**Oak Creek 4<sup>rd</sup> Addition**  
**Wichita, Sedgwick County, Kansas**  
05/23/07



Oak Creek 4<sup>rd</sup> Addition is a 9.50 acre residential development. This development is part of the Oak Creek Development Master Plan. Oak Creek is a 154.5 acre, commercial and residential development on the southwest corner of 21<sup>st</sup> Street North and Greenwich Road within the city limits of Wichita in Sedgwick County, Kansas. The 5 lot development consists of existing streets and storm sewer. This report contains a drawing of the drainage plan, supporting calculations and data for the Oak Creek 3<sup>rd</sup> Addition which included all the calculations for whole development. I have also included the Oak Creek 4<sup>rd</sup> plat and drainage plan in this report.

**Hydrology**

The proposed plat lies in the NE 1/4, Section 9, T27S, R2E. The soil on-site is comprised primarily of Goessel Silty clay, Irwin silty clay loam and Rosehill silty clay, which are all classified in hydrologic group D. Elandco silt loam is present along the West Fork of Four Mile Creek. The land is currently vacant, with the exception of streets and the storm water system for Oak Creek 2<sup>nd</sup> and 3<sup>rd</sup> Additions, and is wooded/ grassland throughout. The site is bordered to the north by 21<sup>st</sup> Street North, to the south by the Burlington Northern Railroad, to the east by Greenwich Road and to the west by the Remington Place Development. The West Fork of Four Mile Creek cuts through this site from the north property line to the east property line and has approximately 1.60 square miles of contributing area to the north of this site. Existing Basin A drains to the north to the storm sewer system along 21<sup>st</sup> Street North and eventually to the West Fork of Four Mile Creek. Existing Basin B drains to the south and east into the West Fork of Four Mile Creek. Existing Basin C drains to the south and west to the Remington Place 3<sup>rd</sup> Addition. Existing Basin D drains to the east Greenwich Road to a 36" RCP under Greenwich Road. Proposed Basin A, B, C, D & E drain through the pond system labeled #2, 3, 4, 5 & 6 on the drainage map and ponds A-E in the HEC-1 output files. These

ponds will drain to the east into the West Fork of Four Mile Creek. Proposed Basin F drains to an existing pond labeled pond #1 on the drainage map and Pond F in the HEC-1 output files. This pond then drains into the West Fork of Four Mile Creek. Proposed Basin G drains directly to the West Fork of Four Mile Creek. Proposed Basin H drains eventually to the southeast corner of the site to the existing 36" RCP under Greenwich. It is important to note that no water will drain west to the Remington 3<sup>rd</sup> Addition after development and that significant changes will be made to the West Fork of Four Mile Creek on this site as shown on the Drainage Map. The channelization of the West Fork of Four Mile Creek (in the future) will require permits from the Division of Water Resources and a review by the Corps of Engineers. Oak Creek 3<sup>rd</sup> Addition has large residential lots located next to the West Fork of Four Mile Creek. Oak Creek 4<sup>th</sup> Addition was originally planned to be commercial property and since has been changed to be residential properties. Oak Creek 4<sup>th</sup> Addition is located in Post Development Basin G which will drain directly into the West Branch of Four Mile Creek. This concept has been approved previously with Oak Creek, Oak Creek 2 and 3<sup>rd</sup> additions. As shown in the drainage plan the overall discharge from the site is less than the pre-development discharge rate. This is the case even though no detention will be placed in the area surrounding the creek. The detention pond system throughout all the Oak Creek Additions (1, 2 & 3) will decrease the discharge rate enough to enable development to occur next to the creek without detention.

Runoff coefficients were estimated based on tables presented in the Design Aids section of this report using fully developed conditions. Time of concentration was based on slope, flow velocity and length of flow through each basin (TR-55 Method) and was not allowed to be less than 15 minutes. The HEC-1 computer program was used for the pre-development runoff rate and also to route the runoff through the ponds and determine the post-development conditions leaving the site.

The analysis was made based on the available site data which includes the following: 1" = 100' topographic map with 2' contours of the site, a Sedgwick County Soil Survey Map and noted references.

## Storm Sewer Design

The storm sewer is included in this submittal but was designed and included in the Oak Creek, Oak Creek 2<sup>nd</sup> and Oak Creek 3<sup>rd</sup> Addition drainage report submittals. For the storm sewer hydrologic analysis, the Rational Method was used. Runoff coefficients were estimated using the charts in the design aids section of this report. For this development, a uniform assumption of the minimum time of concentration of 10 minutes was deemed appropriate. Travel time for flow through defined channels, pipes, etc, for these basins were estimated on the basis of Manning's Equation.

In the hydraulic analysis, the storm sewers are designed for the minor storm, with major storm overflows to be routed through easements and rights-of-way to an appropriate outlet. The minor storm has a recurrence interval of two years. The major storm evaluated has a recurrence interval of one hundred years. To simplify this analysis, the time of concentration is identical for both the major and minor storms.

For each inlet, street flooding and inlet capacity were checked for the minor storm. Conveyance in the street is based on the Modified Manning's Equation, as expressed in the Design of Urban Highway Drainage – The State of the Art, Equation (5-1), pages 5-9. It has been assumed that Tc for street flow is equal to Tc for pipe flow. This is a simplifying, but conservative, assumption since pipe flow velocities generally exceed street flow velocities. For local streets, curb-deep flow is tolerable for the minor storm. For collector streets, a single eight-foot lane should remain unflooded for the minor storm.

Inlet capacities were determined by the methods described in Drainage of Highway Pavements, Hydraulic Engineering Circular #12, using Chart #12 as found in the Design Aids section. City of Wichita Type 1A inlets and 3/8 inch per foot cross slopes have been assumed. Minimum walk grade has been assumed to be 0.3 feet above the top of

curb, unless otherwise noted. Streets have been assumed to have 6-5/8 inch standard curb, unless otherwise noted.

Hydraulic computation for the storm sewer pipe system was performed using PEC's STORM computer program. This program uses Manning's Equation to calculate friction losses for pipes flowing full. Minor losses are computed by momentum principles at each structure. All pipe area is assumed to be reinforced concrete with a Manning's "n" of 0.012. It is desirable to keep the hydraulic grade line at least one foot below the top of curb for the minor storm. The calculations and the STORM analyses for the storm sewers are included in this report.

### **Design Aids**

This section includes material used to assist in designing the drainage system. A 1" = 100' scale Drainage Plan map (Attachment A) and a 1" = 100' scale Four-Corner Plan map (Attachment B) are enclosed in the pockets.

### **References**

Design of Urban Highway Drainage – The State of the Art, by Reitz & Jens, Inc., April 1980.

Drainage of Highway Pavements, Hydraulic Engineering Circular #12, by Tye Engineering, Inc., March 1984.

Interim Drainage and Storm Sewer Policy for Design Criteria and Documentation, City of Wichita, Kansas, 1985.

Soil Survey of Sedgwick County, Kansas, US Department of Agriculture, Soil Conservation Service, 1979.

**TABLE 1****PRE VS. POST-DEVELOPMENT DISCHARGE RATES**

[REDACTED]							
A	BOTH	38	68		20	109	
B	BOTH	47	153		20	26	
C	BOTH	39	7		20	57	
D	BOTH	62	52		20	15	
E	POST	N/A	N/A		20	20	
F	POST	N/A	N/A		25	60	
G	POST	N/A	N/A		25	165	
H	POST	N/A	N/A		30	38	
<b>TOTAL DISCHARGE</b>			280			278	

\*\*\*\* Note: Only ponds D, F, G & H discharge in the post-development conditions.

# OAK CREEK 3RD ADDITION FOUR MILE CREEK WATER SURFACE ELEVATIONS

		Water Surface Elevations				
		Existing		Post	Allowable	
Sta		Conditions		Development	1 Foot	
16.37		1359.00		1359.00	0.00	
405.91		1359.29		1359.26	0.03	
828.54		1359.63		1359.68	0.05	
1184.83		1359.88		1360.25	0.37	
1363.99		1359.85		1360.71	0.86	
1550.64		1360.23		1361.09	0.86	
1810.00		1360.58		1361.08	0.50	
2170.00		N/A		N/A		
2176.24		1361.78		1362.43	0.65	

**OAK CREEK 4TH ADDITION  
PRE. VS. POST RUNOFF CALCULATION**

BASIN	2 YEAR STORM EVENT DISCHARGE (CFS)		5 YEAR STORM EVENT DISCHARGE (CFS)	
	PRE.	POST	PRE	POST
A	20.00	13.00	30.00	19.00
B	46.00	22.00	68.00	30.00
C	2.00	5.00	3.00	7.00
D	16.00	5.00	23.00	5.00
E	N/A	11.00	N/A	13.00
F	N/A	10.00	N/A	25.00
G	N/A	64.00	N/A	87.00
H	N/A	5.00	N/A	5.00
<b>TOTAL DISCHARGE FROM SITE</b>	<b>84.00</b>	<b>84.00</b>	<b>124.00</b>	<b>122.00</b>
Note: Ponds A, B, C & D drain into Pond D in post development				

revout.txt

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1*****
#*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* ENGINEERS
* JUN 1998
* CENTER
* VERSION 4.1
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* RUN DATE 28SEP06 TIME 14:14:37
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* U.S. ARMY CORPS OF
* HYDROLOGIC ENGINEERING
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.  
 THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT  
 STRUCTURE.  
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

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revout.txt  
 HEC-1 ANALYSIS FOR OAK CREEK w/ 2nd & 3RD ADDITION BASIN  
 PROPOSED CONDITIONS - DETENTION BASINS ONLY  
 100-YEAR STORM - POST DEVELOPMENT

ID	ID	ID	*DIAGRAM	15 27SEP06	1200	0 28SEP06	2000													
4	IT	15		27SEP06	1200	0	28SEP06	2000												
5	IN	15		27SEP06	1200															
6	IO	0		5																
7	JR	PREC		3.5	4.5	5.3	6.1	7.0	7.8											
8	KK	A																		
9	KO	5																		
10	BA	0.0149																		
11	PB	1.00																		
12	PC	0.000		0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025								
13	PC	0.029		0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060								
14	PC	0.064		0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105								
15	PC	0.110		0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172								
16	PC	0.181		0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699								
17	PC	0.735		0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843								
18	PC	0.850		0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903								
19	PC	0.907		0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947								
20	PC	0.952		0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979								
21	PC	0.982		0.985	0.988	0.991	0.994	0.997	1.000											
22	LS	0		85	40															
23	UD	0.200																		
24	KK	PONDA																		
25	KO	5																		
26	RS	1		ELEV	1388.0															
27	SA	0.50		0.61	0.72	0.84														
28	SE	1388.0		1389.0	1390.0	1391.0														
29	SQ	0		1.8	5.7	11.5	19.2	29.1	41.1	55.4	72.1	91.3								
30	SQ	113.1																		
31	SE	1388.0		1388.25	1388.50	1388.75	1389.00	1389.25	1389.50	1389.75	1390.00	1390.30								
32	SE	1390.5																		
33	KK	E																		
34	KO	5																		
35	BA	0.0150																		

\*\*\* LIST \*\*\*  
 \*\*\* FREE \*\*\*

LINE		1	2	3	4	5	6	7	8	9	10
36	PB	1.00	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
37	PC	0.000	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
38	PC	0.029	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
39	PC	0.064	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
40	PC	0.110	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
41	PC	0.181	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
42	PC	0.735									
					HEC-1	INPUT					
LINE	ID	1	2	3	4	5	6	7	8	9	10

43	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
44	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
45	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
46	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
47	LS	0	85								
48	UD	0.200		20							

LINE											
49	KK	PONDE									
50	KO	5									
51	RS	1	ELEV	1365.0							
52	SA	0.30	0.38	0.47	0.57						
53	SE	1373.0	1374.0	1375.0	1376.0						
54	SQ	0	3.7	8.2	10.1	11.6	13.0	14.3	15.4	16.5	17.5
55	SQ	18.4	19.3	20.2	21.0	21.8	22.6	23.3			
56	SE	1373.0	1373.25	1373.50	1373.75	1374.00	1374.25	1374.50	1374.75	1375.00	1375.30
57	SE	1375.5	1375.75	1376.00	1376.25	1376.50	1376.75	1377.00			

58	KK	RTEL									
59	KO	5									
60	RT	0	0	1							

61	KK	B									
62	KO	5									
63	BA	0.0197									
64	PB	1.00									
65	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
66	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060

LINE	ID	1	2	3	4	5	6	7	8	9	10
67	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
68	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
69	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
70	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
71	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
72	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
73	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
74	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
75	LS	0	85	50							
76	UD	0.200									

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
77	KK	PONDB									
78	KO	5									
79	RS	1	ELEV	1367.0							
80	SA	0.25	0.32	0.40	0.49						
81	SE	1375.0	1376.0	1377.0	1378.0						
82	SQ	0	6	12	18	24	30	36	42	48	54
83	SQ	60									
84	SE	1375.0	1375.53	1375.85	1376.11	1376.34	1376.56	1376.76	1376.95	1377.13	1377.30
85	SE	1377.5									

LINE	ID	1	2	3	4	5	6	7	8	9	10
86	KK	RTEZ									
87	KO	5									
88	RT	0	0	1							
89	KK	C									
90	KO	5									
91	BA	0.0206									
92	PB	1.00									
93	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
94	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
95	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
96	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
97	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
98	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
99	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
100	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
101	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
102	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			

revout.txt

103	LS	0	85	45					
104	UD	0.200							
	*								
	*								
105	KK	PONDC							
106	KO	5							
107	RS	1	ELEV	1372.0					
108	SA	1.41	1.59	1.69					
109	SE	1372.0	1374.0	1375.0					
110	SQ	0	8	24	32	40	48	56	64
111	SQ	80							72
112	SE	1372.0	1373.41	1374.16	1375.06	1376.25	1377.75	1379.89	1385.51
113	SE	1436.2							
	*								
	*								

114	KK	RTE3							
115	KO	5							
116	RT	0	0	1					
	*								
	*								

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
117	KK	D	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
118	KO	5	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
119	BA	0.0152	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
120	PB	1.00	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
121	PC	0.000	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
122	PC	0.029	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
123	PC	0.064	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
124	PC	0.110	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
125	PC	0.181	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
126	PC	0.735	0.985	0.988	0.991	0.994	0.997	1.000			
127	PC	0.850									
128	PC	0.907									
129	PC	0.952									
130	PC	0.982									
131	LS	0	85	45							
132	UD	0.250									
	*										
	*										
	*										
	*										
	*										

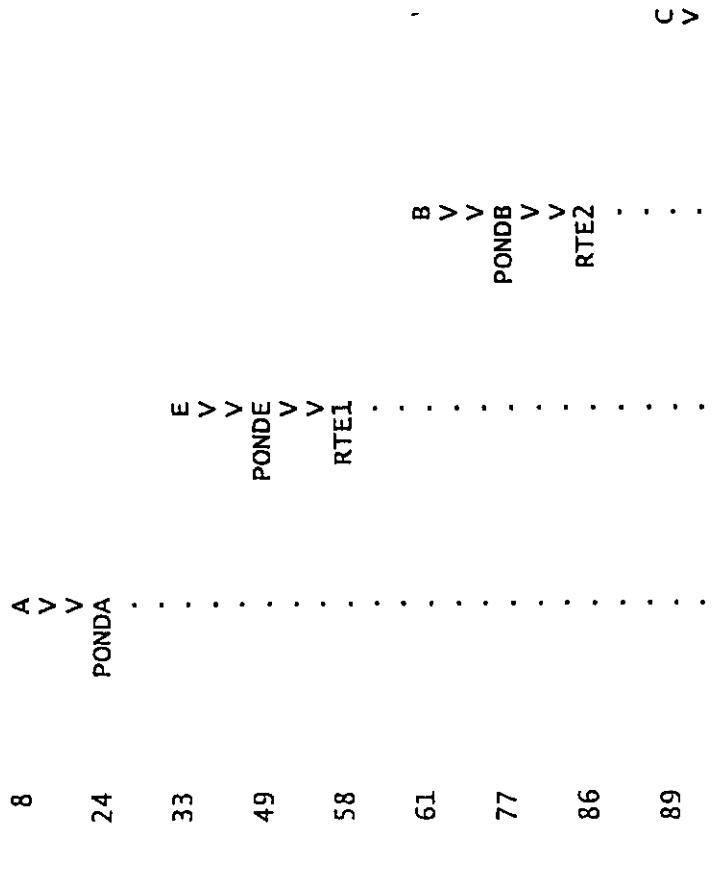
133	KK	PONDD								
134	KO	5								
135	RS	1	ELEV	1365.0						
136	SA	0.53	0.58	0.64	0.69					
137	SE	1365.0	1365.0	3167.0	1368.0					
138	SQ	0	10	20	30					
139	SQ	100								
140	SE	1365.0	1366.45	1367.19	1367.87	1368.20	1368.29	1368.37	1368.43	1368.49
141	SE	1378.6								

142

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SCHEMATIC DIAGRAM OF STREAM NETWORK

(V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW



revout.txt

105 . . . . . V  
POND C  
114 . . . . . V  
RTE3  
117 . . . . .  
D  
V  
V  
133 . . . . . POND D

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

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\* U.S. ARMY CORPS OF  
\* HYDROLOGIC ENGINEERING  
\* 609 SECOND STREET  
\* DAVIS, CALIFORNIA 95616  
\* (916) 756-1104  
\*

HEC-1 ANALYSIS FOR OAK CREEK W/ 2ND & 3RD ADDITION BASIN  
PROPOSED CONDITIONS - DETENTION BASINS ONLY  
100-YEAR STORM - POST DEVELOPMENT

6 IO OUTPUT CONTROL VARIABLES  
IPRNT 0 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA 15 MINUTES IN COMPUTATION INTERVAL  
NMIN 27SEP 6 STARTING DATE

revout.txt

ITIME 1200 STARTING TIME  
 NQ 129 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 28SEP 6 ENDING DATE  
 NDTIME 2000 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .25 HOURS  
 TOTAL TIME BASE 32.00 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION 1 NUMBER OF PLANS  
 NPLAN

JR MULTI-RATIO OPTION 6.10 7.00 7.80  
 RATIOS OF PRECIPITATION 5.30  
 3.50 4.50

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8 KK

9 KO OUTPUT CONTROL VARIABLES  
 IPRINT 5 PRINT CONTROL  
 IPLOT 5 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

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revout.txt

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\* PONDA \*  
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24 KK

25 KO            OUTPUT CONTROL VARIABLES  
                  IPRNT            5    PRINT CONTROL  
                  IPLOT            5    PLOT CONTROL  
                  QSCAL            0.    HYDROGRAPH PLOT SCALE

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33 KK

34 KO            OUTPUT CONTROL VARIABLES  
                  IPRNT            5    PRINT CONTROL  
                  IPLOT            5    PLOT CONTROL  
                  QSCAL            0.    HYDROGRAPH PLOT SCALE

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\*            PONDE        \*  
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49 KK

50 KO            OUTPUT CONTROL VARIABLES  
                  IPRNT            5    PRINT CONTROL  
                  IPLOT            5    PLOT CONTROL  
                  QSCAL            0.    HYDROGRAPH PLOT SCALE

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\* RTE1 \*  
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58 KK

59 KO            OUTPUT CONTROL VARIABLES  
                  IPRNT            5    PRINT CONTROL  
                  IPLOT            5    PLOT CONTROL  
                  QSCAL            0.    HYDROGRAPH PLOT SCALE

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61 KK

62 KO            OUTPUT CONTROL VARIABLES  
                  IPRNT            5    PRINT CONTROL  
                  IPLOT            5    PLOT CONTROL  
                  QSCAL            0.    HYDROGRAPH PLOT SCALE

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\*            PONDB            \*  
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\*\*\*\*\*

77 KK

78 KO            OUTPUT CONTROL VARIABLES  
                  IPRNT            5    PRINT CONTROL  
                  IPLOT            5    PLOT CONTROL  
                  QSCAL            0.    HYDROGRAPH PLOT SCALE



revout.txt  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\*\*\* \*\* \*\* \*\*

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\* RTE3 \*  
\*  
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114 KK

OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

115 KO

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117 KK

OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

118 KO

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\* PONDD \*  
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133 KK

134 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 5 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION					
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6
HYDROGRAPH AT	A	.01	1	19.	26.	32.	38.	44.	50.
+				12.00	12.00	12.00	12.00	12.00	12.00
ROUTED TO	PONDA	.01	1	13.	19.	24.	29.	35.	40.
+				12.25	12.25	12.25	12.25	12.25	12.25
				** PEAK STAGES IN FEET **					
			1	1388.80	1389.00	1389.13	1389.26	1389.38	1389.48
				12.25	12.25	12.25	12.25	12.25	12.25
HYDROGRAPH AT	E	.01	1	18.	25.	31.	36.	43.	49.
+				12.00	12.00	12.00	12.00	12.00	12.00
ROUTED TO	PONDE	.01	1	11.	13.	15.	17.	19.	20.
+				12.25	12.50	12.50	12.50	12.50	12.50
				** PEAK STAGES IN FEET **					
			1	1373.88	1374.34	1374.75	1375.15	1375.58	1375.96
				12.25	12.50	12.50	12.50	12.50	12.50
ROUTED TO	RTE1	.01	1	11.	13.	15.	17.	19.	20.
+				12.50	12.75	12.75	12.75	12.75	12.75
HYDROGRAPH AT	B	.02	1	27.	36.	43.	51.	59.	67.
+				12.00	12.00	12.00	12.00	12.00	12.00

```

ROUTED TO          +
+                POND B      .02      1  FLOW          22.      30.      36.      43.      50.      56.
                TIME        12.25  12.25  12.25  12.25  12.25  12.25
                ** PEAK STAGES IN FEET **
                1  STAGE    1376.26  1376.55  1376.77  1376.97  1377.18  1377.37
                TIME        12.25  12.25  12.25  12.25  12.25  12.25
ROUTED TO          +
+                RTEZ      .02      1  FLOW          22.      30.      36.      43.      50.      56.
                TIME        12.50  12.50  12.50  12.50  12.50  12.50
HYDROGRAPH AT    +
+                C        .02      1  FLOW          27.      37.      45.      53.      62.      69.
                TIME        12.00  12.00  12.00  12.00  12.00  12.00
ROUTED TO          +
+                PONDC     .02      1  FLOW          5.       7.       9.       12.      14.      17.
                TIME        12.75  12.75  12.75  12.75  12.75  12.75
                ** PEAK STAGES IN FEET **
                1  STAGE    1372.93  1373.26  1373.51  1373.75  1374.01  1374.23
                TIME        12.75  12.75  12.75  12.75  12.75  12.75
ROUTED TO          +
+                RTE3     .02      1  FLOW          5.       7.       9.       12.      14.      17.
                TIME        13.00  13.00  13.00  13.00  13.00  13.00
HYDROGRAPH AT    +
+                D        .02      1  FLOW          17.      23.      28.      33.      38.      43.
                TIME        12.00  12.00  12.00  12.00  12.00  12.00
ROUTED TO          +
+                PONDD     .02      1  FLOW          8.       11.      15.      18.      22.      26.
                TIME        12.50  12.50  12.50  12.50  12.50  12.50
                ** PEAK STAGES IN FEET **
                1  STAGE    1366.13  1366.53  1366.81  1367.07  1367.36  1367.61
                TIME        12.50  12.50  12.50  12.50  12.50  12.50

```

\*\*\* NORMAL END OF HEC-1 \*\*\*



\*\*\* LIST \*\*\*  
\*\*\* FREE \*\*\*

1  
2 ID 100-YEAR, 24-HOUR STORM

ID	DIAGRAM	06SEP06	1200	06SEP06	2000	7.0	7.8
3	IT 15	06SEP06	1200	06SEP06	2000		
4	IN 15	06SEP06	1200				
5	IO 0	5	4.5	5.3	6.1	7.0	7.8
6	JR PREC	3.5					

*							
*							
*							

7 KK A  
8 KO 5

34.55 ACRES

9	BA	0.0540					
10	PB	1.00	0.1446	0.2449	0.3146	0.3741	0.4259
11	PC	0.0000	0.6096	0.6293	0.6485	0.6647	0.6803
12	PC	0.5882	0.7560	0.7670	0.7758	0.7823	0.7901
13	PC	0.7455	0.8206	0.8299	0.8372	0.8384	0.8433
14	PC	0.8206	0.8774	0.8810	0.8857	0.8896	0.8929
15	PC	0.8730	0.9252	0.9286	0.9314	0.9337	0.9380
16	PC	0.9212	0.9654	0.9695	0.9732	0.9766	0.9795
17	PC	0.9609	0.9995	1.0000			
18	PC	0.9987	0	0			
19	LS		0.38	0			
20	UD						

21 KK B  
22 KO 5

87.14 ACRES

23	BA	0.1261					
24	PB	1.00	0.1446	0.2449	0.3146	0.3741	0.4259
25	PC	0.0000	0.6096	0.6293	0.6485	0.6647	0.6803
26	PC	0.5882	0.7560	0.7670	0.7758	0.7823	0.7901
27	PC	0.7455	0.8260	0.8299	0.8372	0.8384	0.8433
28	PC	0.8206	0.8774	0.8810	0.8857	0.8896	0.8929
29	PC	0.8730	0.9252	0.9286	0.9314	0.9337	0.9380
30	PC	0.9212	0.9654	0.9695	0.9732	0.9766	0.9795

UNOUT.TXT  
 31 PC 0.9609 0.9654 0.9695 0.9732 0.9766 0.9795 0.9821 0.9875 0.9926 0.9974  
 32 PC 0.9987 0.9995 1.0000  
 33 LS 0 85  
 34 UD 0.47  
 \*

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

35 KK C  
 36 KO S  
 \* 3.33 ACRES  
 \*  
 37 BA 0.0052  
 38 PB 1.00  
 39 PC 0.0000  
 40 PC 0.5882  
 41 PC 0.7455  
 42 PC 0.8206  
 43 PC 0.8730  
 44 PC 0.9212  
 45 PC 0.9609  
 46 PC 0.9987  
 47 LS 0  
 48 UD 0.39  
 \*

49 KK D  
 50 KO S  
 \* 29.45 ACRES  
 \*

51 BA 0.0460  
 52 PB 1.00  
 53 PC 0.0000  
 54 PC 0.5882  
 55 PC 0.7455  
 56 PC 0.8206  
 57 PC 0.8730  
 58 PC 0.9212  
 59 PC 0.9609  
 60 PC 0.9987  
 61 LS 0  
 62 UD 0.62

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63  
Schematic Diagram of Stream Network

INPUT LINE (V) ROUTING (---->) DIVERSION OR PUMP FLOW  
NO. (.) CONNECTOR (<----) RETURN OF DIVERTED OR PUMPED FLOW

7	A	.	.	.	.
21	.	.	B	.	.
35	.	.	.	C	.
49	.	.	.	.	D

(\*\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION  
1  
\*\*\*\*\*

\* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* ENGINEERS \* JUN 1998 \*  
 \* CENTER \* VERSION 4.1 \*  
 \* \* \*  
 \* RUN DATE 28SEP06 TIME 15:32:35 \*  
 \* \* \*  
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 \*\*\*\*\*

\* U.S. ARMY CORPS OF  
 \* HYDROLOGIC ENGINEERING  
 \* 609 SECOND STREET  
 \* DAVIS, CALIFORNIA 95616  
 \* (916) 756-1104  
 \*





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UNOUT.TXT

50 KO                    OUTPUT CONTROL VARIABLES

                          IPRINT                    5                    PRINT CONTROL

                          IPLOT                    5                    PLOT CONTROL

                          QSCAL                    0.                    HYDROGRAPH PLOT SCALE

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS

                          FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES

                          TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION						
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6	
HYDROGRAPH AT	A	.05	1	20.	30.	39.	48.	58.	68.	
				1.50	1.25	1.25	1.25	1.00	1.00	
HYDROGRAPH AT	B	.13	1	46.	68.	87.	108.	131.	153.	
				1.50	1.50	1.25	1.25	1.25	1.25	
HYDROGRAPH AT	C	.01	1	2.	3.	4.	5.	6.	7.	
				1.50	1.25	1.25	1.25	1.00	1.00	
HYDROGRAPH AT	D	.05	1	16.	23.	30.	37.	45.	52.	
				1.75	1.50	1.50	1.50	1.50	1.50	

\*\*\* NORMAL END OF HEC-1 \*\*\*

000T.TXT

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1*****
+*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* ENGINEERS
* JUN 1998
* CENTER
* VERSION 4.1
*
* RUN DATE 02OCT06 TIME 09:24:41
*
*
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*
* U.S. ARMY CORPS OF
* HYDROLOGIC ENGINEERING
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
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X X X X X X
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1G5, HEC1DB, AND HEC1KW.  
 THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT  
 STRUCTURE.  
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

oout.txt  
 HEC-1 ANALYSIS FOR OAK CREEK W/ 2nd & 3RD ADDITION BASIN  
 PROPOSED CONDITIONS - DETENTION BASINS ONLY  
 100-YEAR STORM - POST DEVELOPMENT

ID	DIAGRAM	15 27SEP06	1200	0 28SEP06	2000															
1	IT	15	27SEP06	1200	0	28SEP06	2000													
2	IN	15	27SEP06	1200																
3	IO	0	5																	
4	JR	PREC	3.5	4.5	5.3	6.1	7.0	7.8												
5	*																			
6	*																			
7																				
8	KK	A																		
9	KO	5																		
10	BA	0.0149																		
11	PB	1.00																		
12	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025									
13	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060									
14	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105									
15	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172									
16	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699									
17	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843									
18	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903									
19	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947									
20	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979									
21	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000												
22	LS	0	85	40																
23	UD	0.200																		
24	*																			
25	*																			
26	*																			
27	KK	PONDA																		
28	KO	5																		
29	RS	1	ELEV	1388.0																
30	SA	0.50	0.61	0.72	0.84															
31	SE	1388.0	1389.0	1390.0	1391.0															
32	SQ	0	1.8	5.7	11.5	19.2	29.1	41.1	55.4	72.1	91.3									
33	SQ	113.1																		
34	SE	1388.0	1388.25	1388.50	1388.75	1389.00	1389.25	1389.50	1389.75	1390.00	1390.30									
35	SE	1390.5																		
36	*																			
37	*																			
38	KK	E																		
39	KO	5																		
40	BA	0.0150																		

\*\*\* LIST \*\*\*  
 \*\*\* FREE \*\*\*

oout.txt

36	PB	1.00	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
37	PC	0.000	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
38	PC	0.029	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
39	PC	0.064	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
40	PC	0.110	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
41	PC	0.181	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
42	PC	0.735									

LINE	ID	1	2	3	4	5	6	7	8	9	10
43	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
44	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
45	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
46	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
47	LS	0	85	50							
48	UD	0.250									
	*										
	*										
	*										
	*										

49	KK	PONDE									
50	KO	5									
51	RS	1	ELEV	1365.0							
52	SA	0.30	0.38	0.47	0.57						
53	SE	1373.0	1374.0	1375.0	1376.0						
54	SQ	0	3.7	8.2	10.1	11.6	13.0	14.3	15.4	16.5	17.5
55	SQ	18.4	19.3	20.2	21.0	21.8	22.6	23.3			
56	SE	1373.0	1373.25	1373.50	1373.75	1374.00	1374.25	1374.50	1374.75	1375.00	1375.30
57	SE	1375.5	1375.75	1376.00	1376.25	1376.50	1376.75	1377.00			
	*										
	*										
	*										

58	KK	RTE1									
59	KO	5									
60	RT	0	0	1							
	*										
	*										
	*										

61	KK	B									
62	KO	5									
63	BA	0.0197									
64	PB	1.00									
65	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
66	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060

LINE	ID	1	2	3	4	5	6	7	8	9	10
67	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
68	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
69	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.563	0.699
70	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
71	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
72	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
73	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
74	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
75	LS	0	85	50							
76	UD	0.200									

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HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
77	KK	PONDB									
78	KO	5									
79	RS	1	ELEV	1367.0							
80	SA	0.25	0.32	0.40	0.49						
81	SE	1375.0	1376.0	1377.0	1378.0						
82	SQ	0	6	12	18	24	30	36	42	48	54
83	SQ	60									
84	SE	1375.0	1375.53	1375.85	1376.11	1376.34	1376.56	1376.76	1376.95	1377.13	1377.30
85	SE	1377.5									

86	KK	RTE2									
87	KO	5									
88	RT	0	0	1							

89	KK	C									
90	KO	5									
91	BA	0.0320									
92	PB	1.00									
93	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
94	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
95	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
96	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
97	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
98	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
99	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
100	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
101	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
102	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			

oout.txt

103	LS	0	85	45					
104	UD	0.200							
	*								
	*								
105	KK	PONDC							
106	KO	5							
107	RS	1	ELEV	1372.0					
108	SA	1.41	1.59	1.69					
109	SE	1372.0	1374.0	1375.0					
110	SQ	0	8	16	24	32	40	48	56
111	SQ	80							
112	SE	1372.0	1373.41	1374.16	1375.06	1376.25	1377.75	1379.89	1385.51
113	SE	1436.2							

114	KK	RTE3							
115	KO	5							
116	RT	0	0	1					
	*								
	*								

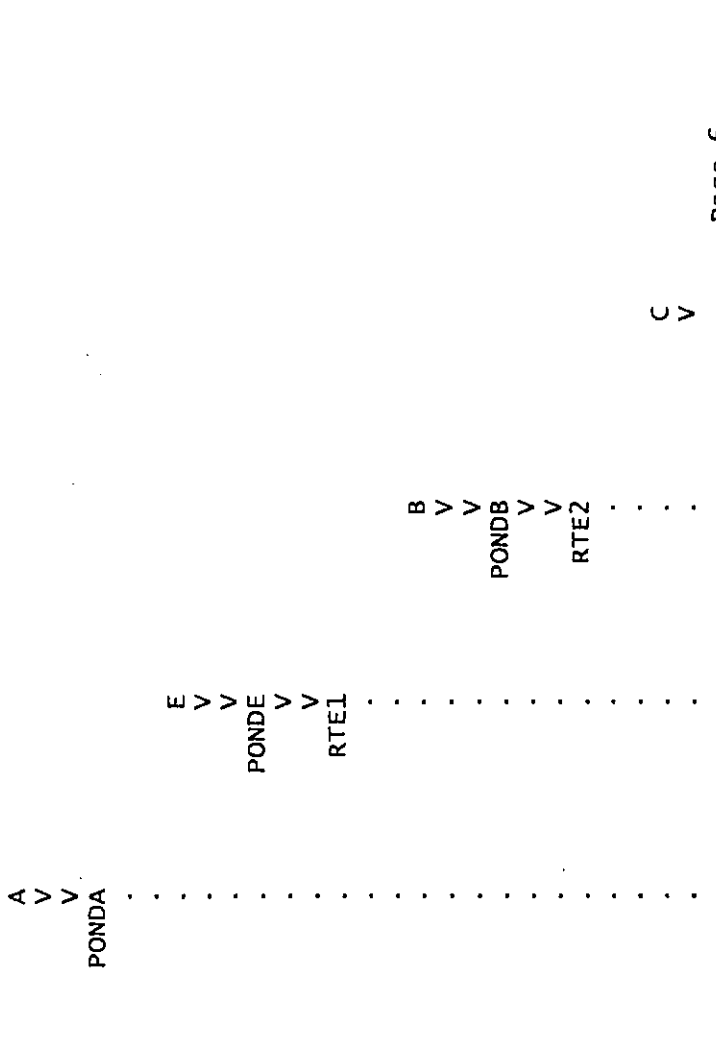
HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
117	KK	D									
118	KO	5									
119	BA	0.0152									
120	PB	1.00									
121	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
122	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
123	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
124	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
125	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
126	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
127	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
128	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
129	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
130	PC	0.982	0.985	0.988	0.991	0.994	0.997	0.970	0.973	0.976	0.979
131	LS	0	85								
132	UD	0.250	45								
	*										
	*										
	*										
	*										
	*										

133	KK	PONDD																		
134	KO	5																		
135	RS	1	ELEV	1365.0																
136	SA	0.53	0.58	0.64	0.69															
137	SE	1365.0	1365.0	3167.0	1368.0															
138	SQ	0	10	20	30															
139	SQ	100																		
140	SE	1365.0	1366.45	1367.19	1367.87	1368.20	1368.29	1368.37	1368.43	1368.49	1368.55									
141	SE	1378.6																		
	*																			
	*																			
	*																			
	*																			
142	ZZ																			

SCHEMATIC DIAGRAM OF STREAM NETWORK

(V) ROUTING (---->) DIVERSION OR PUMP FLOW  
 (.) CONNECTOR (<----) RETURN OF DIVERTED OR PUMPED FLOW



oout.txt

105 . . . . . V  
     . . . . . PONDC  
     . . . . . V  
 114 . . . . . V  
     . . . . . RTE3  
     . . . . .  
 117 . . . . . D  
     . . . . . V  
     . . . . . V  
 133 . . . . . PONDD

(\*\*\* RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
 1 \*\*\*\*\*  
 \*\*\*\*\*  
 \*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 ENGINEERS \*  
 \* JUN 1998 \*  
 CENTER \*  
 \* VERSION 4.1 \*  
 \* \*  
 \* \*  
 \* RUN DATE 02OCT06 TIME 09:24:41 \*  
 \* \*  
 \* \*\*\*\*\*  
 \*\*\*\*\*

\*  
 \* U.S. ARMY CORPS OF  
 \* HYDROLOGIC ENGINEERING  
 \* 609 SECOND STREET  
 \* DAVIS, CALIFORNIA 95616  
 \* (916) 756-1104  
 \*

HEC-1 ANALYSIS FOR OAK CREEK w/ 2nd & 3RD ADDITION BASIN  
 PROPOSED CONDITIONS - DETENTION BASINS ONLY  
 100-YEAR STORM - POST DEVELOPMENT

6 IO OUTPUT CONTROL VARIABLES  
     IPRNT 0 PRINT CONTROL  
     IPLOT 5 PLOT CONTROL  
     QSCAL 0. HYDROGRAPH PLOT SCALE  
  
 IT HYDROGRAPH TIME DATA  
     NMIN 15 MINUTES IN COMPUTATION INTERVAL  
     IDATE 27SEP 6 STARTING DATE

oout.txt

ITIME 1200 STARTING TIME  
 NQ 129 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 28SEP 6 ENDING DATE  
 NDTIME 2000 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .25 HOURS  
 TOTAL TIME BASE 32.00 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION 1 NUMBER OF PLANS  
 NPLAN

JR MULTI-RATIO OPTION  
 RATIOS OF PRECIPITATION  
 3.50 4.50 6.10 7.00 7.80

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8 KK

9 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 5 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

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00out.txt

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\*  
\* PONDA \*  
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24 KK

25 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* E \*  
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33 KK

34 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* PONDE \*  
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49 KK

50 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* RTE1 \*  
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58 KK

59 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

59 KO

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\* B \*  
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61 KK

62 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

62 KO

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\* PONDB \*  
\*  
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77 KK

78 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

78 KO





oout.txt

134 KO OUTPUT CONTROL VARIABLES  
IPRINT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION					
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6
HYDROGRAPH AT	A	.01	1	19.	26.	32.	38.	44.	50.
+				12.00	12.00	12.00	12.00	12.00	12.00

ROUTED TO	PONDA	.01	1	13.	19.	24.	29.	35.	40.
+				12.25	12.25	12.25	12.25	12.25	12.25

\*\* PEAK STAGES IN FEET \*\*

1	STAGE	1388.80	1389.00	1389.13	1389.26	1389.38	1389.48
	TIME	12.25	12.25	12.25	12.25	12.25	12.25

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION					
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6
HYDROGRAPH AT	E	.01	1	17.	23.	28.	33.	38.	43.
+				12.00	12.00	12.00	12.00	12.00	12.00

ROUTED TO	PONDE	.01	1	12.	14.	16.	17.	19.	20.
+				12.50	12.50	12.50	12.50	12.50	12.50

\*\* PEAK STAGES IN FEET \*\*

1	STAGE	1373.99	1374.48	1374.87	1375.25	1375.66	1376.01
	TIME	12.50	12.50	12.50	12.50	12.50	12.50

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION					
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6
ROUTED TO	RTE1	.01	1	12.	14.	16.	17.	19.	20.
+				12.75	12.75	12.75	12.75	12.75	12.75

HYDROGRAPH AT	B	.02	1	27.	36.	43.	51.	59.	67.
+				12.00	12.00	12.00	12.00	12.00	12.00

oout.txt

ROUTED TO	+	PONDB	.02	1	FLOW TIME	22. 12.25	30. 12.25	36. 12.25	43. 12.25	50. 12.25	56. 12.25
				**	PEAK STAGES IN FEET						
				1	STAGE	1376.26	1376.55	1376.77	1376.97	1377.18	1377.37
					TIME	12.25	12.25	12.25	12.25	12.25	12.25
ROUTED TO	+	RTE2	.02	1	FLOW TIME	22. 12.50	30. 12.50	36. 12.50	43. 12.50	50. 12.50	56. 12.50
HYDROGRAPH AT	+	C	.03	1	FLOW TIME	42. 12.00	57. 12.00	70. 12.00	82. 12.00	96. 12.00	108. 12.00
ROUTED TO	+	PONDC	.03	1	FLOW TIME	8. 12.75	13. 12.75	17. 12.75	20. 12.75	23. 12.75	26. 12.75
				**	PEAK STAGES IN FEET						
				1	STAGE	1373.43	1373.87	1374.22	1374.57	1374.96	1375.30
					TIME	12.75	12.75	12.75	12.75	12.75	12.75
ROUTED TO	+	RTE3	.03	1	FLOW TIME	8. 13.00	13. 13.00	17. 13.00	20. 13.00	23. 13.00	26. 13.00
HYDROGRAPH AT	+	D	.02	1	FLOW TIME	17. 12.00	23. 12.00	28. 12.00	33. 12.00	38. 12.00	43. 12.00
ROUTED TO	+	PONDD	.02	1	FLOW TIME	8. 12.50	11. 12.50	15. 12.50	18. 12.50	22. 12.50	26. 12.50
				**	PEAK STAGES IN FEET						
				1	STAGE	1366.13	1366.53	1366.81	1367.07	1367.36	1367.61
					TIME	12.50	12.50	12.50	12.50	12.50	12.50

\*\*\* NORMAL END OF HEC-1 \*\*\*

fout.txt

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1*****
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
ENGINEERS *
* JUN 1998
CENTER *
* VERSION 4.1
*
*
* RUN DATE 28SEP06 TIME 17:27:47
*
*
*****
*****

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*
* U.S. ARMY CORPS OF
* HYDROLOGIC ENGINEERING
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
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X X X

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

fout.txt  
 HEC-1 ANALYSIS FOR OAK CREEK W/ 2nd & 3RD ADDITION BASIN  
 PROPOSED CONDITIONS - DETENTION BASIN F ONLY  
 100-YEAR 24-HOUR STORM - POST DEVELOPMENT

1  
 2  
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\*\*\* LIST \*\*\*  
 \*\*\* FREE \*\*\*

\*DIAGRAM  
 IT 15 27SEP06 1200 0 28SEP06 2000  
 IN 15 27SEP06 1200  
 IO 0 4  
 JR PREC 3.5 4.5 7.8  
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 23

KK F  
 KO 5  
 BA 0.0330  
 PB 1.00  
 PC 0.000 0.003 0.006 0.008 0.011 0.014 0.017 0.019 0.022 0.02  
 PC 0.029 0.032 0.035 0.038 0.042 0.045 0.048 0.052 0.056 0.06  
 PC 0.064 0.068 0.072 0.076 0.080 0.085 0.090 0.095 0.100 0.10  
 PC 0.110 0.115 0.120 0.127 0.134 0.140 0.147 0.155 0.163 0.17  
 PC 0.181 0.193 0.204 0.220 0.235 0.259 0.283 0.387 0.663 0.69  
 PC 0.735 0.754 0.772 0.786 0.799 0.810 0.820 0.828 0.835 0.84  
 PC 0.850 0.858 0.865 0.873 0.880 0.885 0.889 0.894 0.898 0.90  
 PC 0.907 0.912 0.916 0.921 0.925 0.929 0.934 0.938 0.943 0.94  
 PC 0.952 0.955 0.958 0.961 0.964 0.967 0.970 0.973 0.976 0.97  
 LS 0 85  
 UD 0.250 20  
 \*  
 \*

24  
 25  
 26  
 27  
 28  
 29  
 30  
 31  
 32

KK PONDF 5  
 KO 1  
 RS 1  
 SA 0.42 ELEV 1370.5  
 SE 1370.5 1371.0 1372.0 1374.0 1375.0 1.00  
 SQ 0 5.0 10.0 15.0 20.0 25.0 30.0 35.0 40.0 45.0  
 SQ 60.0 65.0  
 SE 1370.5 1370.60 1370.66 1370.74 1370.92 1371.16 1371.45 1371.80 1372.20 1372.65  
 SE 1373.5 1374.77  
 \*  
 \*  
 \*  
 ZZ

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

8 F  
 V  
 V  
 24 PONDF

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION  
 \*\*\*\*\*  
 \*\*\*\*\*  
 \*\*\*\*\*

\* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* ENGINEERS \*  
 \* JUN 1998 \*  
 \* CENTER \*  
 \* VERSION 4.1 \*  
 \* \*  
 \* \*  
 \* RUN DATE 28SEP06 TIME 17:27:47 \*  
 \* \*  
 \* \*  
 \*\*\*\*\*  
 \*\*\*\*\*

\* U.S. ARMY CORPS OF  
 \* HYDROLOGIC ENGINEERING  
 \* 609 SECOND STREET  
 \* DAVIS, CALIFORNIA 95616  
 \* (916) 756-1104  
 \*

HEC-1 ANALYSIS FOR OAK CREEK W/ 2nd & 3RD ADDITION BASIN  
 PROPOSED CONDITIONS - DETENTION BASIN F ONLY  
 100-YEAR 24-HOUR STORM - POST DEVELOPMENT

6 IO OUTPUT CONTROL VARIABLES  
 IPRINT 0 PRINT CONTROL  
 IPLOT 4 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 15 MINUTES IN COMPUTATION INTERVAL  
 IDATE 27SEP 6 STARTING DATE  
 ITIME 1200 STARTING TIME

fout.txt  
NUMBER OF HYDROGRAPH ORDINATES

NQ 129  
NDDATE 28SEP 6  
NDTIME 2000  
ICENT 19

COMPUTATION INTERVAL .25 HOURS  
TOTAL TIME BASE 32.00 HOURS

ENGLISH UNITS  
DRAINAGE AREA SQUARE MILES  
PRECIPITATION DEPTH INCHES  
LENGTH, ELEVATION FEET  
FLOW CUBIC FEET PER SECOND  
STORAGE VOLUME ACRE-FEET  
SURFACE AREA ACRES  
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION 1 NUMBER OF PLANS  
NPLAN

JR MULTI-RATIO OPTION  
RATIOS OF PRECIPITATION  
3.50 4.50 7.80

\*\*\* \*\*

\*\*\*\*\*  
\*  
\* F \*  
\* \*  
\*\*\*\*\*

8 KK

9 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 4 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

\*\*\*\*\*

fout.txt

\*  
\* POND F  
\*  
\*\*\*\*\*

24 KK

25 KO

OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 4 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
TIME TO PEAK IN HOURS

RATIOS APPLIED TO PRECIPITATION  
RATIO 1 RATIO 2 RATIO 3  
3.50 4.50 7.80

OPERATION STATION AREA PLAN

HYDROGRAPH AT

+ F .03 1 32. 46. 90.  
12.00 12.00 12.00

ROUTED TO

+ POND F .03 1 28. 35. 60.  
12.25 12.25 12.50

\*\* PEAK STAGES IN FEET \*\*  
1 STAGE 1371.31 1371.82 1373.56  
TIME 12.25 12.25 12.50

\*\*\* NORMAL END OF HEC-1 \*\*\*

gout.txt

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
ENGINEERS *
* JUN 1998
CENTER *
, * VERSION 4.1
*
*
* RUN DATE 28SEP06 TIME 15:23:55
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*
* U.S. ARMY CORPS OF
* HYDROLOGIC ENGINEERING
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*

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X X XXXXXXXX XXXXX X
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X X X X X X
XXXXXXX XXXX X
X X X X X X
X X X X X X
X X XXXXXXXX XXXXX
X X X XXXX XXXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

GOUT.TXT  
 HEC-1 ANALYSIS FOR OAK CREEK W/ 2nd & 3RD ADDITION BASIN  
 PROPOSED CONDITIONS - DETENTION BASIN G ONLY  
 100-YEAR STORM - POST DEVELOPMENT

ID	DIAGRAM	15 27SEP06	1200	0 28SEP06	2000	0.017	0.019	0.022	0.025
IT	15	27SEP06	1200	0	28SEP06	2000	0.017	0.019	0.022
IN	15	27SEP06	1200				0.052	0.056	0.060
IO	0	5					0.095	0.100	0.105
JR	PREC	3.5	4.5	5.3	6.1	7.0	0.155	0.163	0.172
*							0.387	0.663	0.699
*							0.828	0.835	0.843
*							0.894	0.898	0.903
KK	G						0.938	0.943	0.947
KO	5						0.973	0.976	0.979
BA	0.0580						1.000		
PB	1.00								
PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.022	0.025
PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056
PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100
PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163
PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.699
PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.835	0.843
PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.903
PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.947
PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.979
PC	0.982	0.985	0.988	0.991	0.994	0.997			
LS	0	85	46						
UD	0.250								
*									
*									
ZZ									

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

8 G

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

1 \*\*\*\*\*  
 \*\*\*\*\*  
 \*\*\*\*\*

\* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*

\* U.S. ARMY CORPS OF

gout.txt

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ENGINEERS * JUN 1998 *
* CENTER * VERSION 4.1 *
* * *
* * *
* RUN DATE 28SEP06 TIME 15:23:55 *
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* HYDROLOGIC ENGINEERING
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*

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HEC-1 ANALYSIS FOR OAK CREEK W/ 2nd & 3RD ADDITION BASIN  
 PROPOSED CONDITIONS - DETENTION BASIN G ONLY  
 100-YEAR STORM - POST DEVELOPMENT

```

6 IO OUTPUT CONTROL VARIABLES
IPRNT 0 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

```

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IT HYDROGRAPH TIME DATA
NMIN 15 MINUTES IN COMPUTATION INTERVAL
IDATE 27SEP 6 STARTING DATE
ITIME 1200 STARTING TIME
NQ 129 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 28SEP 6 ENDING DATE
NDTIME 2000 ENDING TIME
ICENT 19 CENTURY MARK

```

```

COMPUTATION INTERVAL .25 HOURS
TOTAL TIME BASE 32.00 HOURS

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ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

```

gout.txt

JP MULTI-PLAN OPTION  
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION  
RATIOS OF PRECIPITATION  
3.50 4.50 5.30 6.10 7.00 7.80

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\*  
\* G \*  
\* \* \*  
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9 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION					
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6
HYDROGRAPH AT	G	.06	1	64.	87.	106.	125.	146.	165.
+				12.00	12.00	12.00	12.00	12.00	12.00
				3.50	4.50	5.30	6.10	7.00	7.80

\*\*\* NORMAL END OF HEC-1 \*\*\*



hout.txt  
 HEC-1 ANALYSIS FOR OAK CREEK W/ 2nd & 3RD ADDITION BASIN  
 PROPOSED CONDITIONS - DETENTION BASIN H ONLY  
 100-YEAR STORM - POST DEVELOPMENT

1  
 2  
 3

\*\*\* LIST \*\*\*  
 \*\*\* FREE \*\*\*

ID	DIAGRAM	15 27SEP06	1200	0 28SEP06	2000	0.017	0.019	0.022	0.025
4	IT	15 27SEP06	1200	0 28SEP06	2000	0.017	0.019	0.022	0.025
5	IN	15 27SEP06	1200			0.048	0.052	0.056	0.060
6	IO	0				0.090	0.095	0.100	0.105
7	JR	PREC 3.5	4.5	5.3	6.1	7.0	7.8		
*									
*									
*									
*									
8	KK	H				0.014	0.017	0.019	0.022
9	KO	5				0.045	0.048	0.052	0.056
10	BA	0.0544				0.085	0.090	0.095	0.100
11	PB	1.00				0.140	0.147	0.155	0.163
12	PC	0.000	0.003	0.008	0.011	0.014	0.017	0.019	0.022
13	PC	0.029	0.032	0.038	0.042	0.045	0.048	0.052	0.056
14	PC	0.064	0.068	0.076	0.080	0.085	0.090	0.095	0.100
15	PC	0.110	0.115	0.127	0.134	0.140	0.147	0.155	0.163
16	PC	0.181	0.193	0.220	0.235	0.259	0.283	0.387	0.699
17	PC	0.735	0.754	0.786	0.799	0.810	0.820	0.828	0.835
18	PC	0.850	0.858	0.873	0.880	0.885	0.889	0.894	0.898
19	PC	0.907	0.912	0.925	0.925	0.929	0.934	0.938	0.947
20	PC	0.952	0.955	0.961	0.964	0.967	0.970	0.973	0.979
21	PC	0.982	0.985	0.991	0.994	0.997	1.000		
22	L5	0	85						
23	UD	0.300	45						

ID	DIAGRAM	18	24	30	36	42	48	54
24	KK							
25	KO							
26	RS	1						
27	SA	0.50	ELEV					
28	SE	1365.0	2.00					
29	SQ	0	1366.0	6	12	18	24	30
30	SQ	60						
31	SE	1364.5	1365.88	1366.92	1368.55	1370.78	1375.05	1375.17
32	SE	1375.5	1375.5	1375.5	1375.5	1375.5	1375.5	1375.5
*								
*								
*								

33 ZZ

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

8 H  
 V  
 V  
 24 PONDH

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

1\*\*\*\*\*

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\* U.S. ARMY CORPS OF  
 \* HYDROLOGIC ENGINEERING  
 \* 609 SECOND STREET  
 \* DAVIS, CALIFORNIA 95616  
 \* (916) 756-1104  
 \*

HEC-1 ANALYSIS FOR OAK CREEK W/ 2nd & 3RD ADDITION BASIN  
 PROPOSED CONDITIONS - DETENTION BASIN H ONLY  
 100-YEAR STORM - POST DEVELOPMENT

6 IO OUTPUT CONTROL VARIABLES  
 IPRNT 0 PRINT CONTROL  
 IPLOT 5 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA 15 MINUTES IN COMPUTATION INTERVAL  
 NMIN



hout.txt

\*\*\*\*\*  
\*  
\* PONDH \*  
\*  
\*\*\*\*\*

24 KK

25 KO

OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION					
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6
				3.50	4.50	5.30	6.10	7.00	7.80
HYDROGRAPH AT	H	.05	1	60.	81.	98.	115.	134.	151.
+				12.25	12.25	12.25	12.25	12.25	12.25
ROUTED TO	PONDH	.05	1	12.	14.	16.	18.	20.	21.
+				13.00	13.25	13.25	13.25	13.25	13.25
			** PEAK STAGES IN FEET **						
	1	1366.96	1367.58	1368.10	1368.62	1369.17	1369.66		
		13.00	13.25	13.25	13.25	13.25	13.25		

\*\*\* NORMAL END OF HEC-1 \*\*\*

## Time of concentration (Tc) or travel time (Tt)

Project : Oak Creek Addition - Basin A  
 Location : Wichita, Kansas

By: SB  
 Checked: \_\_\_\_\_

Date: 9/8/2008  
 Date: \_\_\_\_\_

Circle One:  Present  Developed

Circle One:  Tc  Tt through subarea

NOTES: Space for as many as two segments per flow type can be used for each worksheet.  
 Include map, schematic, or description of flow segments.

### Sheet flow (Applicable to Tc only)

1. Surface description (Table 3-1)
2. Mannings roughness coeff., n (Table 3-1)
3. Flow length, L (total L < 300 ft.)
4. Two-yr 24-hr rainfall, P2
5. Calculated Land slope, s
- 5a. Land Elevation For Upper End Of Flow Path
- 5b. Land Elevation For Lower End Of Flow Path
6. Compute Tt

Segment ID

AB	
Short Grass	
	0.15
ft	300
in	3.60
ft/ft	0.013
	1400.0
	1396.0
hr	0.44

= 0.44

### Shallow concentrated flow

7. Surface description (Paved or Unpaved)
8. Flow length, L
9. Calculated Watercourse slope, s
- 9a. Land Elevation For Upper End Of Flow Path
- 9b. Land Elevation For Lower End Of Flow Path
10. Average velocity, V (Figure 3-1)
11.  $Tt = L/3600V$  Compute Tt

Segment ID

BC	
Unpaved	
	944
ft/ft	0.013
	1396.0
	1383.5
ft/s	1.86
hr	0.14

= 0.14

### Channel Flow

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius,  $r = a/Pw$  Compute r
15. Channel slope, s
16. Manning's roughness coeff., n
17.  $V = 1.49(r^{0.667})(s^{0.50})/n$  Compute V
18. Flow length, L
19.  $Tt = L/3600V$  Compute Tt
20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19)

Segment ID

CD	
sf	30.00
ft	19
ft	1.579
ft/ft	0.010
	0.041
ft/s	4.9
ft	1000
hr	0.058

= 0.06  
 hr 0.63

Reference: Urban Hydrology for Small Watersheds  
 Technical Release 55, Soil Conservation Service  
 U.S. Department of Agriculture, June 1986

Use Time Of Concentration =

38 Minutes

### Time of concentration (Tc) or travel time (Tt)

Project : Oak Creek Addition - Basin B  
 Location : Wichita, Kansas

By: SB Date: 9/8/2006  
 Checked: \_\_\_\_\_ Date: \_\_\_\_\_

Circle One:  Present  Developed

Circle One:  Tc  Tt through subarea

NOTES: Space for as many as two segments per flow type can be used for each worksheet.  
 Include map, schematic, or description of flow segments.

**Sheet flow** (Applicable to Tc only)

1. Surface description (Table 3-1)
2. Mannings roughness coeff., n (Table 3-1)
3. Flow length, L (total L < 300 ft.)
4. Two-yr 24-hr rainfall, P2
5. Calculated Land slope, s
- 5a. Land Elevation For Upper End Of Flow Path
- 5b. Land Elevation For Lower End Of Flow Path
6. Compute Tt

Segment ID

<b>AB</b>	
Short Grass	
	0.15
ft	300
in	3.60
ft/ft	0.023
	1380.3
	1373.5
hr	0.35

= 0.35

**Shallow concentrated flow**

7. Surface description (Paved or Unpaved)
8. Flow length, L
9. Calculated Watercourse slope, s
- 9a. Land Elevation For Upper End Of Flow Path
- 9b. Land Elevation For Lower End Of Flow Path
10. Average velocity, V (Figure 3-1)
11.  $Tt = L/3600V$  Compute Tt

Segment ID

<b>BC</b>	
Unpaved	
	793
ft	793
ft/ft	0.018
	1373.5
	1359.0
ft/s	2.18
hr	0.10

= 0.10

**Channel Flow**

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a/Pw Compute r
15. Channel slope, s
16. Manning's roughness coeff., n
17.  $V = 1.49(r^{0.667})(s^{0.50})/n$  Compute V
18. Flow length, L
19.  $Tt = L/3600V$  Compute Tt
20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19)

Segment ID

<b>CD</b>	
sf	25.00
ft	14
ft	1.788
ft/ft	0.002
	0.041
ft/s	2.4
ft	2875
hr	0.334

= 0.33  
 hr 0.79

Reference: Urban Hydrology for Small Watersheds  
 Technical Release 55, Soil Conservation Service  
 U.S. Department of Agriculture, June 1988

Use Time Of Concentration =

47 Minutes

### Time of concentration (Tc) or travel time (Tt)

Project : Oak Creek Addition - Basin C  
 Location : Wichita, Kansas

By: SB Date: 9/8/2006  
 Checked: \_\_\_\_\_ Date: \_\_\_\_\_

Circle One:  Present  Developed

Circle One:  Tc  Tt through subarea

NOTES: Space for as many as two segments per flow type can be used for each worksheet.  
 Include map, schematic, or description of flow segments.

**Sheet flow** (Applicable to Tc only)

1. Surface description (Table 3-1)
2. Mannings roughness coeff., n (Table 3-1)
3. Flow length, L (total L < 300 ft.)
4. Two-yr 24-hr rainfall, P2
5. Calculated Land slope, s
- 5a. Land Elevation For Upper End Of Flow Path
- 5b. Land Elevation For Lower End Of Flow Path
6. Compute Tt

Segment ID

AB	
Short Grass	
	0.15
ft	300
in	3.60
ft/ft	0.008
	1399.6
	1397.4
hr	0.55
=	0.55

**Shallow concentrated flow**

7. Surface description (Paved or Unpaved)
8. Flow length, L
9. Calculated Watercourse slope, s
- 9a. Land Elevation For Upper End Of Flow Path
- 9b. Land Elevation For Lower End Of Flow Path
10. Average velocity, V (Figure 3-1)
11. Tt = L/3600V Compute Tt

Segment ID

BC	
Unpaved	
	697
ft/ft	0.015
	1397.4
	1387.0
ft/s	1.97
hr	0.10
=	0.10

**Channel Flow**

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a/Pw Compute r
15. Channel slope, s
16. Manning's roughness coeff., n
17.  $V = 1.49(r^{0.667})(s^{0.50})/n$  Compute V
18. Flow length, L
19. Tt = L/3600V Compute Tt
20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19)

Segment ID

sf	
ft	
ft	
ft/ft	
ft/s	
ft	
hr	
=	0.00
hr	0.65

Reference: Urban Hydrology for Small Watersheds  
 Technical Release 55, Soil Conservation Service  
 U.S. Department of Agriculture, June 1986

Use Time Of Concentration =

39 Minutes

### Time of concentration (Tc) or travel time (Tt)

Project : Oak Creek Addition - Basin D  
 Location : Wichita, Kansas

By: SB Date: 9/8/2006  
 Checked: \_\_\_\_\_ Date: \_\_\_\_\_

Circle One:  Present  Developed

Circle One:  Tc  Tt through subarea

NOTES: Space for as many as two segments per flow type can be used for each worksheet.  
 Include map, schematic, or description of flow segments.

**Sheet flow** (Applicable to Tc only)

1. Surface description (Table 3-1)
2. Mannings roughness coeff., n (Table 3-1)
3. Flow length, L (total L < 300 ft.)
4. Two-yr 24-hr rainfall, P2
5. Calculated Land slope, s
- 5a. Land Elevation For Upper End Of Flow Path
- 5b. Land Elevation For Lower End Of Flow Path
6. Compute Tt

Segment ID

AB	
Short Grass	
	0.15
ft	300
in	3.80
ft/ft	0.005
	1400.0
	1398.5
hr	0.65

=

**Shallow concentrated flow**

7. Surface description (Paved or Unpaved)
8. Flow length, L
9. Calculated Watercourse slope, s
- 9a. Land Elevation For Upper End Of Flow Path
- 9b. Land Elevation For Lower End Of Flow Path
10. Average velocity, V (Figure 3-1)
11. Tt = L/3600V Compute Tt

Segment ID

BC	
Unpaved	
	1175
ft	1175
ft/ft	0.007
	1398.5
	1390.0
ft/s	1.37
hr	0.24

=

**Channel Flow**

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a/Pw Compute r
15. Channel slope, s
16. Manning's roughness coeff., n
17. V = 1.49(r<sup>0.667</sup>)(s<sup>0.50</sup>)/n Compute V
18. Flow length, L
19. Tt = L/3600V Compute Tt
20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19)

Segment ID

CD	
sf	150.00
ft	70
ft	2.143
ft/ft	0.004
	0.041
ft/s	3.8
ft	2025
hr	0.147

=   
 hr

Reference: Urban Hydrology for Small Watersheds  
 Technical Release 55, Soil Conservation Service  
 U.S. Department of Agriculture, June 1986

Use Time Of Concentration =

62 Minutes



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 www.pec1.com • designers@pec1.com

Project OAT CREEK 3<sup>rd</sup> ADDITION Date 9/28/06  
 Item STORM WATER Calcs. By STB

PIPE/ORIFICE SIZES TO MEET 2.5 yr. Storm Events.

POND D:

Will cut  $Q_2$  From 8 cfs to 5 cfs

$$Q = 0.6 A [(2)(g)(4 - \frac{D}{2})]^{\frac{1}{2}}$$

$$5 = 0.6 (\frac{1}{4} D^2) [64.4 (4 - \frac{D}{2})]^{\frac{1}{2}}$$

$$D = 0.517 \text{ ft. or } 6.2''$$

USE 6" orifice

Will use SAME orifice for 5 yr. storm also  $Q_5 = 5 \text{ cfs}$ .

POND H:

Will cut  $Q_2$  &  $Q_5$  From 10 & 13 to  $Q = 5 \text{ cfs}$

SAME AS ABOVE  $D = 6''$

POND F:

Will cut  $Q_2$  from 28 cfs to 1 cfs and  $Q_5$  from 35 cfs to 25 cfs

$$Q_2 = 10 \text{ cfs}$$

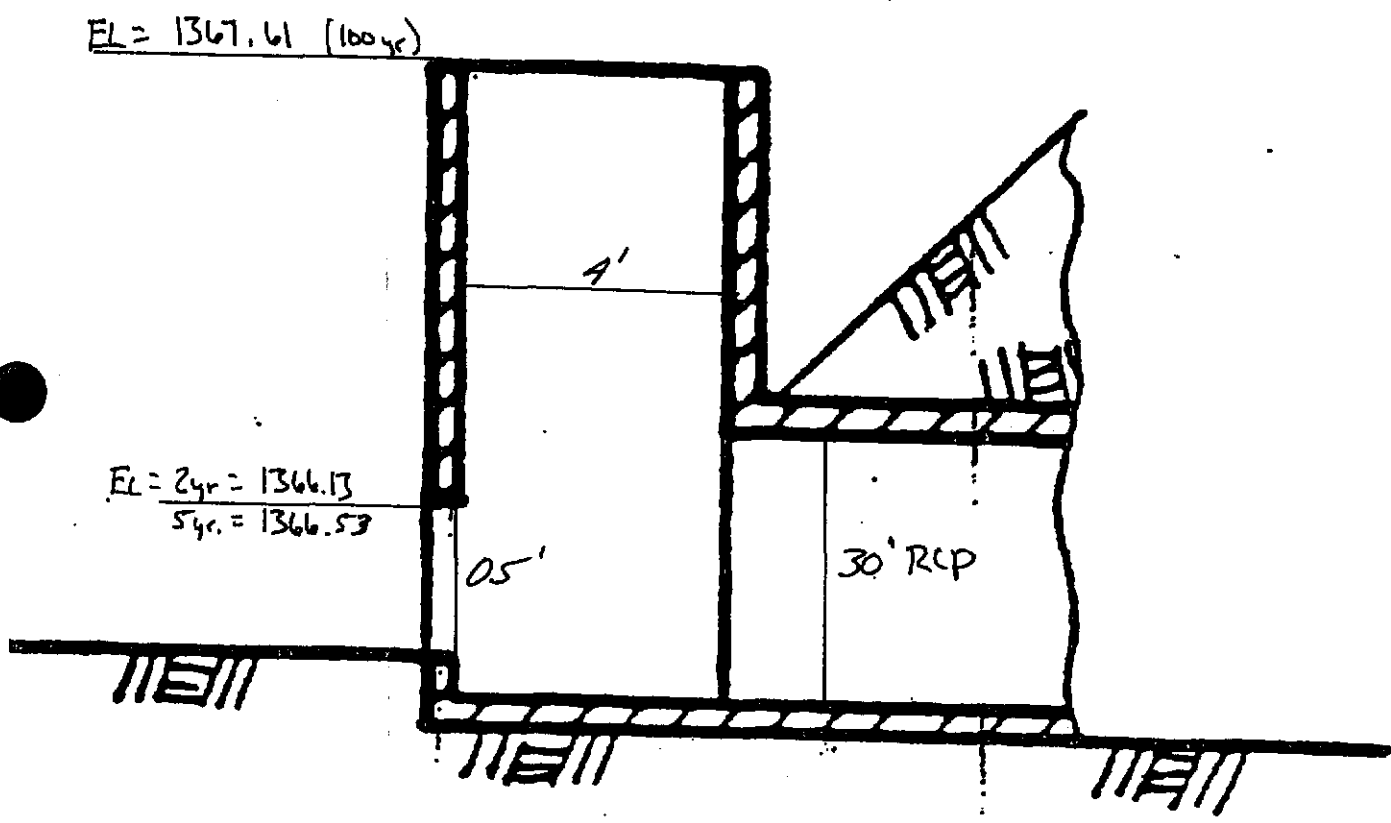
$$Q_5 = 25 \text{ cfs}$$

$$Q_2 = 0.6 A [(2)(g)(4 - \frac{D}{2})]^{\frac{1}{2}}$$

$$D_2 = 0.568' = 7''$$

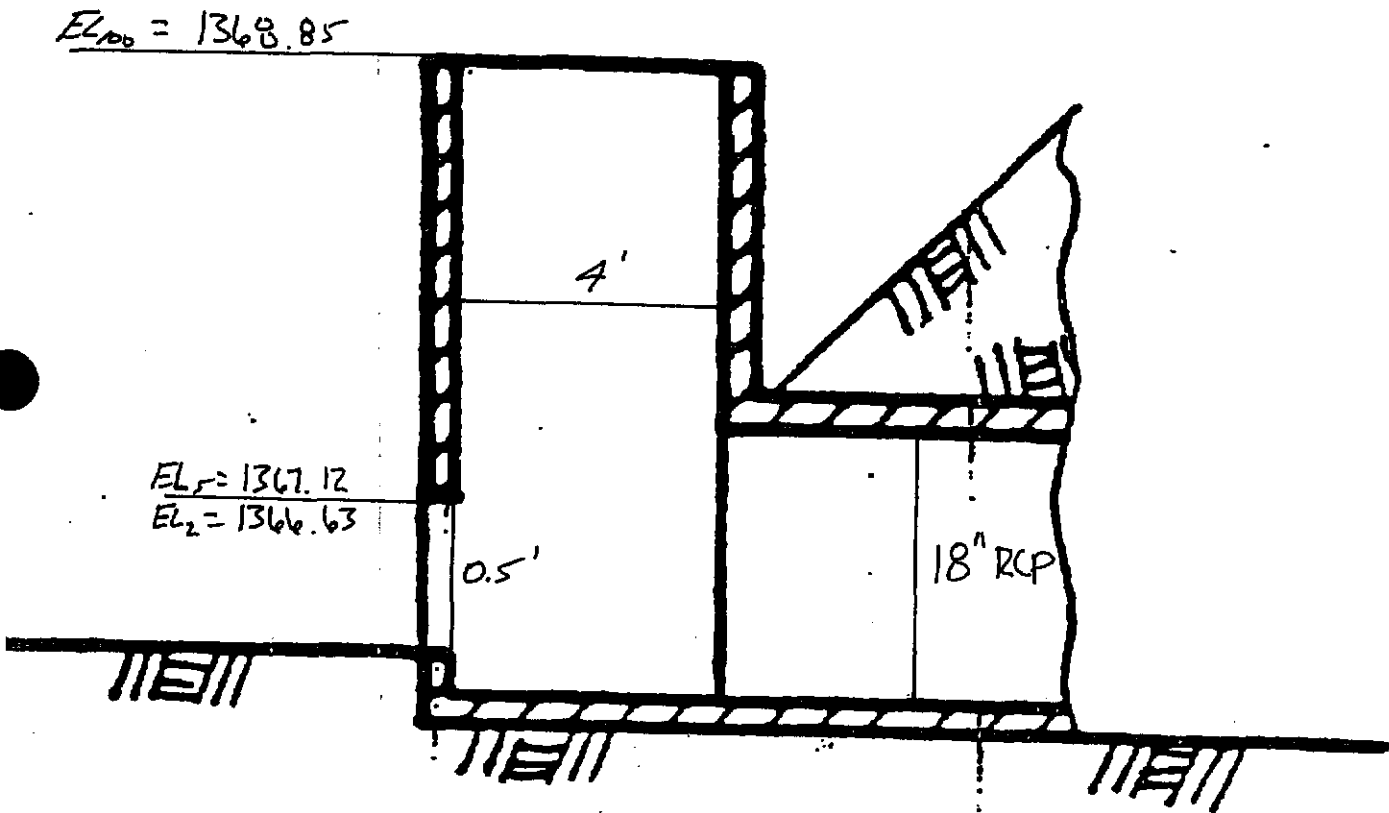
$Q_5 = 11$  Additional cfs

$$D = 0.60 \text{ or } 7''$$



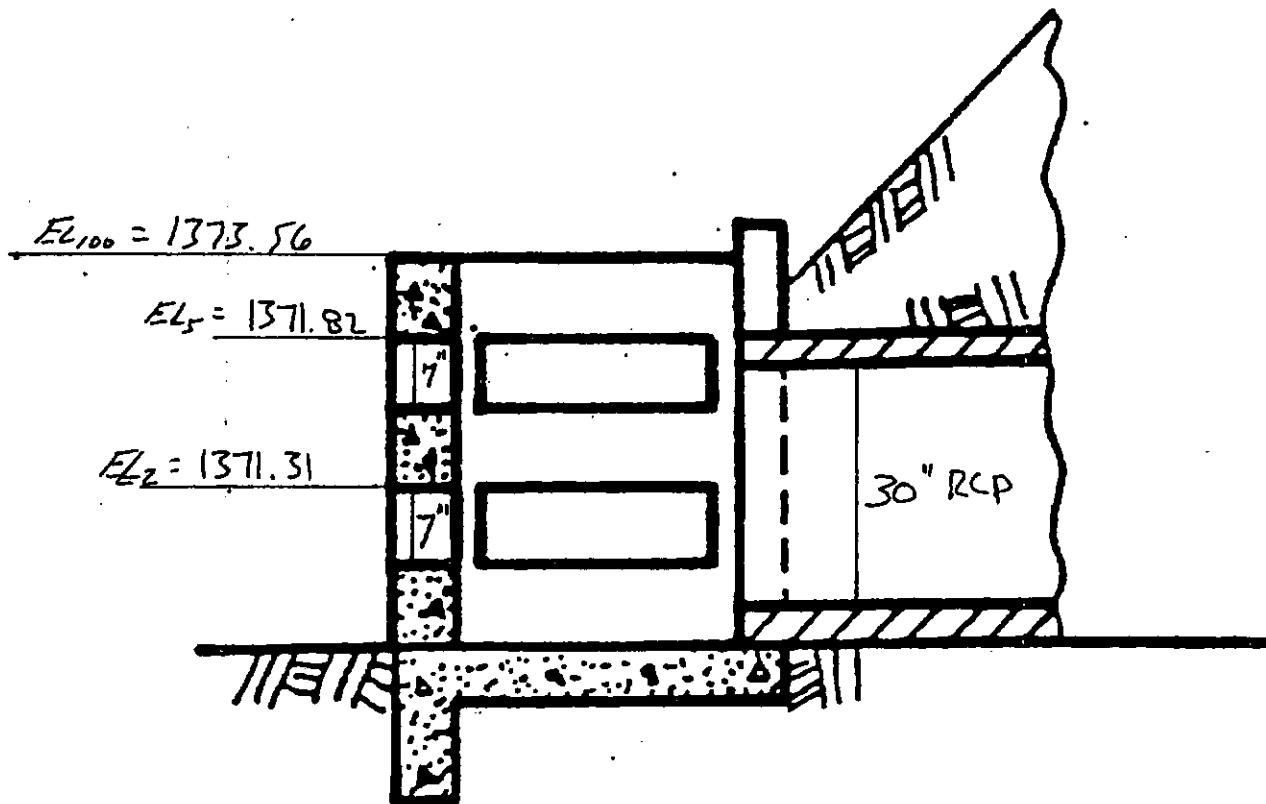
**SINGLE STAGE RISER**

POND "D" DRAINAGE OUTFALL STRUCTURE



# SINGLE STAGE RISER

POND "H" DRAINAGE OUTFALL STRUCTURE



**MULTIPLE STAGE CONCRETE INLET**

POND "F" DRAINAGE OUTFALL STRUCTURE

9/11/06

TONAS KUTUP PIPE SIZE:

1/2

Basin A

$$A = 1.02 \text{ AC}$$

$$t_c = 15 \text{ min}$$

$$i_c = 3.83 \text{ in}$$

$$C = \frac{(0.62)(0.98) + (0.40)(0.25)}{1.02}$$

$$C = 0.694$$

$$Q_c = (0.694)(3.83 \text{ in})(1.02 \text{ AC}) = \underline{\underline{2.71 \text{ cfs}}}$$

Basin B

$$A = 0.91 \text{ AC}$$

$$t_c = 15 \text{ min}$$

$$i_c = 3.83 \text{ in}$$

$$C = \frac{(0.60)(0.98) + (0.71)(0.25)}{0.91} = 0.731$$

$$Q_c = (0.731)(3.83 \text{ in})(0.91 \text{ AC}) = 2.55 \text{ cfs}$$

3/11/06

21

Basin D

$$A = 0.16 \text{ ac}$$

$$T_p = 10 \text{ min}$$

$$i_2 = 4.52 \text{ in}$$

$$C = \frac{(0.082)(0.9^\circ) + (0.078)(0.25)}{0.16} = 0.624$$

$$Q_2 = (0.16)(0.624)(4.52) = 0.45 \text{ cfs}$$

Size of pipe:

manhole fec:  $Q = \frac{1.49}{n} A R^{4/3} S^{1/2}$

$$Q = (1)(124.166)(2.14 r^2)(.5 r)^{4/3}(.1)$$

$$Q = 2.71$$

$$n = 0.012$$

$$A = \pi r^2$$

$$S = 1\%$$

$$R = \frac{A}{P}$$

$$P = 2\pi r$$

$$r = 0.476' \text{ or } D = 0.872' = 10.5''$$

Use  $D = 15''$  on all systems.

CURRENT DATE: 09-18-2006  
CURRENT TIME: 10:39:24

FILE DATE: 09-18-2006  
FILE NAME: OAK3P

```

AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
UAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
* C *                               *                               *
* U *                               *                               *
* L * INLET   OUTLET  CULVERT * BARRELS *
* V * ELEV.   ELEV.  LENGTH * SHAPE    * SPAN   RISE  MANNING  INLET *
* NO. * (ft)   (ft)   (ft)  * MATERIAL * (ft)   (ft)   n      TYPE  *
* 1 * 1372.00 1362.00 410.12 * 1 RCP  * 2.00   2.00  .012  CONVENTIONAL *
* 2 *                               *                               *
* 3 *                               *                               *
* 4 *                               *                               *
* 5 *                               *                               *
* 6 *                               *                               *
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAU

```

AA  
SUMMARY OF CULVERT FLOWS (cfs) FILE: OAK3P DATE: 09-18-2006

ELEV (ft)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
1372.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	1
1373.61	10.0	10.0	0.0	0.0	0.0	0.0	0.0	0.00	1
1374.59	20.0	20.0	0.0	0.0	0.0	0.0	0.0	0.00	1
1375.20	30.0	24.9	0.0	0.0	0.0	0.0	0.0	4.98	6
1375.39	40.0	26.3	0.0	0.0	0.0	0.0	0.0	13.47	4
1375.54	50.0	27.4	0.0	0.0	0.0	0.0	0.0	22.48	4
1375.68	60.0	28.3	0.0	0.0	0.0	0.0	0.0	31.26	3
1375.81	70.0	29.1	0.0	0.0	0.0	0.0	0.0	40.46	3
1375.93	80.0	29.9	0.0	0.0	0.0	0.0	0.0	49.79	3
1376.04	90.0	30.6	0.0	0.0	0.0	0.0	0.0	59.13	3
1376.14	100.0	31.2	0.0	0.0	0.0	0.0	0.0	68.51	3
1375.00	23.4	23.4	0.0	0.0	0.0	0.0	0.0	OVERTOPPING	

AA  
SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: OAK3P DATE: 09-18-2006

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
1372.00	0.000	0.00	0.00	0.00
1373.61	0.000	10.00	0.00	0.00
1374.59	0.000	20.00	0.00	0.00
1375.20	-0.008	30.00	0.11	0.37
1375.39	-0.003	40.00	0.25	0.63
1375.54	-0.007	50.00	0.14	0.28
1375.68	-0.005	60.00	0.44	0.73
1375.81	-0.004	70.00	0.40	0.57
1375.93	-0.003	80.00	0.31	0.39
1376.04	-0.003	90.00	0.28	0.31
1376.14	-0.002	100.00	0.24	0.24

AA  
<1> TOLERANCE (ft) = 0.010 <2> TOLERANCE (%) = 1.000  
AA

CURRENT TIME: 10:39:24

FILE NAME: OAK3P

PERFORMANCE CURVE FOR CULVERT 1 - 1( 2.00 (ft) BY 2.00 (ft)) RCP

Table with columns: DIS-CHARGE (cfs), HEAD-ELEV. (ft), INLET CONTROL DEPTH (ft), OUTLET CONTROL DEPTH (ft), FLOW TYPE <F4>, NORMAL DEPTH (ft), CRIT. DEPTH (ft), OUTLET DEPTH (ft), TW DEPTH (ft), OUTLET VEL. (fps), TW VEL. (fps). Rows show flow data from 0.00 to 31.24 cfs.

El. inlet face invert 1372.00 ft El. outlet invert 1362.00 ft
El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

\*\*\*\*\* SITE DATA \*\*\*\*\* CULVERT INVERT \*\*\*\*\*
INLET STATION 0.00 ft
INLET ELEVATION 1372.00 ft
OUTLET STATION 410.00 ft
OUTLET ELEVATION 1362.00 ft
NUMBER OF BARRELS 1
SLOPE (V/H) 0.0244
CULVERT LENGTH ALONG SLOPE 410.12 ft

\*\*\*\*\* CULVERT DATA SUMMARY \*\*\*\*\*
BARREL SHAPE CIRCULAR
BARREL DIAMETER 2.00 ft
BARREL MATERIAL CONCRETE
BARREL MANNING'S n 0.012
INLET TYPE CONVENTIONAL
INLET EDGE AND WALL BEVELED EDGE (1.5:1)
INLET DEPRESSION NONE

CURRENT DATE: 09-18-2006
CURRENT TIME: 10:39:24

FILE DATE: 09-18-2006
FILE NAME: OAK3P

TAILWATER

CONSTANT WATER SURFACE ELEVATION
0.00

ROADWAY OVERTOPPING DATA

WEIR COEFFICIENT

2.80



CURRENT DATE: 09-28-2006  
CURRENT TIME: 14:31:01

FILE DATE: 09-28-2006  
FILE NAME: OAKRET

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UAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
* C *                               * SITE DATA *                               * CULVERT SHAPE, MATERIAL, INLET *
* U *                               *                               *                               *
* L * INLET   OUTLET  CULVERT * BARRELS
* V * ELEV.   ELEV.  LENGTH * SHAPE      SPAN    RISE   MANNING  INLET
* NO.* (ft)   (ft)   (ft)   * MATERIAL  (ft)   (ft)   n        TYPE
* 1 * 1364.50 1364.25 35.00 * 1 RCP     1.50   1.50  .012    CONVENTIONAL
* 2 *
* 3 *
* 4 *
* 5 *
* 6 *
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAU

```

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AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
SUMMARY OF CULVERT FLOWS (cfs)          FILE: OAKRET          DATE: 09-28-2006

```

ELEV (ft)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
1364.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	1
1365.88	6.0	6.0	0.0	0.0	0.0	0.0	0.0	0.00	1
1366.92	12.0	12.0	0.0	0.0	0.0	0.0	0.0	0.00	1
1368.55	18.0	18.0	0.0	0.0	0.0	0.0	0.0	0.00	1
1370.78	24.0	24.0	0.0	0.0	0.0	0.0	0.0	0.00	1
1375.05	30.0	28.7	0.0	0.0	0.0	0.0	0.0	1.02	22
1375.17	36.0	28.8	0.0	0.0	0.0	0.0	0.0	6.99	6
1375.26	42.0	28.9	0.0	0.0	0.0	0.0	0.0	12.96	5
1375.33	48.0	28.9	0.0	0.0	0.0	0.0	0.0	18.78	4
1375.40	54.0	29.0	0.0	0.0	0.0	0.0	0.0	24.79	4
1375.46	60.0	29.0	0.0	0.0	0.0	0.0	0.0	30.39	3
1375.00	28.7	28.7	0.0	0.0	0.0	0.0	0.0	0.0	OVERTOPPING

```

AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
SUMMARY OF ITERATIVE SOLUTION ERRORS   FILE: OAKRET          DATE: 09-28-2006

```

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
1364.50	0.000	0.00	0.00	0.00
1365.88	0.000	6.00	0.00	0.00
1366.92	0.000	12.00	0.00	0.00
1368.55	0.000	18.00	0.00	0.00
1370.78	0.000	24.00	0.00	0.00
1375.05	-0.004	30.00	0.25	0.83
1375.17	-0.004	36.00	0.20	0.56
1375.26	-0.004	42.00	0.17	0.40
1375.33	-0.006	48.00	0.29	0.60
1375.40	-0.005	54.00	0.23	0.43
1375.46	-0.004	60.00	0.59	0.98

```

AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
<1> TOLERANCE (ft) = 0.010          <2> TOLERANCE (%) = 1.000
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA

```

OAKRET.LST

FILE NAME: OAKRET

CURRENT TIME: 14:31:01

PERFORMANCE CURVE FOR CULVERT 1 - 1( 1.50 (ft) BY 1.50 (ft)) RCP

Table with columns: DIS-CHARGE FLOW (cfs), HEAD-WATER ELEV. (ft), INLET CONTROL DEPTH (ft), OUTLET CONTROL DEPTH (ft), FLOW TYPE <F4>, NORMAL DEPTH (ft), CRIT. DEPTH (ft), OUTLET DEPTH (ft), TW DEPTH (ft), OUTLET VEL. (fps), TW VEL. (fps). Rows show flow rates from 0.00 to 29.02 cfs.

El. inlet face invert 1364.50 ft El. outlet invert 1364.25 ft
El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

\*\*\*\*\* SITE DATA \*\*\*\*\* CULVERT INVERT \*\*\*\*\*
INLET STATION 0.00 ft
INLET ELEVATION 1364.50 ft
OUTLET STATION 35.00 ft
OUTLET ELEVATION 1364.25 ft
NUMBER OF BARRELS 1
SLOPE (V/H) 0.0071
CULVERT LENGTH ALONG SLOPE 35.00 ft

\*\*\*\*\* CULVERT DATA SUMMARY \*\*\*\*\*
BARREL SHAPE CIRCULAR
BARREL DIAMETER 1.50 ft
BARREL MATERIAL CONCRETE
BARREL MANNING'S n 0.012
INLET TYPE CONVENTIONAL
INLET EDGE AND WALL BEVELED EDGE (1.5:1)
INLET DEPRESSION NONE

0 3

CURRENT DATE: 09-28-2006 FILE DATE: 09-28-2006
CURRENT TIME: 14:31:01 FILE NAME: OAKRET

TAILWATER

CONSTANT WATER SURFACE ELEVATION 0.00

ROADWAY OVERTOPPING DATA



## EXHIBIT NO. 1

## SOIL LEGEND

<u>SYMBOL</u>	<u>HYDROLOGIC GROUP</u>	<u>NAME</u>
Aa	B	Albion-Shellabarger sandy loams, 1 to 4 percent slopes
Ab	B	Albion and Shellabarger sandy loams; 7 to 15 percent slopes
Ba	C	Blanket silt loam, 0 to 1 percent slopes
Bb	C	Blanket silt loam, 1 to 3 percent slopes
Ca	B	Canadian fine sandy loam
Cb	B	Canadian-Waldeck fine sandy loams
Cc	D	Carwile fine sandy loam
Cd	B	Clark-Ost clay loams, 1 to 4 percent slopes
Ce	C	Clime silty clay, 3 to 6 percent slopes
Ea	B	Elandco silt loam
Eb	B	Elandco silt loam, occasionally flooded
Ec	B	Elandco silt loam, frequently flooded
Fa	B	Farnum loam, 0 to 1 percent slopes
Fb	B	Farnum loam, 1 to 3 percent slopes
Fc	B	Farnum loam, sandy substratum, 0 to 1 percent slopes
Ga	D	Goessel silty clay, 0 to 1 percent slopes
Gb	D	Goessel silty clay, 1 to 2 percent slopes
Ia	D	Irwin silty clay loam, 1 to 3 percent slopes
Ib	D	Irwin silty clay loam, 3 to 6 percent slopes
Ic	D	Irwin silty clay loam, 2 to 6 percent slopes, eroded
La	C	Lesho loam
Lb	A	Lincoln soils
Ma	B	Milan loam, 1 to 3 percent slopes
Mb	B	Milan form, 3 to 6 percent slopes
Mc	B	Milan clay loam, 2 to 6 percent slopes, eroded
Na	B	Naron fine sandy loam
Oc	D	Owens clay loam, 1 to 3 percent slopes
Od	D	Dwens-Rock outcrop complex, 3 to 10 percent slopes
Pa		Pits
Pb	D	Plevna fine sandy loam
Pc	A	Pratt loamy fine sand, undulating
Pd	A	Pratt-Tivoli complex, rolling
Ra	D	Renfrow silty clay loam, 1 to 3 percent slopes
Rb	D	Renfrow silty clay loam, 3 to 6 percent slopes
Rc	D	Renfrow-Owens clay loams, 1 to 4 percent slopes
Rd	D	Rosehill silty clay, 1 to 3 percent slopes
Sa	B	Shellabarger sandy loam, 1 to 3 percent slopes
Sb	B	Shellabarger sandy loam, 3 to 6 percent slopes
Sc	B	Shellabarger sandy loam, 3 to 6 percent slopes, eroded
Ta	D	Tabler silty clay loam
Tb	D	Tabler-Drummond complex
Ua	B	Urban land-Canadian complex
Ub	B	Urban land-Elandco complex
Uc	B	Urban land-Farnum complex, 0 to 3 percent slopes
Ud	D	Urban land-Irwin complex, 1 to 3 percent slopes
Ue	D	Urban land-Tabler complex
Ya	B	Vanoss silt loam, 0 to 1 percent slopes
Yb	B	Vanoss silt loam, 1 to 3 percent slopes
Yc	B	Vanoss silt loam, 3 to 6 percent slopes
Yd	B	Vanoss silt loam, 3 to 6 percent slopes, eroded
Ye	D	Vernon sandy loam, 1 to 3 percent slopes
Yf	D	Vernon sandy loam, 3 to 6 percent slopes
Wa	C	Waldeck sandy loam

(John sheet 28)

R 2 E



(John sheet 44) 1:250 000 FEET

KS-2-5.

County	Expected 24-hour Storm Rainfall in Inches						Normal Annual Precipitation Inches
	Storm Frequency in Years						
	100	50	25	10	5	2	
Pawnee	6.6	6.0	5.2	4.5	3.7	2.8	23.3
Phillips	6.0	5.5	4.8	4.1	3.4	2.5	23.6
Pottawatomie	7.5	6.6	5.9	5.1	4.3	3.4	33.6
Pratt	7.2	6.4	5.6	4.8	4.1	3.0	24.6
Rawlins	5.5	5.0	4.3	3.6	3.1	2.3	21.0
Reno	7.4	6.6	5.8	5.0	4.2	3.2	27.7
Republic	6.8	6.0	5.4	4.6	3.9	2.9	28.6
Rice	7.3	6.4	5.6	4.8	4.1	3.0	26.6
Riley	7.4	6.5	5.8	5.1	4.3	3.3	33.5
Rooks	6.1	5.7	4.9	4.1	3.4	2.5	23.9
Rush	6.5	5.9	5.0	4.3	3.6	2.7	23.3
Russell	6.7	5.9	5.2	4.4	3.7	2.8	26.8
Saline	7.3	6.4	5.7	4.9	4.1	3.1	28.4
Scott	5.7	5.3	4.5	3.8	3.2	2.4	20.2
Sedgwick	7.8	7.0	6.1	5.3	4.5	3.5	30.6
Seward	6.0	5.7	4.8	4.2	3.5	2.6	19.8
Shawnee	7.8	6.8	6.1	5.3	4.5	3.5	34.7
Sheridan	5.7	5.3	4.5	3.8	3.2	2.4	21.3
Sherman	5.3	4.8	4.2	3.5	3.0	2.2	16.7
Smith	6.3	5.7	5.0	4.2	3.5	2.6	24.4
Stafford	7.1	6.2	5.5	4.7	4.0	2.9	25.1
Stanton	5.6	5.2	4.5	3.8	3.2	2.4	15.8
Stevens	5.9	5.5	4.7	4.1	3.4	2.5	19.7
Sumner	8.0	7.1	6.2	5.4	4.6	3.6	34.0

$s\text{-slope} = \frac{3}{8} \sqrt{4} = 0.0375$

$z = \frac{1}{2} \text{slope} = \frac{1}{2} \times 0.0375 = 0.01875$

$n = 0.016$

$\frac{z}{n} = \frac{0.01875}{0.016} = 1.17$   
always



EQUATION OF DAY (1)  $Q = 1.49 A R^{2/3} S^{1/2}$   
 R IS ROUNDED OFFICIENT IN CHOOSING FORMULA APPROPRIATE TO MATERIAL IN BOTTOM OF CHANNEL  
 S IS HORIZONTAL OF SLOPE  
 REFERENCE: U.S.S. PROCEEDINGS 1944, PAGE 60, EQUATION 604

**EXAMPLE (SEE INSTRUCTION 1)**

RIVER:  $B = 400$   
 $s = .02$   
 $n = .02$   $z/n = 1.17$   
 $d = 1.0$   
 FIND:  $Q =$  SIZE OF FLOWING CHANNEL

RATIO  $z/n$

10000  
9000  
8000  
7000  
6000  
5000  
4000  
3000  
2000

1000  
900  
800  
700  
600  
500  
400  
300  
200  
100  
90  
80  
70  
60  
50  
40  
30  
20  
10

TURNING LINE

DISCHARGE (Q) IN CFS

1000  
900  
800  
700  
600  
500  
400  
300  
200  
100  
90  
80  
70  
60  
50  
40  
30  
20  
10

SLOPE OF CHANNEL (S) IN FT./FT.

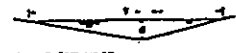
0.10  
0.08  
0.07  
0.06  
0.05  
0.04  
0.03  
0.02  
0.01

DEPTH AT CURB OR DEEPEST POINT (d) IN FT.

1.0  
0.9  
0.8  
0.7  
0.6  
0.5  
0.4  
0.3  
0.2  
0.1

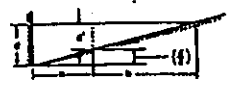
**INSTRUCTIONS**

1. CONNECT  $z/n$  RATIO WITH SLOPE (S) AND CONNECT DISCHARGE (Q) WITH POINT WHERE LINE CROSSES TURNING LINE. DEPTH AT CURB (d) CAN BE FOUND FROM Q BY CONNECTING Q WITH CROSSING OF TURNING LINE

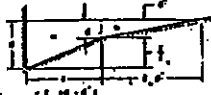


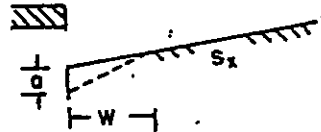
2. FOR SHALLOW "V-SHAPED" CHANNEL AS SHOWN USE NOMOGRAPH AS EXPLAINED IN INSTRUCTION 1 BUT WITH  $z = \frac{1}{2} s$

3. TO DETERMINE DISCHARGE  $Q_1$  IN PORTION OF CHANNEL HAVING WIDTH  $B_1$  DETERMINE DEPTH  $d$  FOR TOTAL DISCHARGE IN ENTIRE SECTION AS EXPLAINED IN THIS NOMOGRAPH TO DETERMINE  $Q_2$  IN SECTION OF WIDTH  $B_2$  FOR DEPTH  $d = d_1 \left( \frac{B_1}{B_2} \right)^{3/2}$  THEN  $Q_1 = Q_2 \left( \frac{B_1}{B_2} \right)^{3/2}$



4. TO DETERMINE DISCHARGE  $Q_1$  IN COMPOSITE SECTION: FOLLOW INSTRUCTION 3 TO OBTAIN DISCHARGE  $Q_2$  IN SECTION  $n_2$  AT DETERMINED DEPTH  $d$  BASED ON AN EXTENSION OF SLOPE RATIO  $s_2$  TO INTERSECT WATER SURFACE; OBTAIN  $Q_3$  FOR SLOPE RATIO  $s_1$  AND DEPTH  $d'$ ;  $d' = d \frac{s_2}{s_1}$  THEN  $Q_1 = Q_2 + Q_3$

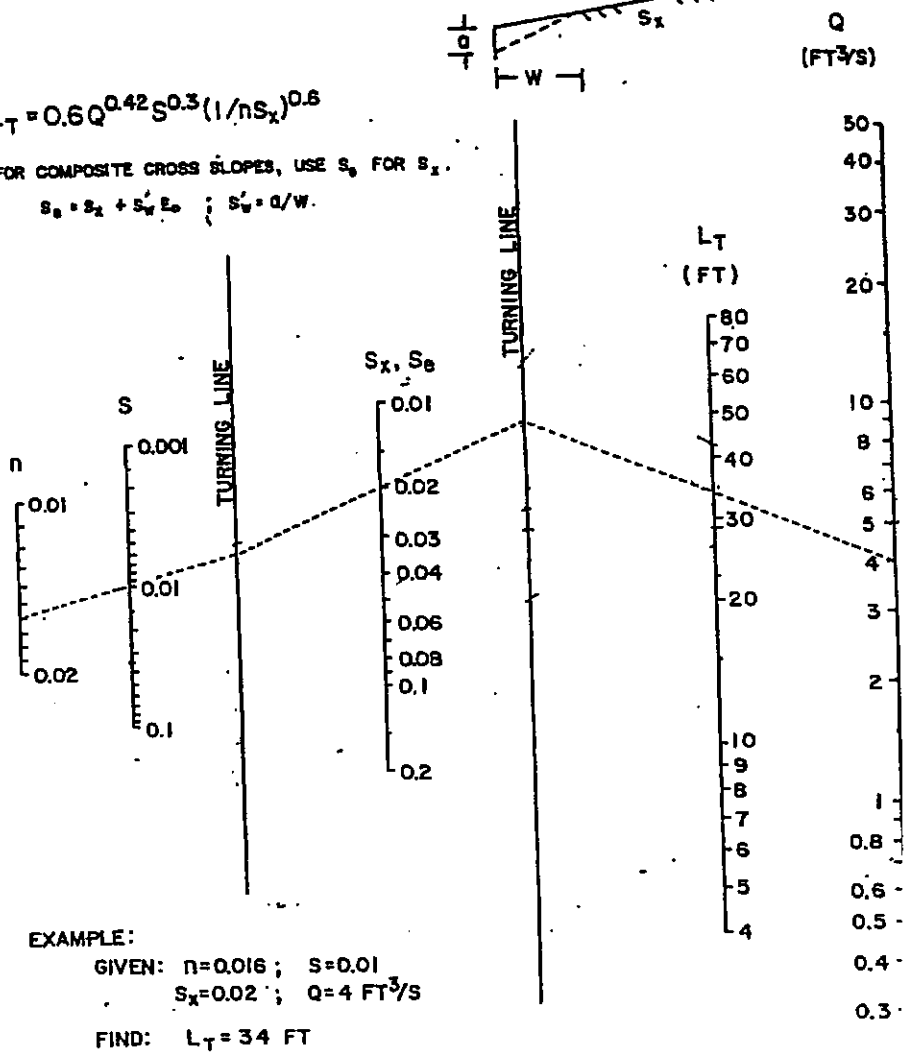




$$L_T = 0.6Q^{0.42} S^{0.3} (1/nS_x)^{0.6}$$

FOR COMPOSITE CROSS SLOPES, USE  $S_c$  FOR  $S_x$ .

$$S_c = S_x + S_w' E_c ; S_w' = a/W.$$



**CHART 9. Curb-opening and slotted drain inlet length for total interception.**

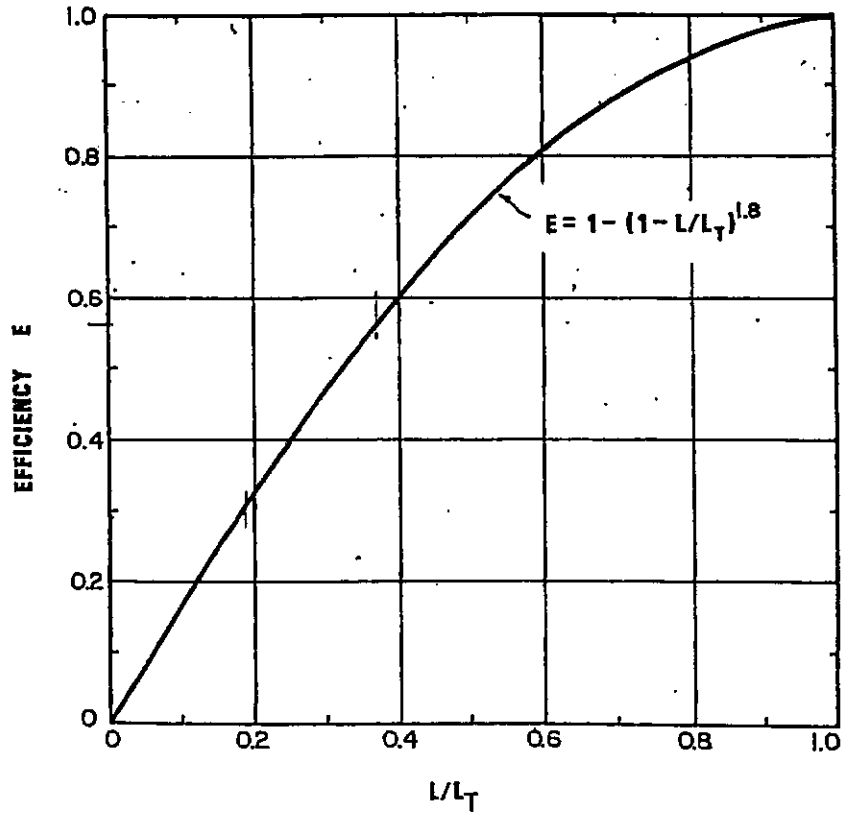


CHART 10. Curb-opening and slotted drain inlet interception efficiency.

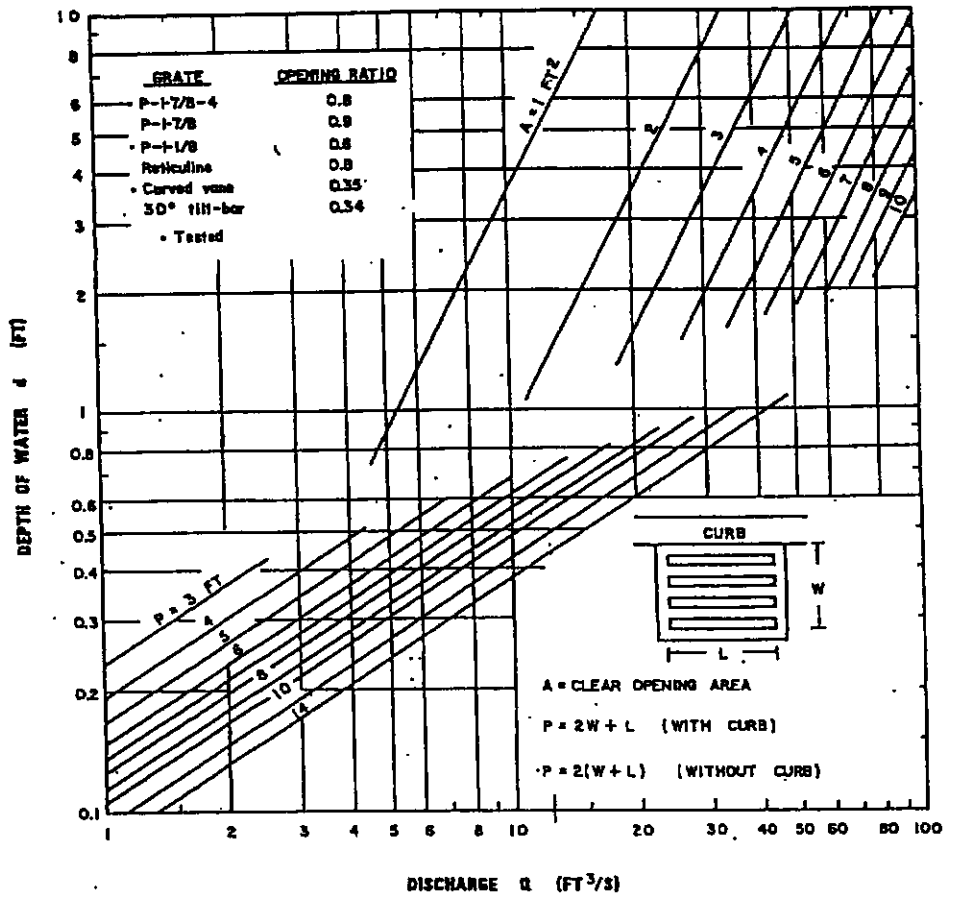


CHART 11. Grate inlet capacity in sump conditions.

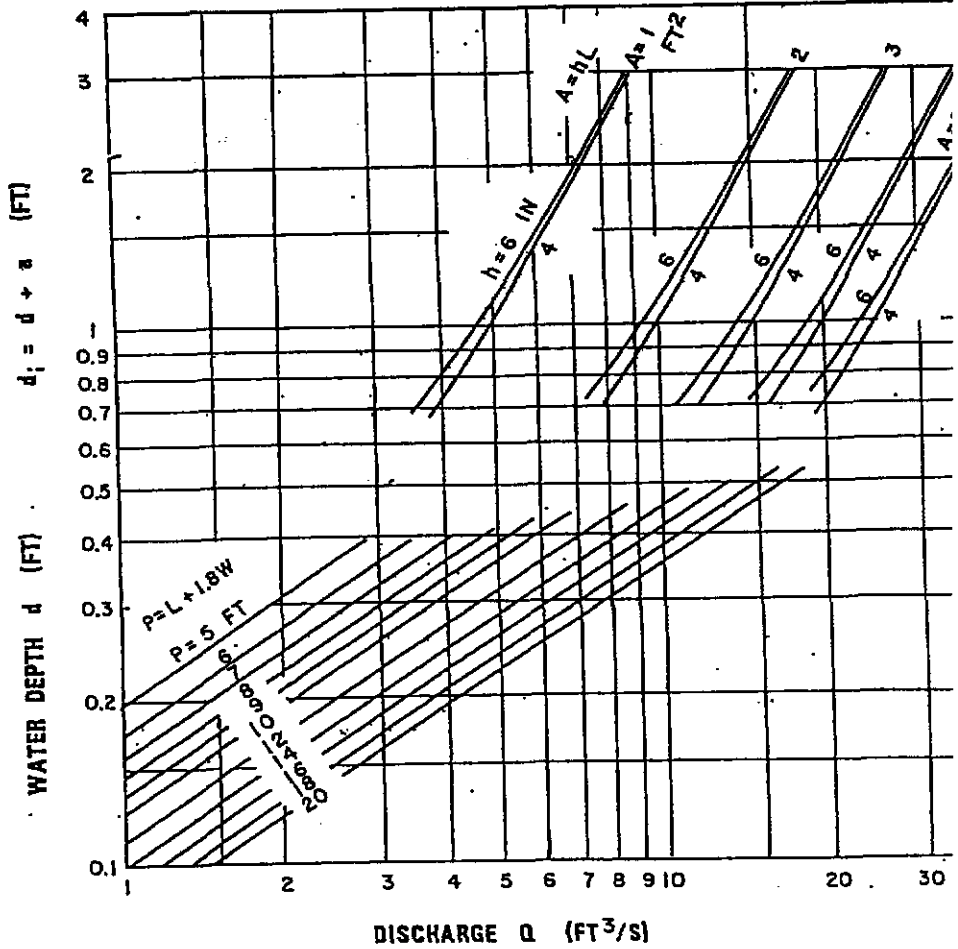
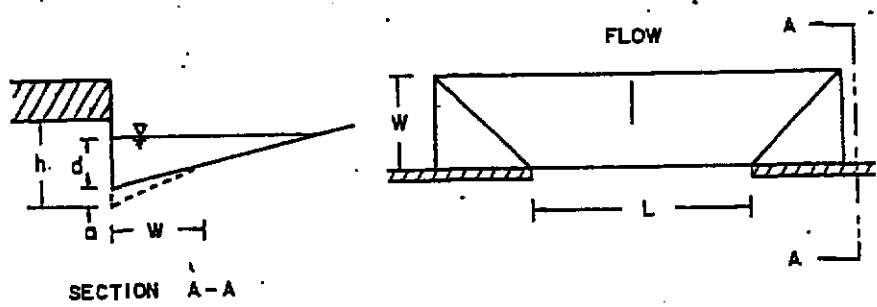


CHART 12. Depressed curb-opening inlet capacity in sump locations.

ATTACHMENT A  
DRAINAGE CRITERIA MANUAL

RAINFALL INTENSITY TABLE FOR SEDGWICK COUNTY, KANSAS

The following tabulation contains rainfall intensity in inches per hour as derived from ESSA Weather Bureau Technical Paper 40 Modified to NWS Hydro-35, 1977 During First Hour

DURATION IN MINUTES	RETURN PERIODS OF						
	1-YR	2-YR	5-YR	10-YR	25-YR	50-YR	100
5	4.18	5.57	6.53	7.41	8.52	9.48	10
6	3.99	5.32	6.25	7.09	8.16	9.09	9
7	3.81	5.09	5.99	6.81	7.84	8.74	9
8	3.66	4.89	5.75	6.55	7.55	8.42	8
9	3.52	4.70	5.54	6.31	7.28	8.13	8
10	3.39	4.52	5.34	6.09	7.04	7.86	8
11	3.27	4.36	5.16	5.89	6.81	7.61	8
12	3.18	4.21	4.99	5.71	6.60	7.38	8
13	3.05	4.08	4.84	5.53	6.41	7.17	8
14	2.96	3.95	4.69	5.37	6.23	6.97	8
15	2.87	3.83	4.56	5.22	6.06	6.78	8
16	2.78	3.72	4.43	5.08	5.90	6.59	8
17	2.71	3.61	4.31	4.95	5.75	6.44	8
18	2.63	3.51	4.20	4.83	5.61	6.29	8
19	2.56	3.42	4.10	4.71	5.47	6.14	8
20	2.50	3.33	4.00	4.60	5.35	6.00	8
21	2.44	3.25	3.90	4.50	5.23	5.87	8
22	2.38	3.17	3.81	4.40	5.12	5.75	8
23	2.32	3.10	3.73	4.31	5.01	5.63	8
24	2.27	3.03	3.65	4.22	4.91	5.52	8
25	2.22	2.96	3.57	4.13	4.81	5.41	8
26	2.20	2.90	3.50	4.05	4.72	5.31	8
27	2.16	2.84	3.43	3.98	4.63	5.21	8
28	2.14	2.78	3.37	3.90	4.55	5.12	8
29	2.11	2.72	3.30	3.83	4.47	5.03	8
30	2.08	2.67	3.24	3.76	4.39	4.94	8
31	2.05	2.62	3.19	3.70	4.32	4.86	8
32	2.02	2.57	3.10	3.63	4.25	4.79	8
33	1.99	2.52	3.05	3.57	4.18	4.71	8
34	1.96	2.48	3.01	3.51	4.11	4.63	8
35	1.93	2.44	2.98	3.46	4.05	4.56	8
36	1.91	2.39	2.93	3.41	3.99	4.50	8
37	1.89	2.35	2.88	3.36	3.93	4.43	8
38	1.87	2.32	2.84	3.31	3.87	4.37	8
39	1.85	2.28	2.80	3.26	3.82	4.31	8
40	1.83	2.24	2.76	3.22	3.76	4.25	8
41	1.81	2.21	2.72	3.17	3.71	4.19	8
42	1.79	2.18	2.68	3.13	3.66	4.13	8
43	1.77	2.14	2.64	3.09	3.61	4.08	8
44	1.75	2.11	2.61	3.05	3.57	4.03	8
45	1.73	2.08	2.57	3.01	3.52	3.98	8

ATTACHMENT A CONTINUED  
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DURATION IN MINUTES	RETURN PERIODS OF						100
	1-YR	2-YR	5-YR	10-YR	25-YR	50-YR	
46	1.70	2.05	2.54	2.97	3.48	3.93	4
47	1.67	2.02	2.50	2.93	3.44	3.88	4
48	1.66	2.00	2.47	2.90	3.39	3.84	4
49	1.64	1.97	2.44	2.86	3.35	3.79	4
50	1.61	1.95	2.41	2.83	3.32	3.75	4
51	1.59	1.92	2.38	2.79	3.28	3.71	4
52	1.56	1.89	2.35	2.76	3.24	3.67	4
53	1.54	1.86	2.33	2.73	3.20	3.63	4
54	1.52	1.84	2.30	2.70	3.17	3.59	4
55	1.50	1.81	2.27	2.67	3.14	3.55	4
56	1.47	1.79	2.25	2.64	3.10	3.51	4
57	1.45	1.76	2.22	2.61	3.07	3.48	4
58	1.43	1.74	2.20	2.59	3.04	3.44	4
59	1.42	1.72	2.18	2.56	3.01	3.41	4
60	1.40	1.69	2.15	2.53	2.98	3.37	4
61	1.38	1.67	2.13	2.51	2.95	3.34	4
62	1.36	1.65	2.11	2.48	2.92	3.31	4
63	1.34	1.63	2.09	2.46	2.89	3.28	4
64	1.33	1.61	2.07	2.44	2.86	3.25	4
65	1.31	1.59	2.05	2.41	2.84	3.22	4
66	1.30	1.57	2.03	2.39	2.81	3.19	4
67	1.28	1.56	2.01	2.37	2.79	3.16	4
68	1.26	1.54	1.99	2.35	2.76	3.13	4
69	1.25	1.52	1.97	2.33	2.74	3.10	4
70	1.24	1.50	1.95	2.31	2.71	3.08	4
71	1.22	1.49	1.93	2.28	2.69	3.05	4
72	1.21	1.47	1.92	2.26	2.67	3.02	4
73	1.20	1.46	1.90	2.25	2.64	3.00	4
74	1.18	1.44	1.88	2.23	2.63	2.98	4
75	1.17	1.43	1.86	2.21	2.61	2.95	4
76	1.16	1.41	1.85	2.19	2.58	2.93	4
77	1.15	1.40	1.83	2.17	2.55	2.90	4
78	1.13	1.38	1.82	2.15	2.53	2.88	4
79	1.12	1.37	1.80	2.14	2.50	2.86	4
80	1.11	1.36	1.79	2.12	2.48	2.84	4
81	1.10	1.34	1.77	2.10	2.46	2.82	4
82	1.09	1.33	1.76	2.08	2.43	2.79	4
83	1.08	1.32	1.74	2.06	2.41	2.76	4
84	1.07	1.31	1.73	2.04	2.39	2.74	4
85	1.06	1.30	1.72	2.02	2.37	2.71	4
86	1.05	1.28	1.70	2.00	2.34	2.69	4
87	1.04	1.27	1.69	1.99	2.32	2.66	4
88	1.03	1.26	1.68	1.97	2.30	2.64	4
89	1.02	1.25	1.68	1.95	2.28	2.62	4
90	1.01	1.24	1.66	1.93	2.26	2.59	4

ATTACHMENT A CONTINUED.  
Page 3

DURATION IN MINUTES	RETURN PERIODS OF						100-
	1-YR	2-YR	5-YR	10-YR	25-YR	50-YR	
91	1.00	1.23	1.65	1.92	2.24	2.57	2
92	1.00	1.22	1.63	1.90	2.22	2.55	2
93	0.99	1.21	1.62	1.89	2.20	2.53	2
94	0.98	1.20	1.61	1.87	2.19	2.51	2
95	0.97	1.19	1.59	1.85	2.17	2.49	2
96	0.96	1.18	1.58	1.84	2.15	2.46	2
97	0.96	1.17	1.57	1.82	2.13	2.44	2
98	0.95	1.16	1.56	1.81	2.12	2.42	2
99	0.94	1.15	1.54	1.80	2.10	2.41	2
100	0.93	1.14	1.53	1.78	2.08	2.39	2
101	0.93	1.13	1.52	1.77	2.07	2.39	2
102	0.92	1.13	1.51	1.75	2.05	2.35	2
103	0.91	1.12	1.50	1.74	2.04	2.33	2
104	0.90	1.11	1.49	1.73	2.02	2.31	2
105	0.90	1.10	1.47	1.72	2.01	2.30	2
106	0.89	1.09	1.46	1.70	1.99	2.28	2
107	0.88	1.09	1.45	1.69	1.98	2.25	2
108	0.88	1.08	1.44	1.68	1.96	2.25	2
109	0.87	1.07	1.43	1.67	1.95	2.23	2
110	0.87	1.06	1.42	1.65	1.93	2.21	2
111	0.86	1.06	1.41	1.64	1.92	2.20	2
112	0.85	1.05	1.40	1.63	1.91	2.18	2
113	0.85	1.04	1.39	1.62	1.89	2.17	2
114	0.84	1.03	1.38	1.61	1.88	2.15	2
115	0.84	1.03	1.37	1.60	1.87	2.14	2
116	0.83	1.02	1.36	1.59	1.86	2.12	2
117	0.82	1.01	1.35	1.58	1.84	2.11	2
118	0.82	1.01	1.35	1.57	1.83	2.09	2
119	0.81	1.00	1.34	1.56	1.82	2.08	2
120	0.81	0.99	1.33	1.55	1.81	2.07	2

DURATION IN HOURS	RETURN PERIODS OF						1
	1-YR	2-YR	5-YR	10-YR	25-YR	50-YR	
2	0.81	0.99	1.33	1.55	1.81	2.07	1
3	0.59	0.72	0.97	1.13	1.32	1.51	1
4	0.47	0.58	0.78	0.91	1.06	1.21	1
5	0.40	0.49	0.66	0.77	0.89	1.02	1
6	0.35	0.42	0.57	0.67	0.78	0.89	1
8	0.28	0.34	0.46	0.53	0.62	0.71	1
10	0.23	0.29	0.39	0.45	0.52	0.60	1
12	0.20	0.25	0.33	0.39	0.45	0.52	1
18	0.15	0.18	0.24	0.28	0.33	0.38	1
24	0.12	0.15	0.20	0.23	0.27	0.31	1

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ATTACHMENT B  
DRAINAGE CRITERIA MANUAL

INCREMENTAL INFILTRATION VALUES IN INCHES

Time Minutes**	SCS Hydrologic Soil Group			
	A	B	C	D
5	.33	.26	.19	.12
10	.25	.17	.09	.04
15	.18	.11	.05	.02
20	.13	.07	.03	.02
25	.10	.05	.03	.02
30	.08	.05	.03	.02
35	.08	.05	.03	.02
40	.08	.05	.03	.02
45	.08	.05	.03	.02
50	.08	.05	.03	.02
55	.08	.05	.03	.02
60	.08	.05	.03	.02
65	.08	.05	.03	.02
70	.08	.05	.03	.02
75	.08	.05	.03	.02
80	.08	.05	.03	.02
85	.08	.05	.03	.02
90	.08	.05	.03	.02
95	.08	.05	.03	.02
100	.08	.05	.03	.02
105	.08	.05	.03	.02
110	.08	.05	.03	.02
115	.08	.05	.03	.02
120	.08	.05	.03	.02

\*\*Time at end of the time increment

NOTE: Values for 125 minutes and additional 5 minute increments shall be the same as those shown for 120 minutes.

ATTACHMENT C

DRAINAGE CRITERIA MANUAL

DEPRESSION STORAGE LOSSES

<u>Surface Type</u>	<u>Total Loss (Inches)</u>
<b>Impervious:</b>	
Paved Areas	0.1
Flat Roofs	0.1
Sloped Roofs	0.05
<b>Pervious:</b>	
Lawns and Grass	0.3
Wooded Areas and Open Fields	0.4

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ATTACHMENT D.  
DRAINAGE CRITERIA

RECOMMENDED RUNOFF COEFFICIENTS FOR RATIONAL METHOD  
AND PERCENT IMPERVIOUS FOR UNIT HYDROGRAPH METHOD

Land Use or Surface Characteristics	Percent Impervious	Frequency			
		2	5	10	100
<b>1. Business:</b>					
Downtown Areas	95	0.84	0.85	0.87	0.
Neighborhood Areas	70	0.68	0.69	0.73	0.
<b>2. Residential:</b>					
<u>Single Family (Soil Group D)</u>					
1/8 Acre	50	0.57	0.61	0.68	0.
1/4 Acre	38	0.50	0.54	0.62	0.
1/3 Acre	30	0.46	0.50	0.59	0.
1/2 Acre	25	0.42	0.48	0.56	0.
3/4 Acre	22	0.42	0.46	0.55	0.
1 Acre	20	0.41	0.45	0.54	0.
<u>Multi-Family (Soil Group D)</u>					
Multi-Unit (detached)	60	0.62	0.66	0.72	0.
Multi-Unit (attached)	65	0.64	0.68	0.73	0.
Apartments	75	0.70	0.73	0.79	0.
<u>Single Family (Soil Group C)</u>					
1/8 Acre	50	0.55	0.58	0.64	0.
1/4 Acre	38	0.48	0.51	0.57	0.
1/3 Acre	30	0.43	0.46	0.53	0.
1/2 Acre	25	0.40	0.43	0.50	0.
3/4 Acre	22	0.39	0.42	0.49	0.
1 Acre	20	0.37	0.40	0.48	0.
<u>Multi-Family (Soil Group C)</u>					
Multi-Unit (detached)	60	0.60	0.63	0.69	0.
Multi-Unit (attached)	65	0.63	0.66	0.71	0.
Apartments	75	0.68	0.72	0.77	0.
<u>Single-Family (Soil Group B)</u>					
1/8 Acre	50	0.52	0.54	0.59	0.
1/4 Acre	38	0.44	0.46	0.52	0.
1/3 Acre	30	0.39	0.41	0.47	0.
1/2 Acre	25	0.36	0.38	0.44	0.
3/4 Acre	22	0.34	0.36	0.42	0.
1 Acre	20	0.33	0.35	0.40	0.
<u>Multi-Family (Soil Group B)</u>					
Multi-Unit (detached)	60	0.58	0.60	0.65	0.
Multi-Unit (attached)	65	0.61	0.64	0.68	0.
Apartments	75	0.67	0.70	0.74	0.

Land Use or Surface Characteristics	Percent Impervious	Frequency			
		2	5	10	1
<u>Single Family (Soil Group A)</u>					
1/8 Acre	50	0.47	0.50	0.54	C
1/4 Acre	38	0.39	0.41	0.45	C
1/3 Acre	30	0.33	0.35	0.39	C
1/2 Acre	25	0.30	0.31	0.35	C
3/4 Acre	22	0.28	0.29	0.33	C
1 Acre	20	0.26	0.28	0.32	C
<u>Multi-Family (Soil Group A)</u>					
Multi-Unit (detached)	60	0.55	0.57	0.61	C
Multi-Unit (attached)	65	0.58	0.60	0.64	C
Apartments	75	0.65	0.68	0.72	C
3. Industrial:					
Light Areas	70	0.68	0.69	0.73	C
Heavy Areas	80	0.74	0.76	0.79	C
4. Playgrounds:	15	0.33	0.35	0.42	C
5. Schools:	40	0.49	0.51	0.56	C
6. Railroad Yard Areas:	30	0.43	0.45	0.50	C
Undeveloped Urban Areas: Offsite Flow Analysis (when land use not defined)					
8. Streets:					
Paved	99	0.87	0.88	0.90	
Gravel	00	0.24	0.26	0.33	
9. Drive, Parking Lots and Walks:	96	0.87	0.87	0.88	
10. Roofs:	90	0.80	0.85	0.90	
11. Urban Lawn Areas (See Note No. 1 below):					
<u>Soil Group A</u>					
Slope less than 1%	00	0.08	0.09	0.13	
Slope 1% to 4%	00	0.12	0.13	0.17	
Slope more than 4%	00	0.16	0.17	0.21	
<u>Soil Group B</u>					
Slope less than 1%	00	0.16	0.18	0.24	
Slope 1% to 4%	00	0.20	0.22	0.28	
Slope more than 4%	00	0.24	0.26	0.32	
<u>Soil Group C</u>					
Slope less than 1%	00	0.24	0.27	0.35	
Slope 1% to 4%	00	0.26	0.29	0.37	
Slope more than 4%	00	0.28	0.31	0.39	

Land Use or Surface Characteristics	Percent Impervious	Frequency			
		2	5	10	11
<u>Soil Group D</u>					
Slope less than 1%	00	0.28	0.33	0.43	0.
Slope 1% to 4%	00	0.30	0.35	0.45	0.
Slope more than 4%	00	0.32	0.37	0.47	0.

Note No. 1: Coefficients shown in the above table are for pervious open space areas with thick turf which includes pervious areas in parks and cemeteries. Coefficients shown above must be increased 0.02 for use with agricultural pasture areas. Coefficients shown above must be reduced by 0.04 for use with agricultural cultivated areas. Group A soils are well-drained, coarse textured sands with high infiltration rates. Group B soils are moderately well-drained, moderately coarse textured soils with moderate infiltration rates. Group C soils are moderately poor-drained, moderately fine textured soils with slow infiltration rates. Group D soils are poor-drained, fine textured soils with very slow infiltration rates.

GENERAL NOTE: These Rational Formula Coefficients may not be valid for basins 320 acres or larger.

ATTACHMENT E  
DRAINAGE CRITERIA

AVERAGE OVERLAND FLOW VELOCITY FOR USE WITH URBANIZED AREAS

Surface Type	VELOCITY IN FEET/SECOND FOR SLOPES IN PERCENT SHOWN																			
	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0	20.0
Forest with Heavy Ground Litter or Meadow	0.03	0.04	0.06	0.07	0.08	0.09	0.10	0.11	0.12	0.13	0.16	0.21	0.28	0.33	0.39	0.46	0.53	0.60	0.72	1.10
Fallow or Minimum Tillage Cultivation	0.06	0.08	0.10	0.12	0.13	0.14	0.16	0.17	0.18	0.19	0.29	0.40	0.51	0.66	0.78	0.91	1.05	1.20	1.44	2.10
Short Grass Pasture or Lawns	0.09	0.13	0.15	0.18	0.20	0.21	0.23	0.25	0.26	0.28	0.45	0.60	0.77	0.96	1.17	1.33	1.50	1.68	1.98	3.20
Almost Bare Ground	0.16	0.22	0.28	0.31	0.35	0.38	0.41	0.44	0.46	0.49	0.70	0.93	1.05	1.26	1.50	1.75	2.03	2.32	2.79	4.40
Grassed Waterway	0.35	0.48	0.58	0.67	0.77	0.84	0.91	0.98	1.05	1.12	1.54	1.82	2.10	2.38	2.78	3.20	3.66	4.14	4.56	7.00
Paved Areas (Sheet Flow) or Shallow Gutter Flow	0.44	0.62	0.77	0.91	1.05	1.12	1.19	1.26	1.33	1.40	2.00	2.35	3.20	3.83	4.41	5.04	5.70	6.00	6.70	9.00

ATTACHMENT F

DETERMINATION OF DIMENSIONLESS  
WATERSHED CONVEYANCE FACTOR ( $\theta$ )

$$\theta = \theta_1 + \theta_2$$

$\theta_1$	Classification
0.6	Extensive channel improvement and storm sewer system, closed conduit channel system
0.7	Moderate channel improvement and storm sewer system.
0.8	Some channel improvement and storm sewers, mainly cleaning and enlargement of existing channel.
0.9	Little channel improvement and storm sewers.
1.0	Natural channel conditions.
$\theta_2$	Classification
0.0	No channel vegetation.
0.1	Light channel vegetation.
0.2	Moderate channel vegetation.
0.3	Heavy channel vegetation.

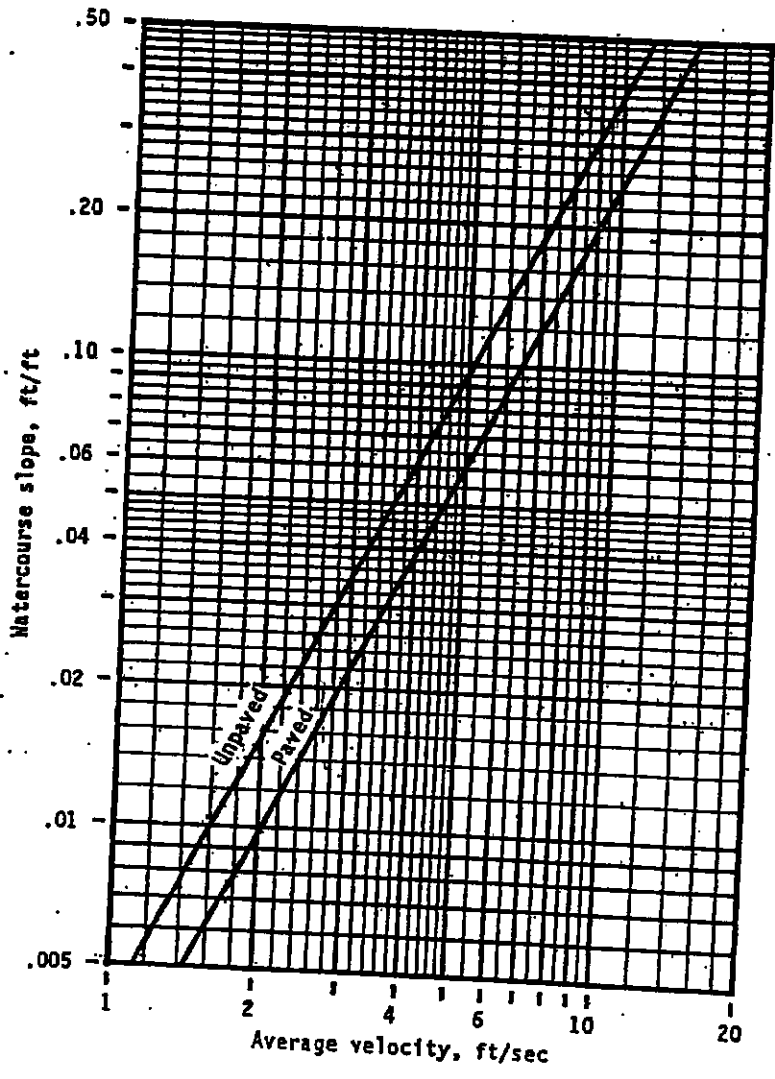


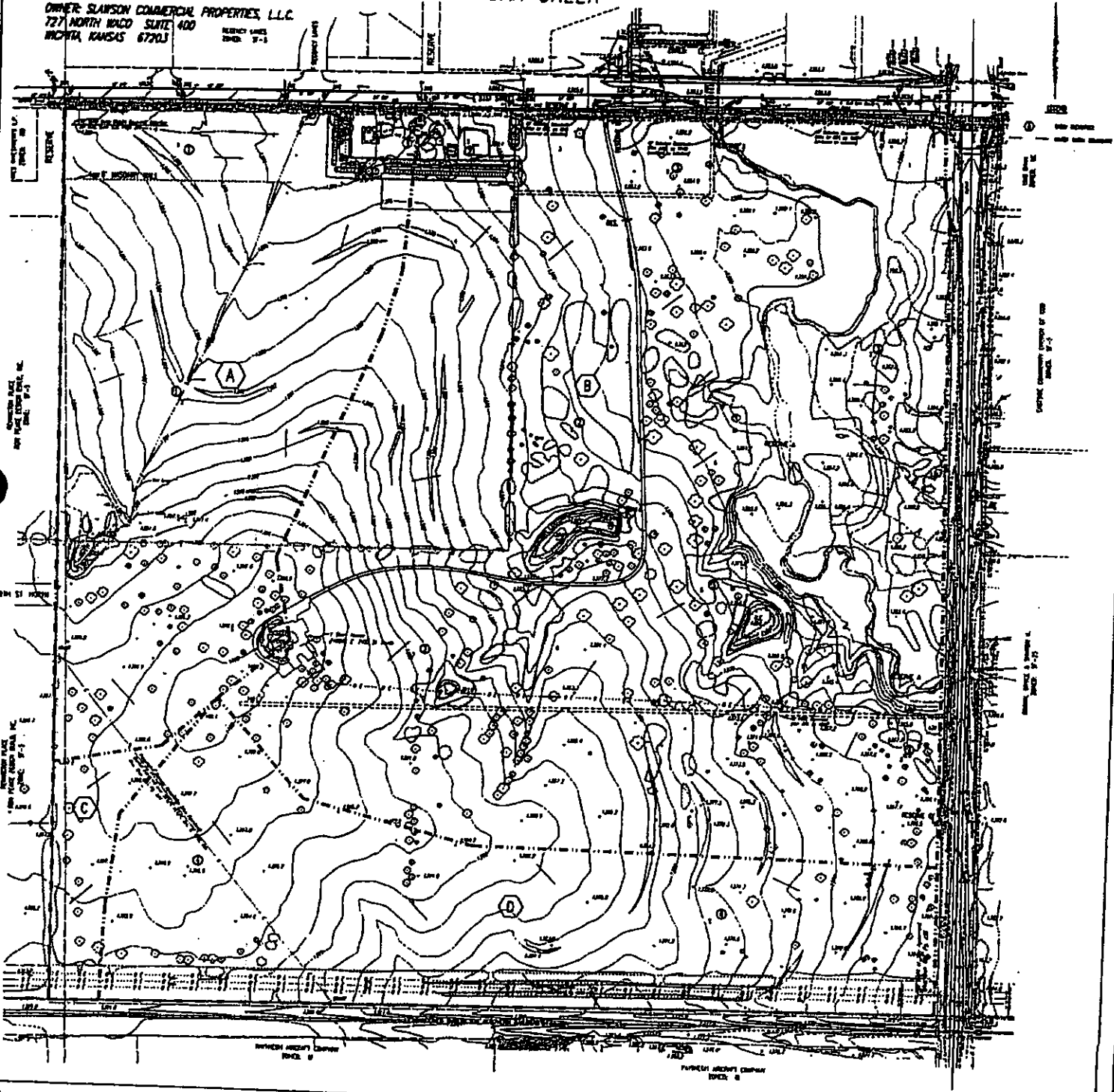
Figure 3-1.—Average velocities for estimating travel time for shallow concentrated flow.

(210-VI-TR-55, Second Ed., June 1986)

# OAK CREEK

OWNER: SLANSON COMMERCIAL PROPERTIES, L.L.C.  
727 NORTH WACO STATE 400  
WICHITA, KANSAS 67203

REVISION NUMBER: 0000  
DATE: 7-1



INTERIOR DESIGN COMPANY  
PROJECT #

PAPERMAN ARCHITECTS COMPANY  
PROJECT #

MAP SCALE 1" = 500'



PANEL 0377E

**FIRM**  
**FLOOD INSURANCE RATE MAP**  
**SEDGWICK COUNTY,**  
**KANSAS**  
**AND INCORPORATED AREAS**

PANEL 377 OF 700

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

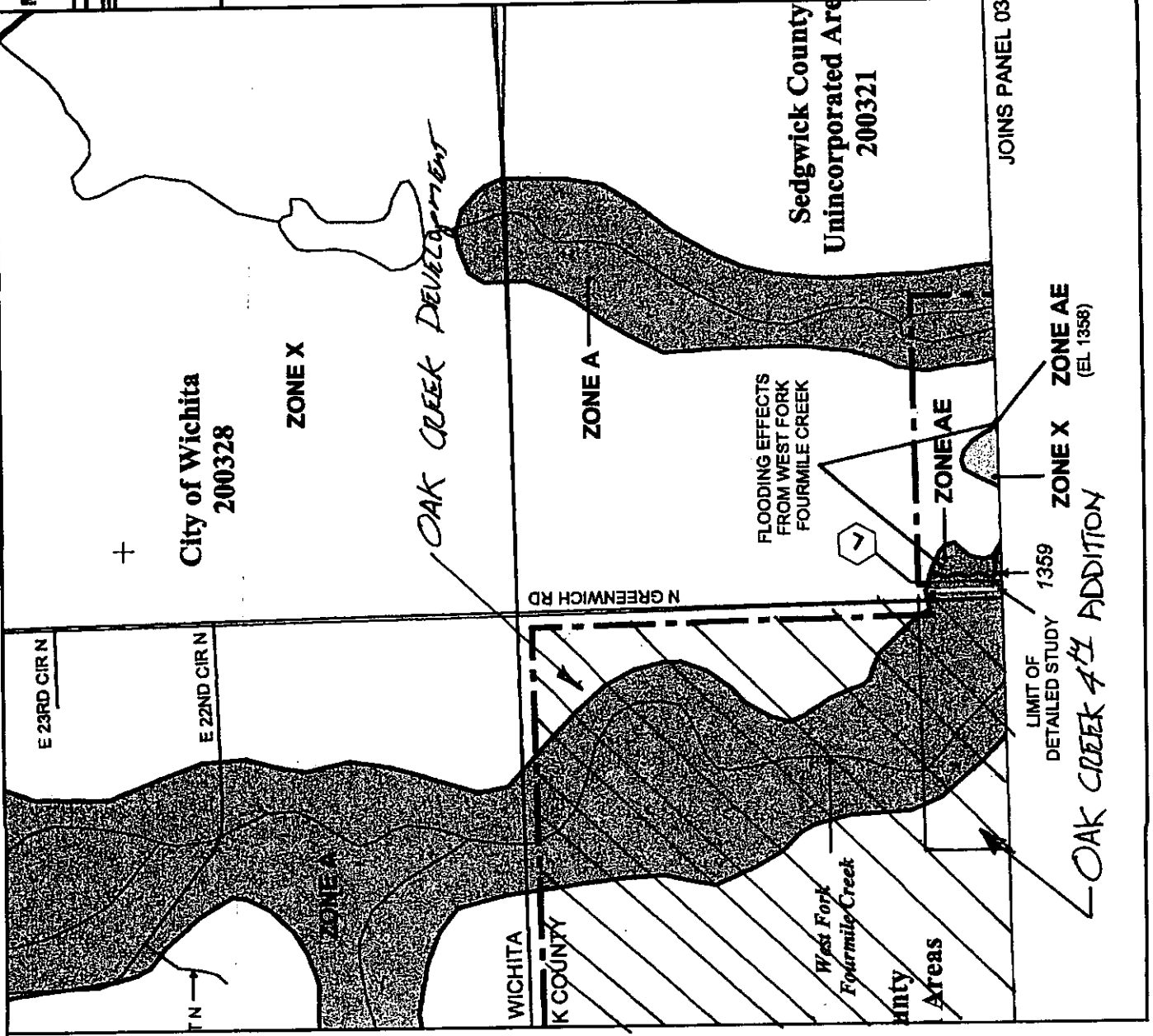
CONTAINS:			
COMMUNITY	NUMBER	PANEL	BUEDEX
SEDGWICK COUNTY	200321	0377	E
WICHITA, CITY OF	200328	0377	E

Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject community.



**MAP NUMBER**  
**20173C0377E**  
**EFFECTIVE DATE**  
**FEBRUARY 2, 2007**  
 Federal Emergency Management Agency

This is an official copy of a portion of the above referenced flood map. It was extracted using F-MIT On-Line. This map does not reflect changes or amendments which may have been made subsequent to the date on the title block. For the latest product information about National Flood Insurance Program flood maps check the FEMA Flood Map Store at [www.msc.fema.gov](http://www.msc.fema.gov)



MAP SCALE 1" = 500'



PANEL 0379E

**FIRM**  
**FLOOD INSURANCE RATE MAP**  
**SEDGWICK COUNTY,**  
**KANSAS**  
**AND INCORPORATED AREAS**

PANEL 379 OF 700

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:	NUMBER	PANEL	SUBAREA
COMMUNITY	200321	0379	E
SEDGWICK COUNTY	200328	0379	E
WICHITA, CITY OF			

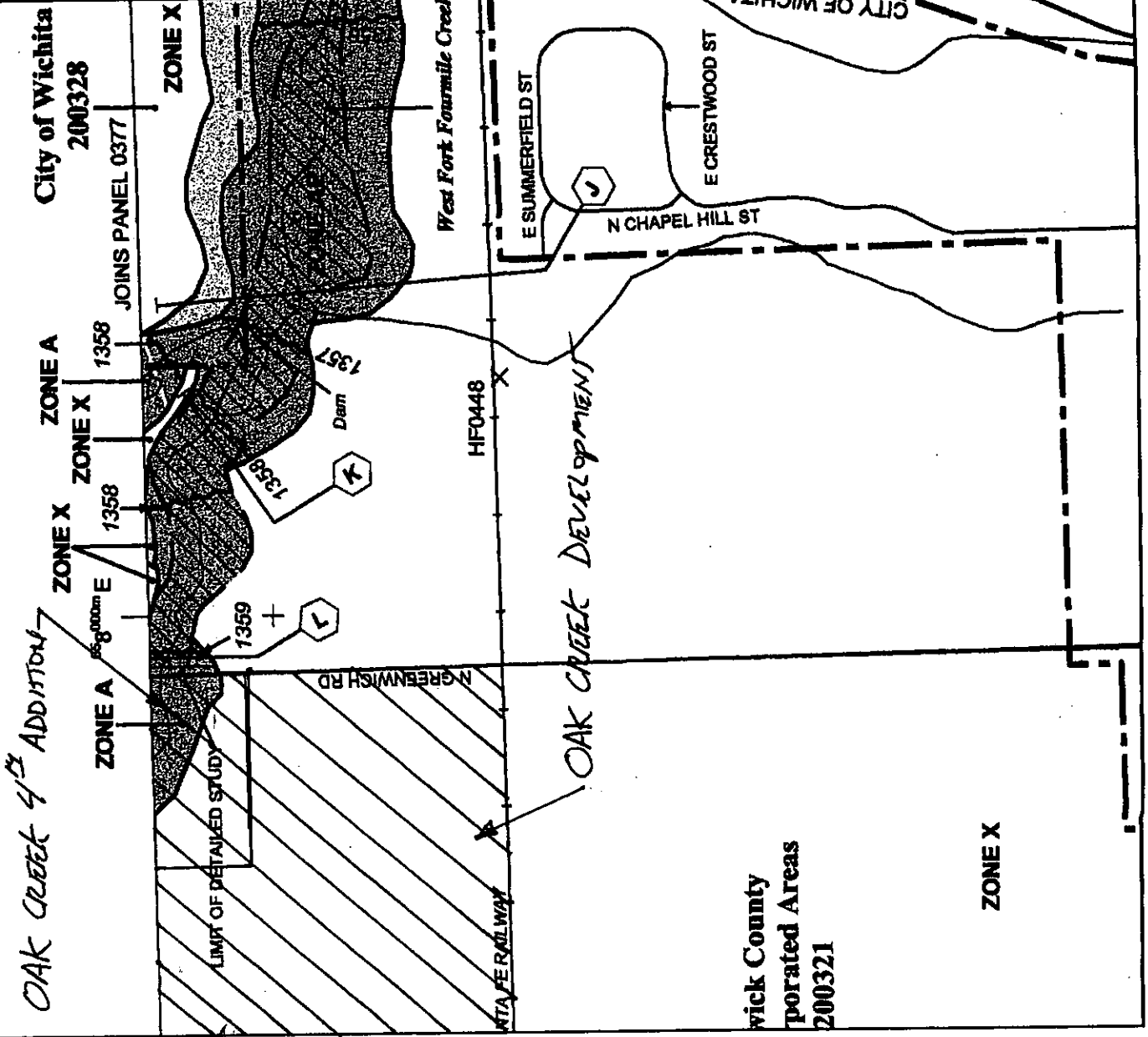
Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject community.



**MAP NUMBER**  
**20173C0379E**

**EFFECTIVE DATE**  
**FEBRUARY 2, 2007**  
**Federal Emergency Management Agency**

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OAK Creek 4<sup>th</sup> ADDITION

City of Wichita  
200328

ZONE A

ZONE X

ZONE X

ZONE A

ZONE X

ZONE A

ZONE X

N GREENWISH RD

West Fork Fourmile Creek

HF0448

E SUMMERFIELD ST

N CHAPEL HILL ST

E CRESTWOOD ST

CITY OF WICHITA

OAK CREEK DEVELOPMENTS

Wichita County  
Incorporated Areas  
200321

ZONE X

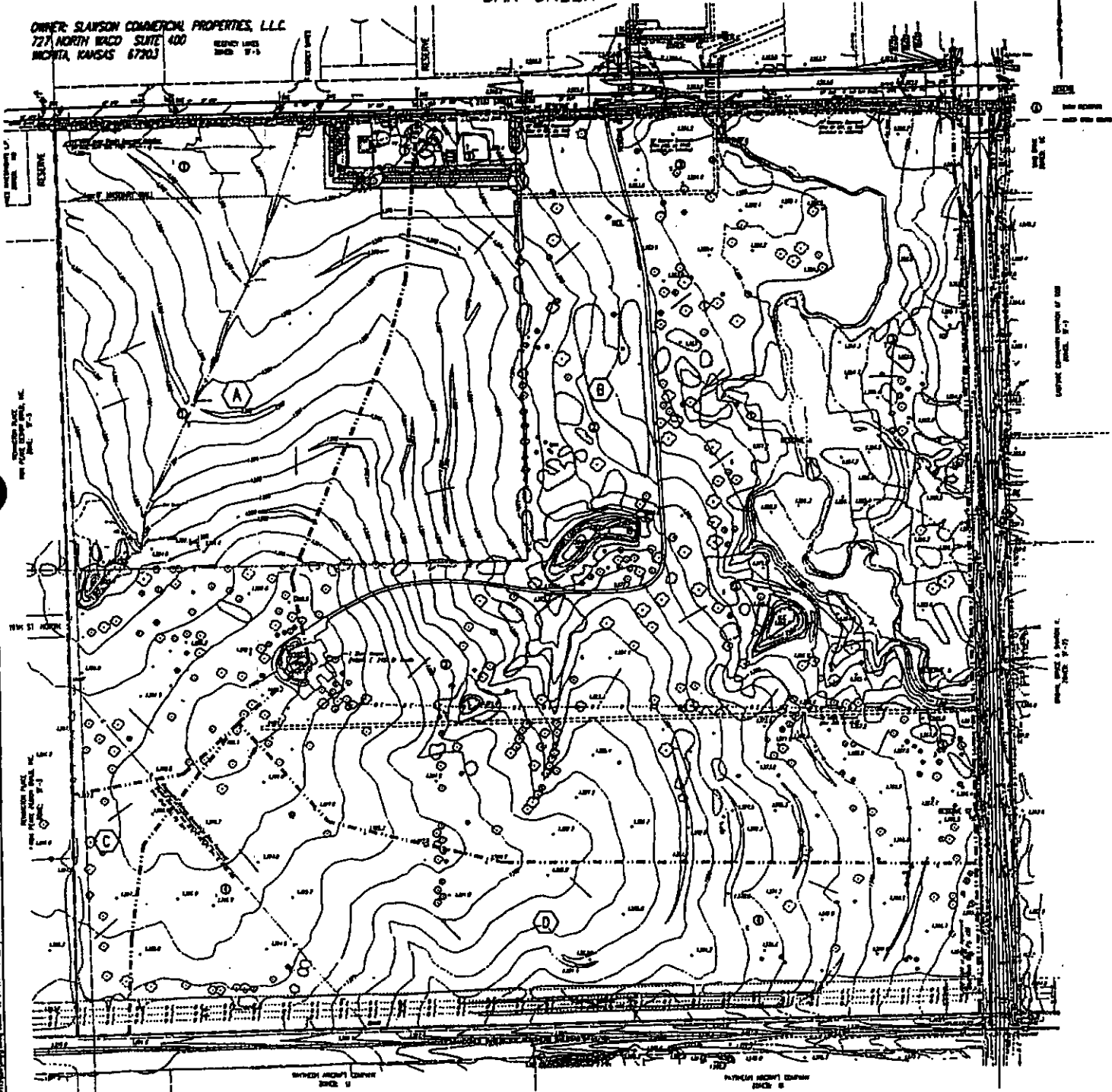
TABLE 2 - SUMMARY OF DISCHARGES (Continued)

FLOODING SOURCE AND LOCATION	DRAINAGE AREA SQ MILES	PEAK DISCHARGES (CFS)		
		10-YEAR	50-YEAR	100-YEAR
MIDDLE BRANCH GYPSUM CREEK At 13th Street	2.3	740	1,090	1,240
FOURMILE CREEK At county boundary	27.2	11,680	17,390	20,100
Upstream of confluence of Brookhaven Creek	8.4	3,220	4,760	5,500
Upstream of confluence of West Fork Fourmile Creek	2.2	1,410	2,070	2,400
WEST FORK FOURMILE CREEK At mouth at Fourmile Creek	4.2	2,110	3,120	3,600
At 13th Street North	3.2	2,200	3,270	3,780
BROOKHAVEN CREEK At mouth at Fourmile Creek	4.0	2,470	3,620	4,180
At Interstate 35	1.8	2,190	3,190	3,780
MIDDLE FORK CHISHOLM CREEK Upstream of confluence of Tributary M1	11.7	2,990	5,280	6,190
At 53rd Street North	9.5	2,580	4,570	5,360
EAST FORK CHISHOLM CREEK At 45th Street North	1.6	860	1,270	1,545
CENTER DRAIN EAST TRIBUTARY At City of Wichita corporate limits	1.5	630	1,010	1,190
				500-YEAR
				1,590
				26,800
				7,100
				3,130
				4,770
				4,850
				5,420
				5,170
				8,920
				7,720
				2,240
				1,600

# OAK CREEK

OWNER: SLAYSON COMMERCIAL PROPERTIES, L.L.C.  
727 NORTH WACO SUITE 400  
MICHOTA, KANSAS 67203

RECORD NO. 100  
DATE 7-1



OWNER: SLAYSON COMMERCIAL PROPERTIES, L.L.C.  
727 NORTH WACO SUITE 400  
MICHOTA, KANSAS 67203

RECORD NO. 100  
DATE 7-1

RESERVE

ST. 100

ST. 100

RESERVE

ST. 100

ST. 100

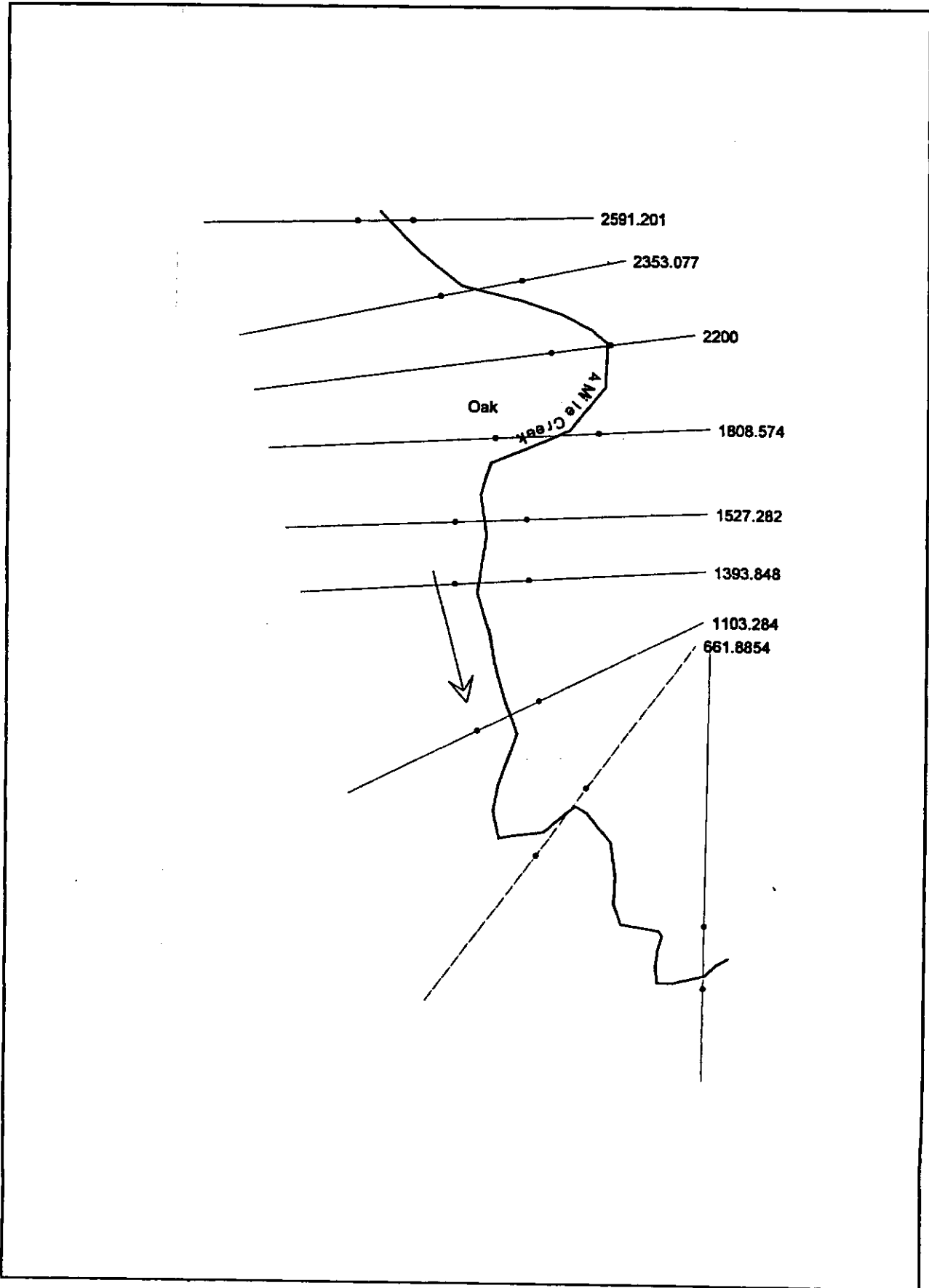
ST. 100

ST. 100

ST. 100

WITHIN AREA'S BOUNDARY

WITHIN AREA'S BOUNDARY



HEC-RAS Plan: Plan 01 River: 4 Mile Creek Reach: Oak Profile: PF 1

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.B. Elev (ft)	Crit W.B. (ft)	E.O. Elev (ft)	SE.O. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Ch
Oak	2591.201	PF 1	1817.00	1357.59	1361.80		1361.85	0.003063	2.20	1211.88	646.97	0.26
Oak	2163.077	PF 1	1817.00	1357.60	1361.34		1361.36	0.001417	1.58	1526.97	853.77	0.18
Oak	2200	PF 1	1817.00	1357.32	1360.97		1360.90	0.001662	1.97	1461.17	834.01	0.19
Oak	1908.574	PF 1	1817.00	1356.21	1360.58		1360.59	0.000473	1.27	1660.04	811.42	0.11
Oak	1627.262	PF 1	1817.00	1355.50	1360.20		1360.33	0.004294	3.18	715.64	306.50	0.32
Oak	1393.846	PF 1	1817.00	1354.84	1359.99		1360.03	0.001233	2.02	1310.09	806.84	0.18
Oak	1103.284	PF 1	1817.00	1353.60	1359.84		1359.85	0.000327	1.17	2141.58	491.34	0.09
Oak	881.8854	PF 1	1817.00	1352.56	1359.51		1359.58	0.001390	2.21	1001.80	409.13	0.18
Oak	64.06447	PF 1	2049.00	1351.33	1359.00	1355.55	1359.03	0.000658	1.74	1656.43	409.08	0.14

Plan: Plan 01 4 Mile Creek Oak RS: 2591.201 Profile: PF 1

E.G. Elev (ft)	1361.85	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.04	Wt n-Val	0.100	0.065	0.100
W.S. Elev (ft)	1361.80	Reach Len. (ft)	238.12	238.12	238.00
Crit W.S. (ft)		Flow Area (sq ft)	828.01	269.23	114.64
E.G. Slope (ft/ft)	0.003083	Area (sq ft)	828.01	269.23	114.64
Q Total (cfs)	1817.00	Flow (cfs)	1145.69	592.39	78.92
Top Width (ft)	646.97	Top Width (ft)	379.18	117.40	150.39
Vel Total (ft/s)	1.50	Avg Vel. (ft/s)	1.38	2.20	0.69
Max Chl Dpth (ft)	4.21	Hydr. Depth (ft)	2.18	2.29	0.76
Conv. Total (cfs)	32724.8	Conv. (cfs)	20634.2	10669.1	1421.5
Length Wid. (ft)	238.11	Wetted Per. (ft)	381.24	117.96	150.40
Min Ch El (ft)	1357.59	Shear (lb/sq ft)	0.42	0.44	0.15
Alpha	1.25	Stream Power (lb/ft s)	0.58	0.97	0.10
Frctn Loss (ft)	0.48	Cum Volume (acre-ft)	29.76	37.32	22.27
C & E Loss (ft)	0.01	Cum SA (acres)	11.48	9.55	9.82

Plan: Plan 01 4 Mile Creek Oak RS: 2353.077 Profile: PF 1

E.G. Elev (ft)	1361.36	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.03	Wt n-Val	0.100	0.065	0.100
W.S. Elev (ft)	1361.34	Reach Len. (ft)	300.00	309.31	320.00
Crit W.S. (ft)		Flow Area (sq ft)	712.30	432.15	382.52
E.G. Slope (ft/ft)	0.001417	Area (sq ft)	712.30	432.15	382.52
Q Total (cfs)	1817.00	Flow (cfs)	854.52	683.18	279.31
Top Width (ft)	653.77	Top Width (ft)	224.43	172.83	256.51
Vel Total (ft/s)	1.19	Avg Vel. (ft/s)	1.20	1.58	0.73
Max Chl Dpth (ft)	3.73	Hydr. Depth (ft)	3.17	2.50	1.49
Conv. Total (cfs)	48261.9	Conv. (cfs)	22697.1	18146.0	7418.7
Length Wid. (ft)	310.77	Wetted Per. (ft)	226.83	173.59	256.53
Min Ch El (ft)	1357.60	Shear (lb/sq ft)	0.28	0.22	0.13
Alpha	1.20	Stream Power (lb/ft s)	0.33	0.35	0.10
Frctn Loss (ft)	0.46	Cum Volume (acre-ft)	25.55	35.41	20.91
C & E Loss (ft)	0.00	Cum SA (acres)	9.83	8.76	8.70

Plan: Plan 01 4 Mile Creek Oak RS: 2200 Profile: PF 1

E.G. Elev (ft)	1360.90	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.03	Wt n-Val	0.100	0.065	0.100
W.S. Elev (ft)	1360.87	Reach Len. (ft)	412.00	391.43	370.00
Crit W.S. (ft)		Flow Area (sq ft)	102.54	364.04	1014.58
E.G. Slope (ft/ft)	0.001552	Area (sq ft)	102.54	364.04	1014.58
Q Total (cfs)	1817.00	Flow (cfs)	73.91	716.57	1026.52
Top Width (ft)	634.01	Top Width (ft)	75.01	112.58	446.42
Vel Total (ft/s)	1.23	Avg Vel. (ft/s)	0.72	1.97	1.01
Max Chl Dpth (ft)	3.55	Hydr. Depth (ft)	1.37	3.23	2.27
Conv. Total (cfs)	46125.1	Conv. (cfs)	1876.2	18190.3	26058.6
Length Wid. (ft)	386.13	Wetted Per. (ft)	75.05	112.65	446.46
Min Ch El (ft)	1357.32	Shear (lb/sq ft)	0.13	0.31	0.22
Alpha	1.41	Stream Power (lb/ft s)	0.10	0.62	0.22
Frctn Loss (ft)	0.30	Cum Volume (acre-ft)	22.75	32.58	15.78
C & E Loss (ft)	0.00	Cum SA (acres)	8.80	7.75	6.12

Plan: Plan 01 4 Mile Creek Oak RS: 1808.574 Profile: PF 1

E.G. Elev (ft)	1360.59	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.02	Wt. n-Val	0.100	0.065	0.100
W.S. Elev (ft)	1360.58	Reach Len. (ft)	234.91	234.91	234.00
Crit W.S. (ft)		Flow Area (sq ft)	536.83	898.76	524.45
E.G. Slope (ft/ft)	0.000473	Area (sq ft)	536.83	898.76	524.45
Q Total (cfs)	1817.00	Flow (cfs)	373.45	1142.44	301.11
Top Width (ft)	611.42	Top Width (ft)	169.94	219.98	221.50
Vel Total (ft/s)	0.93	Avg. Vel. (ft/s)	0.70	1.27	0.57
Max Chl Dpth (ft)	4.37	Hydr. Depth (ft)	3.16	4.09	2.37
Conv. Total (cfs)	83509.9	Conv. (cfs)	17163.9	52507.0	13839.0
Length Wid. (ft)	234.83	Wetted Per. (ft)	170.08	219.99	221.61
Min Ch El (ft)	1356.21	Shear (lb/sq ft)	0.09	0.12	0.07
Alpha	1.36	Stream Power (lb/ft s)	0.06	0.15	0.04
Frctn Loss (ft)	0.25	Cum Volume (acre-ft)	19.72	26.90	9.24
C & E Loss (ft)	0.01	Cum SA (acres)	7.64	6.25	3.28

Plan: Plan 01 4 Mile Creek Oak RS: 1527.282 Profile: PF 1

E.G. Elev (ft)	1360.33	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.13	Wt. n-Val	0.100	0.065	0.100
W.S. Elev (ft)	1360.20	Reach Len. (ft)	135.00	133.43	131.00
Crit W.S. (ft)		Flow Area (sq ft)	241.90	465.76	7.99
E.G. Slope (ft/ft)	0.004294	Area (sq ft)	241.90	465.76	7.99
Q Total (cfs)	1817.00	Flow (cfs)	326.99	1482.86	7.15
Top Width (ft)	306.50	Top Width (ft)	147.85	149.77	8.88
Vel Total (ft/s)	2.54	Avg. Vel. (ft/s)	1.35	3.18	0.90
Max Chl Dpth (ft)	4.70	Hydr. Depth (ft)	1.64	3.11	0.90
Conv. Total (cfs)	27728.4	Conv. (cfs)	4990.1	22629.2	109.1
Length Wid. (ft)	133.49	Wetted Per. (ft)	147.88	150.32	9.05
Min Ch El (ft)	1355.50	Shear (lb/sq ft)	0.44	0.83	0.24
Alpha	1.33	Stream Power (lb/ft s)	0.59	2.64	0.21
Frctn Loss (ft)	0.28	Cum Volume (acre-ft)	17.63	23.23	7.81
C & E Loss (ft)	0.03	Cum SA (acres)	6.78	5.26	2.67

Plan: Plan 01 4 Mile Creek Oak RS: 1393.848 Profile: PF 1

E.G. Elev (ft)	1360.03	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.05	Wt. n-Val	0.100	0.065	0.100
W.S. Elev (ft)	1359.98	Reach Len. (ft)	290.57	290.57	290.57
Crit W.S. (ft)		Flow Area (sq ft)	336.47	621.14	352.49
E.G. Slope (ft/ft)	0.001233	Area (sq ft)	336.47	621.14	352.49
Q Total (cfs)	1817.00	Flow (cfs)	273.39	1254.40	289.20
Top Width (ft)	506.84	Top Width (ft)	173.06	155.19	178.59
Vel Total (ft/s)	1.39	Avg. Vel. (ft/s)	0.81	2.02	0.82
Max Chl Dpth (ft)	5.14	Hydr. Depth (ft)	1.94	4.00	1.97
Conv. Total (cfs)	51750.6	Conv. (cfs)	7786.6	35727.1	8236.9
Length Wid. (ft)	290.57	Wetted Per. (ft)	173.11	155.63	178.73
Min Ch El (ft)	1354.84	Shear (lb/sq ft)	0.15	0.31	0.15
Alpha	1.57	Stream Power (lb/ft s)	0.12	0.62	0.12
Frctn Loss (ft)	0.17	Cum Volume (acre-ft)	16.73	21.56	7.27
C & E Loss (ft)	0.01	Cum SA (acres)	6.28	4.79	2.38

Plan: Plan 01 4 Mile Creek Oak RS: 1103.284 Profile: PF 1

E.G. Elev (ft)	1359.85	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.01	Wt n-Val	0.100	0.065	0.100
W.S. Elev (ft)	1359.84	Reach Len. (ft)	434.00	441.40	446.00
Crit W.S. (ft)		Flow Area (sq ft)	870.71	688.44	582.53
E.G. Slope (ft/ft)	0.000327	Area (sq ft)	870.71	688.44	582.53
Q Total (cfs)	1817.00	Flow (cfs)	596.29	803.12	417.58
Top Width (ft)	491.34	Top Width (ft)	213.52	144.56	133.27
Vel Total (ft/s)	0.85	Avg. Vel. (ft/s)	0.68	1.17	0.72
Max Chl Dpth (ft)	6.24	Hydr. Depth (ft)	4.08	4.76	4.37
Conv. Total (cfs)	100494.9	Conv. (cfs)	32979.9	44419.3	23095.6
Length Wid. (ft)	440.50	Wetted Per. (ft)	213.94	145.19	133.66
Min Ch El (ft)	1353.60	Shear (lb/sq ft)	0.08	0.10	0.09
Alpha	1.21	Stream Power (lb/ft s)	0.06	0.11	0.06
Frcn Loss (ft)	0.26	Cum Volume (acre-ft)	12.70	17.19	4.15
C & E Loss (ft)	0.01	Cum SA (acres)	4.99	3.79	1.34

Plan: Plan 01 4 Mile Creek Oak RS: 661.8854 Profile: PF 1

E.G. Elev (ft)	1359.58	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.07	Wt n-Val	0.100	0.065	0.100
W.S. Elev (ft)	1359.51	Reach Len. (ft)	592.00	597.80	605.00
Crit W.S. (ft)		Flow Area (sq ft)	206.91	759.07	35.83
E.G. Slope (ft/ft)	0.001390	Area (sq ft)	206.91	759.07	35.83
Q Total (cfs)	1817.00	Flow (cfs)	118.36	1677.25	21.39
Top Width (ft)	409.13	Top Width (ft)	197.04	180.14	31.95
Vel Total (ft/s)	1.81	Avg. Vel. (ft/s)	0.57	2.21	0.60
Max Chl Dpth (ft)	6.95	Hydr. Depth (ft)	1.05	4.21	1.12
Conv. Total (cfs)	48732.3	Conv. (cfs)	3174.4	44984.2	573.8
Length Wid. (ft)	596.62	Wetted Per. (ft)	197.21	181.86	32.02
Min Ch El (ft)	1352.56	Shear (lb/sq ft)	0.09	0.36	0.10
Alpha	1.38	Stream Power (lb/ft s)	0.05	0.80	0.06
Frcn Loss (ft)	0.54	Cum Volume (acre-ft)	7.33	9.86	0.99
C & E Loss (ft)	0.01	Cum SA (acres)	2.95	2.14	0.50

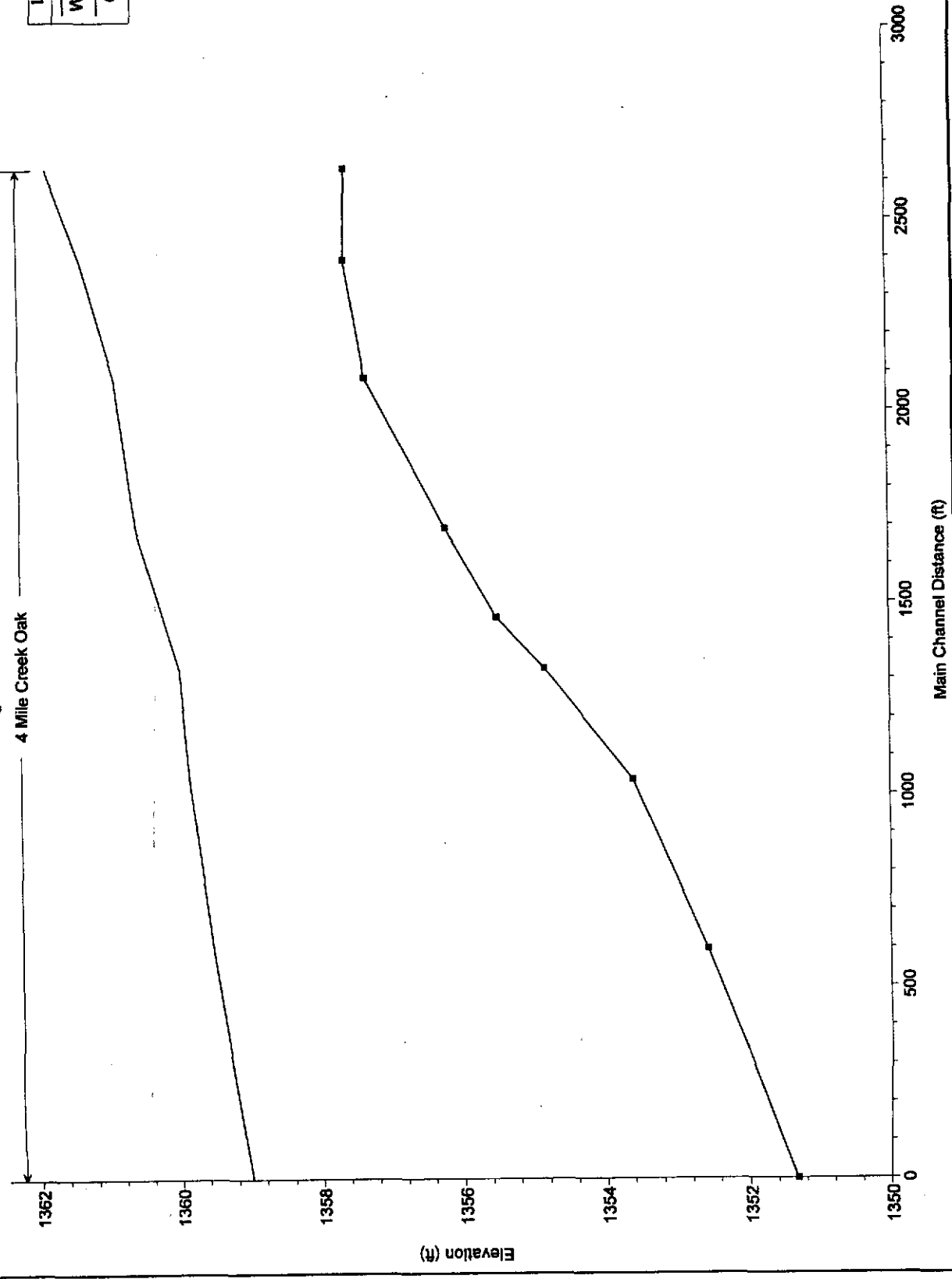
Plan: Plan 01 4 Mile Creek Oak RS: 64.08447 Profile: PF 1

E.G. Elev (ft)	1359.03	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.03	Wt n-Val	0.100	0.065	0.100
W.S. Elev (ft)	1359.00	Reach Len. (ft)			
Crit W.S. (ft)	1355.55	Flow Area (sq ft)	872.42	677.77	106.24
E.G. Slope (ft/ft)	0.000658	Area (sq ft)	872.42	677.77	106.24
Q Total (cfs)	2049.00	Flow (cfs)	792.47	1179.03	77.50
Top Width (ft)	409.08	Top Width (ft)	237.01	132.26	39.80
Vel Total (ft/s)	1.24	Avg. Vel. (ft/s)	0.91	1.74	0.73
Max Chl Dpth (ft)	7.67	Hydr. Depth (ft)	3.68	5.12	2.67
Conv. Total (cfs)	79879.2	Conv. (cfs)	30894.1	45963.9	3021.2
Length Wid. (ft)		Wetted Per. (ft)	237.13	132.65	40.13
Min Ch El (ft)	1351.33	Shear (lb/sq ft)	0.15	0.21	0.11
Alpha	1.36	Stream Power (lb/ft s)	0.14	0.37	0.08
Frcn Loss (ft)		Cum Volume (acre-ft)			
C & E Loss (ft)		Cum SA (acres)			

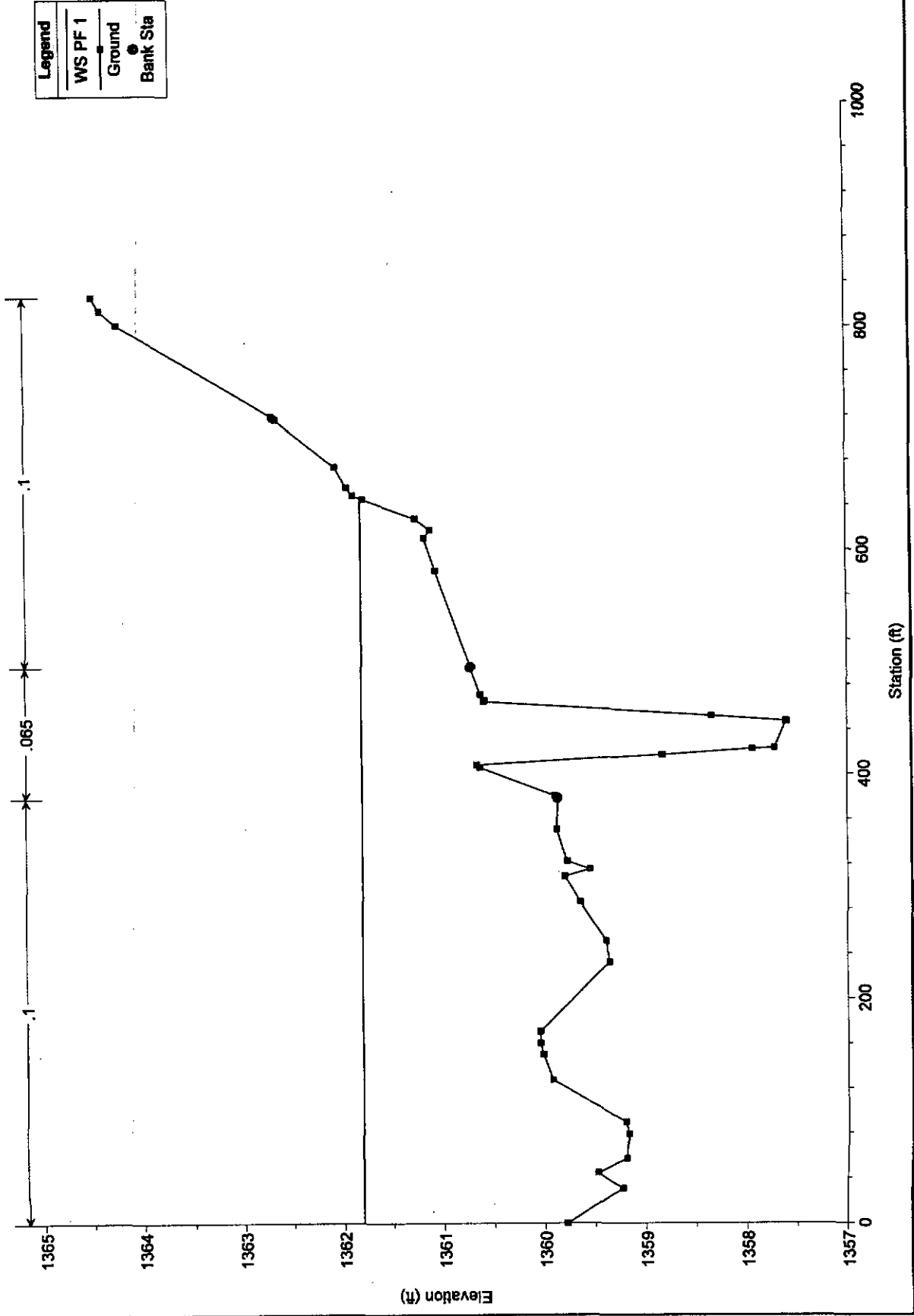
Existing Plan: Plan 01 2/13/2007

4 Mile Creek Oak

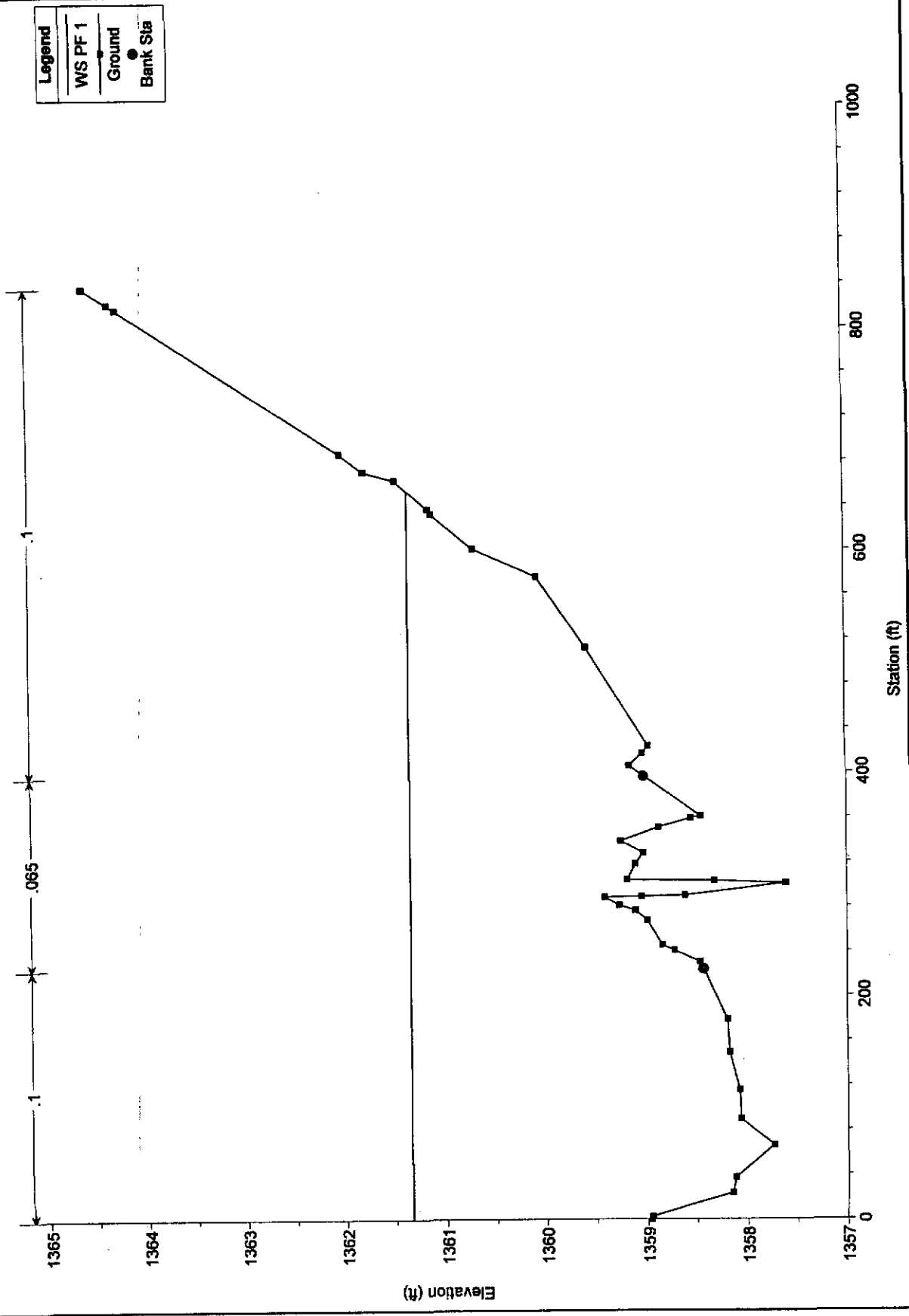
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—●—	Ground



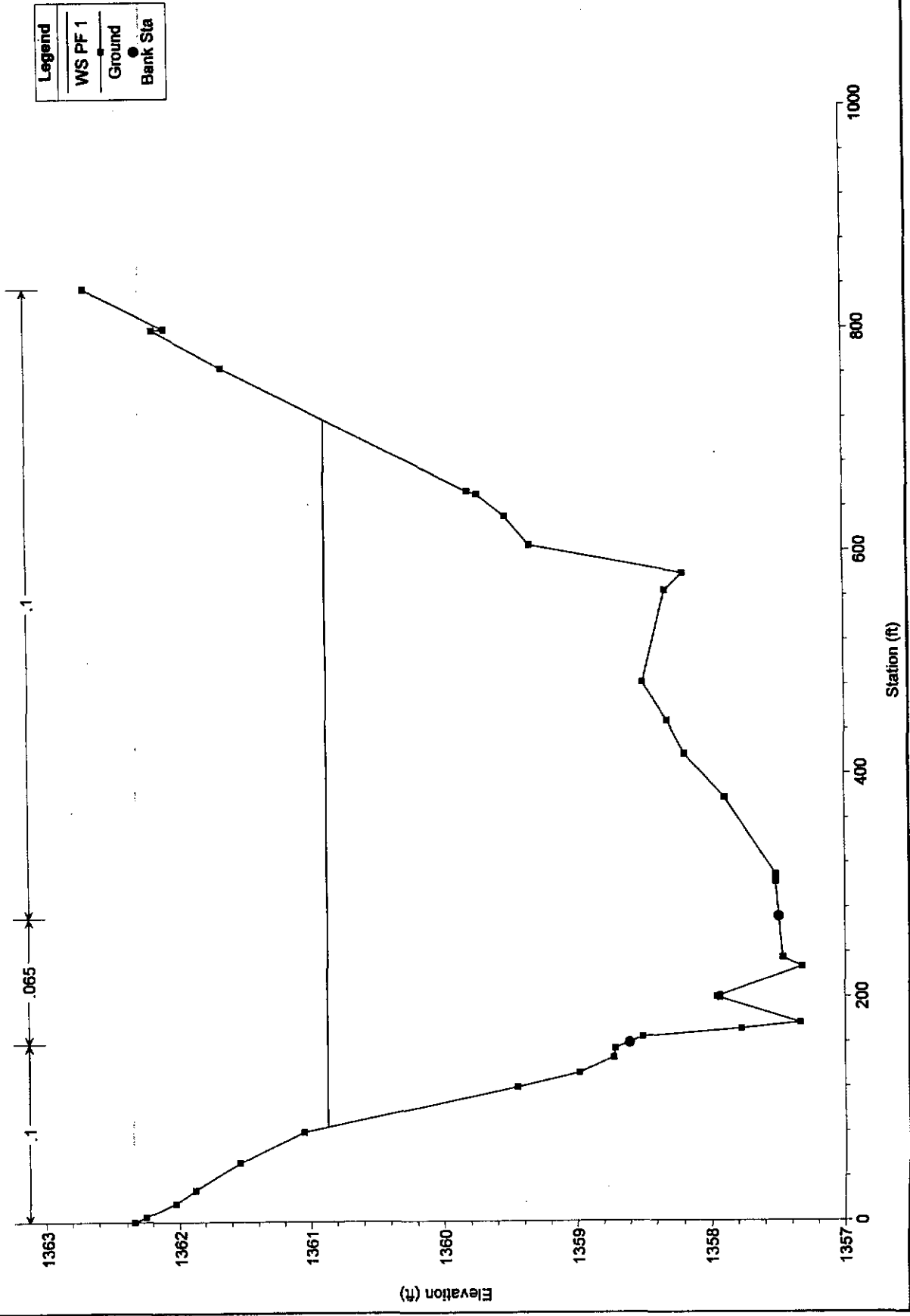
Existing Plan: Plan 01 2/13/2007



Existing Plan: Plan 01 2/13/2007

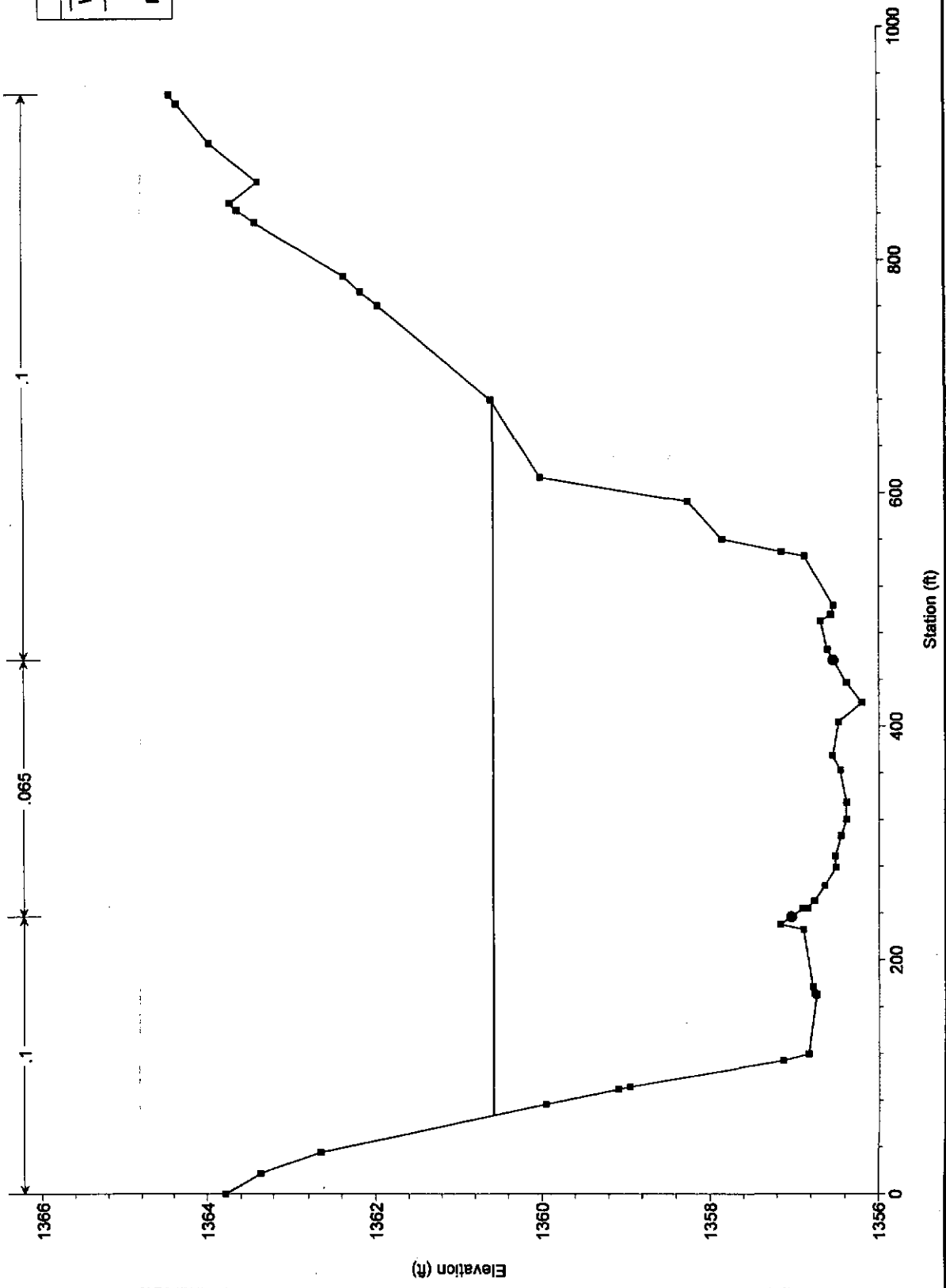


Existing Plan: Plan 01 2/13/2007

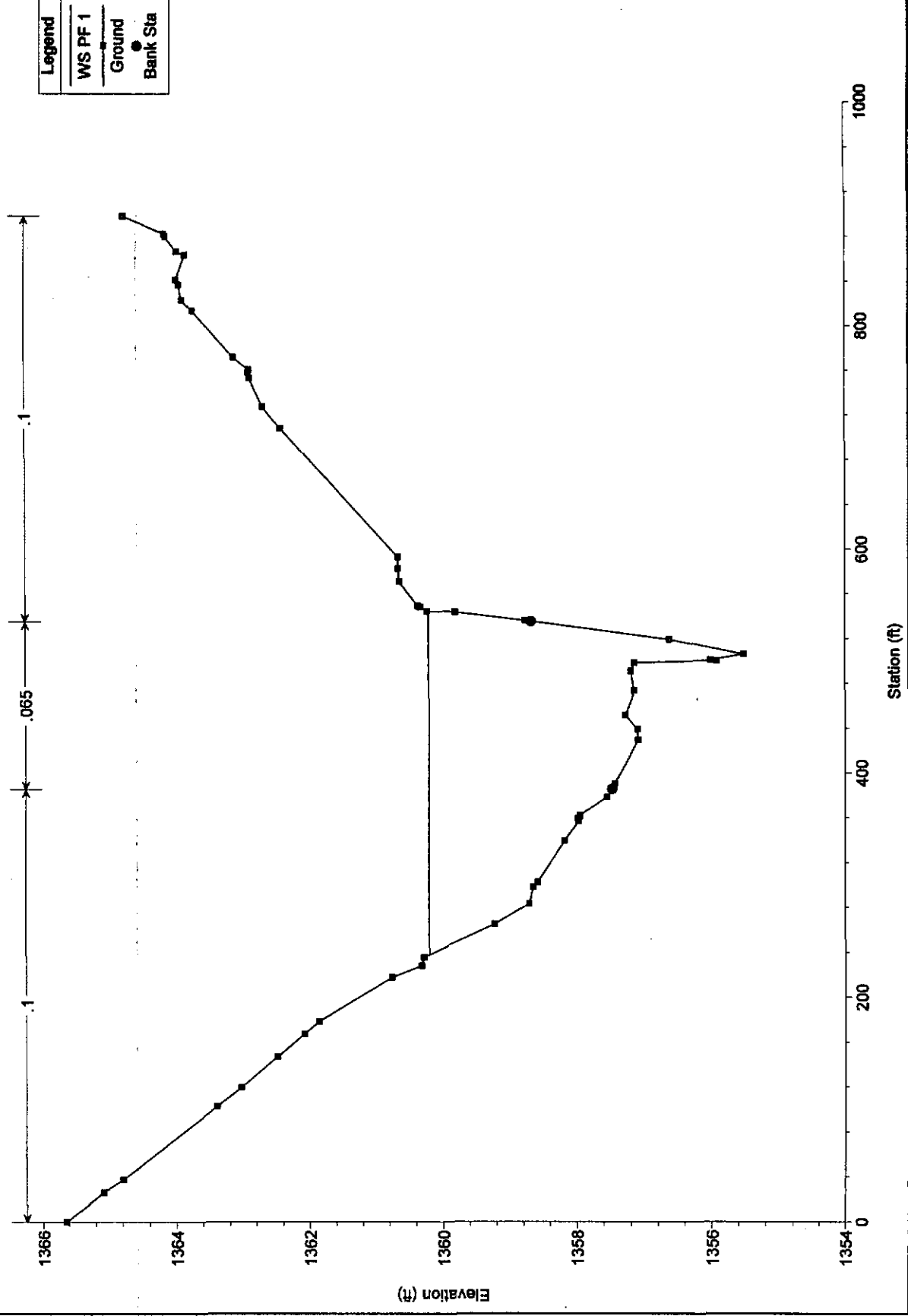


Existing Plan: Plan 01 2/13/2007

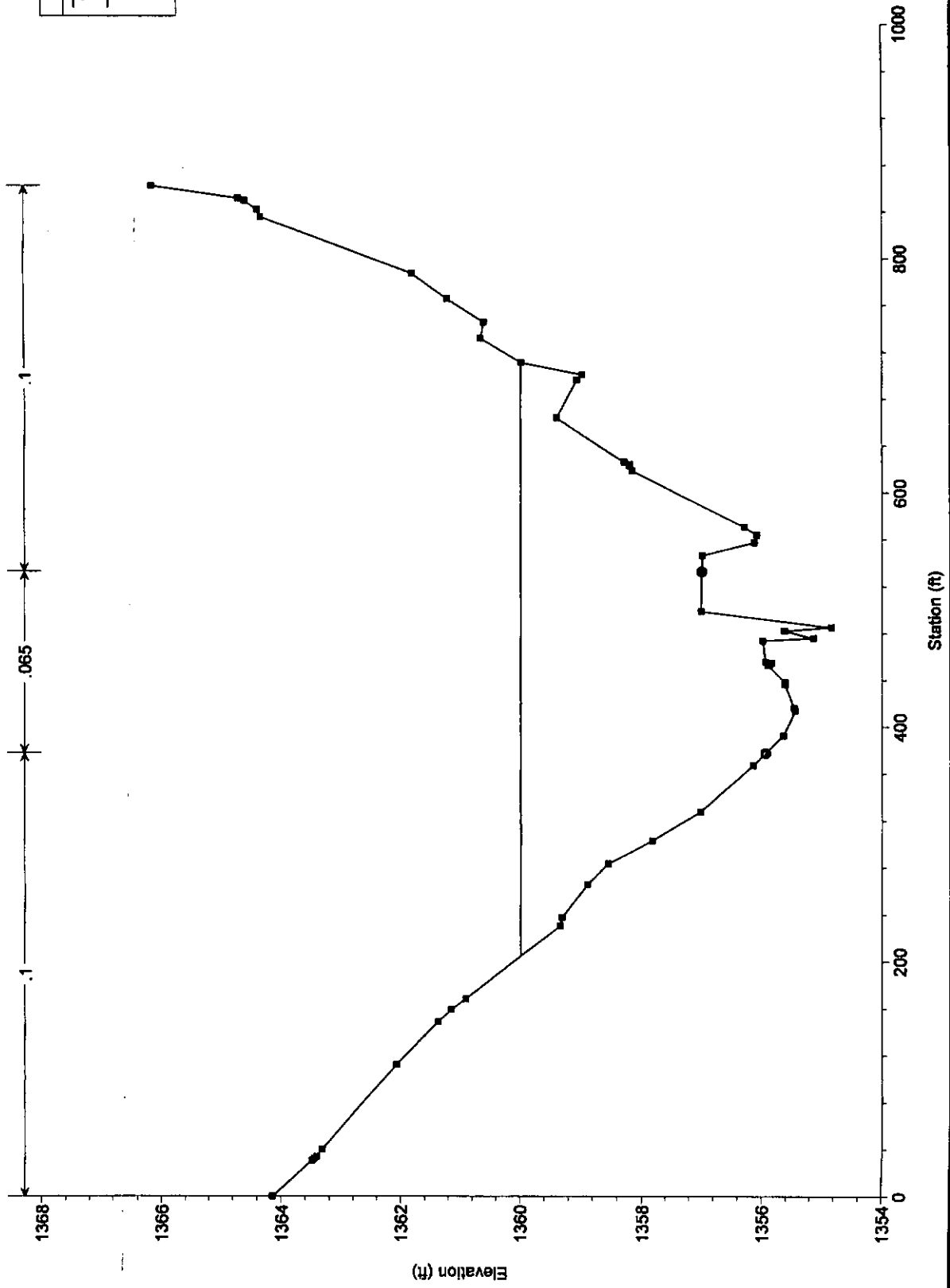
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Existing Plan: Plan 01 2/13/2007

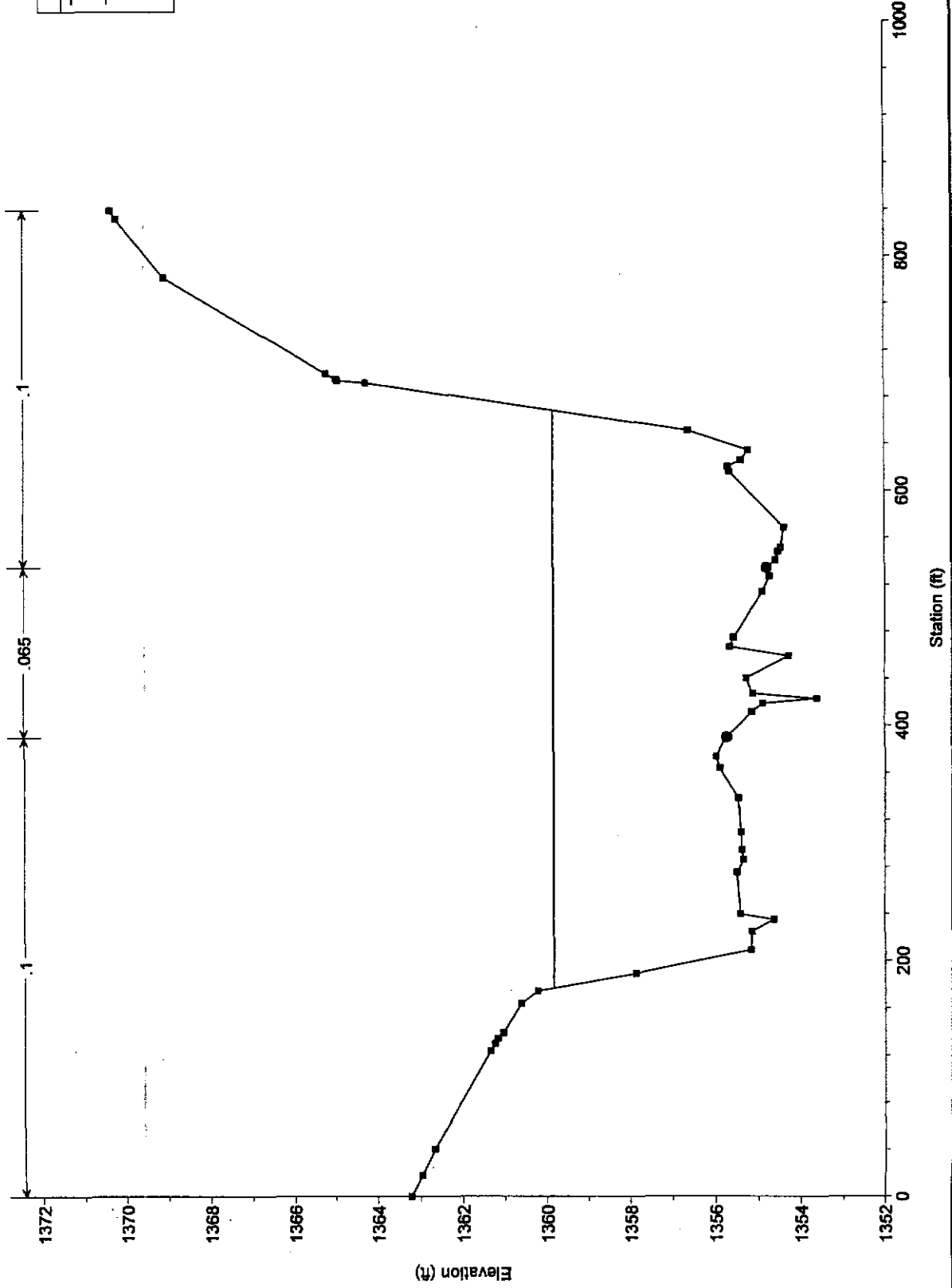


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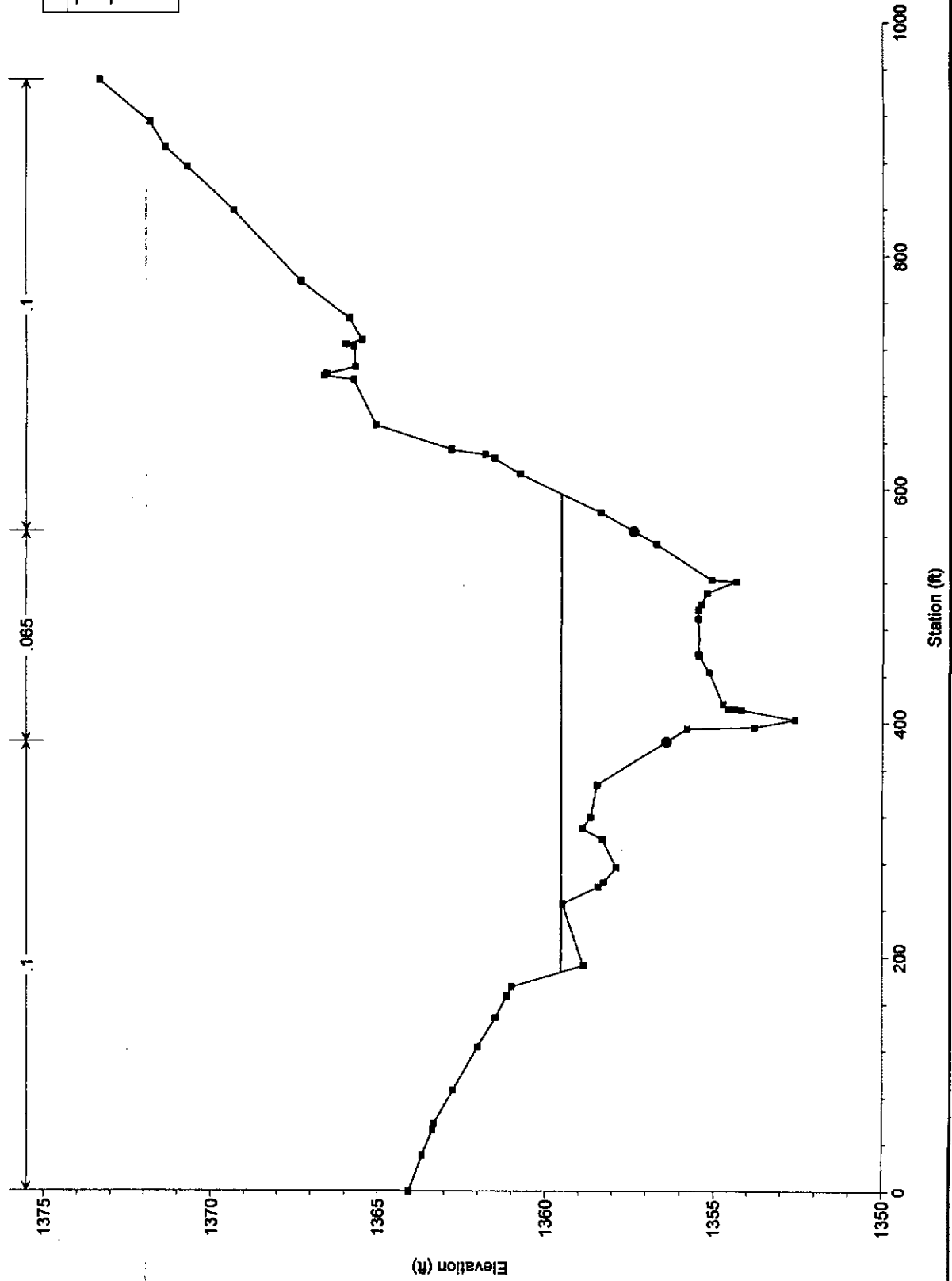


Existing Plan: Plan 01 2/13/2007

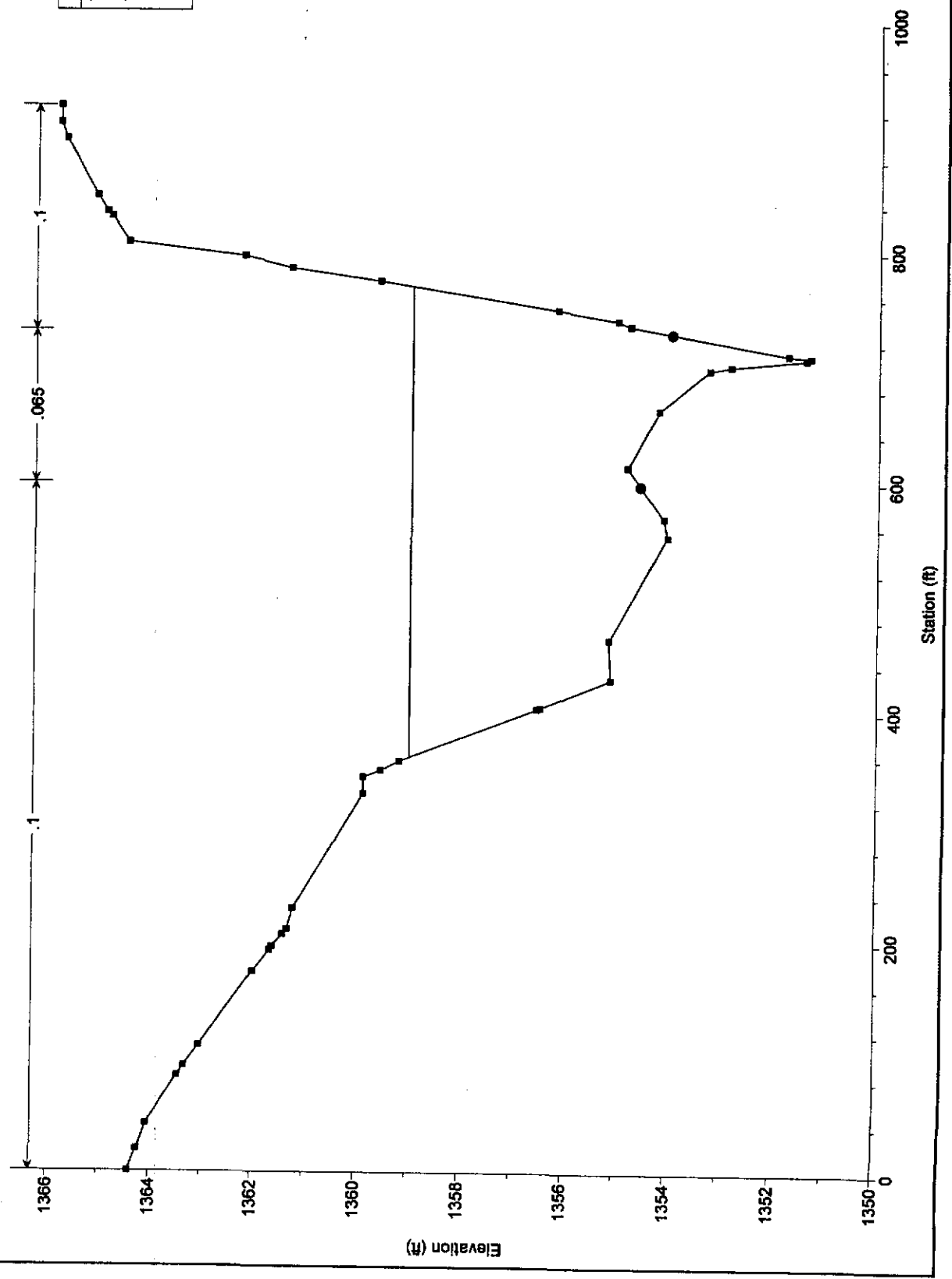
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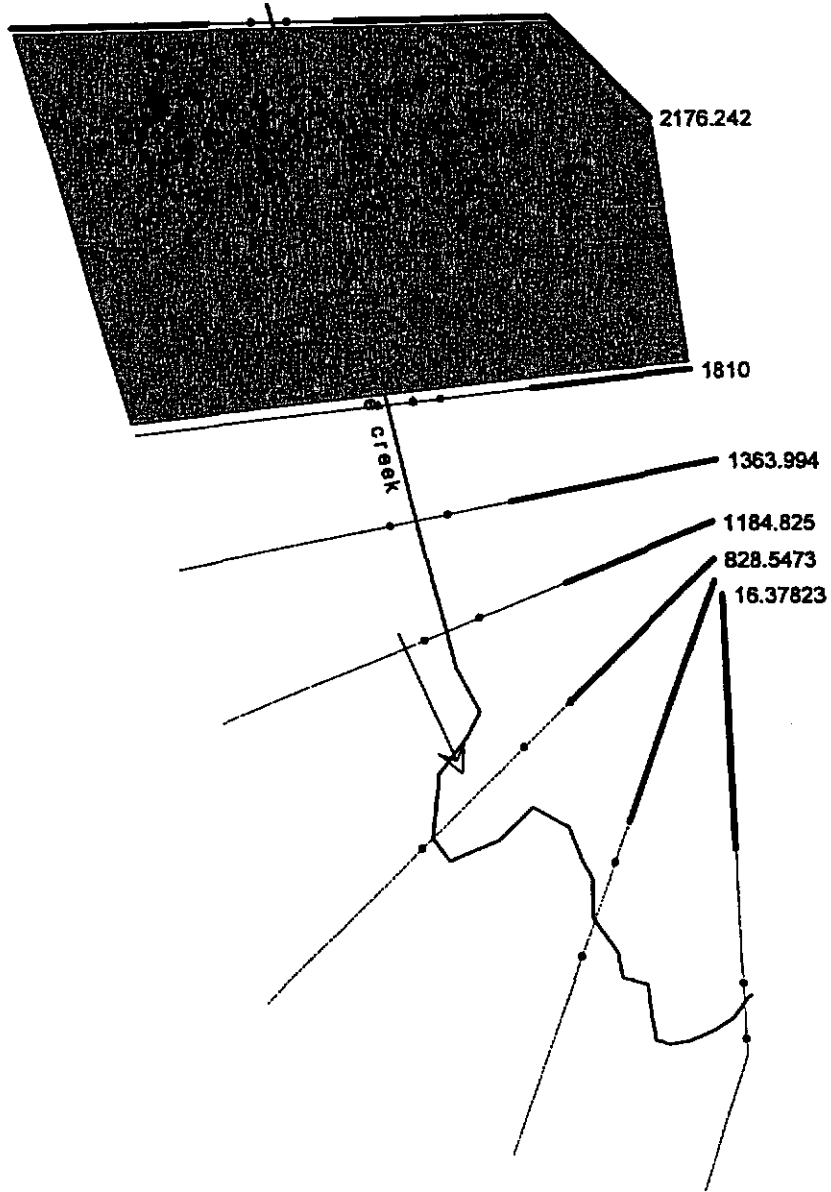
Existing Plan: Plan 01 2/13/2007



Existing Plan: Plan 01 2/13/2007



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HEC-RAS Plan: nproposal4 River: 4 mile creek Reach: oak Profile: PF 1

Reach	River Sta	Profile	C Total	Min Ch. E	W.B. Elev	Crit W.B.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Ch
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
oak	2175.242	PF 1	1817.00	1357.00	1362.43	1360.38	1362.67	0.003911	4.42	809.08	200.00	0.33
oak	2170	Culvert										
oak	1810	PF 1	1817.00	1355.50	1361.08	1358.71	1361.00	0.006573	5.83	311.79	489.70	0.43
oak	1650.843	PF 1	1817.00	1356.20	1361.09	1356.63	1361.13	0.006005	1.84	1278.84	350.00	0.15
oak	1363.864	PF 1	1817.00	1355.00	1360.71	1358.54	1360.79	0.002435	2.72	886.09	280.00	0.25
oak	1194.825	PF 1	1817.00	1354.70	1360.25	1357.83	1360.33	0.002715	2.85	851.81	233.00	0.25
oak	828.5473	PF 1	1817.00	1353.88	1359.68	1357.03	1359.73	0.001119	1.90	1085.49	344.40	0.17
oak	409.8100	PF 1	1817.00	1352.53	1359.28	1355.61	1359.32	0.000880	2.00	1082.08	290.00	0.16
oak	16.37823	PF 1	2049.00	1351.48	1359.00	1355.37	1359.03	0.000822	1.87	1650.08	363.32	0.13

Plan: nproposal4 4 mile creek oak RS: 2176.242 Profile: PF 1

E.G. Elev (ft)	1362.67	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.24	WL n-Val	0.100	0.065	0.100
W.S. Elev (ft)	1362.43	Reach Len (ft)	356.00	366.24	376.00
Crit W.S. (ft)	1360.38	Flow Area (sq ft)	179.87	312.31	116.91
E.G. Slope (ft/ft)	0.003911	Area (sq ft)	179.87	312.31	116.91
Q Total (cfs)	1817.00	Flow (cfs)	289.38	1379.57	148.05
Top Width (ft)	200.00	Top Width (ft)	74.04	57.50	68.46
Vel Total (ft/s)	2.98	Avg Vel (ft/s)	1.61	4.42	1.27
Max Chl Dpth (ft)	5.43	Hydr. Depth (ft)	2.43	5.43	1.71
Conv. Total (cfs)	29055.6	Conv. (cfs)	4627.4	22060.7	2367.5
Length Wtd. (ft)	366.24	Wetted Per. (ft)	78.96	57.50	73.49
Min Ch El (ft)	1357.00	Shear (lb/sq ft)	0.58	1.33	0.39
Alpha	1.73	Stream Power (lb/ft s)	0.89	5.86	0.49
Frcn Loss (ft)		Cum Volume (acre-ft)	23.63	27.13	4.91
C & E Loss (ft)		Cum SA (acres)	6.78	5.97	3.01

Plan: nproposal4 4 mile creek oak RS: 1810 Profile: PF 1

E.G. Elev (ft)	1361.60	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.53	WL n-Val		0.065	
W.S. Elev (ft)	1361.08	Reach Len (ft)	185.00	186.65	187.00
Crit W.S. (ft)	1358.71	Flow Area (sq ft)		311.79	
E.G. Slope (ft/ft)	0.006573	Area (sq ft)	948.25	311.79	65.25
Q Total (cfs)	1817.00	Flow (cfs)		1817.00	
Top Width (ft)	489.70	Top Width (ft)	324.49	55.92	109.29
Vel Total (ft/s)	5.83	Avg Vel (ft/s)		5.83	
Max Chl Dpth (ft)	5.58	Hydr. Depth (ft)		5.58	
Conv. Total (cfs)	22411.1	Conv. (cfs)		22411.1	
Length Wtd. (ft)	186.23	Wetted Per. (ft)		55.92	
Min Ch El (ft)	1355.50	Shear (lb/sq ft)		2.29	
Alpha	1.00	Stream Power (lb/ft s)		13.33	
Frcn Loss (ft)	0.33	Cum Volume (acre-ft)	19.02	24.51	4.13
C & E Loss (ft)	0.15	Cum SA (acres)	5.15	5.50	2.24

Plan: nproposal4 4 mile creek oak RS: 1550.643 Profile: PF 1

E.G. Elev (ft)	1361.13	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.04	WL n-Val	0.100	0.065	0.100
W.S. Elev (ft)	1361.09	Reach Len (ft)	255.00	259.36	264.00
Crit W.S. (ft)	1356.83	Flow Area (sq ft)	746.00	475.81	57.03
E.G. Slope (ft/ft)	0.000805	Area (sq ft)	746.00	475.81	57.03
Q Total (cfs)	1817.00	Flow (cfs)	924.30	876.81	15.88
Top Width (ft)	350.00	Top Width (ft)	145.02	99.00	105.98
Vel Total (ft/s)	1.42	Avg Vel (ft/s)	1.24	1.84	0.28
Max Chl Dpth (ft)	5.89	Hydr. Depth (ft)	5.14	4.81	0.54
Conv. Total (cfs)	64037.2	Conv. (cfs)	32575.6	30901.9	559.8
Length Wtd. (ft)	258.08	Wetted Per. (ft)	148.08	99.37	106.21
Min Ch El (ft)	1355.20	Shear (lb/sq ft)	0.25	0.24	0.03
Alpha	1.20	Stream Power (lb/ft s)	0.31	0.44	0.01
Frcn Loss (ft)	0.34	Cum Volume (acre-ft)	15.43	22.82	3.87
C & E Loss (ft)	0.00	Cum SA (acres)	4.15	5.16	1.78

Plan: nproposal4 4 mile creek oak RS: 1363.994 Profile: PF 1

E.G. Elev (ft)	1360.79	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.08	Wt. n-Val	0.100	0.065	0.100
W.S. Elev (ft)	1360.71	Reach Len. (ft)	179.00	179.17	179.00
Crit W.S. (ft)	1358.54	Flow Area (sq ft)	328.87	351.18	216.04
E.G. Slope (ft/ft)	0.002435	Area (sq ft)	328.87	351.18	216.04
Q Total (cfs)	1817.00	Flow (cfs)	522.37	955.64	338.99
Top Width (ft)	260.00	Top Width (ft)	101.05	92.76	66.19
Vel Total (ft/s)	2.03	Avg Vel. (ft/s)	1.59	2.72	1.57
Max Chl Dpth (ft)	5.71	Hydr. Depth (ft)	3.25	3.79	3.26
Conv. Total (cfs)	36819.4	Conv. (cfs)	10585.3	19364.9	6869.3
Length Wid. (ft)	179.08	Wetted Per. (ft)	103.16	93.74	69.02
Min Ch El (ft)	1355.00	Shear (lb/sq ft)	0.48	0.57	0.48
Alpha	1.24	Stream Power (lb/ft s)	0.77	1.55	0.75
Frctn Loss (ft)	0.46	Cum Volume (acre-ft)	12.28	20.36	3.04
C & E Loss (ft)	0.00	Cum SA (acres)	3.43	4.59	1.26

Plan: nproposal4 4 mile creek oak RS: 1184.825 Profile: PF 1

E.G. Elev (ft)	1360.33	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.08	Wt. n-Val	0.100	0.065	
W.S. Elev (ft)	1360.25	Reach Len. (ft)	350.00	356.28	362.00
Crit W.S. (ft)	1357.83	Flow Area (sq ft)	549.21	302.60	
E.G. Slope (ft/ft)	0.002715	Area (sq ft)	549.21	302.60	
Q Total (cfs)	1817.00	Flow (cfs)	1016.36	800.64	
Top Width (ft)	233.00	Top Width (ft)	146.26	86.74	
Vel Total (ft/s)	2.13	Avg Vel. (ft/s)	1.85	2.65	
Max Chl Dpth (ft)	5.55	Hydr. Depth (ft)	3.75	3.49	
Conv. Total (cfs)	34869.6	Conv. (cfs)	19504.8	15364.9	
Length Wid. (ft)	354.36	Wetted Per. (ft)	148.63	91.42	
Min Ch El (ft)	1354.70	Shear (lb/sq ft)	0.63	0.56	
Alpha	1.10	Stream Power (lb/ft s)	1.16	1.48	
Frctn Loss (ft)	0.59	Cum Volume (acre-ft)	10.48	19.01	2.59
C & E Loss (ft)	0.01	Cum SA (acres)	2.92	4.22	1.12

Plan: nproposal4 4 mile creek oak RS: 828.5473 Profile: PF 1

E.G. Elev (ft)	1359.73	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.05	Wt. n-Val	0.100	0.065	0.100
W.S. Elev (ft)	1359.68	Reach Len. (ft)	380.00	422.64	460.00
Crit W.S. (ft)	1357.03	Flow Area (sq ft)	167.83	884.46	33.19
E.G. Slope (ft/ft)	0.001119	Area (sq ft)	357.55	884.53	33.19
Q Total (cfs)	1817.00	Flow (cfs)	115.21	1677.77	24.02
Top Width (ft)	344.40	Top Width (ft)	99.97	225.88	18.55
Vel Total (ft/s)	1.67	Avg Vel. (ft/s)	0.69	1.90	0.72
Max Chl Dpth (ft)	5.80	Hydr. Depth (ft)	1.68	3.92	1.79
Conv. Total (cfs)	54312.1	Conv. (cfs)	3443.7	50150.3	718.1
Length Wid. (ft)	421.36	Wetted Per. (ft)	103.43	226.42	18.89
Min Ch El (ft)	1353.88	Shear (lb/sq ft)	0.11	0.27	0.12
Alpha	1.20	Stream Power (lb/ft s)	0.08	0.52	0.09
Frctn Loss (ft)	0.41	Cum Volume (acre-ft)	6.83	14.16	2.46
C & E Loss (ft)	0.00	Cum SA (acres)	1.93	2.94	1.05

Plan: nproposal4 4 mile creek oak RS: 405.9100 Profile: PF 1

E.G. Elev (ft)	1359.32	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.06	Wt. n-Val	0.100	0.065	0.100
W.S. Elev (ft)	1359.26	Reach Len. (ft)	375.00	389.53	403.00
Crit W.S. (ft)	1355.61	Flow Area (sq ft)	144.28	808.20	139.60
E.G. Slope (ft/ft)	0.000860	Area (sq ft)	144.28	808.20	139.60
Q Total (cfs)	1817.00	Flow (cfs)	102.29	1814.57	100.15
Top Width (ft)	290.00	Top Width (ft)	68.06	156.56	65.38
Vel Total (ft/s)	1.66	Avg. Vel. (ft/s)	0.71	2.00	0.72
Max Chl Dpth (ft)	6.73	Hydr. Depth (ft)	2.12	5.16	2.14
Conv. Total (cfs)	61951.2	Conv. (cfs)	3487.5	55049.2	3414.5
Length Wtd. (ft)	386.53	Wetted Per. (ft)	69.54	157.14	66.10
Min Ch El (ft)	1352.53	Shear (lb/sq ft)	0.11	0.28	0.11
Alpha	1.30	Stream Power (lb/ft s)	0.08	0.55	0.08
Frcin Loss (ft)	0.28	Cum Volume (acre-ft)	4.64	5.94	1.54
C & E Loss (ft)	0.01	Cum SA (acres)	1.20	1.09	0.60

Plan: nproposal4 4 mile creek oak RS: 16.37823 Profile: PF 1

E.G. Elev (ft)	1359.03	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.03	Wt. n-Val	0.100	0.065	0.100
W.S. Elev (ft)	1359.00	Reach Len. (ft)			
Crit W.S. (ft)	1355.37	Flow Area (sq ft)	934.57	521.36	194.13
E.G. Slope (ft/ft)	0.000622	Area (sq ft)	934.57	521.36	194.13
Q Total (cfs)	2049.00	Flow (cfs)	926.51	973.74	148.75
Top Width (ft)	363.32	Top Width (ft)	211.17	87.10	65.05
Vel Total (ft/s)	1.24	Avg. Vel. (ft/s)	0.99	1.87	0.77
Max Chl Dpth (ft)	7.52	Hydr. Depth (ft)	4.43	5.99	2.98
Conv. Total (cfs)	82172.9	Conv. (cfs)	37158.6	39050.6	5965.6
Length Wtd. (ft)		Wetted Per. (ft)	213.53	87.91	65.27
Min Ch El (ft)	1351.48	Shear (lb/sq ft)	0.17	0.23	0.12
Alpha	1.39	Stream Power (lb/ft s)	0.17	0.43	0.09
Frcin Loss (ft)		Cum Volume (acre-ft)			
C & E Loss (ft)		Cum SA (acres)			

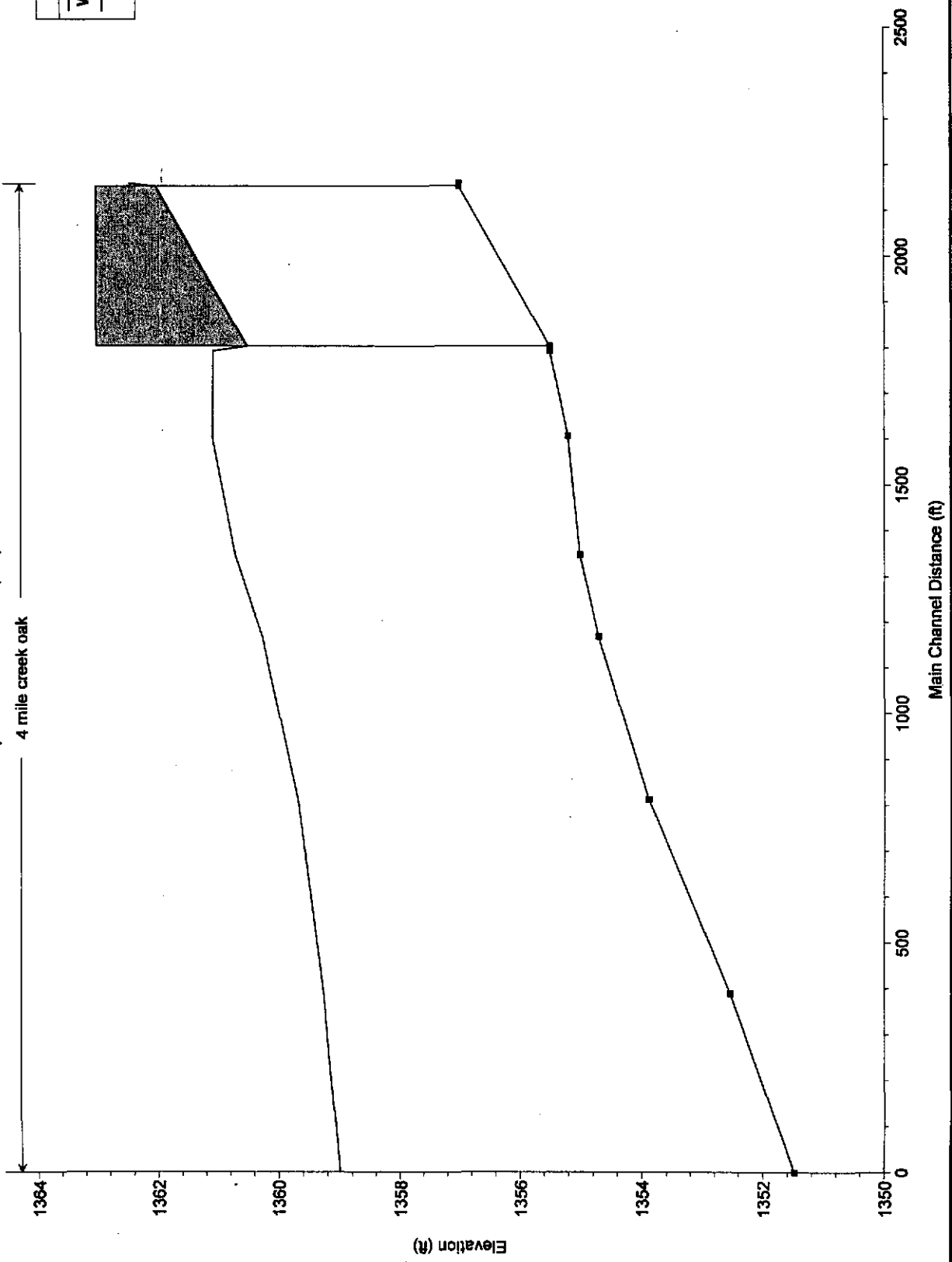
HEC-RAS Plan: nproposal4 River: 4 mile creek Reach: oak Profile: PF 1

Reach	River Sta	Profile	Q Total (cfs)	Min Chl El (ft)	W/S Elev (ft)	Crit W/S (ft)	E/G Elev (ft)	E/G Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Frictula # Chl
oak	2+76.242	PF-1	1817.00	1357.00	1362.43	1360.38	1362.67	0.003911	4.42	609.09	200.00	0.33
oak	2+70		Culvert									
oak	1810	PF-1	1817.00	1355.50	1361.08	1358.71	1361.60	0.006573	5.83	311.79	488.70	0.43
oak	1550.843	PF-1	1817.00	1355.20	1361.09	1358.83	1361.13	0.000805	1.84	1278.84	350.00	0.15
oak	1363.994	PF-1	1817.00	1355.00	1360.71	1358.54	1360.79	0.002435	2.72	896.09	260.00	0.25
oak	1184.825	PF-1	1817.00	1354.70	1360.25	1357.83	1360.33	0.002715	2.65	851.81	233.00	0.25
oak	828.5473	PF-1	1817.00	1353.88	1359.68	1357.03	1359.73	0.001119	1.90	1085.49	344.40	0.17
oak	405.9100	PF-1	1817.00	1352.53	1359.26	1355.61	1359.32	0.000860	2.00	1092.08	290.00	0.15
oak	16.37823	PF-1	2049.00	1351.48	1359.00	1355.37	1359.03	0.000622	1.87	1650.06	363.32	0.13

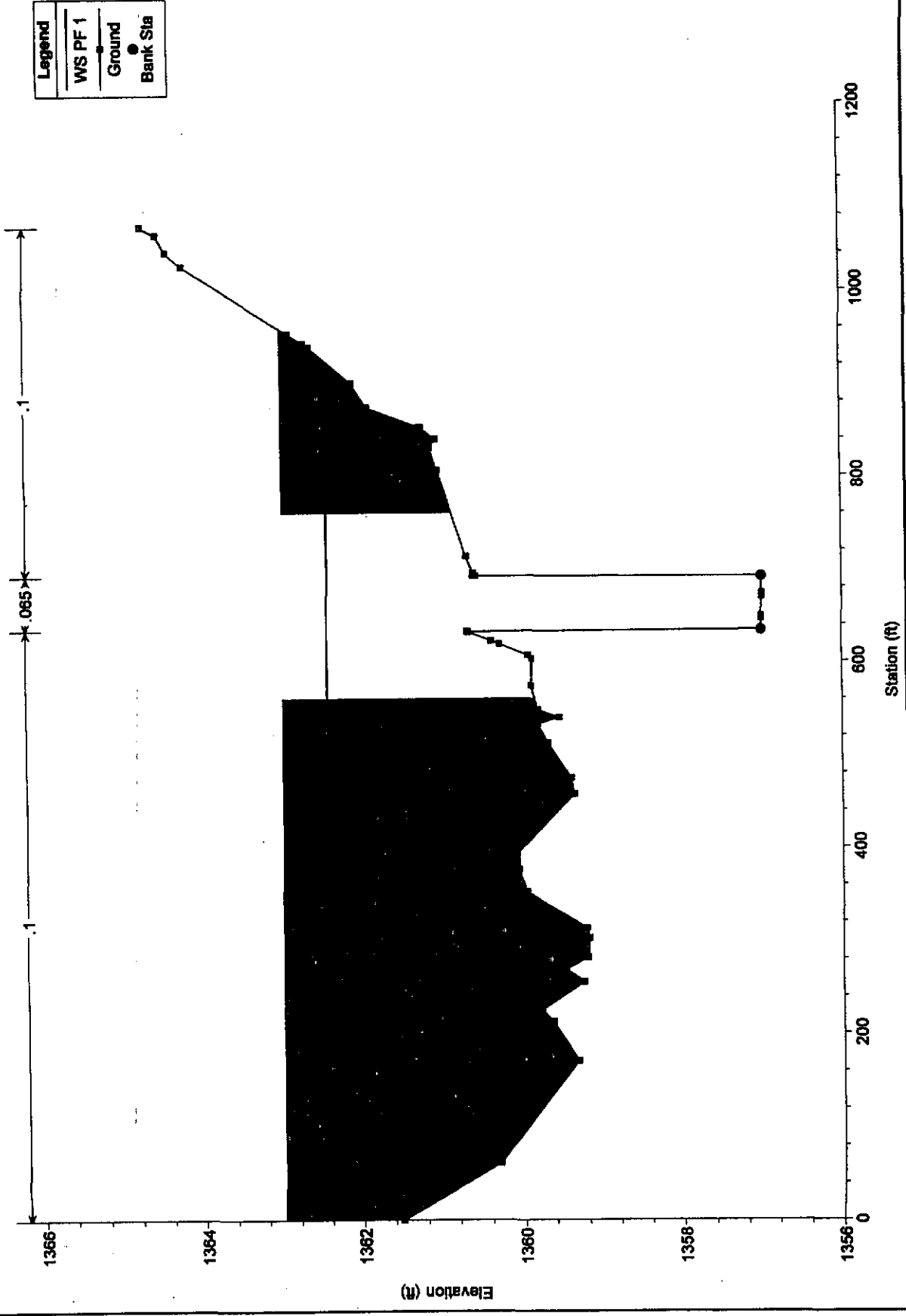
NP Proposed Plan: nproposal4 2/8/2007

4 mile creek oak

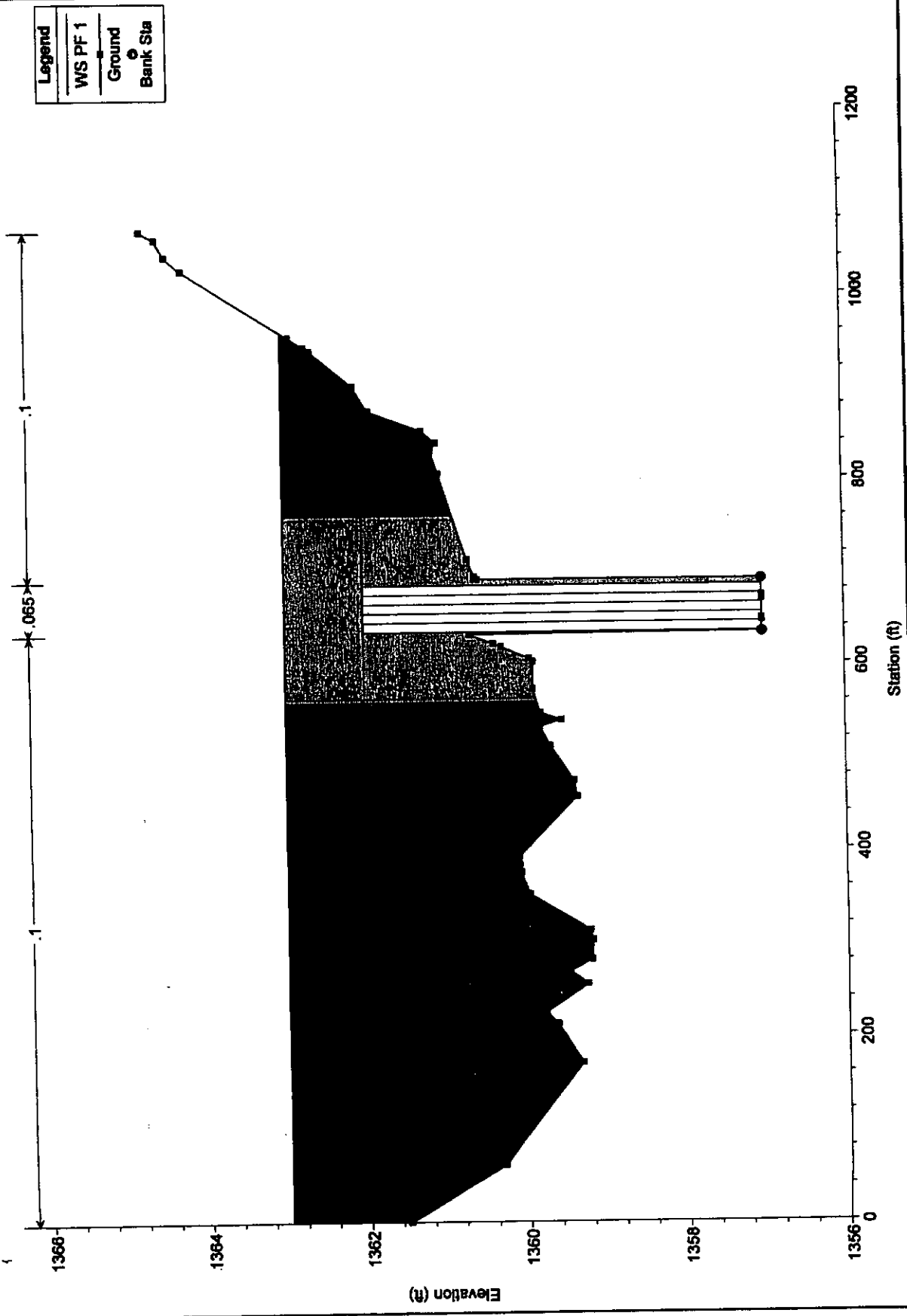
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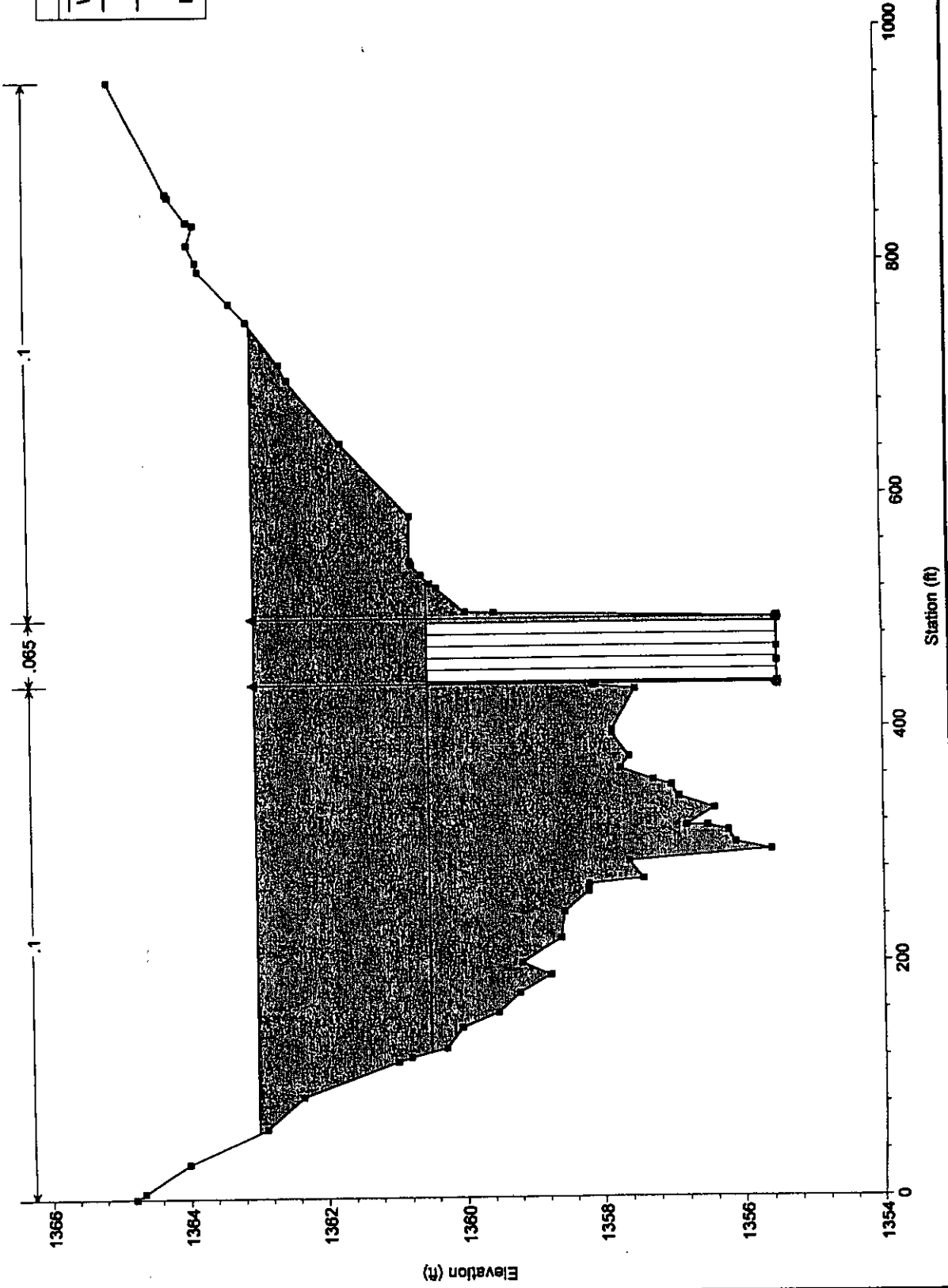


NProposed Plan: nproposal4 2/13/2007

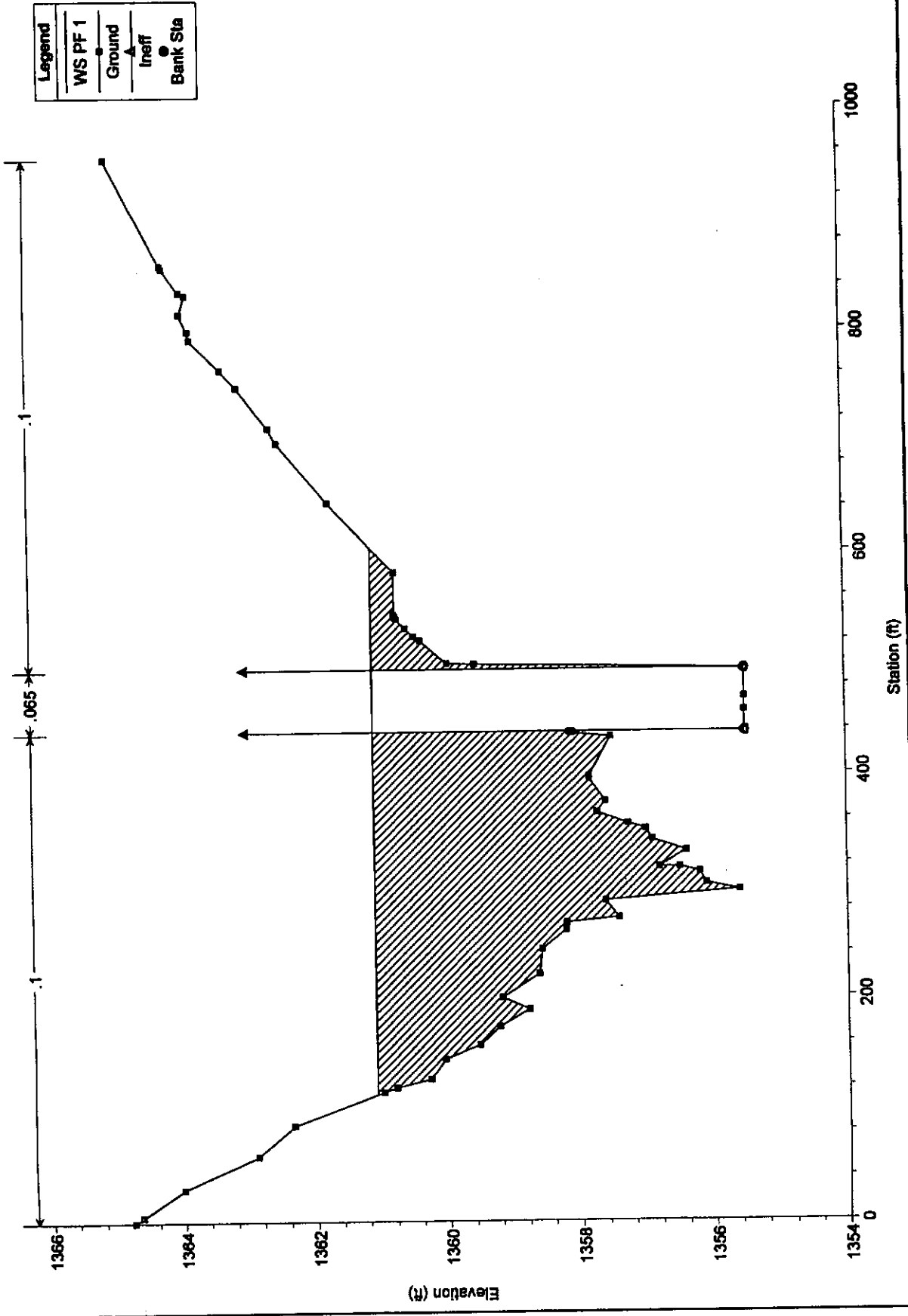


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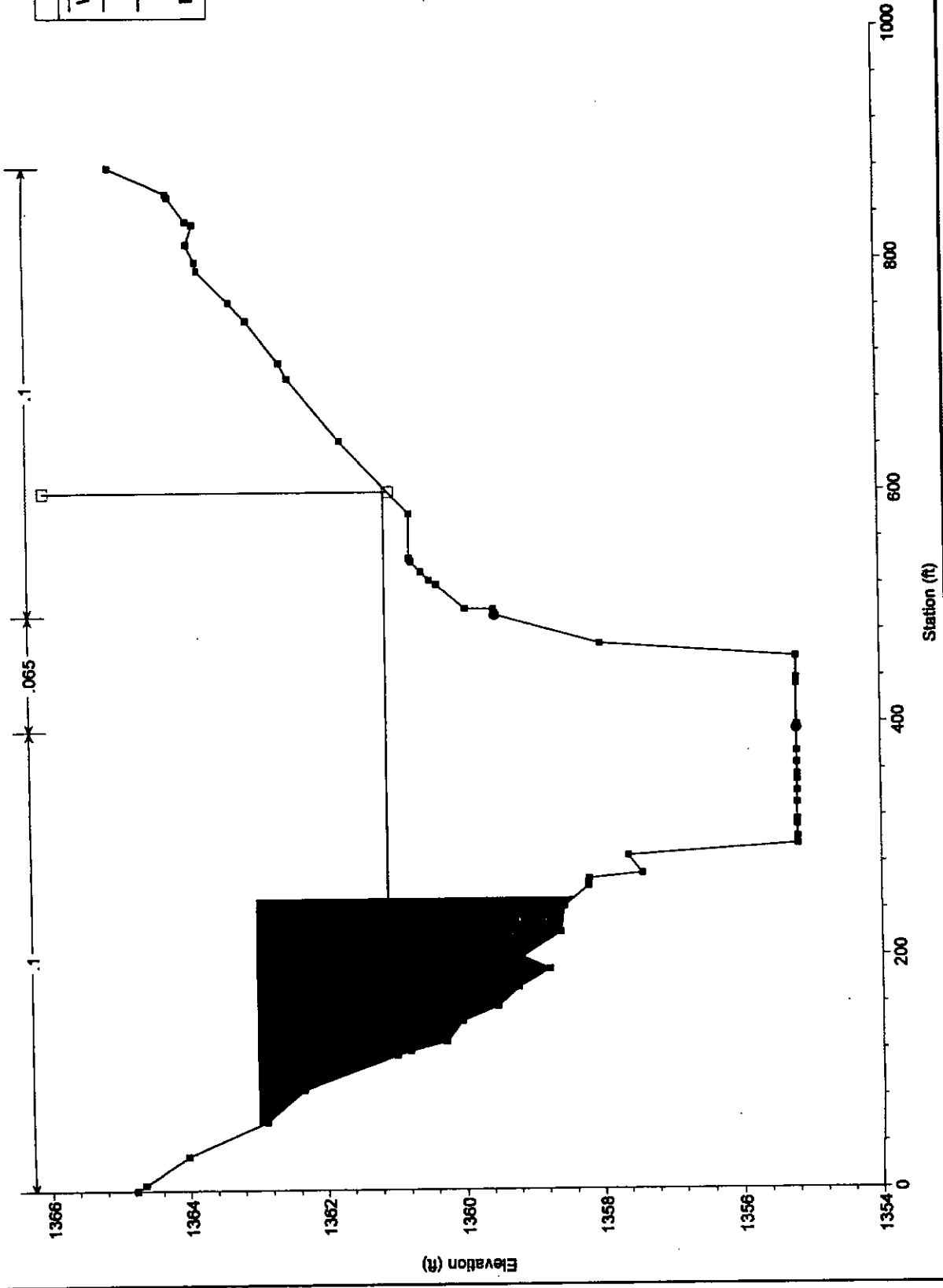


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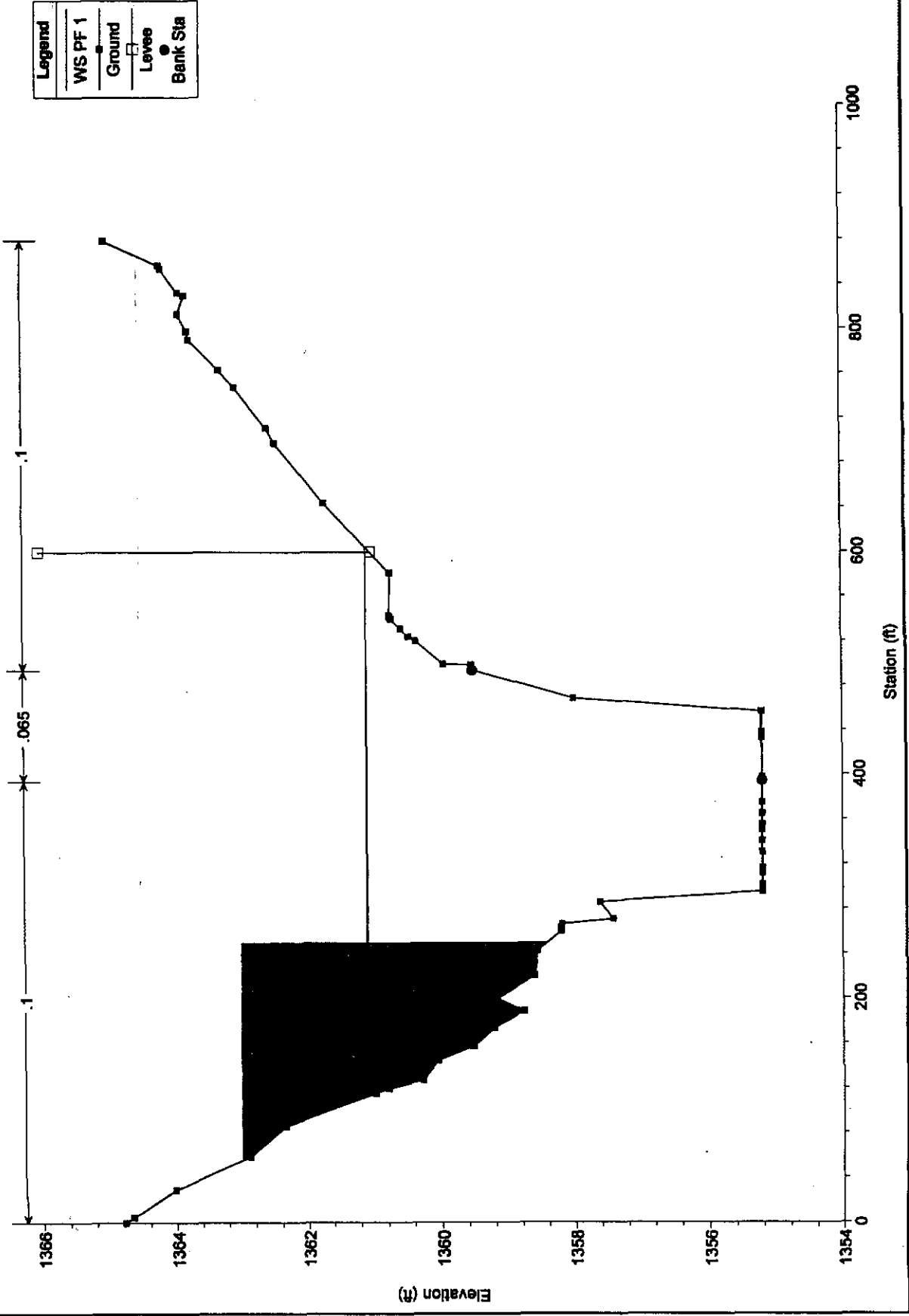


NProposed Plan: nproposak4 2/13/2007

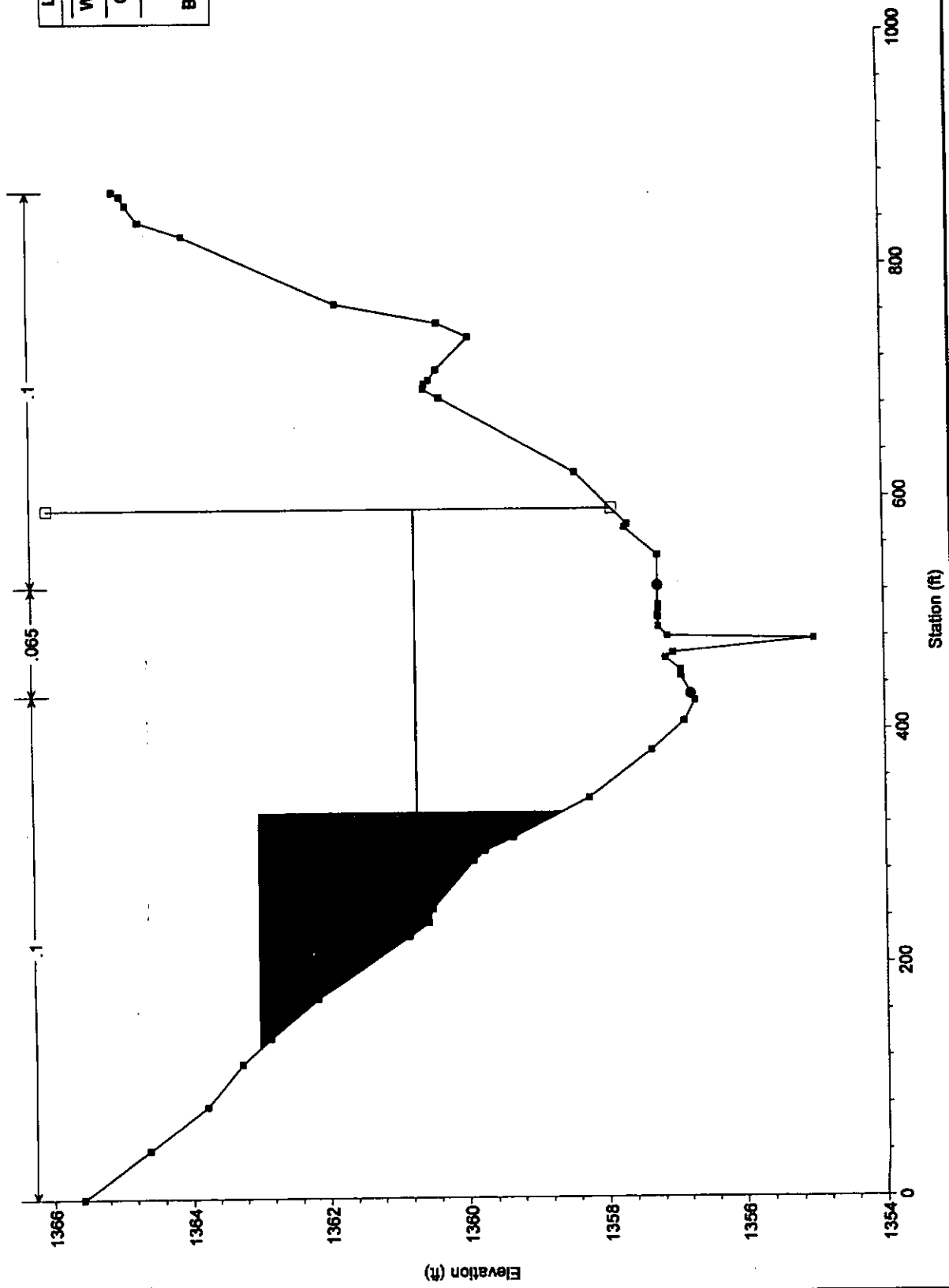
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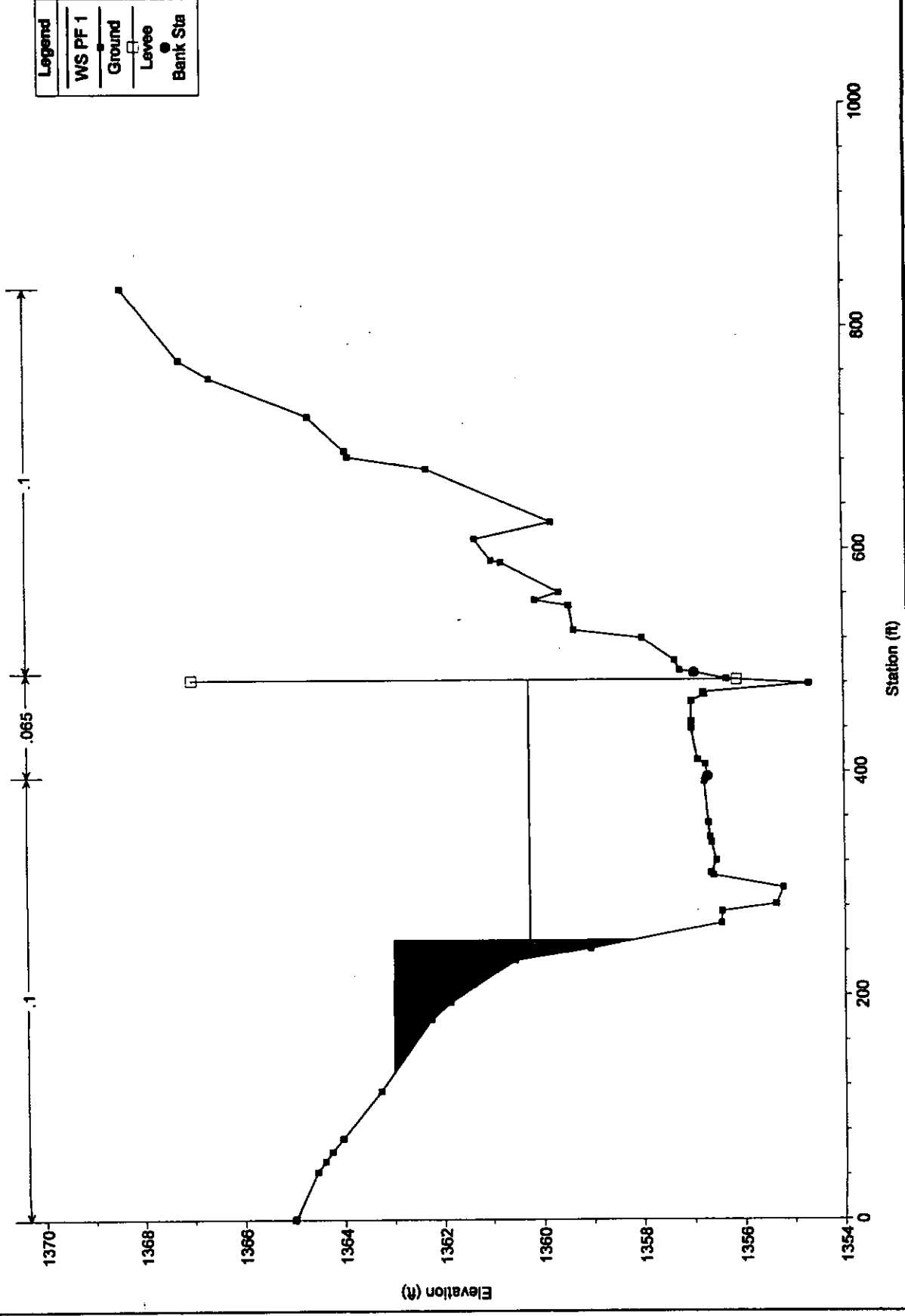
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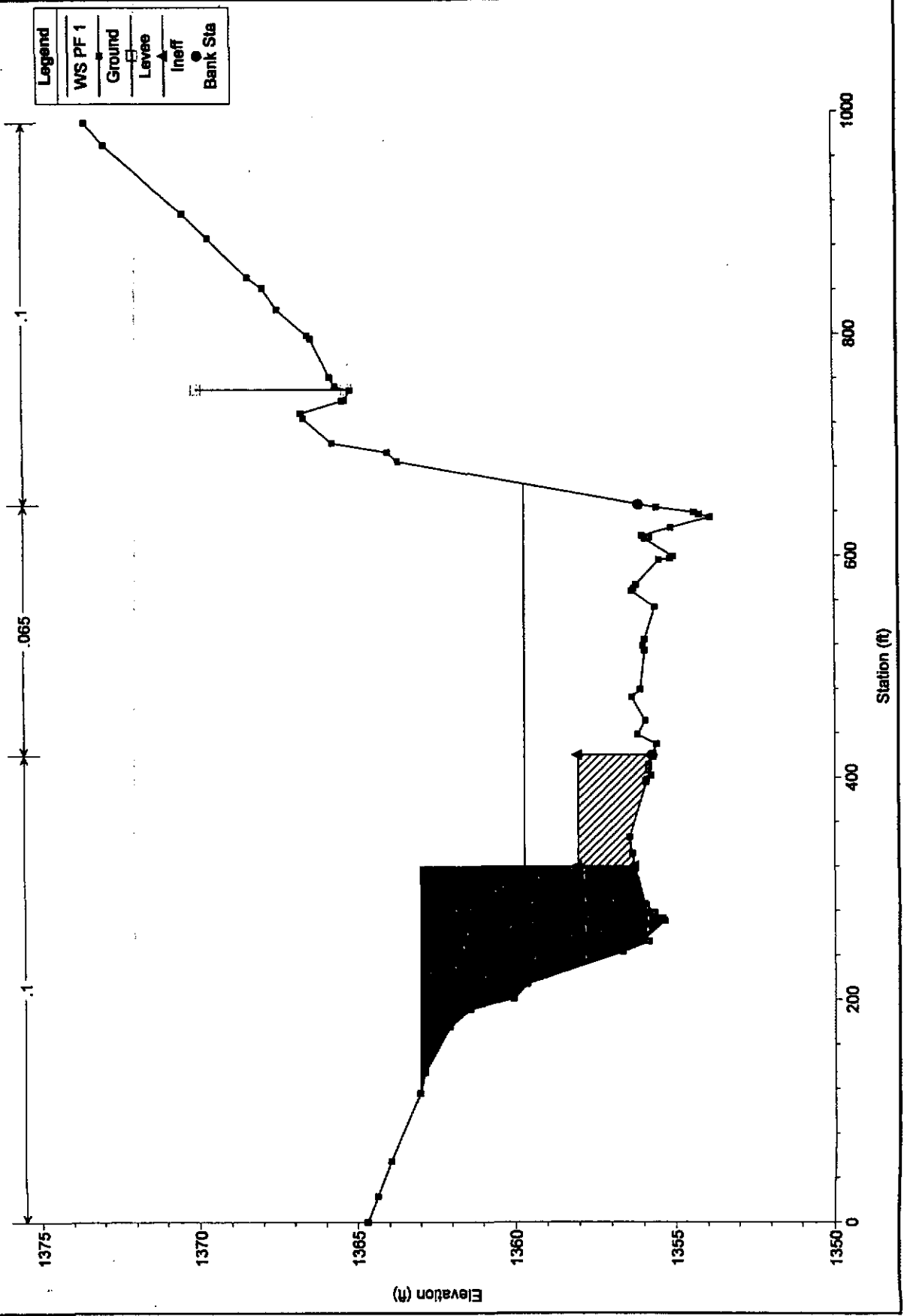
NProposed Plan: nproposal4 2/13/2007



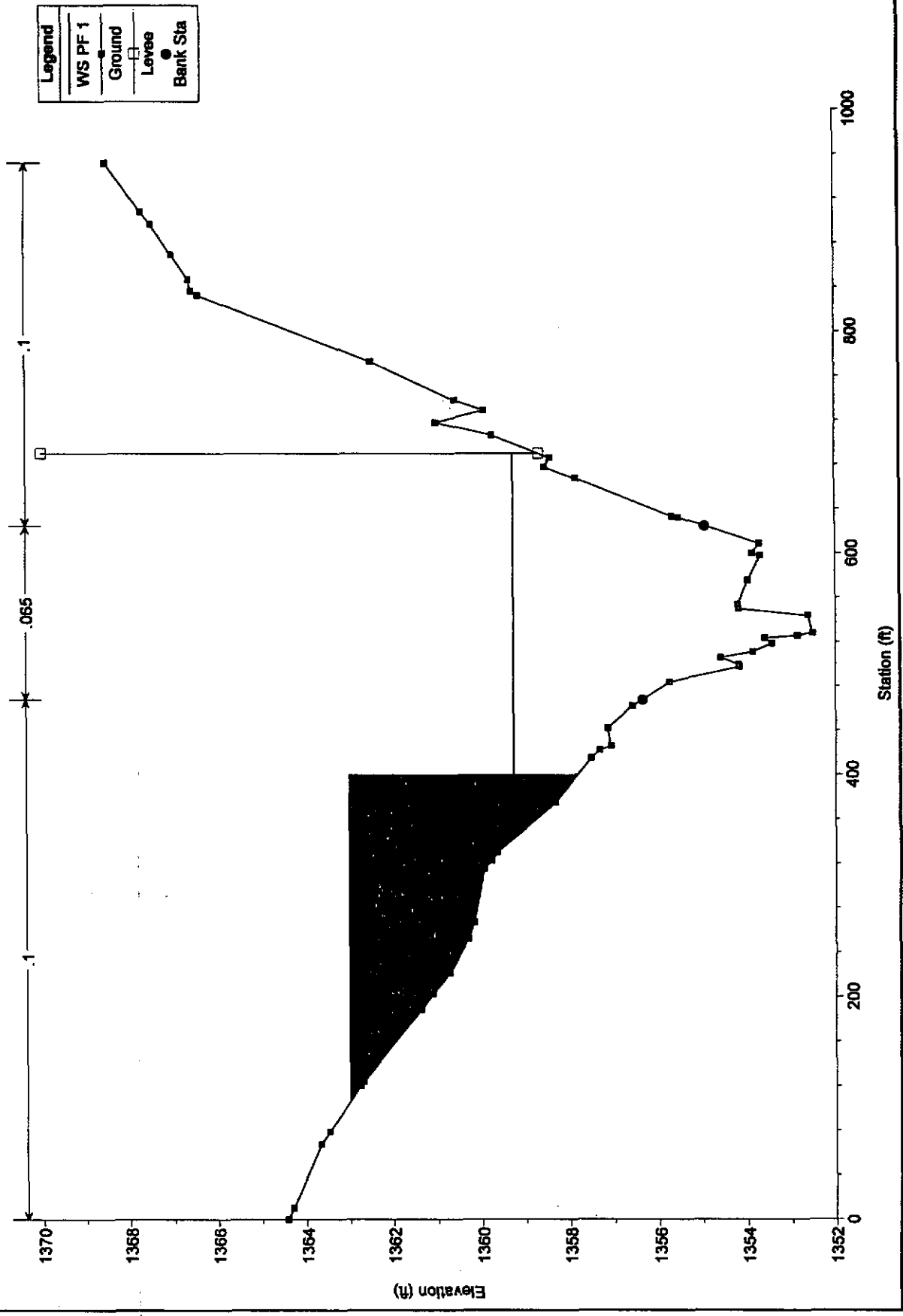
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