

DRAINAGE PLAN
WATERWALK WEST
ADDITION
TO
WICHITA, SEDGWICK COUNTY, KANSAS

PREPARED BY



20 JULY 2012

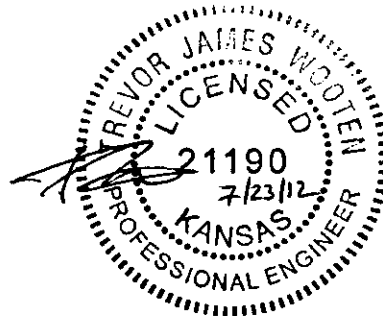


DRAINAGE PLAN WATERWALK WEST ADDITON

FINAL REPORT

**Prepared by Baughman Company, P.A.
20 JULY 2012**

**By Trevor Wooten, P.E., LEED A.P.
N. Brent Wooten, P.E., L.S.**



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PROJECT NARRATIVE

EXISTING CONDITIONS

The site is located just south of Maple Street and just west of McLean Boulevard in Wichita, Sedgwick County, Kansas. The proposed plat is a re-plat of existing lots previously platted as Winne's Addition and Shirk's 1st Subdivision. This area was previously completely developed, with most of the homes razed. Some of the previous infrastructure is still in place. Currently, the portion of the site that will be re-platted has existing storm sewer adjacent to the property serving some smaller areas. This area drains via sheet flow and old City right of way storm sewer into the Kellogg (US-54) Right of Way storm sewer.

PROPOSED CONDITIONS

The property will be developed into two residential apartment complexes with associated parking lots, utilities, and drainage conveyance systems. This proposed plat will not have a detention pond due to its close proximity to the Arkansas River. The storm water from the site will sheet drain off of roofs, grassed common areas, and paved parking and walking surfaces to curb and area inlets and into underground storm sewer systems. The storm sewer systems all eventually collect at a common point where the storm water will be treated for water quality before draining into the existing storm sewer system in Maple Street.

OFFSITE CONDITIONS

The proposed re-plat site is on a fairly flat piece of ground and drains to the east and south. Other than a small portion of the Kellogg (US-54) Right of Way, the surrounding properties do not drain onto this site.

The USGS Quadrangle Sheet can be seen with the site location plotted as Exhibit 1. The Aerial for this area can be viewed as Exhibit 2.

EXISTING CONDITIONS RUNOFF CALCULATIONS

DRAINAGE METHODS & STANDARDS

The following methods and standards, although not a complete list, were used in calculating the existing conditions runoff values.

- STORM SERIES
 - 24-hour; 2-yr, 5-yr, 10-yr, 25-yr, 100-yr Storm Events Modeled
 - 2-yr Rainfall Depth = 3.5 in
 - 10-yr Rainfall Depth = 5.3 in
 - 100-yr Rainfall Depth = 7.9 in

- FLOW DATA
 - Areas per LIDAR data, USGS Quadrangle Sheet, Aerial Photos, and Site Visits
 - Rational Method used for Existing Flows ($C = 0.73$)
 - Time of Concentration: Lag Method (minimum 15 min)

SITE CHARACTERISTICS

The site consists of approximately 4.4 acres of currently platted and mass graded residential subdivision. The proposed area has storm water sewer adjacent and is graded to drain to the south and east, although the site was graded a long time ago and has almost certainly changed from its original drainage design. The existing site characteristics can be seen from the aerial exhibit (Exhibit 2).

EXISTING CONDITIONS HYDROLOGIC ANALYSIS

The site was analyzed for pre-development conditions using the rational method for the entire storm event series. A Rational 'C' Coefficient of 0.73 was used for existing conditions as was used. A Time of Concentration of 15 minutes was used as is the minimum T_c in the City of Wichita.

DOWNSTREAM DRAINAGE CAPACITY

The site currently flows to the south and into the existing KDOT storm sewer system. This site was originally designed as a residential subdivision with interior streets and other infrastructure. The site will drain into the Arkansas River through the adjacent, large, existing storm sewer.

POST-DEVELOPMENT HYDROLOGIC ANALYSIS

DRAINAGE METHODS & STANDARDS

The following methods and standards, although not a complete list, were used in developing the drainage and grading plans.

- **STORM SERIES**
 - 24-hour; 2-yr, 10-yr, 100-yr Storm Events Modeled
 - Hydrograph Method utilized for Developed Flows
 - $C = 0.80$ for the 100 year event (Soil Type C Downtown Residential)
 - $C = 0.69$ for the 5 year event (Soil Type C Downtown Residential)
 - Time of Concentration; Lag Method, minimum $T_c = 15\text{min}$

- **GRADING CONSTRAINTS**
 - All perimeter lot grades matched
 - Tying into existing storm sewer with flows lines set in place
 - Minimum and maximums parking lot slopes and ADA compliance

DEVELOPED CONDITIONS HYDROLOGIC ANALYSIS

The site is proposed to be re-platted and developed into two residential apartment buildings, with related parking lots and storm sewers. A Rational "C" coefficient of 0.80, although conservative, was used for the basins representing the areas to be re-developed.

DETENTION FACILITIES

There will be no detention facility on this lot due to the proximity to the Arkansas River.

DISCHARGE POINTS SUMMARY

The site will discharge to the north via the existing 42" RCP and into the Arkansas River. The storm water from this site will be treated for storm water quality prior to entering the existing 42" RCP

WATER QUALITY

Water quality volume calculation on the site is included in the Appendices. The storm water runoff generated by the site will be treated for water quality with a proprietary device. The water quality volume calculated was approximately 0.4 ac-ft of storage needed. This device will adequately satisfy the WQv requirement.

DOWNSTREAM CHANNEL PROTECTION

Downstream channel protection calculations are not required for this site because the site is less than 5 acres.

POTENTIAL UPSTREAM/DOWNSTREAM IMPACTS

No adverse upstream or downstream impacts are expected with this plat. Due to the proximity of the site to the Arkansas River, the peak runoff from this storm will be conveyed through the existing storm sewer system as soon as possible to leave as much capacity as possible in the existing storm sewer. The proprietary water quality device will treat the water for quality before the water enters the Arkansas River.

FLOODPLAIN SUBMITTAL

SOURCE OF FLOODPLAIN INFORMATION

The site lies within a FEMA Zone X - Shaded. The location of the property, on FEMA FIRM Panel 365 of 700 for Sedgwick County, Kansas, effective February 2, 2007, is attached as Exhibit 6.

FEDERAL, STATE, & LOCAL PERMITTING

US ARMY CORPS OF ENGINEERS

There does not appear to be any jurisdictional waters of the US on this portion of the site.

KANSAS DEPT OF AGRICULTURE – DWR PERMITTING

There does not appear to be any DWR permitting needed on the proposed site at this time.

FEMA

There is no mapped floodplain located upon the proposed site. Therefore, no FEMA permitting is expected at this time.

KANSAS DEPT OF TRANSPORTATION

There does not appear to be any KDOT permitting needed on the proposed project.

SEDGWICK COUNTY PERMITTING

There does not appear to be any Sedgwick County permitting needed at this time.

EXHIBITS

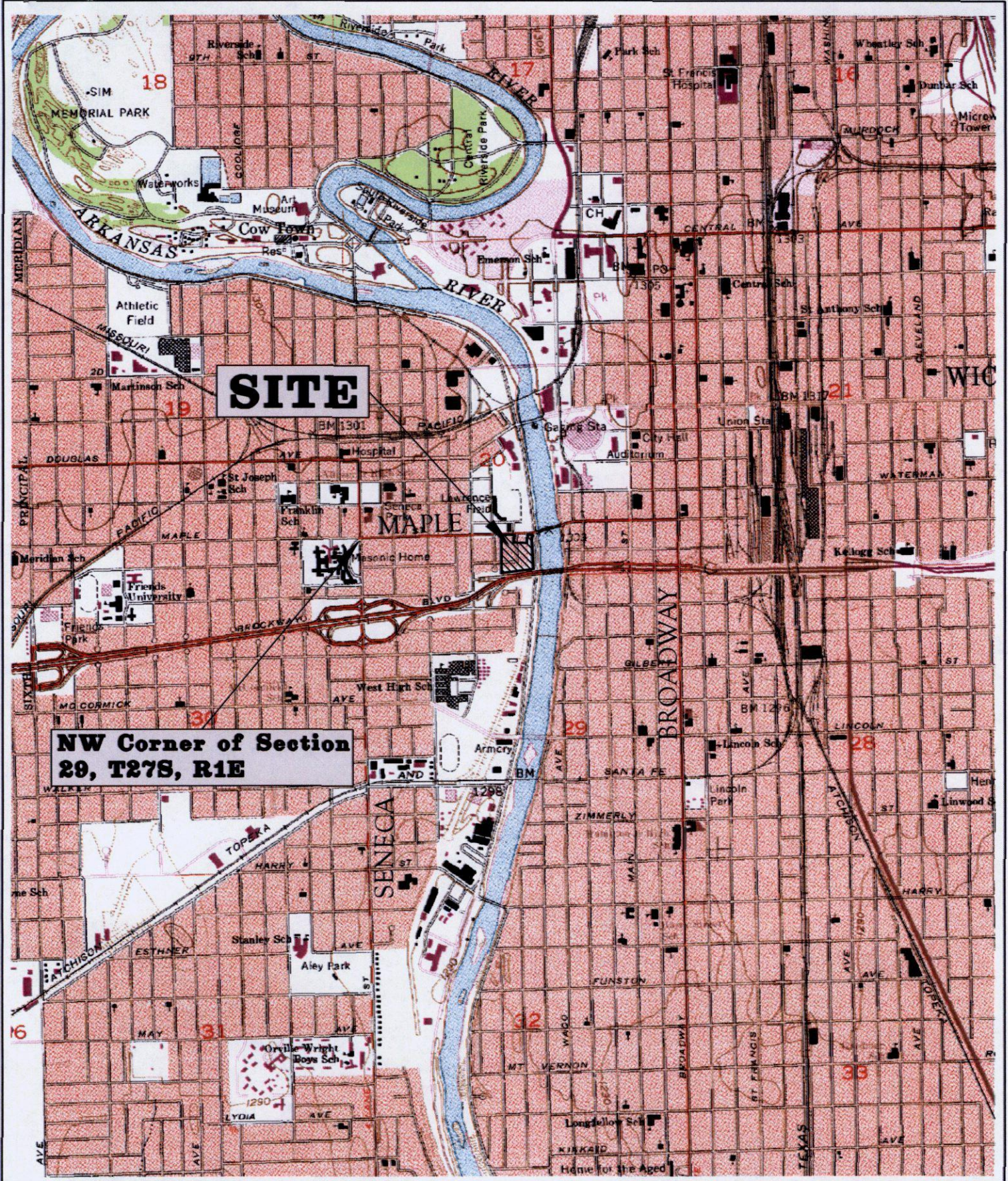
EXHIBIT 1: Site Location Map

EXHIBIT 2: Aerial Photo Exhibit with Lidar Topography

EXHIBIT 3: Plat – Half Scale

EXHIBIT 4: Grading & Drainage Plan – Half Scale

EXHIBIT 5: Floodplain Location (FIRM)

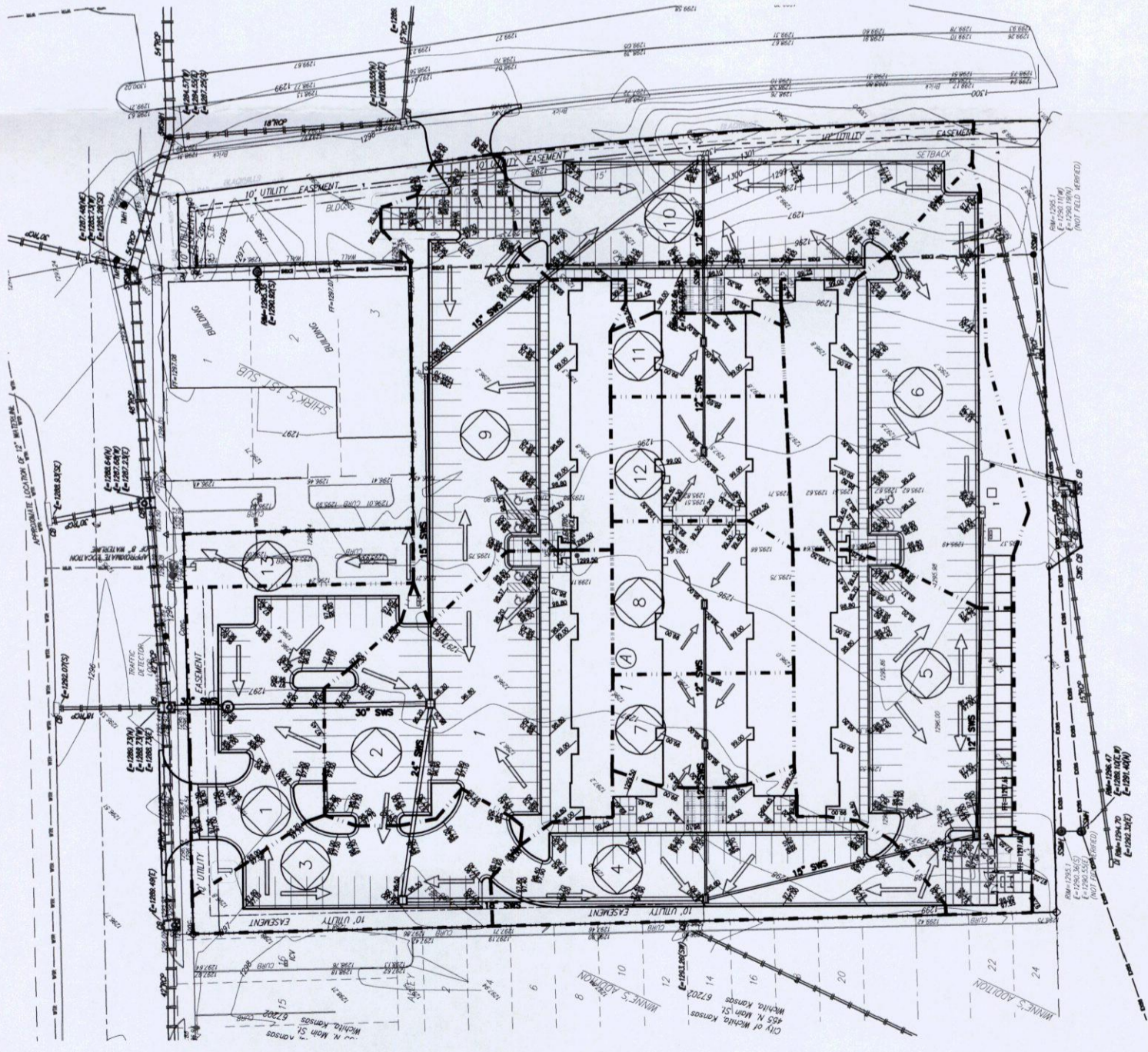


LOCATION MAP:
Waterwalk West Addition
 Lot 1
 WICHITA, SEDGWICK COUNTY, KANSAS



Baughman Company, P.A.
 315 Ellis Wichita, KS 67213





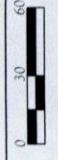
BENCHMARK

Crease cut inside square cut on top of curb, East side of lot
 of Lot 11, Block A, Waterwerk West Addition, Wichita, Sedgewick County,
 Kansas. Elevation = 1297.75 NAVD83
 Chiselled square on Kellogg P/W fence footing, 1.5' S. of the SW
 corner of Lot 11, Block A, Waterwerk West Addition, Wichita,
 Sedgewick County, Kansas. Elevation = 1298.14 NAVD83

LEGAL DESCRIPTION

Lot 1, Block A, Waterwerk West Addition, Wichita, Sedgewick County,
 Kansas.

SITE GRADING PLAN
 Scale 1" = 30.0'



Water Quality Calculations

Waterwerk West Addition Water Quality Data & Computations
 DATE: 10/26/2012
 NOTES & ASSUMPTIONS:

Item	Area	Runoff Coefficient	Runoff
1	4.4	0.30	1.32
2	4.4	0.30	1.32
TOTAL	8.8	0.30	2.64

Estimation	Runoff
Impervious Cover %	0.30
Impervious Area (Acres)	8.8
Runoff Coefficient	0.30
Runoff (Acres)	2.64
Runoff (CFS)	1.32

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SUPPORTING CALCULATIONS

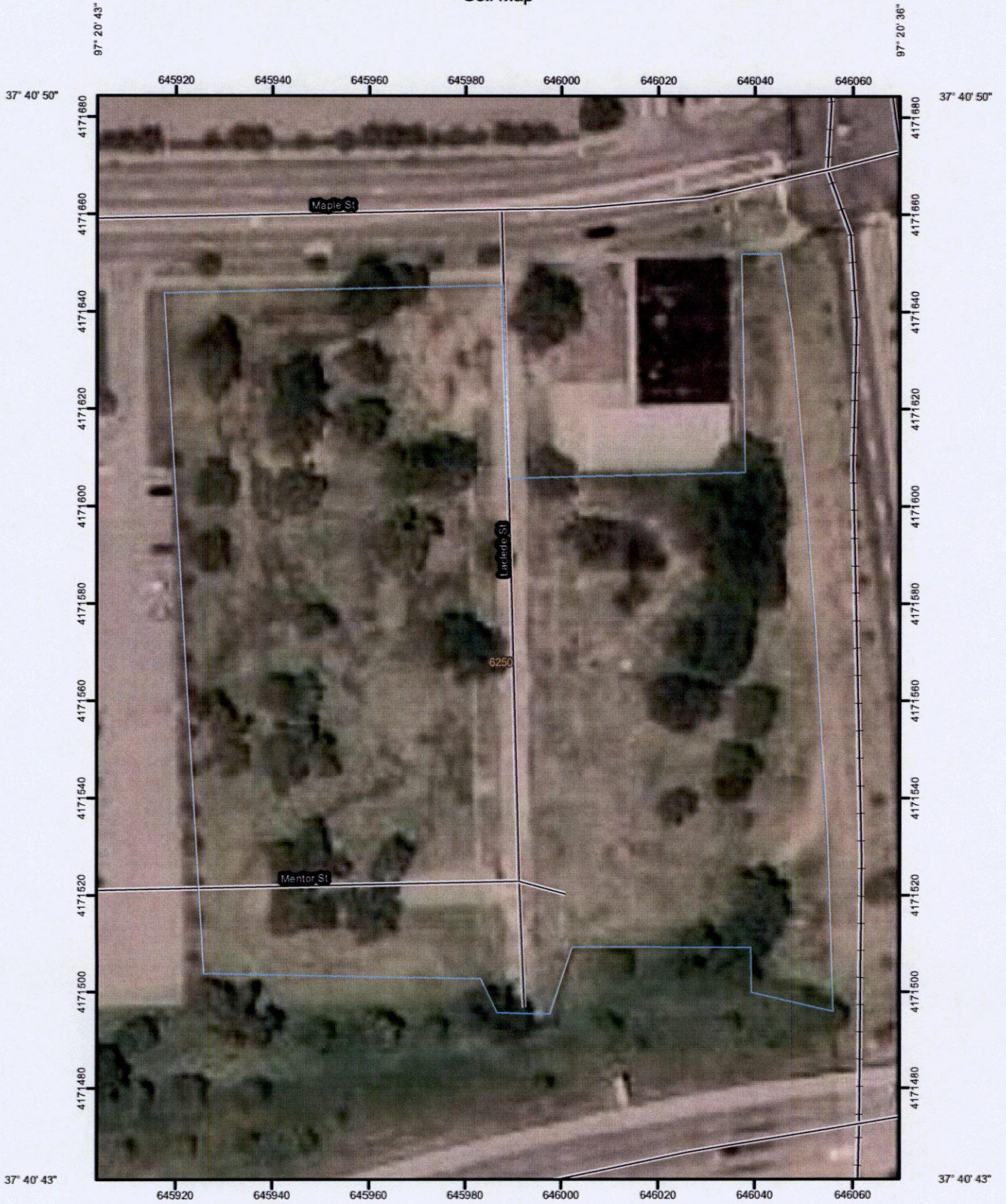
APPENDIX A: USGS Soils Survey

**APPENDIX B : HydraFlow Hydrographs
Site Flow**

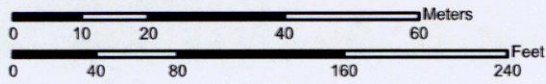
APPENDIX C : Water Quality Volume Calculations

USGS Soils Survey

Custom Soil Resource Report
Soil Map



Map Scale: 1:1,060 if printed on A size (8.5" x 11") sheet.



MAP LEGEND

 Area of Interest (AOI)	 Very Stony Spot
 Soils	 Wet Spot
 Area of Interest (AOI)	 Other
 Soil Map Units	
Special Point Features	Special Line Features
 Blowout	 Gully
 Borrow Pit	 Short Steep Slope
 Clay Spot	 Other
 Closed Depression	Political Features
 Gravel Pit	 Cities
 Gravelly Spot	Water Features
 Landfill	 Streams and Canals
 Lava Flow	Transportation
 Marsh or swamp	 Ralls
 Mine or Quarry	 Interstate Highways
 Miscellaneous Water	 US Routes
 Perennial Water	 Major Roads
 Rock Outcrop	 Local Roads
 Saline Spot	
 Sandy Spot	
 Severely Eroded Spot	
 Sinkhole	
 Slide or Slip	
 Sodic Spot	
 Spoil Area	
 Stony Spot	

MAP INFORMATION

Map Scale: 1:1,060 if printed on A size (8.5" x 11") sheet.
 The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.
 Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for accurate map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL: <http://websoilsurvey.nrcs.usda.gov>
 Coordinate System: UTM Zone 14N NAD83

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Sedgwick County, Kansas
 Survey Area Data: Version 7, Nov 30, 2010

Date(s) aerial images were photographed: 6/20/2006

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Sedgwick County, Kansas (KS173)			
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
6250	Urban land-Canadian complex, 0 to 3 percent slopes	4.1	100.0%
Totals for Area of Interest		4.1	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Custom Soil Resource Report

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Sedgwick County, Kansas

6250—Urban land-Canadian complex, 0 to 3 percent slopes

Map Unit Setting

Elevation: 800 to 1,300 feet

Mean annual precipitation: 24 to 31 inches

Mean annual air temperature: 45 to 66 degrees F

Frost-free period: 195 to 225 days

Map Unit Composition

Urban land: 70 percent

Canadian and similar soils: 30 percent

Description of Canadian

Setting

Landform: Flood plains

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Alluvium

Properties and qualities

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water capacity: Moderate (about 8.3 inches)

Interpretive groups

Land capability (nonirrigated): 1

Ecological site: Sandy Terrace (PE 17-20) (R079XY024KS)

Typical profile

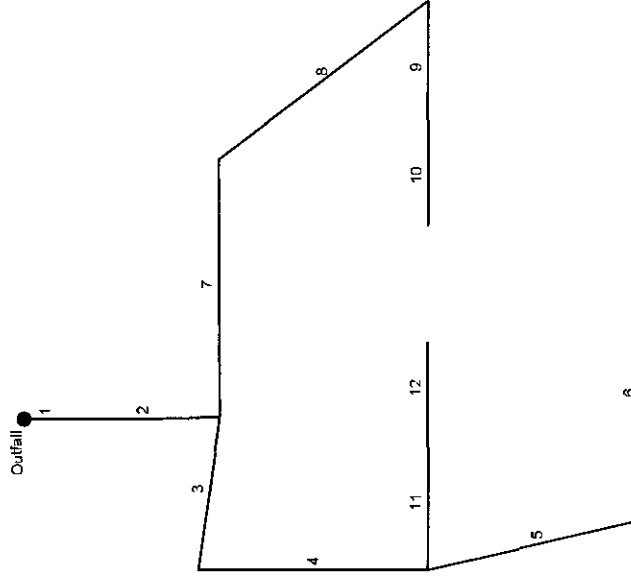
0 to 20 inches: Fine sandy loam

20 to 35 inches: Fine sandy loam

35 to 60 inches: Fine sandy loam

HydraFlow Hydrographs
Site Flow

Hydraflow Storm Sewers Extension for AutoCAD® Civil 3D® 2011 Plan



Storm Sewer Inventory Report

Line No.	Alignment				Flow Data				Physical Data						Line ID		
	Dnstr Line No.	Line Length (ft)	Defl angle (deg)	Junc Type	Known Q (cfs)	Drng Area (ac)	Runoff Coeff (C)	Inlet Time (min)	Invert EI Dn (ft)	Line Slope (%)	Invert EI Up (ft)	Line Size (in)	Line Shape	N Value (n)		J-Loss Coeff (K)	Inlet/ Rim EI (ft)
1	End	30.66	89.86	None	0.00	0.31	0.69	15.0	1289.75	0.42	1289.88	30	Cir	0.013	0.15	1295.77	Pipe - (13)
2	1	114.92	-0.45	DrGrt	0.00	0.48	0.69	15.0	1289.88	0.23	1290.15	30	Cir	0.013	2.25	1296.20	Pipe - (14)
3	2	113.05	99.00	DrGrt	0.00	0.23	0.69	15.0	1290.65	0.22	1290.90	24	Cir	0.013	1.50	1296.50	Pipe - (15)
4	3	172.27	-98.42	DrGrt	0.00	0.36	0.69	15.0	1291.15	0.32	1291.70	18	Cir	0.013	1.50	1296.60	Pipe - (16)
5	4	158.09	-13.11	DrGrt	0.00	0.56	0.69	15.0	1291.95	0.38	1292.55	15	Cir	0.013	1.46	1297.00	Pipe - (17)
6	5	183.01	-75.88	DrCrb	0.00	0.71	0.69	15.0	1292.80	0.52	1293.75	12	Cir	0.013	1.00	1297.00	Pipe - (18)
7	2	189.01	-89.87	DrGrt	0.00	0.53	0.69	15.0	1291.40	0.72	1292.77	15	Cir	0.013	1.26	1296.27	Pipe - (21)
8	7	196.28	53.68	DrCrb	0.00	0.48	0.69	15.0	1292.87	0.48	1293.82	15	Cir	0.013	1.50	1297.32	Pipe - (22)
9	8	103.17	126.77	DrGrt	0.00	0.10	0.69	15.0	1294.07	0.51	1294.60	12	Cir	0.013	0.50	1298.00	Pipe - (23)
10	9	61.85	0.00	DrGrt	0.00	0.17	0.69	15.0	1294.70	0.65	1295.10	12	Cir	0.013	1.00	1298.00	Pipe - (24)
11	4	88.00	-90.00	DrGrt	0.00	0.15	0.69	15.0	1292.34	1.32	1293.50	12	Cir	0.013	0.50	1298.00	Pipe - (19)
12	11	79.47	0.00	DrGrt	0.00	0.20	0.69	15.0	1293.60	0.50	1294.00	12	Cir	0.013	1.00	1298.00	Pipe - (20)

Project File: Waterwalk West rev pat.stm

Number of lines: 12

Date: 6/26/2012

Structure Report

Struct No.	Structure ID	Junction Type	Rim Elev (ft)	Structure			Line Out			Line In		
				Shape	Length (ft)	Width (ft)	Size (in)	Shape	Invert (ft)	Size (in)	Shape	Invert (ft)
1	Structure - (15)	None	1295.77	n/a	n/a	30	Cir	1289.88	30	Cir	1289.88	
2	Structure - (16)	DropGrate	1296.20	Cir	0.00	30	Cir	1290.15	24	Cir	1290.65	
3	Structure - (17)	DropGrate	1296.50	Cir	0.00	24	Cir	1290.90	15	Cir	1291.40	
4	Structure - (18)	DropGrate	1296.60	Cir	0.00	18	Cir	1291.70	18	Cir	1291.15	
5	Structure - (19)	DropGrate	1297.00	Cir	0.00	15	Cir	1292.55	15	Cir	1291.95	
6	Null Structure	DropCurb	1297.00	Cir	0.00	12	Cir	1293.75	12	Cir	1292.34	
7	Structure - (21)	DropGrate	1296.27	Cir	0.00	15	Cir	1292.77	15	Cir	1292.87	
8	Structure - (22)	DropCurb	1297.32	Cir	0.00	15	Cir	1293.82	12	Cir	1294.07	
9	Structure - (23)	DropGrate	1298.00	Cir	0.00	12	Cir	1294.60	12	Cir	1294.70	
10	Null Structure	DropGrate	1298.00	Cir	0.00	12	Cir	1295.10	12	Cir	1293.60	
11	Structure - (20)	DropGrate	1298.00	Cir	0.00	12	Cir	1293.50	12	Cir		
12	Null Structure	DropGrate	1298.00	Cir	0.00	12	Cir	1294.00	12	Cir		

Storm Sewer Summary Report

Line No.	Line ID	Flow rate (cfs)	Line Size (in)	Line shape	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line Slope (%)	HGL Down (ft)	HGL Up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns Line No.	Junction Type
1	Pipe - (13)	11.32	30	Cir	30.66	1289.75	1289.88	0.424	1292.23	1292.25	0.01	1292.26	End	None
2	Pipe - (14)	10.70	30	Cir	114.92	1289.88	1290.15	0.235	1292.26	1292.32	0.20	1292.51	1	DropGrate
3	Pipe - (15)	6.30	24	Cir	113.05	1290.65	1290.90	0.221	1292.51	1292.58	0.12	1292.70	2	DropGrate
4	Pipe - (16)	5.77	18	Cir	172.27	1291.15	1291.70	0.319	1292.70	1293.19	0.25	1293.44	3	DropGrate
5	Pipe - (17)	3.87	15	Cir	158.09	1291.95	1292.55	0.380	1293.44*	1294.01*	0.23	1294.23	4	DropGrate
6	Pipe - (18)	2.23	12	Cir	183.01	1292.80	1293.75	0.519	1294.23*	1294.95*	0.13	1295.08	5	DropCurb
7	Pipe - (21)	3.54	15	Cir	189.01	1291.40	1292.77	0.725	1292.51	1293.52	n/a	1293.52 j	2	DropGrate
8	Pipe - (22)	2.16	15	Cir	196.28	1292.87	1293.82	0.484	1293.52	1294.41	0.33	1294.75	7	DropCurb
9	Pipe - (23)	0.81	12	Cir	103.17	1294.07	1294.60	0.514	1294.75	1294.99	0.07	1295.05	8	DropGrate
10	Pipe - (24)	0.53	12	Cir	61.85	1294.70	1295.10	0.647	1295.05	1295.41	n/a	1295.41 j	9	DropGrate
11	Pipe - (19)	1.05	12	Cir	88.00	1292.34	1293.50	1.318	1293.44	1293.93	n/a	1293.93 j	4	DropGrate
12	Pipe - (20)	0.63	12	Cir	79.47	1293.60	1294.00	0.503	1293.94	1294.34	0.11	1294.45	11	DropGrate

Project File: Waterwalk West rev pat.stm

Number of lines: 12

Run Date: 6/26/2012

NOTES: Return period = 5 Yrs. ; *Surcharged (HGL above crown). ; j - Line contains hyd. jump.

Inlet Report

Line No	Inlet ID	Q = CIA (cfs)	Q carry (cfs)	Q capt (cfs)	Q Byp (cfs)	Junc Type	Curb Inlet		Grate Inlet			Gutter						Inlet		Byp Line No			
							Ht (in)	L (ft)	Area (sqft)	L (ft)	W (ft)	So (ft/ft)	W (ft)	Sw (ft/ft)	Sx (ft/ft)	n	Depth (ft)	Spread (ft)	Depth (ft)		Spread (ft)	Depth (ft)	Spread (ft)
1	Structure - (15)	0.97	0.00	0.00	0.97	None	0.0	0.00	0.00	0.00	Sag	0.00	0.000	0.000	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.0	Off
2	Structure - (16)	1.51	0.00	1.51	0.00	DrGrt	0.0	0.00	0.33	2.50	Sag	2.00	0.020	0.020	0.000	0.72	74.43	0.72	74.43	0.72	74.43	0.0	Off
3	Structure - (17)	0.72	0.00	0.72	0.00	DrGrt	0.0	0.00	0.51	4.00	Sag	2.00	0.020	0.020	0.000	0.07	10.89	0.07	10.89	0.07	10.89	0.0	Off
4	Structure - (18)	1.13	0.00	1.13	0.00	DrGrt	0.0	0.00	0.25	4.00	Sag	2.00	0.020	0.020	0.000	0.73	77.50	0.73	77.50	0.73	77.50	0.0	Off
5	Structure - (19)	1.76	0.00	1.76	0.00	DrGrt	0.0	0.00	0.38	4.00	Sag	2.00	0.020	0.020	0.000	0.73	74.59	0.73	74.59	0.73	74.59	0.0	Off
6	Null Structure	2.23	0.00	2.23	0.00	DrCrb	6.0	5.00	0.00	0.00	Sag	0.00	0.020	0.020	0.000	0.28	13.94	0.28	13.94	0.28	13.94	0.0	Off
7	Structure - (21)	1.66	0.00	1.66	0.00	DrGrt	0.0	0.00	0.57	1.00	Sag	2.00	0.020	0.020	0.000	0.30	32.00	0.30	32.00	0.30	32.00	0.0	Off
8	Structure - (22)	1.51	0.00	1.51	0.00	DrCrb	6.0	5.00	0.00	0.00	Sag	0.00	0.020	0.020	0.000	0.21	10.72	0.21	10.72	0.21	10.72	0.0	Off
9	Structure - (23)	0.31	0.00	0.31	0.00	DrGrt	0.0	0.00	0.11	1.00	Sag	2.00	0.020	0.020	0.000	0.30	32.00	0.30	32.00	0.30	32.00	0.0	Off
10	Null Structure	0.53	0.00	0.53	0.00	DrGrt	0.0	0.00	0.18	1.00	Sag	2.00	0.020	0.020	0.000	0.30	32.00	0.30	32.00	0.30	32.00	0.0	Off
11	Structure - (20)	0.47	0.00	0.47	0.00	DrGrt	0.0	0.00	0.16	1.00	Sag	2.00	0.020	0.020	0.000	0.30	32.00	0.30	32.00	0.30	32.00	0.0	Off
12	Null Structure	0.63	0.00	0.63	0.00	DrGrt	0.0	0.00	0.21	1.00	Sag	2.00	0.020	0.020	0.000	0.30	32.00	0.30	32.00	0.30	32.00	0.0	Off

Project File: Waterwalk West rev.pat.stm

Number of lines: 12

Run Date: 6/26/2012

NOTES: Inlet N-Values = 0.016; Intensity = 52.62 / (Inlet time + 11.20) ^ 0.75; Return period = 5 Yrs. ; * Indicates Known Q added. All curb inlets are throat.

Line No.	Area Dn (sqft)	Area Up (sqft)	Byp Ln No	Coef C1 (C)	Coef C2 (C)	Coef C3 (C)	Capac Full (cfs)	Crit Depth (ft)	Cross Sl, Sw (ft/ft)	Cross Sl, Sx (ft/ft)	Curb Len (ft)	Defl Ang (Deg)	Depth Dn (ft)	Depth Up (ft)	DnStm Ln No	Dmg Area (ac)	Easting X (ft)	EGL Dn (ft)	EGL Up (ft)	Energy Loss (ft)
1	4.90	4.81	n/a	0.20	0.50	0.90	26.71	1.12	89.86	2.48	2.37	Outfall	0.31	5150.30	1292.31	1292.33	0.021
2	4.82	4.52	Sag	0.20	0.50	0.90	19.88	1.09	0.020	0.020	...	-0.45	2.38	2.17	1	0.48	5151.49	1292.34	1292.41	0.070
3	3.05	2.82	Sag	0.20	0.50	0.90	10.64	0.89	0.020	0.020	...	99.00	1.86	1.68	2	0.23	5039.65	1292.58	1292.66	0.080
4	1.77	1.77	Sag	0.20	0.50	0.90	5.93	0.92	0.020	0.020	...	-98.42	1.50	1.49	3	0.36	5039.68	1292.86	1293.36	0.505
5	1.23	1.23	Sag	0.20	0.50	0.90	3.98	0.79	0.020	0.020	...	-13.11	1.25	1.25	4	0.56	5075.57	1293.60	1294.16	0.567
6	0.79	0.79	Sag	0.20	0.50	0.90	2.57	0.63	0.020	0.020	5.00	-75.88	1.00	1.00	5	0.71	5258.55	1294.36	1295.08	0.717
7	1.15	0.77	Sag	0.20	0.50	0.90	5.50	0.75	0.020	0.020	...	-89.87	1.11	0.75**	2	0.53	5340.49	1292.66	1293.85	0.873
8	0.65	0.57	Sag	0.20	0.50	0.90	4.49	0.59	0.020	0.020	5.00	53.68	0.65	0.59**	7	0.48	5458.01	1293.70	1294.63	0.913
9	0.56	0.28	Sag	0.20	0.50	0.90	2.55	0.38	0.020	0.020	...	126.77	0.68	0.38**	8	0.10	5354.84	1294.78	1295.12	0.315
10	0.25	0.21	Sag	0.20	0.50	0.90	2.66	0.31	0.020	0.020	...	0.00	0.35	0.31**	9	0.17	5292.99	1295.12	1295.51	0.259
11	0.79	0.33	Sag	0.20	0.50	0.90	4.09	0.43	0.020	0.020	...	-90.00	1.00	0.43**	4	0.15	5127.68	1293.47	1294.09	0.288
12	0.23	0.24	Sag	0.20	0.50	0.90	2.53	0.34	0.020	0.020	...	0.00	0.34	0.34**	11	0.20	5207.15	1294.05	1294.45	0.401

Project File: Waterwalk West rev pat.stm

Number of lines: 12

Date: 6/26/2012

NOTES: ** Critical depth

Flow Rate (cfs)	Sf Ave (ft/ft)	Sf Dn (ft/ft)	Grate Area (sqft)	Grate Len (ft)	Grate Width (ft)	Gnd/Rim El Dn (ft)	Gnd/Rim El Up (ft)	Gutter Depth (ft)	Gutter Slope (ft/ft)	Gutter Spread (ft)	Gutter Width (ft)	HGL Dn (ft)	HGL Up (ft)	HGL Jnct (ft)	HGL Jmp Dn (ft)	HGL Jmp Up (ft)	Incr CxA	Incr Q (cfs)	Inlet Depth (ft)	Inlet Eff (%)
11.32	0.068	0.071	1295.77	1295.77	1292.23	1292.25	1292.26	0.21	0.97
10.70	0.061	0.059	0.33	2.50	2.50	1296.77	1296.20	0.72	Sag	74.43	2.00	1292.26	1292.32	1292.51	0.33	1.51	0.72	100
6.30	0.071	0.067	0.51	4.00	4.00	1296.20	1296.50	0.07	Sag	10.89	2.00	1292.51	1292.58	1292.70	0.16	0.72	0.07	100
5.77	0.293	0.302	0.25	4.00	4.00	1296.50	1296.60	0.73	Sag	77.50	2.00	1292.70	1293.19	1293.44	0.25	1.13	0.73	100
3.87	0.359	0.359	0.38	4.00	2.00	1296.60	1297.00	0.73	Sag	74.59	2.00	1293.44	1294.01	1294.23	0.39	1.76	0.73	100
2.23	0.392	0.392	1297.00	1297.00	0.28	Sag	13.94	...	1294.23	1294.95	1295.08	0.49	2.23	0.28	100
3.54	0.462	0.266	0.57	1.00	2.00	1296.20	1296.27	0.30	Sag	32.00	2.00	1292.51	1293.52 j	1293.52	1292.56	1292.44	0.37	1.66	0.30	100
2.16	0.465	0.389	1296.27	1297.32	0.21	Sag	10.72	...	1293.52	1294.41	1294.75	0.33	1.51	0.21	100
0.81	0.305	0.082	0.11	1.00	2.00	1297.32	1298.00	0.30	Sag	32.00	2.00	1294.75	1294.99	1295.05	0.07	0.31	0.30	100
0.53	0.419	0.321	0.18	1.00	2.00	1298.00	1298.00	0.30	Sag	32.00	2.00	1295.05	1295.41 j	1295.41	1295.33	1295.32	0.12	0.53	0.30	100
1.05	0.327	0.087	0.16	1.00	2.00	1296.60	1298.00	0.30	Sag	32.00	2.00	1293.44	1293.93 j	1293.93	1293.44	1293.19	0.10	0.47	0.30	100
0.63	0.504	0.524	0.21	1.00	2.00	1298.00	1298.00	0.30	Sag	32.00	2.00	1293.94	1294.34	1294.45	0.14	0.63	0.30	100

Project File: Waterwalk West rev.pat.shtm

Number of lines: 12

Date: 6/26/2012

NOTES: ** Critical depth

MyReport

Inlet ID	Inlet Loc	Inlet Spread (ft)	Inlet Time (min)	i Sys (in/hr)	i Inlet (in/hr)	Invert Dn (ft)	Invert Up (ft)	Jump Loc (ft)	Jump Len (ft)	Vel Hd Jump Dn (ft)	Vel Hd Jump Up (ft)	J-Loss Coeff	Junct Type	Known Q (cfs)	Cost RCP	Cost CMP	Cost PVC	Line ID
Structure - (15)	Sag	15.0	3.83	4.55	1289.75	1289.88	0.00	0.00	0.15	None	0.00	1,620	1,458	1,377	Pipe - (13)
Structure - (16)	Sag	74.43	15.0	3.91	4.55	1289.88	1290.15	0.00	0.00	2.25	Dp-Grate	0.00	5,910	5,319	5,024	Pipe - (14)
Structure - (17)	Sag	10.89	15.0	4.13	4.55	1290.65	1290.90	0.00	0.00	1.50	Dp-Grate	0.00	5,092	4,583	4,328	Pipe - (15)
Structure - (18)	Sag	77.50	15.0	4.22	4.55	1291.15	1291.70	0.00	0.00	1.50	Dp-Grate	0.00	7,000	6,300	5,950	Pipe - (16)
Structure - (19)	Sag	74.59	15.0	4.41	4.55	1291.95	1292.55	0.00	0.00	1.46	Dp-Grate	0.00	5,650	5,085	4,803	Pipe - (17)
Null Structure	Sag	13.94	15.0	4.55	4.55	1292.80	1293.75	0.00	0.00	1.00	Dp-Curb	0.00	5,301	4,771	4,506	Pipe - (18)
Structure - (21)	Sag	32.00	15.0	4.00	4.55	1291.40	1292.77	37.80	4.41	0.23	0.35	1.26	Dp-Grate	0.00	6,350	5,715	5,398	Pipe - (21)
Structure - (22)	Sag	10.72	15.0	4.18	4.55	1292.87	1293.82	0.00	0.00	1.50	Dp-Curb	0.00	5,980	5,382	5,083	Pipe - (22)
Structure - (23)	Sag	32.00	15.0	4.36	4.55	1294.07	1294.60	0.00	0.00	0.50	Dp-Grate	0.00	2,984	2,686	2,536	Pipe - (23)
Null Structure	Sag	32.00	15.0	4.55	4.55	1294.70	1295.10	49.48	1.56	0.10	0.12	1.00	Dp-Grate	0.00	1,822	1,640	1,549	Pipe - (24)
Structure - (20)	Sag	32.00	15.0	4.34	4.55	1292.34	1293.50	35.20	3.19	0.06	0.29	0.50	Dp-Grate	0.00	2,760	2,484	2,346	Pipe - (19)
Null Structure	Sag	32.00	15.0	4.55	4.55	1293.60	1294.00	0.00	0.00	1.00	Dp-Grate	0.00	2,470	2,223	2,100	Pipe - (20)

Project File: Waterwalk West rev pat.stm

Number of lines: 12

Date: 6/26/2012

NOTES: intensity = 52.62 / (inlet time + 11.20) ^ 0.75 -- Return period = 5 Yrs. ; ** Critical depth

Line Length (ft)	Line Size (in)	Line Slope (%)	Line Type	Local Depr (in)	n-val Gutter	n-val Pipe	Minor Loss (ft)	Northing Y (ft)	Pipe Travel (min)	Q Byp (cfs)	Q Capt (cfs)	Q Carry (cfs)	Line Rise (in)	Runoff Coeff (C)	Line Span (in)	Area A1 (ac)	Area A2 (ac)	Area A3 (ac)	Tc (min)	Throat Ht (in)	Total Area (ac)
30.66	30	0.42	Cir	0.013	0.01	4991.06	0.21	30	0.69	30	0.00	0.00	0.00	21.7	...	4.28
114.92	30	0.23	Cir	0.013	0.20	4876.15	0.83	0.00	1.51	0.00	30	0.69	30	0.00	0.00	0.00	20.9	...	3.97
113.05	24	0.22	Cir	0.013	0.12	4892.69	0.92	0.00	0.72	0.00	24	0.69	24	0.00	0.00	0.00	18.6	...	2.21
172.27	18	0.32	Cir	0.013	0.25	4720.42	0.86	0.00	1.13	0.00	18	0.69	18	0.00	0.00	0.00	17.7	...	1.96
158.09	15	0.38	Cir	0.013	0.23	4566.45	0.83	0.00	1.76	0.00	15	0.69	15	0.00	0.00	0.00	16.1	...	1.27
183.01	12	0.52	Cir	0.013	0.13	4563.26	1.07	0.00	2.23	0.00	12	0.69	12	0.00	0.00	0.00	15.0	60	0.71
189.01	15	0.72	Cir	0.013	n/a	4877.67	1.02	0.00	1.66	0.00	15	0.69	15	0.00	0.00	0.00	19.9	...	1.28
196.28	15	0.48	Cir	0.013	0.33	4720.46	1.75	0.00	1.51	0.00	15	0.69	15	0.00	0.00	0.00	18.1	60	0.75
103.17	12	0.51	Cir	0.013	0.07	4720.44	1.61	0.00	0.31	0.00	12	0.69	12	0.00	0.00	0.00	16.5	...	0.27
61.85	12	0.65	Cir	0.013	n/a	4720.43	1.52	0.00	0.53	0.00	12	0.69	12	0.00	0.00	0.00	15.0	...	0.17
88.00	12	1.32	Cir	0.013	n/a	4720.43	1.06	0.00	0.47	0.00	12	0.69	12	0.00	0.00	0.00	16.7	...	0.35
79.47	12	0.50	Cir	0.013	0.11	4720.44	1.66	0.00	0.63	0.00	12	0.69	12	0.00	0.00	0.00	15.0	...	0.20

Project File: Waterwalk West rev pat.stm

Number of lines: 12

Date: 6/26/2012

NOTES: ** Critical depth

MyReport

Total CxA	Total Runoff (cfs)	Vel Ave (ft/s)	Vel Dn (ft/s)	Vel Hd Dn (ft)	Vel Hd Up (ft)	Vel Up (ft/s)	Cover Dn (ft)	Cover Up (ft)	Storage (cft)
2.95	11.32	2.33	2.31	0.08	0.09	2.35	3.52	3.39	149.04
2.74	10.70	2.29	2.22	0.08	0.09	2.37	3.39	3.55	538.08
1.52	6.30	2.15	2.07	0.07	0.08	2.24	3.55	3.60	332.41
1.37	5.77	3.27	3.27	0.17	0.17	3.27	3.85	3.40	304.33
0.88	3.87	3.15	3.15	0.15	0.15	3.15	3.40	3.20	193.97
0.49	2.23	2.84	2.84	0.13	0.13	2.84	3.20	2.25	143.71
0.88	3.54	3.82	3.06	0.15	0.33	4.58	3.55	2.25	184.48
0.52	2.16	3.56	3.34	0.17	0.22	3.78	2.15	2.25	119.72
0.19	0.81	2.18	1.44	0.03	0.13	2.92	2.25	2.40	43.56
0.12	0.53	2.37	2.17	0.07	0.10	2.58	2.30	1.90	14.01
0.24	1.05	2.27	1.34	0.03	0.16	3.21	3.26	3.50	54.27
0.14	0.63	2.67	2.71	0.11	0.11	2.63	3.40	3.00	18.68

Project File: Waterwalk West rev pat.sfm

Number of lines: 12

Date: 6/26/2012

NOTES: ** Critical depth

Storm Sewer Inlet Time Tabulation

Line No.	Line ID	Tc Method	Sheet Flow				Shallow Concentrated Flow				Channel Flow						Total Travel Time (min)		
			n-Value	flow Length (ft)	2-yr 24h P (in)	Land Slope (%)	Travel Time (min)	flow Length (ft)	Water Slope (%)	Surf Descr	Ave Vel (ft/s)	Travel Time (min)	X-sec Area (sqft)	Wetted Perim (ft)	Chan Slope (%)	n-Value		Vel	flow Length (ft)
1	Pipe - (13)	User																	15.00
2	Pipe - (14)	User																	15.00
3	Pipe - (15)	User																	15.00
4	Pipe - (16)	User																	15.00
5	Pipe - (17)	User																	15.00
6	Pipe - (18)	User																	15.00
7	Pipe - (21)	User																	15.00
8	Pipe - (22)	User																	15.00
9	Pipe - (23)	User																	15.00
10	Pipe - (24)	User																	15.00
11	Pipe - (19)	User																	15.00
12	Pipe - (20)	User																	15.00
Project File: Waterwalk West rev pat.stm			Min. Tc used for intensity calculations = 5 min							Number of lines: 12							Date: 6/26/2012		

Hydraulic Grade Line Computations

Line Size (in)	Q (cfs)	Downstream						Len (ft)	Upstream						Check Ave Sf (%)	JL coeff (K)	Minor loss (ft)					
		Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)		EGL elev (ft)	Sf (%)	Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)				Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Energy loss (ft)
1	30	1269.75	1292.23	2.48	4.90	2.31	0.08	1292.31	0.071	30.66	1289.88	1292.25	2.37	4.81	2.35	0.09	1292.33	0.066	0.068	0.021	0.15	0.01
2	30	1269.88	1292.26	2.38	4.82	2.22	0.08	1292.34	0.059	114.92	1290.15	1292.32	2.17	4.52	2.37	0.09	1292.41	0.062	0.061	0.070	2.25	0.20
3	24	1290.65	1292.51	1.86	3.05	2.07	0.07	1292.58	0.067	113.05	1290.90	1292.58	1.68	2.82	2.24	0.08	1292.66	0.074	0.071	0.080	1.50	0.12
4	18	1291.15	1292.70	1.50	1.77	3.27	0.17	1292.86	0.302	172.27	1291.70	1293.19	1.49	1.77	3.27	0.17	1293.36	0.284	0.293	0.505	1.50	0.25
5	15	1291.95	1293.44	1.25	1.23	3.15	0.15	1293.60	0.359	158.09	1292.55	1294.01	1.25	1.23	3.15	0.15	1294.16	0.359	0.359	0.567	1.46	0.23
6	12	1292.80	1294.23	1.00	0.79	2.84	0.13	1294.36	0.392	183.01	1293.75	1294.95	1.00	0.79	2.84	0.13	1295.08	0.392	0.392	0.717	1.00	0.13
7	15	1291.40	1292.51	1.11	1.15	3.06	0.15	1292.66	0.266	189.01	1292.77	1293.52 j	0.75**	0.77	4.58	0.33	1293.65	0.657	0.462	n/a	1.26	n/a
8	15	1292.87	1293.52	0.65	0.65	3.34	0.17	1293.70	0.389	196.28	1293.82	1294.41	0.59**	0.57	3.78	0.22	1294.63	0.542	0.465	0.913	1.50	0.33
9	12	1294.07	1294.75	0.68	0.56	1.44	0.03	1294.78	0.082	103.17	1294.60	1294.99	0.38**	0.28	2.92	0.13	1295.12	0.529	0.305	0.315	0.50	0.07
10	12	1294.70	1295.05	0.35	0.25	2.17	0.07	1295.12	0.321	61.85	1295.10	1295.41 j	0.31**	0.21	2.58	0.10	1295.51	0.517	0.419	n/a	1.00	n/a
11	12	1292.34	1293.44	1.00	0.79	1.34	0.03	1293.47	0.087	88.00	1293.50	1293.93 j	0.43**	0.33	3.21	0.16	1294.09	0.567	0.327	n/a	0.50	0.08
12	12	1293.60	1293.94	0.34*	0.23	2.71	0.11	1294.05	0.524	79.47	1294.00	1294.34	0.34**	0.24	2.63	0.11	1294.45	0.484	0.504	0.401	1.00	0.11

Project File: Waterwalk West rev pat.stm

Number of lines: 12

Run Date: 6/26/2012

Notes: * depth assumed, ** Critical depth, j-Line contains hyd. jump, ; c = cir e = ellip b = box

**Water Quality Volume
Spreadsheet Calculations**

Waterwalk West Addition Water Quality Data & Computations

Completed by: TJW
Date: 7/20/2012

Notes & Assumptions:

Basin	Area	Effect
1	4.4	Buildings, parking lots, green spaces
Total	4.4	

Impervious Cover %	0.38
Hydrologic Soil Group	Rv Values
Undisturbed Woods	$R_{vu} = 0.04$
Turf/ Disturbed Soils	$R_{vd} = 0.22$
Impervious Cover	$R_{vi} = 0.95$

Equations
$WQ_v = R_v * A / 10$
$R_v = R_{vu} * U + R_{vd} * D + R_{vi} * I$
U = undisturbed/total area
D = dist. perv./total area
I = impervious/total area

Basin	Drainage Bas		Pond		Treatment		Undisturbed		Disturbed		Impervious	
	Area	Acres	Area	Acres	Area	Acres	Area	Acres	Area	Acres	Area	Acres
1	4.4	4.4	0.0	0.0	4.4	4.4	0.0	0.0	0.9	0.9	3.5	3.5
Totals:	4.4	4.4	0.0	0.0	4.4	4.4	27.8	0.9	0.9	3.5	3.5	

Calculations			
U	D	I	Totals
0.00	0.20	0.80	1.0

Calculations			
Rv	Area	Area	WQv
	Acres	Acres	Acres-Ft.
0.8	4.4	4.4	0.4
	4.4	4.4	0.4

Drainage Plan
1:30 Scale