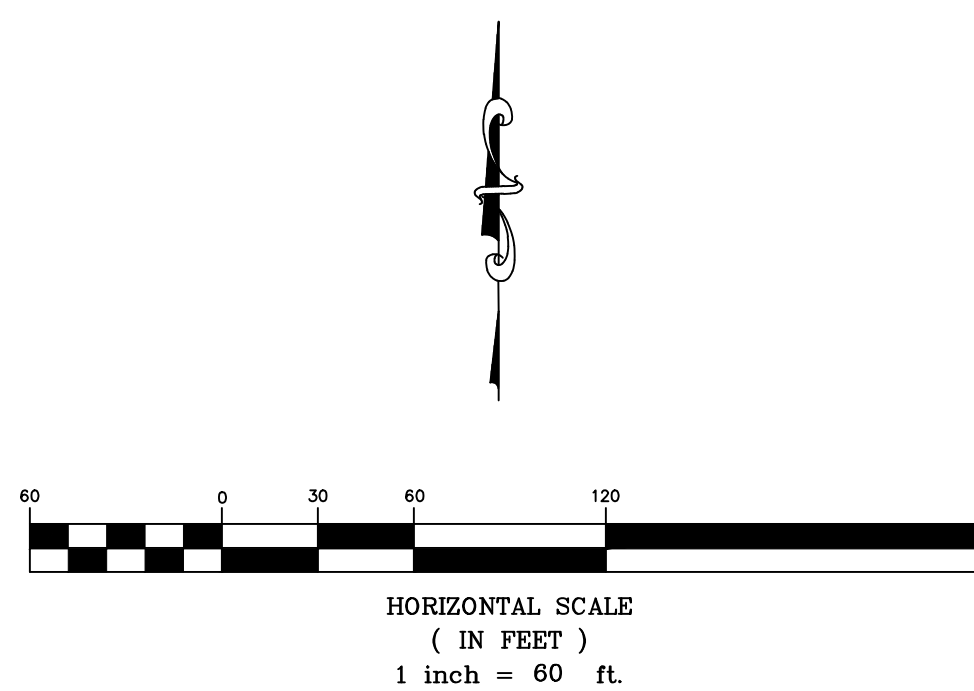


**Concrete Weir Detail**

**Engineer's Notes:**

1. Site drainage calculations were developed using the SCS Method for peak flow. Weighted CN and I values were established based on existing and proposed site conditions. Impervious area is assumed for commercial development with 85% of as indicated in drainage manual.
2. The site drainage will be maintained to the north ditch of I-35.
3. Future grading plan shall follow the drainage pattern as shown on plan indicated by flow arrows.
4. The property is not in designated 100-yr floodplain (FIRM Panel 20173C0387E, February, 2 2007.)
5. Design of Internal storm sewer system and/or surface drainage is required to drain all of the site to the proposed detention basin when site evolves.



**Project Narrative:**

The site is located between Kellogg and I-35 (Kansas Turnpike), about 1/4 mile west of the intersection. The total site is about 9.22 acres. The entire site is undeveloped and covered by grass. Site is zoned limited commercial (LC) and will remain same in developed condition. The proposed use of the land is to develop in to a commercial area with buildings, parking lot and other impervious stone display area for stone company. The entire site is the drainage basin of the north turnpike ditch which drains to the south of turnpike through culverts. The drainage condition remains same in developed condition. An extended detention basin is proposed at southeast corner for channel protection and flood detention.

**Water Quality and TSS Removal Calculation:**

| Water Quality Volume (WQv) Calculation               |       |                |  |
|--|-------|----------------|--|
| Calculation for water quality volume (WQv=P*RV*A/12) |       | Soil Group 'D' |  |
| 85th percentile storm event (1.2 inches), P =        | 1.20  | inches         | Calculation of Rv                                  |
| Total area, A =                                      | 9.22  | acres          | Coeff.   |
| Rainfall Coeff, Rv =                                 | 0.845 | cf             | Area   |
| Required Vol. for Water Quality =                    | 0.78  | ac-ft          | Coeff for undisturbed area, R <sub>VU</sub> =      |
| Corresponding Water Quality Peak Flow =              | 7.57  | cfs            | Coeff for turf cover, disturbed, R <sub>VT</sub> = |
|  |       |                | Coeff for impervious area, R <sub>VI</sub> =       |
|  |       | Weighted, Rv = |  |
|  |       | 0.845          |  |

Total water quality volume will be treated in one or more proprietary systems. Total water quality flow needs to treated = 7.57 cfs

No of HG-5 (Hydroguard) unit required = 3. Each Hydroguard unit (HG-5) will be sized to accommodate about 2.70 cfs of treatment flow for 80 % TSS removal. The location and drainage basin for each hydroguard unit will be designed as the site evolves.

**Water Quality Peak Flow Calculation**

|   |             |              |
|---|-------------|--------------|
| Aera =                                  | 9.22        | acres        |
| WQv =                                   | 1.014       | inches       |
| Pond and Swamp Factor, F <sub>p</sub> = | 0.700       |              |
| Calculated CN =                         | 98.3        |              |
| S =                                     | 0.174       | inches       |
| la =                                    | 0.035       | inches       |
| la/P =                                  | 0.029       |              |
| qu                                      | 740.0       | cfs/sq.mi/in |
| <b>Water quality peak flow</b>          | <b>7.57</b> | <b>cfs</b>   |

**Water Quality and TSS Removal Calculation:**

Channel protection volume for entire site (1) is detained in extended detention basin located at southeast corner of the property. The required extended detention is archived by 3" orifice located at an elevation of 1351.00 on the wall of proposed weir structure. Detention time for CP<sub>v</sub> = 24.05 hrs (centroid-centroid)

| Channel Protection Volume Calculation |       |                  |                   |       |                      |                  |                   |       |                      |
|---------------------------------------|-------|------------------|-------------------|-------|----------------------|------------------|-------------------|-------|----------------------|
| Drainage Basin                        | Acres | Developed        |                   |       | Existing             |                  |                   |       |                      |
|                                       |       | 24 hr 1 yr Storm | Curve Number (CN) | S     | Runoff Volume inches | 24 hr 1 yr Storm | Curve Number (CN) | S     | Runoff Volume inches |
| 1                                     | 9.22  | 2.80             | 96                | 0.417 | 2.36                 | 2.80             | 84                | 1.905 | 1.35                 |

**Runoff Calculations (2-, 5-, 10-, 25-, and 100-yr)**

**EXISTING CONDITION:**

Onsite Area, A<sub>1</sub> = 9.22 acres, Impervious Area = None, Grass Area = 100%, Hydrological Soil Group = D

| EXISTING SITE |       |                    |    |       |       |       |       |       |                       |
|---------------|-------|--------------------|----|-------|-------|-------|-------|-------|-----------------------|
| DRAINAGE AREA | ACRES | T <sub>c</sub> min | CN | Q2    | Q5    | Q10   | Q25   | Q100  | REMARKS               |
| On-site (1)   | 9.22  | 21                 | 84 | 19.15 | 27.76 | 33.86 | 41.78 | 56.81 | Onsite draining south |
| Off-site (2)  | 0.81  | 21                 | 84 | 1.63  | 2.44  | 2.97  | 3.67  | 4.99  | Kellogg Right of Way  |

**DEVELOPED CONDITION:**

Onsite Area, A<sub>1</sub> = 9.22 acres, Impervious Area = 85% for commercial use, Grass Area = 15%, Land use: LC Hydrological Soil Group = D

| DEVELOPED SITE |       |                    |    |       |       |       |       |       |                       |
|----------------|-------|--------------------|----|-------|-------|-------|-------|-------|-----------------------|
| DRAINAGE AREA  | ACRES | T <sub>c</sub> min | CN | Q2    | Q5    | Q10   | Q25   | Q100  | REMARKS               |
| On-site (1)    | 9.22  | 15                 | 96 | 33.47 | 43.68 | 50.79 | 59.90 | 77.03 | Onsite draining south |
| Off-site (2)   | 0.81  | 15                 | 96 | 2.94  | 3.84  | 4.46  | 5.28  | 6.77  | Kellogg Right of Way  |

| OUTFLOW        |       |      |       |       |       |       |                              |
|----------------|-------|------|-------|-------|-------|-------|------------------------------|
| DRAINAGE AREA  | ACRES | Q2   | Q5    | Q10   | Q25   | Q100  | REMARKS                      |
| Off-site (1+2) | 10.03 | 4.81 | 15.05 | 24.06 | 37.90 | 61.82 | Total area draining to basin |

**BENCHMARK:**

COW Disc in the center median on the west side of the intersection of Zelta and Kellogg. Approximately 57 feet southwest of a fire hydrant and 11 feet south of the south edge of asphalt of the westbound lane. Elevation = 1362.64 NAVD 88

Absolute Natural Stone Addition  
**Drainage Plan**  
Wichita, Kansas

PROJECT NUMBER

|                                |               |               |              |                     |
|--------------------------------|---------------|---------------|--------------|---------------------|
| <b>kemiller</b><br>engineering | KEM NO. 12018 | FILE drainage | DATE 02/2013 | SHEET<br><b>1.0</b> |
|                                | DESIGN GP     | DRAWN GP      | REVISED      |                     |

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