

DRAINAGE PLAN AND SUPPORTING  
CALCULATIONS FOR  
NEWMARKET OFFICE TO WICHITA,  
SEDGWICK COUNTY, KANSAS  
PEC PROJECT NO. 36-06136-5707



# LETTER OF TRANSMITTAL

**Professional Engineering Consultants, P.A.**  
303 S. TOPEKA - WICHITA, KANSAS 67202 • 316-262-2691 • FAX 316-262-3003  
www.pocl.com • designers@pocl.com

TO: City of Wichita  
Storm Water Management  
7<sup>th</sup> Floor - City Hall  
455 N. Main  
Wichita, KS 67202

DATE: December 6, 2006  
PROJECT NO.: 35-06136  
PROJECT: New Market Office

ATTENTION: Scott Lindebak  
FROM: Shawn Bryan

REFERENCE: Drainage Plan Comments

WE ARE SENDING YOU:  Attached  Under separate cover via \_\_\_\_\_ the following items:  
 Shop drawings  Prints  Plans  Samples  Specifications  
 Copy of letter  Change order  \_\_\_\_\_

COPIES	DATE	NO.	DESCRIPTION
1	12/06/2006	1	Response Drainage Plan Comments

**THESE ARE TRANSMITTED as checked below:**

For approval  Approved as submitted  Resubmit \_\_\_\_\_ copies for approval  
 For your use  Approved as noted  Submit \_\_\_\_\_ copies for distribution  
 As requested  Returned for corrections  Return \_\_\_\_\_ corrected prints  
 For review and comment  \_\_\_\_\_  
 FOR BIDS DUE \_\_\_\_\_  PRINTS RETURNED AFTER LOAN TO US

REMARKS: Scott here is a copy of the revised drainage plan and supporting documentation in response to your comments for New Market Office. If you have any questions please feel free to contact me.

Thanks.

COPIES TO: File

By: Shawn R. Bryan

If enclosures are not as noted, kindly notify us at once.

December 5, 2006

City of Wichita  
Attn: Scott Lindebak  
Storm Water Management  
7<sup>th</sup> Floor, City Hall  
Wichita, KS 67202

Subject: New Market Office Comments

Mr. Lindebak:

Here are the replies to your comments that are in your email letter dated 4/17/06 for New Market Office. I have included this letter with the revision package for your use.

- 1 The plan, report and models should be submitted in electronic format, including the HEC-1 input files.

*The drainage plan will be submitted in PDF format once it has been approved.*

2. The flow path used for the TC calculations is not included in the plan, for both pre-developed conditions and post-developed conditions.

*Included in the drainage report is the Tc flow path for the pre-development condition. It is standard engineering practice to assume a Tc for the post-development conditions of 15 to 20 minutes depending on size of the site. The drainage report has been updated with the revised post-development HEC-1 model. Once the design has started for the project PEC can submit the StormCAD or pipe sizing calculations to your office with the revised Tc if necessary.*

3. An exhibit should be included in the plan that delineates the location of the sub-basins used in the HEC-1 modeling. For example: BSN5, POND7, BSN4, POND 5, BSN6, OFFST, BSN8, POND4, BSN10, POND3, BSN3 BSN2, POND1, POND2, NORTH, & NM-UND.

*In the HEC-1 model all the basins and pond nodes that you referenced above are located in the Fontana Addition which was previously approved by all of the committee's and City Council. I have enclosed the drainage plan for Fontana Addition. The north basin is the 10 acre tract directly north of the site location and NM-UND is the undeveloped New Market site, 40 acres.*

4. The north offsite 10 ac basin is using a UD of 0.40, The TC for the 40 acres site is shown as 40 min. and the 50 acres is 50.4 minutes. A UD of .4 would translate to a TC of 36 minutes. Please clarify. Thanks.

*The 40 acres site has a Tc of 40 minutes for the pre-development condition and 20 minutes for the post-development condition. The 10 acre site north of the property is accounted for in the post-development conditions with a Tc of 40 minutes. Since the pre vs. post development policy is for the developed property this 10 acres passes through New Market Office detention ponds. The ponds have been sized to pass this extra flow but there is no need to detain any of this runoff since it is off site flow. Using the HEC-1 model a Tc of 40 minutes translates into a UD of 0.4.  $Tc = 40 \text{ minutes} * (1 \text{ Hr.} / 60 \text{ minutes}) * (0.6 \text{ Lag}) = 0.40$*

5. The developed conditions HEC-1 run is identical to the existing conditions run. Please revise.

*The two models are very similar with only the last page or two being different. There is a section with a basin "North & Dev - 1" that is the difference in the models. I have included another copy of the post-development HEC-1 model for your use.*

6. The HEC-1 calculations for Fontana should be revised with the RS card elevations set to the starting water surface elevation of the pond. Example: Pond 2 elevation is set at elevation 158.0, however the static pool is 166.0.

*This change can be made in the HEC-1 RS card. It is unnecessary, if you look at the SE card the elevation is set to start at 166.0 and not 158.0 this is also the case for the SQ card that shows an elevation of 166.0, the flow over the weir would be 0.00. Therefore it has no effect on the model outcome if the static elevation is set lower than 166.0.*

7. The stage, storage, and discharge calculations for each detention pond should be included to support the HEC-1 SA/SE/SQ routing cards.

*The rating curve has been included in the revision package.*

8. The detention ponds should be platted in within a drainage reserve.

*The drainage plan has been revised to show the detention ponds located within the "Drainage Reserve."*

9. The site should be located on a copy of the FIRM.

*This is included in the revision package.*

10. The subdivision should be submitted using an approved datum.

*The drainage plan is in City Datum which is an approved datum unless the City of Wichita, Engineering Dept., has changed their policy. All elevations on the drainage plan will need to have 1187.4 added to them to convert to NAVD 29 datum.*

11. The existing conditions model should take into account existing storage that may be occurring due to the road elevation and 30-inch cross culvert. It appears the stormwater runoff is leaving the site at both the southeast corner of the plat and the east line of the plat near the FEMA Zone A designation. The landowner to the east will need to accommodate some of the runoff, if the Baughman design can not handle the entire 321 cfs. Please contact Baughman Company and get a copy of the design flow rates used to size the future RCB. What is the capacity of the 30" culvert (your plan states 24") when the road is overtopped and what is that elevation? What is the split flow rate from the east to the southeast? My site visit last fall found a sizable head cutting into an empty pond south of the cell tower. Photos and last August rain ponded water up to or near the 164 contour.

*PEC has contacted Jeff Bradley with Baughman about the design of the new RCB that will be constructed within the 29<sup>th</sup> Street North right of way. Mr. Bradley has had conversations with the City of Wichita stating the size of the RCB is not adequate to handle the 100 year storm event and 29<sup>th</sup> Street will back water up on the New Market Office Addition. This box culvert needs to be enlarged to handle the additional flow. The capacity of the 30" culvert underneath 29<sup>th</sup> Street will flood during a 100 year storm event and probably can't even handle the 2 year storm event. 29<sup>th</sup> Street North is in the process of being designed for improvements in this area.*

12. What are the match elevations along the east property line? Can you turn on the spot elevations?

*The spot elevations at the property lines and on the adjacent properties have been included on the revised drainage plan.*

13. The drainage plan should demonstrate in a summary table that post-developed conditions do not exceed existing conditions for all ranges of storm events up to the 100-year 24 hour event. Include the minimum 2, 5, 10, 100-year 24 hour events for comparison.

*A table including the pre vs. post development discharge rates for the 2, 5 & 100 year has been included in this package.*

14. A detail of the ponds and their outfall structures should be included on the plan with necessary elevations, side slopes and dimensions.

*These are design issues and will be address in the construction plans.*

15. The plan should include contours for the proposed detention facility to verify storage volumes to be included in the developed conditions model.

*This is another design issue and will be addressed in the construction plans.*

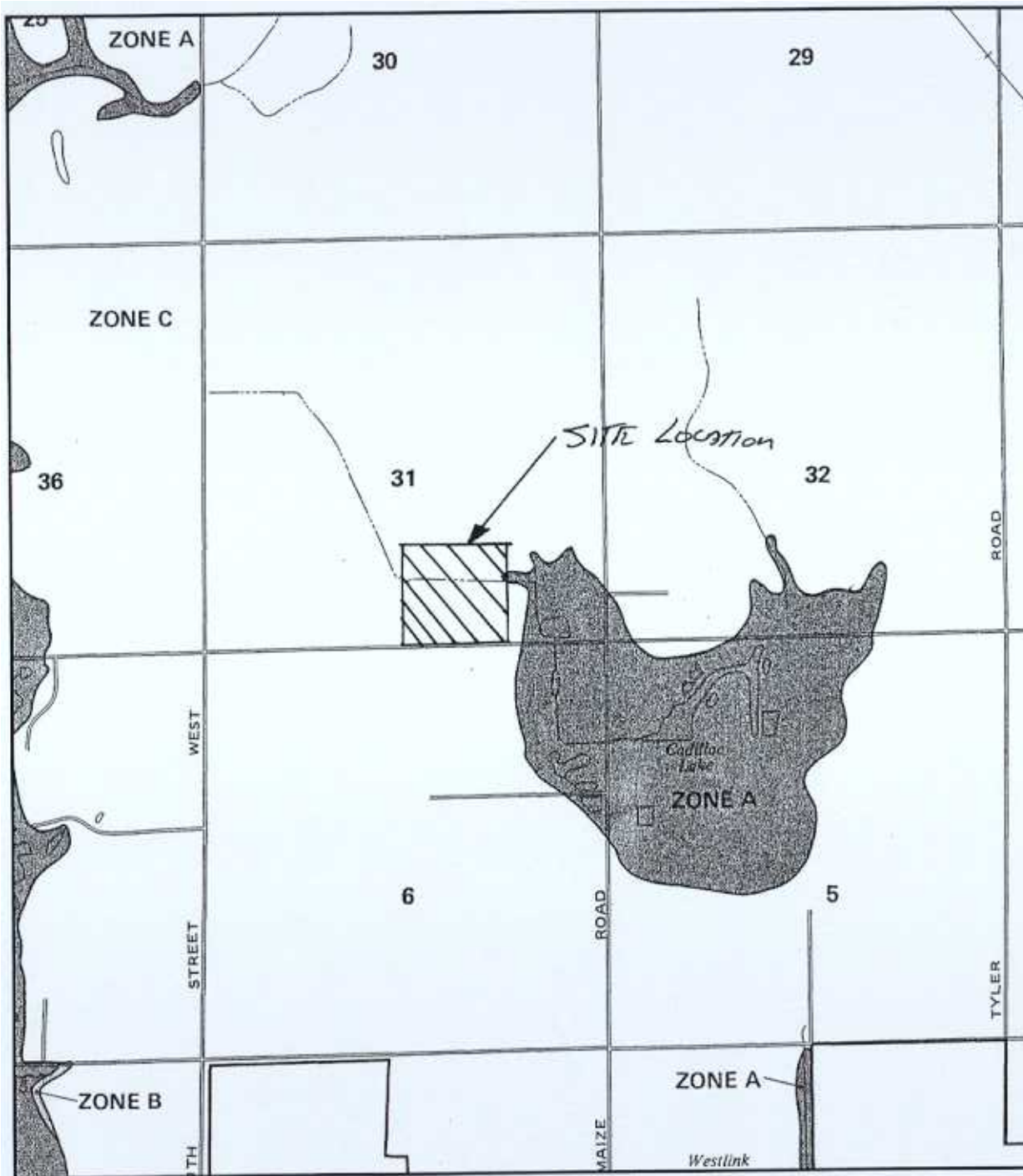
If you have any questions feel free to contact me at (316) 206-1316.

Sincerely,



Shawn R. Bryan, P.E.  
PEC  
303 S. Topeka  
Wichita, KS 67202

cc: File



APPROXIMATE SCALE  
 2000 0 2000 FEET

NATIONAL FLOOD INSURANCE PROGRAM

**FIRM**  
 FLOOD INSURANCE RATE MAP

SEDGWICK,  
 COUNTY,  
 KANSAS  
 (UNINCORPORATED AREAS)

PANEL 125 OF 300

COMMUNITY-PANEL NUMBER  
 200321 0125 A

EFFECTIVE DATE:  
 JUNE 3, 1986



Federal Emergency Management Agency

This is an official copy of a portion of the above referenced flood map. It was extracted using F-MIT On-Line. This map does not reflect changes or amendments which may have been made subsequent to the date on the title block. For the latest product information about National Flood Insurance Program flood maps check the FEMA Flood Map Store at [www.msc.fema.gov](http://www.msc.fema.gov)

This assumes a Weir Coefficient of 3.09

<u>Water Surface Elevation</u>	<u>Top of Lower Weir Elevation</u>	<u>Lower Weir Length (feet)</u>	<u>H1 (feet)</u>	<u>q1 (cfs/foot)</u>	<u>Top of Upper Weir Elevation</u>	<u>Upper Weir Length (feet)</u>	<u>H2 (feet)</u>	<u>q2 (cfs/foot)</u>	<u>Total Q (cfs)</u>
159.00	159.00	4.00	0.00	0.00	165.00	8.00	0.00	0.00	0.0
160.00	159.00	4.00	1.00	3.09	165.00	8.00	0.00	0.00	12.4
161.00	159.00	4.00	2.00	8.74	165.00	8.00	0.00	0.00	34.9
162.00	159.00	4.00	3.00	16.05	165.00	8.00	0.00	0.00	64.2
163.00	159.00	4.00	4.00	24.71	165.00	8.00	0.00	0.00	98.8
164.00	159.00	4.00	5.00	34.53	165.00	8.00	0.00	0.00	138.1
167.00	159.00	4.00	8.00	69.89	165.00	8.00	2.00	8.74	349.5

# NEW MARKET OFFICE ADDITION

## PRE VS. POST DISCHARGE RATE TABLE

Pre-Development			Post-Development		
Storm Event		Q, cfs		Q, cfs	
2 yr.		226		226	
5 yr.		245		239	
100 yr.		321		288	

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* JUN 1998
CENTER *
* VERSION 4.1
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* RUN DATE 06DEC06 TIME 11:36:32
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*
* U.S. ARMY CORPS OF
* HYDROLOGIC ENGINEERING
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

STRUCTURE. THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

LINE ID.....1.... .2 .3 .4.....5 .6 .7.....8.....9.....10

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ID MODIFIED FONTANA DRAINAGE PLAN (40-AC NEW MARKET OFFICE SPACE TRACT ADDED)  
ID DEVELOPED CONDITIONS  
ID BY BLB DATE 03-13-04, MODIFIED BY PDF 4/10/06

\*\*\* LIST \*\*\*  
\*\*\* FREE \*\*\*

	*DIAGRAM										
4	IT	15	01JAN04	1200		0	02JAN04	2000			
5	IN	15	01JAN04	1200							
6	IO	0	5								
7	JR	PREC	3.5	4.5	7.8						
	*										
	*										
8	KK	BSN5									
9	KO	5									
10	BA	0.023									
11	PB	1.00									
12	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
13	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
14	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
15	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
16	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
17	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
18	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
19	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
20	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
21	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
22	LS	0	68	10							
23	UD	0.600									
	*										
	*										
24	KK	POND7									
25	KO	5									
26	RS	1	ELEV	162.0							
27	SA	2.55	2.71	2.88	3.06						
28	SE	171.0	172.0	173.0	174.0						
29	SQ	0	3.2	6.4	9.6	12.8	16.0	19.2	22.4	25.6	28.8
30	SQ	32.0									
31	SE	171.0	171.35	171.56	171.73	171.88	172.02	172.16	172.28	172.40	172.52
32	SE	172.6									
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	*										
33	KK	BSN4									
34	KO	5									
35	BA	0.020									
36	PB	1.00									

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		0.000	0.003	006	0.008	0.011	0.014	017	019	0.022	0.025
		0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
		0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
		0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
41		0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
		0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903

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		0.982	0.985	0.988	0.991	0.994	0.997	0.000			

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		170.0	171	172	173.0		11	13			
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	SE	175									

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		0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
		0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
		0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
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	0.982	0.985	0.988	0.991	0.994	0.997	000			
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SE	167	168.0	169.0	170.0						
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	169.6									

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	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
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	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
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0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
0.982	0.985	0.988	0.991	0.994	0.997	1.000			

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0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
0.982	0.985	0.988	0.991	0.994	0.997	0.000			

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			3.42		
	166.0	167.0	168.0	169.0	
	158.0		0.6		
	167	0.00	3.0	1.	

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BSN10

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PC

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	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	100	0.105
	110	0.115	120	127	134	140	147	0.155	163	172
	181	193	0.204	220	235	0.259	0.283	387	0.663	0.699
	735	754	772	0.786	799	0.810	0.820	0.828	0.835	0.843
	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
	0.982	0.985	0.988	0.991	0.994	0.997	000			
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POND3

			162		12					
171										
172										
173		166.0	167.0	168.0	169.0					
174		158		0.6						
175		168.0	0.00	3.0						
176		BSN3								
177		0.024								
178		0.024								
179		0.024								
180	PC	0.000	003	0.006	008	0.011	.014	0.017	.019	0.025
181		0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.060
182		0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.105
183		110	115	120	127	134	0.140	147	155	172
184		181	193	204	220	235	259	283	387	0.663
185		735	754	0.772	786	0.799	0.810	0.820	0.828	0.835
186		0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898
187		0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943
188		0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976
189		0.982	0.985	0.988	0.991	0.994	0.997	0.000		
190		580								
191		580								
192		BSN2								
193		0.025								
194		0.025								
195		0.025								
196		0.000	003	0.006	008	0.011	.014	0.017	0.019	0.025
197		0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.060
198		0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.105
199		0.110	115	120	127	134	140	147	0.155	163
200	PC	181	0.193	204	0.220	235	0.259	283	387	0.663
201		0.735	754	772	786	799	0.810	0.820	0.828	0.835
202	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898
203	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943
204		0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976
205		0.982	0.985	0.988	0.991	0.994	0.997	1.000		
206	LS	0.670								
207		0.670								

HEC INPUT

PAGE

nmo.txt

208 KK POND1  
 209 KO 5  
 210 RS 1 ELEV 162.0  
 211 SA 0.36 0.43 0.49 0.57  
 212 SE 170.0 171.0 172.0 173.0  
 213 SQ 0 3.2 6.4 9.6 12.8 16.0 19.2 22.4 25.6 28.8  
 214 SQ 32.0  
 215 SE 170.0 170.17 170.27 170.35 170.42 170.49 170.56 170.62 170.67 170.73  
 216 SE 170.8  
 \*  
 \*

217 KK 3PD1&3  
 218 KO 5  
 219 HC 3 0  
 \*  
 \*

220 KK POND2  
 221 KO 5  
 222 RS 1 ELEV 158.0  
 223 SA 2.08 2.23 2.38 2.54  
 224 SE 166.0 167.0 168.0 169.0  
 225 SQ 0 26.9 53.8 80.7 107.6 134.5 161.4 188.3 215.2 242.1  
 226 SQ 269.0  
 227 SE 166.0 166.50 166.79 167.03 167.25 167.45 167.63 167.81 167.98 168.14  
 228 SE 168.3  
 \*  
 \*  
 \*

229 KK PONDA  
 230 KO 5  
 \*  
 \* ASSUMED OUTLET - 6.5' WEIR AT ELEV. 161.0  
 \*

231 RS 1 ELEV 161.0  
 232 SA 1.75 1.75  
 233 SE 161.0 170.0  
 234 SQ 0 15.4 45.9 91.6 148.0 213.1 286.0  
 235 SE 161.0 162.0 163.00 164.00 165.00 166.00 167.00  
 \*  
 \* 10 ACRES NORTH OF PROPOSED DEVELOPMENT  
 \*

236 KK NORTH

nmo.txt

237	KO	5									
238	BA	0.0156									
239	PB	1.00									
240	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
241	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
242	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
243	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
244	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699

HEC-1 INPUT

1

LINE	ID	1	2	3	4	5	6	7	8	9	10
245	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
246	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
247	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
248	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
249	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
250	LS	0	70	0							
251	UD	0.40									

\*  
\*  
\*

252	KK	OFFSTE									
253	KO	5									
254	HC	2	0								

\*  
\*  
\*  
\*  
\*  
\*  
\*  
\*  
\*

ADDED 40 ACRES DEVELOPED OFFICE PARK - Tc=20 MINUTED, 50% IMPERVIOUS

255	KK	DEV-1									
256	KO	5									
257	BA	0.0625									
258	PB	1.00									
259	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
260	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
261	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
262	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
263	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
264	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
265	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
266	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
267	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
268	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
269	LS	0	70	50							

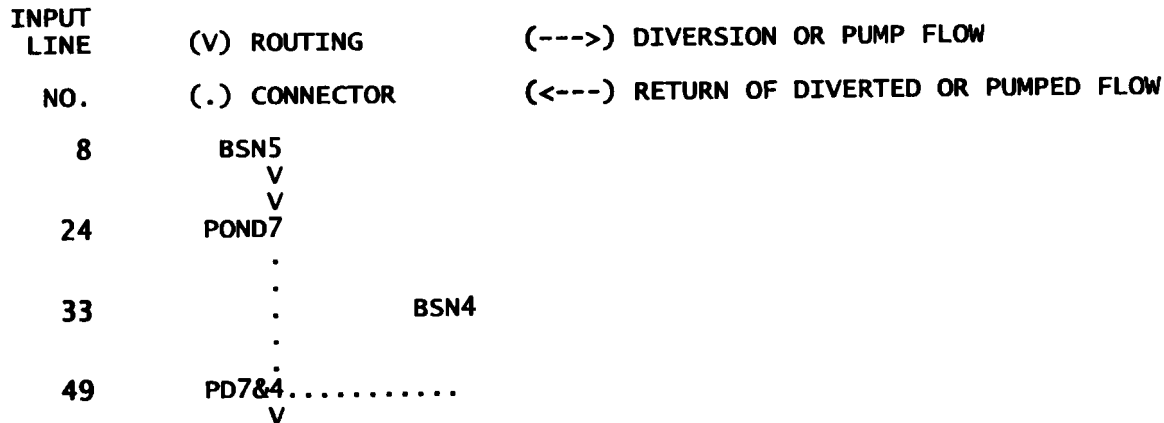
270 UD 0.20  
 \*  
 \*  
 \*  
 271 KK 29TH  
 272 KO 5  
 273 HC 2 0  
 \*  
 \*  
 \*  
 274 KK PONDB  
 275 KO 5  
 \*  
 \* ASSUMED OUTLET 4 & 8' WEIR AT ELEV. 159.0  
 \*  
 276 RS 1 ELEV 159.0  
 277 SA 8.00 8.00  
 HEC-1 INPUT

1

LINE	ID	1	2	3	4	5	6	7	8	9	10
278	SE	159.0	170.0								
279	SQ	0	12.4	34.9	64.2	98.8	138.1	349.5			
280	SE	159.0	160.00	161.00	162.00	163.00	164.00	167.00			
	*										
	*										
	*										
281	ZZ										

1

SCHMATIC DIAGRAM OF STREAM NETWORK



52	POND6			
		BSN7		
	7PD6			
	POND5			
		BSN6		
105		RTE6		
108			OFFST	
124				BSN8
140	608P5			
143	POND4			
150		BSN10		
166	10PD4			
169	POND3			
176		BSN3		
192			BSN2	
208			POND1	

```

217 3PD1&3 .....
      V
      V
220 POND2
      V
      V
229 PONDA
      .
      .
236 . NORTH
      .
      .
252 OFFSTE.....
      .
      .
255 . DEV-1
      .
      .
271 29TH.....
      V
      V
274 PONDB

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
ENGINEERS *
* JUN 1998 *
CENTER *
* VERSION 4.1 *
*
*
* RUN DATE 06DEC06 TIME 11:36:32 *
*
*
*****
*****

```

```

* U.S ARMY CORPS OF
* HYDROLOGIC ENGINEERING
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*

```

nmo.txt  
 MODIFIED FONTANA DRAINAGE PLAN (40-AC NEW MARKET OFFICE SPACE TRACT ADDED)  
 DEVELOPED CONDITIONS  
 BY BLB DATE 03-13-04, MODIFIED BY PDF 4/10/06

6 IO OUTPUT CONTROL VARIABLES  
 IPRNT 0 PRINT CONTROL  
 IPLOT 5 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 15 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1JAN 4 STARTING DATE  
 ITIME 1200 STARTING TIME  
 NQ 129 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 2JAN 4 ENDING DATE  
 NDTIME 2000 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .25 HOURS  
 TOTAL TIME BASE 32.00 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION  
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION  
 RATIOS OF PRECIPITATION  
 3.50 4.50 7.80

\*\*\* \*\*  
 \*\*\* \*\*

8 KK \*\*\*\*\*  
 \* \*  
 \* BSN5 \*  
 \* \*  
 \*\*\*\*\*

9 KO            OUTPUT CONTROL VARIABLES  
                  IPRNT            5   PRINT CONTROL  
                  IPLOT            5   PLOT CONTROL  
                  QSCAL            0.   HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
 \*\*\* \*\*

24 KK           \*\*\*\*\*  
                  \*                   \*  
                  \*        POND7   \*  
                  \*                   \*  
                  \*\*\*\*\*

25 KO            OUTPUT CONTROL VARIABLES  
                  IPRNT            5   PRINT CONTROL  
                  IPLOT            5   PLOT CONTROL  
                  QSCAL            0.   HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
 \*\*\* \*\*

33 KK            \*\*\*\*\*  
                  \*                   \*  
                  \*        BSN4   \*  
                  \*                   \*  
                  \*\*\*\*\*

34 KO            OUTPUT CONTROL VARIABLES  
                  IPRNT            5   PRINT CONTROL  
                  IPLOT            5   PLOT CONTROL  
                  QSCAL            0.   HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
 \*\*\* \*\*

\*\*\*\*\*  
 \*                   \*



49 KK \* PD7&4 \*  
\* \*  
\*\*\*\*\*

50 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
\*\*\* \*\*

\*\*\*\*\*  
\* \*  
52 KK \* POND6 \*  
\* \*  
\*\*\*\*\*

53 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
\*\*\* \*\*

\*\*\*\*\*  
\* \*  
61 KK \* BSN7 \*  
\* \*  
\*\*\*\*\*

62 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
\*\*\* \*\*



```
*****  
*           *  
77 KK      *   7PD6  *  
*           *  
*****
```

```
78 KO      OUTPUT CONTROL VARIABLES  
            IPRNT      5  PRINT CONTROL  
            IPLOT      5  PLOT CONTROL  
            QSCAL      0.  HYDROGRAPH PLOT SCALE
```

```
*** **  
*** **
```

```
*****  
*           *  
80 KK      *   POND5  *  
*           *  
*****
```

```
81 KO      OUTPUT CONTROL VARIABLES  
            IPRNT      5  PRINT CONTROL  
            IPLOT      5  PLOT CONTROL  
            QSCAL      0.  HYDROGRAPH PLOT SCALE
```

```
*** **  
*** **
```

```
*****  
*           *  
89 KK      *   BSN6   *  
*           *  
*****
```

```
90 KO      OUTPUT CONTROL VARIABLES  
            IPRNT      5  PRINT CONTROL  
            IPLOT      5  PLOT CONTROL  
            QSCAL      0.  HYDROGRAPH PLOT SCALE
```

\*\*\* \*\*  
\*\*\* \*\*

105 KK \*\*\*\*\*  
\* \*  
\* RTE6 \*  
\* \*  
\*\*\*\*\*

106 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
\*\*\* \*\*

108 KK \*\*\*\*\*  
\* \*  
\* OFFST \*  
\* \*  
\*\*\*\*\*

109 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
\*\*\* \*\*

124 KK \*\*\*\*\*  
\* \*  
\* BSN8 \*  
\* \*  
\*\*\*\*\*

125 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE



\*\*\* \*\*  
\*\*\* \*\*

140 KK \*\*\*\*\*  
\* \*  
\* 608P5 \*  
\* \*  
\*\*\*\*\*

141 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
\*\*\* \*\*

143 KK \*\*\*\*\*  
\* \*  
\* POND4 \*  
\* \*  
\*\*\*\*\*

144 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
\*\*\* \*\*

150 KK \*\*\*\*\*  
\* \*  
\* BSN10 \*  
\* \*  
\*\*\*\*\*

151 KO OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	5	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
 \*\*\* \*\*

166 KK \*\*\*\*\*  
 \* \*  
 \* 10PD4 \*  
 \* \*  
 \*\*\*\*\*

167 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 5 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
 \*\*\* \*\*

169 KK \*\*\*\*\*  
 \* \*  
 \* POND3 \*  
 \* \*  
 \*\*\*\*\*

170 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 5 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
 \*\*\* \*\*

176 KK \*\*\*\*\*  
 \* \*  
 \* BSN3 \*  
 \* \*

\*\*\*\*\*

177 KO            OUTPUT CONTROL VARIABLES  
                   IPRNT            5   PRINT CONTROL  
                   IPLOT            5   PLOT CONTROL  
                   QSCAL            0.   HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
 \*\*\* \*\*

\*\*\*\*\*

192 KK           \*            \*  
                  \*        BSN2   \*  
                  \*            \*  
                  \*\*\*\*\*

193 KO            OUTPUT CONTROL VARIABLES  
                   IPRNT            5   PRINT CONTROL  
                   IPLOT            5   PLOT CONTROL  
                   QSCAL            0.   HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
 \*\*\* \*\*

\*\*\*\*\*

208 KK           \*            \*  
                  \*        POND1   \*  
                  \*            \*  
                  \*\*\*\*\*

209 KO            OUTPUT CONTROL VARIABLES  
                   IPRNT            5   PRINT CONTROL  
                   IPLOT            5   PLOT CONTROL  
                   QSCAL            0.   HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
 \*\*\* \*\*

\*\*\*\*\*



217 KK \* 3PD1&3 \*  
\* \*  
\*\*\*\*\*

218 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
\*\*\* \*\*

220 KK \*\*\*\*\*  
\* \*  
\* POND2 \*  
\* \*  
\*\*\*\*\*

221 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
\*\*\* \*\*

229 KK \*\*\*\*\*  
\* \*  
\* PONDA \*  
\* \*  
\*\*\*\*\*

230 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
\*\*\* \*\*

236 KK \*\*\*\*\*  
\* \*  
\* NORTH \*  
\* \*  
\*\*\*\*\*

237 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
\*\*\* \*\*

252 KK \*\*\*\*\*  
\* \*  
\* OFFSTE \*  
\* \*  
\*\*\*\*\*

253 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*  
\*\*\* \*\*

255 KK \*\*\*\*\*  
\* \*  
\* DEV-1 \*  
\* \*  
\*\*\*\*\*

256 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE



\*\*\* \*\*  
\*\*\* \*\*

\*\*\*\*\*  
\*  
\* 29TH \*  
\*  
\*\*\*\*\*

271 KK

OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

272 KO

\*\*\* \*\*  
\*\*\* \*\*

\*\*\*\*\*  
\*  
\* PONDB \*  
\*  
\*\*\*\*\*

274 KK

OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

275 KO

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION		
				RATIO 1	RATIO 2	RATIO 3
				3.50	4.50	7.80
HYDROGRAPH AT						
+	BSN5	.02	1	7. 12.50	12. 12.50	32. 12.50

ROUTED TO

				nmo.txt			
+	POND7	.02	1	FLOW TIME	2. 14.00	3. 13.75	12. 13.50
			**	PEAK STAGES	IN FEET	**	
			1	STAGE TIME	171.22 14.00	171.36 13.75	171.83 13.50
+	HYDROGRAPH AT BSN4	.02	1	FLOW TIME	5. 12.75	8. 12.75	22. 12.75
+	2 COMBINED AT PD7&4	.04	1	FLOW TIME	7. 13.00	11. 13.00	31. 13.00
+	ROUTED TO POND6	.04	1	FLOW TIME	2. 17.50	3. 17.00	10. 15.50
			**	PEAK STAGES	IN FEET	**	
			1	STAGE TIME	170.59 17.75	170.90 17.00	172.05 15.50
+	HYDROGRAPH AT BSN7	.05	1	FLOW TIME	14. 12.75	23. 12.75	61. 12.75
+	2 COMBINED AT 7PD6	.10	1	FLOW TIME	14. 12.75	24. 12.75	64. 12.75
+	ROUTED TO POND5	.10	1	FLOW TIME	6. 14.50	11. 14.25	35. 13.75
			**	PEAK STAGES	IN FEET	**	
			1	STAGE TIME	167.50 14.50	167.77 14.25	168.73 13.75
+	HYDROGRAPH AT BSN6	.01	1	FLOW TIME	3. 12.50	4. 12.50	12. 12.50
+	ROUTED TO RTE6	.01	1	FLOW TIME	3. 13.25	4. 13.25	12. 13.25

HYDROGRAPH AT

+	OFFST	.36	1	FLOW TIME	nmo.txt 66. 13.75	109. 13.50	273. 13.50
+	HYDROGRAPH AT BSN8	.03	1	FLOW TIME	9. 12.50	15. 12.50	40. 12.25
+	4 COMBINED AT 608P5	.49	1	FLOW TIME	76. 13.50	126. 13.50	326. 13.50
+	ROUTED TO POND4	.49	1	FLOW TIME	200. .25	200. .25	232. 14.50
				** PEAK STAGES IN FEET **			
			1	STAGE TIME	166.00 .25	166.00 .25	168.71 14.50
+	HYDROGRAPH AT BSN10	.02	1	FLOW TIME	6. 12.50	10. 12.50	27. 12.50
+	2 COMBINED AT 10PD4	.51	1	FLOW TIME	206. 12.50	211. 12.50	236. 14.50
+	ROUTED TO POND3	.51	1	FLOW TIME	203. 13.50	205. 13.50	224. 15.50
				** PEAK STAGES IN FEET **			
			1	STAGE TIME	166.72 13.50	166.86 13.50	168.52 15.50
+	HYDROGRAPH AT BSN3	.02	1	FLOW TIME	8. 12.50	13. 12.50	33. 12.50
+	HYDROGRAPH AT BSN2	.03	1	FLOW TIME	7. 12.50	12. 12.50	32. 12.50
+	ROUTED TO POND1	.03	1	FLOW TIME	7. 12.75	12. 12.75	31. 12.75

\*\* PEAK STAGES IN FEET \*\*

				nmo.txt			
			1	STAGE TIME	170.29 12.75	170.40 12.75	170.78 12.75
+ 3 COMBINED AT	3PD1&3	.56	1	FLOW TIME	216. 12.75	227. 12.75	270. 12.50
+ ROUTED TO	POND2	.56	1	FLOW TIME	215. 13.00	226. 12.75	267. 12.75
				** PEAK STAGES IN FEET **			
			1	STAGE TIME	167.98 13.00	168.04 12.75	168.29 12.75
+ ROUTED TO	PONDA	.56	1	FLOW TIME	214. 13.25	223. 13.25	260. 13.00
				** PEAK STAGES IN FEET **			
			1	STAGE TIME	166.01 13.25	166.14 13.25	166.64 13.00
+ HYDROGRAPH AT	NORTH	.02	1	FLOW TIME	6. 12.25	10. 12.25	27. 12.25
+ 2 COMBINED AT	OFFSTE	.58	1	FLOW TIME	216. 13.25	227. 13.00	269. 13.00
+ HYDROGRAPH AT	DEV-1	.06	1	FLOW TIME	65. 12.00	91. 12.00	184. 12.00
+ 2 COMBINED AT	29TH	.64	1	FLOW TIME	270. 12.00	299. 12.00	409. 12.00
+ ROUTED TO	PONDB	.64	1	FLOW TIME	226. 13.00	239. 13.00	288. 13.25
				** PEAK STAGES IN FEET **			
			1	STAGE TIME	165.25 13.00	165.43 13.00	166.12 13.25



xt

NORMAL END

Pag



**NEWMARKET SQUARE**  
**Wichita, Sedgwick County, Kansas**  
04/10/06

NewMarket Square is a 40.0 acre, commercial office development located in the northwest part of Wichita in Sedgwick County, Kansas. The future 40 acre development will consist of parking lots, buildings, storm sewer and detention ponds. This report contains a drawing of the drainage plan, supporting calculations and data for the NewMarket Square Drainage Plan.

**Hydrology**

The proposed plat lies in the SE 1/4, Section 31, T26S, R1W. The soil on-site is comprised of Shellabarger sandy loam (Sa), Vanoss silt loam (Va) and Waurika silt loam (Wb), which are classified in hydrologic groups B, B and D, respectively. The land is currently used for agricultural purposes and has short grass and bare ground throughout. The site is bordered to the north and east by residential properties, to the south by 29<sup>th</sup> Street North, and to the west currently by agriculture land. The area to the west of the proposed NewMarket Development will be a developed 137.5 acre residential development consisting of 233 lots, streets, and detention ponds. A natural drainage channel cuts through this site from the west property line (Fontana Development) to the east property line and then flowing to the south to 29<sup>th</sup> street where it passes through a 24" culvert. Existing site drains to the channel that runs through the property with an additional 267 cfs being contributed from the Fontana property. The proposed Basin A drains to the same outfall as the pre-developed flow. This post-development flow will flow through the series of ponds, with structures, and eventually to the natural drainage channel on the south side of 29<sup>th</sup> street. It was assumed in the design of this drainage plan that the culvert underneath 29<sup>th</sup> street would be improved along with the 29<sup>th</sup> street in the future and the flowline elevation set at 159.00.

The Rational Method was used to calculate runoff quantities. Runoff coefficients were estimated based on tables presented in the Design Aids section of this report using fully

developed conditions. Time of concentration was based on slope, flow velocity and length of flow through each basin and was not allowed to be less than 20 minutes. It was assumed in the post-development calculations that the proposed office park would be 50% impervious. The HEC-1 computer program was used to route the runoff through the ponds and determine the post-development conditions leaving the site.

The analysis was made based on the available site data which includes the following: 1" = 100' topographic map with 1' contours of the site, a Sedgwick County Soil Survey Map and noted references.

### Design Aids

This section includes material used to assist in designing the drainage system. A 1" = 100' scale Drainage Plan map (Attachment A) and a 1" = 100' scale Four-Corner Plan map (Attachment B) are enclosed in the pockets.

### References

Design of Urban Highway Drainage – The State of the Art, by Reitz & Jens, Inc., April 1980.

Drainage of Highway Pavements, Hydraulic Engineering Circular #12, by Tye Engineering, Inc., March 1984.

Interim Drainage and Storm Sewer Policy for Design Criteria and Documentation, City of Wichita, Kansas, 1985.

Soil Survey of Sedgwick County, Kansas, US Department of Agriculture, Soil Conservation Service, 1979.

## EXISTING CONDITIONS

## Time of concentration (Tc) or travel time (Tt)

Project : NEWMARKET OFFICE  
 Location : Wichita, Kansas

By: SB Date: 4/10/2006  
 Checked: \_\_\_\_\_ Date: \_\_\_\_\_

Circle One  Present  Developed

Circle One  Tc  Tt through subarea

**NOTES:** Space for as many as two segments per flow type can be used for each worksheet.  
 Include map, schematic, or description of flow segments.

**Sheet flow** (Applicable to Tc only)

- Segment ID**
1. Surface description (Table 3-1)
  2. Mannings roughness coeff., n (Table 3-1)
  3. Flow length, L (total L < 300 ft.)
  4. Two-yr 24-hr rainfall, P2
  5. Calculated Land slope, s
  - 5a. Land Elevation For Upper End Of Flow Path
  - 5b. Land Elevation For Lower End Of Flow Path
  6. Compute Tt

AB	
Grass	
0.08	
ft	300
in	3.60
ft/ft	0.022
171.5	
165.0	
hr	0.22

= 0.22

**Shallow concentrated flow**

- Segment ID**
7. Surface description (Paved or Unpaved)
  8. Flow length, L
  9. Calculated Watercourse slope, s
  - 9a. Land Elevation For Upper End Of Flow Path
  - 9b. Land Elevation For Lower End Of Flow Path
  10. Average velocity, V (Figure 3-1)
  11.  $Tt = L/3600V$  Compute Tt

BC	
Unpaved	
900	
ft	900
ft/ft	0.001
165.0	
163.7	
ft/s	0.61
hr	0.41

= 0.41

**Channel Flow**

- Segment ID**
12. Cross sectional flow area, a
  13. Wetted perimeter, Pw
  14. Hydraulic radius,  $r = a/Pw$  Compute r
  15. Channel slope, s
  16. Manning's roughness coeff., n
  17.  $V = 1.49(r^{0.667})(s^{0.50})/n$  Compute V
  18. Flow length, L
  19.  $Tt = L/3600V$  Compute Tt
  20. Watershed or subarea Tc or Tt (add Tt in steps 6,11, and 19)

CD	
sf	100.00
ft	60
ft	1.667
ft/ft	0.001
0.011	
ft/s	6.3
ft	1050
hr	0.046

= 0.05  
**hr** 0.67

**Reference** Urban Hydrology for Small Watersheds  
 Technical Release 55, Soil Conservation Service  
 U.S. Department of Agriculture, June 1986

Use Time Of Concentration =

40 Minutes

Project: **NEWMARKET OFFICE**  
 Date: 4/10/2006  
 Prep. By: SRB

Manual Input

**EXISTING**

Total Area 50.00 Acres

Soil Group	A (% of Total Area)	B (% of Total Area)	C (% of Total Area)	D (% of Total Area)	Total
	0%	60%	0%	40%	100%
Acres	0.00	24.00	0.00	16.00	40.00

Land Use	Commercial (% of Total Area)	Industrial (% of Total Area)	Multi-Family (% of Total Area)	Public (% of Total Area)	Single Family (% of Total Area)	Vacant/Agriculture (% of Total Area)
Existing	0%	0%	0%	0%	20%	80%
Acres	0.00	0.00	0.00	0.00	10.00	40.00

Existing	
Length of Flow	1900 ft
Slope	0.01 %
Waterflow Desc	Bare Ground/Ag.
Avg Velocity	0.63 ft/sec
Tc	0.84 hours

15 min <= Tc <= 24 hrs

Runoff Coefficients \* Used Soil Group C

Return Period (Years)	Commercial	Industrial	Multi-Family	Public	Single Family	Vacant/Agriculture
2	0.68	0.68	0.63	0.49	0.48	0.24
5	0.69	0.69	0.66	0.51	0.51	0.27
10	0.73	0.73	0.71	0.56	0.57	0.35
25	0.75	0.75	0.73	0.59	0.60	0.40
50	0.77	0.77	0.76	0.62	0.64	0.45
100	0.80	0.80	0.79	0.66	0.68	0.51

Existing Conditions

Return Period (Years)	Runoff Coefficient *	Rainfall Intensity (in/hr)	Area (Acres)	Runoff (cfs)
2	0.29	2.24	50.00	32.26
5	0.32	2.76	50.00	43.88
10	0.39	3.22	50.00	63.43
25	0.44	3.76	50.00	82.72
50	0.49	4.25	50.00	103.70
100	0.54	4.66	50.00	126.75

```
*****  
*  
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *  
* FEBRUARY 1981 *  
* REVISED 02 AUG 88 *  
*  
* RUN DATE 04/10/2006 TIME 13:51:39 *  
*  
*****
```

```
*****  
*  
* U.S. ARMY CORPS OF ENGINEERS *  
* THE HYDROLOGIC ENGINEERING CENTER *  
* 609 SECOND STREET *  
* DAVIS, CALIFORNIA 95616 *  
* (916) 551-1748 *  
*  
*****
```

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X X XXXXXX XXXX X  
X X X X X XX  
X X X X X X  
XXXXXX XXXX X XXXX X  
X X X X X X  
X X X X X X  
X X XXXXXX XXXX XXX
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

New Market Sq. - 40-Acre Tract - Prop. Office Park Developm. D/S of Fontana Exist. Cond.

HEC-1 INPUT

PAGE 1

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1         ID      MODIFIED FONTANA DRAINAGE PLAN (40-AC UNDEVELOPED TRACT D/S ADDED)
2         ID      40- ACRE NEW MARKET OFFICE TRACT (PRE-PROJECT CONDITIONS)
3         ID      BY BLB   DATE 03-13-04, MODIFIED BY PDF 4/10/06

*** LIST ***
*** FREE ***

*DIAGRAM
4         IT      15 01JAN04   1200       0 02JAN04   2000
5         IN      15 01JAN04   1200
6         IO      0          5
7         JR      PREC    7.8
*
*
*
8         KK      BSN5
9         KO      5
10        BA      0.023
11        PB      1.00
12        PC      0.000  0.003  0.006  0.008  0.011  0.014  0.017  0.019  0.022  0.025
13        PC      0.029  0.032  0.035  0.038  0.042  0.045  0.048  0.052  0.056  0.060
14        PC      0.064  0.068  0.072  0.076  0.080  0.085  0.090  0.095  0.100  0.105
15        PC      0.110  0.115  0.120  0.127  0.134  0.140  0.147  0.155  0.163  0.172
16        PC      0.181  0.193  0.204  0.220  0.235  0.259  0.283  0.387  0.663  0.699
17        PC      0.735  0.754  0.772  0.786  0.799  0.810  0.820  0.828  0.835  0.843
18        PC      0.850  0.858  0.865  0.873  0.880  0.885  0.889  0.894  0.898  0.903
19        PC      0.907  0.912  0.916  0.921  0.925  0.929  0.934  0.938  0.943  0.947
20        PC      0.952  0.955  0.958  0.961  0.964  0.967  0.970  0.973  0.976  0.979
21        PC      0.982  0.985  0.988  0.991  0.994  0.997  1.000
22        LS      0          68      10
23        UD      0.600
*
*
24        KK      POND7
25        KO      5
26        RS      1      ELEV  162.0
27        SA      2.55  2.71  2.88  3.06
28        SE      171.0  172.0  173.0  174.0
29        SQ      0          3.2    6.4    9.6    12.8   16.0   19.2   22.4   25.6   28.8
30        SQ      32.0
31        SE      171.0  171.35  171.56  171.73  171.88  172.02  172.16  172.28  172.40  172.52
32        SE      172.6
*
*
33        KK      BSN4
34        KO      5
35        BA      0.020
36        PB      1.00
37        PC      0.000  0.003  0.006  0.008  0.011  0.014  0.017  0.019  0.022  0.025
38        PC      0.029  0.032  0.035  0.038  0.042  0.045  0.048  0.052  0.056  0.060
39        PC      0.064  0.068  0.072  0.076  0.080  0.085  0.090  0.095  0.100  0.105
40        PC      0.110  0.115  0.120  0.127  0.134  0.140  0.147  0.155  0.163  0.172
41        PC      0.181  0.193  0.204  0.220  0.235  0.259  0.283  0.387  0.663  0.699
42        PC      0.735  0.754  0.772  0.786  0.799  0.810  0.820  0.828  0.835  0.843
    
```

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
43	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
44	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
45	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
46	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
47	LS	0	68	10							
48	UD	0.850									
	*										
	*										
49	KK	PD7&4									
50	KO	5									
51	HC	2	0								
	*										
	*										
52	KK	POND6									
53	KO	5									
54	RS	1	ELEV	162.0							
55	SA	1.85	1.99	2.14	2.29						
56	SE	170.0	171.0	172.0	173.0						
57	SQ	0	2.2	4.4	6.6	8.8	11.0	13.2	15.4	17.6	19.8
58	SQ	22.0									
59	SE	170.0	170.72	171.11	171.42	171.77	172.21	172.75	173.40	174.14	174.98
60	SE	175.9									
	*										
	*										
61	KK	BSN7									
62	KO	5									
63	BA	0.055									
64	PB	1.00									
65	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
66	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
67	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
68	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
69	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
70	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
71	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
72	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
73	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
74	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
75	LS	0	68	10							
76	UD	0.840									
	*										
	*										
77	KK	7PD6									
78	KO	5									
79	HC	2	0								
	*										
	*										

HCC-1 INPUT

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10										
80	KK	PONDS									
81	KO	5									
82	RS	1	ELEV	159.0							
83	SA	2.67	2.84	3.01	3.19						
84	SE	167.0	168.0	169.0	170.0						
85	SQ	0	6.3	12.6	18.9	25.2	31.5	37.8	44.1	50.4	56.7
86	SQ	63.0									
87	SE	167.0	167.55	167.87	168.14	168.39	168.61	168.82	169.01	169.20	169.38
88	SE	169.6									
	*										
	*										
89	KK	BSN6									
90	KO	5									
91	BA	0.008									
92	PB	1.00									
93	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
94	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
95	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
96	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
97	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
98	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
99	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
100	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
101	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
102	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
103	LS	0	68	10							
104	UD	0.530									
	*										
	*										
105	KK	RTE6									
106	KO	5	5								
107	RT	0	0	3							
	*										
	*										
108	KK	OFFST									
109	BA	0.359									
110	PB	1.00									
111	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
112	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
113	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
114	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
115	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
116	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
117	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
118	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
119	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
120	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
121	LS	0	70	10							
122	UD	1.575									
	*										
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
123	KK	BSN8									
124	KO	5									
125	BA	0.027									
126	PB	1.00									
127	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
128	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
129	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
130	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
131	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
132	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
133	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
134	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
135	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
136	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
137	LS	0	68	10							
138	UD	0.490									
	*										
	*										
139	KK	608P5									
140	KO	5									
141	HC	4	0								
	*										
	*										
142	KK	POND4									
143	KO	5									
144	RS	1	ELEV	158.0							
145	SA	3.06	3.24	3.42	3.61						
146	SE	166.0	167.0	168.0	169.0						
147	SL	158.0	14.73	0.6	0.5						
148	SS	167.0	0.00	3.0	1.5						
	*										
	*										
149	KK	BSN10									
150	KO	5									
151	BA	0.021									
152	PB	1.00									
153	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
154	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
155	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
156	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
157	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
158	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
159	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
160	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
161	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
162	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
163	LS	0	68	10							
164	UD	0.670									
	*										
	*										

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10										
165	KK	10PD4									
166	KO	5									
167	HC	2	0								
	*										
	*										
168	KK	POND3									
169	KO	5									
170	RS	1	ELEV	162.0							
171	SA	1.70	1.83	1.98	2.12						
172	SE	166.0	167.0	168.0	169.0						
173	SL	158.5	14.73	0.6	0.5						
174	SS	168.0	0.00	3.0	1.5						
	*										
	*										
175	KK	BSN3									
176	KO	5									
177	BA	0.024									
178	PB	1.00									
179	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
180	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
181	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
182	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
183	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
184	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
185	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
186	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
187	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
188	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
189	LS	0	68	10							
190	UD	0.580									
	*										
	*										
191	KK	BSN2									
192	KO	5									
193	BA	0.025									
194	PB	1.00									
195	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
196	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
197	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
198	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
199	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
200	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
201	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
202	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
203	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
204	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
205	LS	0	68	10							
206	UD	0.670									
	*										
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10	
207	KK	POND1										
208	KO	5										
209	RS	1	ELEV	162.0								
210	SA	0.36	0.43	0.49	0.57							
211	SE	170.0	171.0	172.0	173.0							
212	SQ	0	3.2	6.4	9.6	12.8	16.0	19.2	22.4	25.6	28.8	
213	SQ	32.0										
214	SE	170.0	170.17	170.27	170.35	170.42	170.49	170.56	170.62	170.67	170.73	
215	SE	170.8										
	*											
	*											
216	KK	3PD1&3										
217	KO	5										
218	HC	3	0									
	*											
	*											
219	KK	POND2										
220	KO	5										
221	RS	1	ELEV	158.0								
222	SA	2.08	2.23	2.38	2.54							
223	SE	166.0	167.0	168.0	169.0							
224	SQ	0	26.9	53.8	80.7	107.6	134.5	161.4	188.3	215.2	242.1	
225	SQ	269.0										
226	SE	166.0	166.50	166.79	167.03	167.25	167.45	167.63	167.81	167.98	168.14	
227	SE	168.3										
	*											
	*											
	*	ROUTE 267 CPS FROM FONTANA TO 29TH STREET										
	*											
228	KK	RTE6										
229	KO	5										
230	RT	0	0	2.0								
	*											
	*											
231	KK	NM-UND										
232	KO	5										
233	BA	0.0625										
234	PB	1.00										
235	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025	
236	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060	
237	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105	
238	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172	
239	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699	
240	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843	
241	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903	
242	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947	
243	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979	
244	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000				
245	LS	0	70	0								

HEC-1 INPUT

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
246	UD 0.40
	*
	*
247	KK 29TH
248	KO 5
249	HC 2 0
	*
	*
	*
250	ZZ

New Market Sq. - 40-Acre Tract - Prop. Office Park Developm. D/S of Fontana Exist. Cond

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE NO.	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
8	BSN5	
	V	
	V	
24	POND7	
	.	
33	.	BSN4
	.	.
49	PD7&4.....	
	V	
	V	
52	POND6	
	.	
61	.	BSN7
	.	.
77	7PD6.....	
	V	
	V	
80	POND5	
	.	
89	.	BSN6
	.	V
	.	V
105	.	RTE6
	.	.
108	.	OFFST
	.	.
123	.	.
	.	BSN8
	.	.
139	60&P5.....	
	V	
	V	
142	POND4	
	.	
149	.	BSN10
	.	.
165	10PD4.....	
	V	
	V	
168	POND3	
	.	
175	.	BSN3
	.	.
191	.	BSN2
	.	V
	.	V
207	.	POND1
	.	.
216	3PD1&3.....	
	V	
	V	
219	POND2	
	V	
	V	
228	RTE6	
	.	
231	.	NM-UND
	.	.
247	29TH.....	

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
\* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
\* FEBRUARY 1981 \*  
\* REVISED 02 AUG 88 \*  
\* RUN DATE 04/10/2006 TIME 13:51:39 \*  
\*\*\*\*\*

\*\*\*\*\*  
\* U.S. ARMY CORPS OF ENGINEERS \*  
\* THE HYDROLOGIC ENGINEERING CENTER \*  
\* 609 SECOND STREET \*  
\* DAVIS, CALIFORNIA 95616 \*  
\* (916) 551-1748 \*  
\*\*\*\*\*

MODIFIED FONTANA DRAINAGE PLAN (40-AC UNDEVELOPED TRACT D/S ADDED)  
40- ACRE NEW MARKET OFFICE TRACT (PRE-PROJECT CONDITIONS)  
BY BLB DATE 03-13-04, MODIFIED BY PDF 4/10/06

6 IO OUTPUT CONTROL VARIABLES  
IPRNT 0 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
NMIN 15 MINUTES IN COMPUTATION INTERVAL  
IDATE 1JAN 4 STARTING DATE  
ITIME 1200 STARTING TIME  
NQ 129 NUMBER OF HYDROGRAPH ORDINATES  
NDDATE 2JAN 4 ENDING DATE  
NDTIME 2000 ENDING TIME  
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .25 HOURS  
TOTAL TIME BASE 32.00 HOURS

ENGLISH UNITS  
DRAINAGE AREA SQUARE MILES  
PRECIPITATION DEPTH INCHES  
LENGTH, ELEVATION FEET  
FLOW CUBIC FEET PER SECOND  
STORAGE VOLUME ACRE-FEET  
SURFACE AREA ACRES  
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION  
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION  
RATIOS OF PRECIPITATION  
7.80

\*\*\* \*\* \*\* \*\* \*\*

\*\*\*\*\*  
\* \*  
8 KK \* BSN5 \*  
\* \*  
\*\*\*\*\*

9 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\*~

\*\*\*\*\*  
\* \*  
24 KK \* POND7 \*  
\* \*  
\*\*\*\*\*

25 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL

IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\*

\*\*\*\*\*  
\* \*  
33 KK \* BSN4 \*  
\* \*  
\*\*\*\*\*

34 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\*

\*\*\*\*\*  
\* \*  
49 KK \* PD7&4 \*  
\* \*  
\*\*\*\*\*

50 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\*

\*\*\*\*\*  
\* \*  
52 KK \* POND6 \*  
\* \*  
\*\*\*\*\*

53 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\*

\*\*\*\*\*  
\* \*  
61 KK \* BSN7 \*  
\* \*  
\*\*\*\*\*

62 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\*

\*\*\*\*\*  
\* \*  
77 KK \* 7PD6 \*  
\* \*  
\*\*\*\*\*

78 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL

I PLOT 5 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\* \*\*

\*\*\*\*\*  
 \* \*  
 80 KK \* POND5 \*  
 \* \*  
 \*\*\*\*\*

81 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 I PLOT 5 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\* \*\*

\*\*\*\*\*  
 \* \*  
 89 KK \* BSN6 \*  
 \* \*  
 \*\*\*\*\*

90 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 I PLOT 5 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\*~

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 \* \*  
 105 KK \* RTE6 \*  
 \* \*  
 \*\*\*\*\*

106 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 I PLOT 5 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\*~

\*\*\*\*\*  
 \* \*  
 108 KK \* OFFST \*  
 \* \*  
 \*\*\*\*\*

5 IN TIME DATA FOR INPUT TIME SERIES  
 JXMIN 15 TIME INTERVAL IN MINUTES  
 JXDATE 1JAN 4 STARTING DATE  
 JXTIME 1200 STARTING TIME

SUBBASIN RUNOFF DATA

109 BA SUBBASIN CHARACTERISTICS  
 TAREA .36 SUBBASIN AREA

PRECIPITATION DATA

110 PB STORM 1.00 BASIN TOTAL PRECIPITATION

111 PI INCREMENTAL PRECIPITATION PATTERN  
 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00  
 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00  
 .00 .00 .00 .00 .01 .01 .00 .01 .00 .01

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.01	.00	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.02	.02	.02	.02	.10	.28	.04	.04	.04
.02	.02	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

121 LS SCS LOSS RATE  
 STRTL .86 INITIAL ABSTRACTION  
 CRVNER 70.00 CURVE NUMBER  
 RTIMP 10.00 PERCENT IMPERVIOUS AREA

122 UD SCS DIMENSIONLESS UNITGRAPH  
 TLAG 1.58 LAG

\*\*\*

UNIT HYDROGRAPH  
 34 END-OF-PERIOD ORDINATES

6.	19.	38.	65.	88.	100.	102.	96.	86.	72.
55.	42.	33.	26.	21.	16.	13.	10.	8.	6.
5.	4.	3.	2.	2.	1.	1.	1.	1.	1.
0.	0.	0.	0.						

\*\*\*\*\*

HYDROGRAPH AT STATION OFFST

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DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	*	DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
1	JAN	1200	1	.00	.00	.00	0.	*	2	JAN	0415	66	.00	.00	.00	1.
1	JAN	1215	2	.00	.00	.00	0.	*	2	JAN	0430	67	.00	.00	.00	1.
1	JAN	1230	3	.00	.00	.00	0.	*	2	JAN	0445	68	.00	.00	.00	1.
1	JAN	1245	4	.00	.00	.00	0.	*	2	JAN	0500	69	.00	.00	.00	1.
1	JAN	1300	5	.00	.00	.00	0.	*	2	JAN	0515	70	.00	.00	.00	1.
1	JAN	1315	6	.00	.00	.00	0.	*	2	JAN	0530	71	.00	.00	.00	1.
1	JAN	1330	7	.00	.00	.00	0.	*	2	JAN	0545	72	.00	.00	.00	1.
1	JAN	1345	8	.00	.00	.00	0.	*	2	JAN	0600	73	.00	.00	.00	1.
1	JAN	1400	9	.00	.00	.00	0.	*	2	JAN	0615	74	.00	.00	.00	1.
1	JAN	1415	10	.00	.00	.00	0.	*	2	JAN	0630	75	.00	.00	.00	1.
1	JAN	1430	11	.00	.00	.00	0.	*	2	JAN	0645	76	.00	.00	.00	1.
1	JAN	1445	12	.00	.00	.00	0.	*	2	JAN	0700	77	.00	.00	.00	1.
1	JAN	1500	13	.00	.00	.00	0.	*	2	JAN	0715	78	.00	.00	.00	1.
1	JAN	1515	14	.00	.00	.00	0.	*	2	JAN	0730	79	.00	.00	.00	1.
1	JAN	1530	15	.00	.00	.00	0.	*	2	JAN	0745	80	.00	.00	.00	1.
1	JAN	1545	16	.00	.00	.00	0.	*	2	JAN	0800	81	.00	.00	.00	1.
1	JAN	1600	17	.00	.00	.00	0.	*	2	JAN	0815	82	.00	.00	.00	1.
1	JAN	1615	18	.00	.00	.00	0.	*	2	JAN	0830	83	.00	.00	.00	1.
1	JAN	1630	19	.00	.00	.00	0.	*	2	JAN	0845	84	.00	.00	.00	1.
1	JAN	1645	20	.00	.00	.00	0.	*	2	JAN	0900	85	.00	.00	.00	1.
1	JAN	1700	21	.00	.00	.00	0.	*	2	JAN	0915	86	.00	.00	.00	1.
1	JAN	1715	22	.00	.00	.00	0.	*	2	JAN	0930	87	.00	.00	.00	0.
1	JAN	1730	23	.00	.00	.00	0.	*	2	JAN	0945	88	.00	.00	.00	0.
1	JAN	1745	24	.00	.00	.00	0.	*	2	JAN	1000	89	.00	.00	.00	0.
1	JAN	1800	25	.00	.00	.00	0.	*	2	JAN	1015	90	.00	.00	.00	0.
1	JAN	1815	26	.01	.00	.00	0.	*	2	JAN	1030	91	.00	.00	.00	0.
1	JAN	1830	27	.01	.00	.00	0.	*	2	JAN	1045	92	.00	.00	.00	0.
1	JAN	1845	28	.00	.00	.00	0.	*	2	JAN	1100	93	.00	.00	.00	0.
1	JAN	1900	29	.01	.00	.00	0.	*	2	JAN	1115	94	.00	.00	.00	0.
1	JAN	1915	30	.00	.00	.00	0.	*	2	JAN	1130	95	.00	.00	.00	0.
1	JAN	1930	31	.01	.00	.00	0.	*	2	JAN	1145	96	.00	.00	.00	0.
1	JAN	1945	32	.01	.00	.00	0.	*	2	JAN	1200	97	.00	.00	.00	0.
1	JAN	2000	33	.00	.00	.00	0.	*	2	JAN	1215	98	.00	.00	.00	0.
1	JAN	2015	34	.01	.01	.00	0.	*	2	JAN	1230	99	.00	.00	.00	0.
1	JAN	2030	35	.01	.01	.00	0.	*	2	JAN	1245	100	.00	.00	.00	0.
1	JAN	2045	36	.01	.01	.00	0.	*	2	JAN	1300	101	.00	.00	.00	0.
1	JAN	2100	37	.01	.01	.00	0.	*	2	JAN	1315	102	.00	.00	.00	0.
1	JAN	2115	38	.01	.01	.00	0.	*	2	JAN	1330	103	.00	.00	.00	0.
1	JAN	2130	39	.01	.01	.00	1.	*	2	JAN	1345	104	.00	.00	.00	0.
1	JAN	2145	40	.01	.01	.00	1.	*	2	JAN	1400	105	.00	.00	.00	0.
1	JAN	2200	41	.01	.01	.00	1.	*	2	JAN	1415	106	.00	.00	.00	0.
1	JAN	2215	42	.01	.01	.00	1.	*	2	JAN	1430	107	.00	.00	.00	0.
1	JAN	2230	43	.01	.01	.00	1.	*	2	JAN	1445	108	.00	.00	.00	0.
1	JAN	2245	44	.02	.01	.00	1.	*	2	JAN	1500	109	.00	.00	.00	0.
1	JAN	2300	45	.02	.01	.00	1.	*	2	JAN	1515	110	.00	.00	.00	0.
1	JAN	2315	46	.02	.02	.00	1.	*	2	JAN	1530	111	.00	.00	.00	0.
1	JAN	2330	47	.02	.02	.00	1.	*	2	JAN	1545	112	.00	.00	.00	0.

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1 JAN 2345	48	.10	.09	.01	1.	*	2 JAN 1600	113	.00	.00	.00	0.
2 JAN 0000	49	.28	.25	.03	1.	*	2 JAN 1615	114	.00	.00	.00	0.
2 JAN 0015	50	.04	.03	.00	2.	*	2 JAN 1630	115	.00	.00	.00	0.
2 JAN 0030	51	.04	.03	.00	3.	*	2 JAN 1645	116	.00	.00	.00	0.
2 JAN 0045	52	.02	.02	.00	4.	*	2 JAN 1700	117	.00	.00	.00	0.
2 JAN 0100	53	.02	.02	.00	5.	*	2 JAN 1715	118	.00	.00	.00	0.
2 JAN 0115	54	.01	.01	.00	5.	*	2 JAN 1730	119	.00	.00	.00	0.
2 JAN 0130	55	.01	.01	.00	5.	*	2 JAN 1745	120	.00	.00	.00	0.
2 JAN 0145	56	.01	.01	.00	5.	*	2 JAN 1800	121	.00	.00	.00	0.
2 JAN 0200	57	.01	.01	.00	5.	*	2 JAN 1815	122	.00	.00	.00	0.
2 JAN 0215	58	.01	.01	.00	4.	*	2 JAN 1830	123	.00	.00	.00	0.
2 JAN 0230	59	.01	.01	.00	4.	*	2 JAN 1845	124	.00	.00	.00	0.
2 JAN 0245	60	.01	.01	.00	3.	*	2 JAN 1900	125	.00	.00	.00	0.
2 JAN 0300	61	.01	.01	.00	3.	*	2 JAN 1915	126	.00	.00	.00	0.
2 JAN 0315	62	.01	.01	.00	2.	*	2 JAN 1930	127	.00	.00	.00	0.
2 JAN 0330	63	.01	.01	.00	2.	*	2 JAN 1945	128	.00	.00	.00	0.
2 JAN 0345	64	.01	.01	.00	2.	*	2 JAN 2000	129	.00	.00	.00	0.
2 JAN 0400	65	.01	.01	.00	1.	*						

\*\*\*\*\*  
 TOTAL RAINFALL = 1.00, TOTAL LOSS = .90, TOTAL EXCESS = .10

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	32.00-HR	
+ 5.	13.50	3.	1.	1.	1.	
		(INCHES)	.069	.103	.104	.104
		(AC-FT)	1.	2.	2.	2.

CUMULATIVE AREA = .36 SQ MI

\*\*\*\*\*  
 HYDROGRAPH AT STATION OFFST  
 PLAN 1, RATIO = 7.80

DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	*	DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
1 JAN 1200	1	.00	.00	.00	0.	*	2 JAN 0415	66	.04	.01	.03	77.				
1 JAN 1215	2	.02	.02	.00	0.	*	2 JAN 0430	67	.03	.00	.03	70.				
1 JAN 1230	3	.02	.02	.00	0.	*	2 JAN 0445	68	.04	.01	.03	64.				
1 JAN 1245	4	.02	.01	.00	0.	*	2 JAN 0500	69	.03	.00	.03	58.				
1 JAN 1300	5	.02	.02	.00	0.	*	2 JAN 0515	70	.04	.01	.03	53.				
1 JAN 1315	6	.02	.02	.00	0.	*	2 JAN 0530	71	.03	.00	.03	49.				
1 JAN 1330	7	.02	.02	.00	1.	*	2 JAN 0545	72	.04	.01	.03	45.				
1 JAN 1345	8	.02	.01	.00	1.	*	2 JAN 0600	73	.03	.00	.03	41.				
1 JAN 1400	9	.02	.02	.00	1.	*	2 JAN 0615	74	.04	.01	.03	39.				
1 JAN 1415	10	.02	.02	.00	1.	*	2 JAN 0630	75	.03	.00	.03	36.				
1 JAN 1430	11	.03	.03	.00	1.	*	2 JAN 0645	76	.03	.00	.03	34.				
1 JAN 1445	12	.02	.02	.00	2.	*	2 JAN 0700	77	.04	.01	.03	33.				
1 JAN 1500	13	.02	.02	.00	2.	*	2 JAN 0715	78	.03	.00	.03	32.				
1 JAN 1515	14	.02	.02	.00	2.	*	2 JAN 0730	79	.04	.01	.03	31.				
1 JAN 1530	15	.03	.03	.00	2.	*	2 JAN 0745	80	.03	.00	.03	30.				
1 JAN 1545	16	.02	.02	.00	2.	*	2 JAN 0800	81	.04	.01	.03	29.				
1 JAN 1600	17	.02	.02	.00	2.	*	2 JAN 0815	82	.02	.00	.02	29.				
1 JAN 1615	18	.03	.03	.00	2.	*	2 JAN 0830	83	.02	.00	.02	28.				
1 JAN 1630	19	.03	.03	.00	2.	*	2 JAN 0845	84	.02	.00	.02	28.				
1 JAN 1645	20	.03	.03	.00	2.	*	2 JAN 0900	85	.02	.00	.02	27.				
1 JAN 1700	21	.03	.03	.00	2.	*	2 JAN 0915	86	.02	.00	.02	26.				
1 JAN 1715	22	.03	.03	.00	2.	*	2 JAN 0930	87	.02	.00	.02	25.				
1 JAN 1730	23	.03	.03	.00	2.	*	2 JAN 0945	88	.02	.00	.02	24.				
1 JAN 1745	24	.03	.03	.00	3.	*	2 JAN 1000	89	.02	.00	.02	23.				
1 JAN 1800	25	.03	.03	.00	3.	*	2 JAN 1015	90	.02	.00	.02	22.				
1 JAN 1815	26	.04	.04	.00	3.	*	2 JAN 1030	91	.02	.00	.02	21.				
1 JAN 1830	27	.04	.04	.00	3.	*	2 JAN 1045	92	.02	.00	.02	21.				
1 JAN 1845	28	.04	.04	.00	3.	*	2 JAN 1100	93	.02	.00	.02	20.				
1 JAN 1900	29	.04	.04	.00	3.	*	2 JAN 1115	94	.02	.00	.02	20.				
1 JAN 1915	30	.04	.04	.00	3.	*	2 JAN 1130	95	.02	.00	.02	20.				
1 JAN 1930	31	.04	.04	.00	3.	*	2 JAN 1145	96	.02	.00	.02	20.				
1 JAN 1945	32	.04	.03	.00	3.	*	2 JAN 1200	97	.02	.00	.02	19.				
1 JAN 2000	33	.04	.03	.00	3.	*	2 JAN 1215	98	.00	.00	.00	19.				
1 JAN 2015	34	.05	.05	.01	3.	*	2 JAN 1230	99	.00	.00	.00	19.				
1 JAN 2030	35	.05	.05	.01	4.	*	2 JAN 1245	100	.00	.00	.00	18.				
1 JAN 2045	36	.05	.04	.01	4.	*	2 JAN 1300	101	.00	.00	.00	16.				
1 JAN 2100	37	.05	.04	.01	4.	*	2 JAN 1315	102	.00	.00	.00	15.				

New Market Sq. - 40-Acre Tract - Prop. Office Park Developm. D/S of Fontana Exist. Cond.

1 JAN 2115	38	.06	.05	.01	5.	*	2 JAN 1330	103	.00	.00	.00	13.
1 JAN 2130	39	.06	.05	.02	5.	*	2 JAN 1345	104	.00	.00	.00	10.
1 JAN 2145	40	.07	.05	.02	6.	*	2 JAN 1400	105	.00	.00	.00	8.
1 JAN 2200	41	.07	.05	.02	7.	*	2 JAN 1415	106	.00	.00	.00	7.
1 JAN 2215	42	.09	.06	.03	8.	*	2 JAN 1430	107	.00	.00	.00	5.
1 JAN 2230	43	.09	.06	.03	10.	*	2 JAN 1445	108	.00	.00	.00	4.
1 JAN 2245	44	.12	.08	.04	11.	*	2 JAN 1500	109	.00	.00	.00	3.
1 JAN 2300	45	.12	.07	.05	14.	*	2 JAN 1515	110	.00	.00	.00	3.
1 JAN 2315	46	.19	.11	.08	16.	*	2 JAN 1530	111	.00	.00	.00	2.
1 JAN 2330	47	.19	.10	.09	20.	*	2 JAN 1545	112	.00	.00	.00	2.
1 JAN 2345	48	.81	.37	.44	27.	*	2 JAN 1600	113	.00	.00	.00	1.
2 JAN 0000	49	2.15	.64	1.51	46.	*	2 JAN 1615	114	.00	.00	.00	1.
2 JAN 0015	50	.28	.06	.22	78.	*	2 JAN 1630	115	.00	.00	.00	1.
2 JAN 0030	51	.28	.06	.22	125.	*	2 JAN 1645	116	.00	.00	.00	1.
2 JAN 0045	52	.15	.03	.12	182.	*	2 JAN 1700	117	.00	.00	.00	0.
2 JAN 0100	53	.14	.03	.11	231.	*	2 JAN 1715	118	.00	.00	.00	0.
2 JAN 0115	54	.11	.02	.09	262.	*	2 JAN 1730	119	.00	.00	.00	0.
2 JAN 0130	55	.10	.02	.08	273.	*	2 JAN 1745	120	.00	.00	.00	0.
2 JAN 0145	56	.09	.02	.07	268.	*	2 JAN 1800	121	.00	.00	.00	0.
2 JAN 0200	57	.08	.01	.06	251.	*	2 JAN 1815	122	.00	.00	.00	0.
2 JAN 0215	58	.06	.01	.05	225.	*	2 JAN 1830	123	.00	.00	.00	0.
2 JAN 0230	59	.05	.01	.05	193.	*	2 JAN 1845	124	.00	.00	.00	0.
2 JAN 0245	60	.06	.01	.05	165.	*	2 JAN 1900	125	.00	.00	.00	0.
2 JAN 0300	61	.05	.01	.05	143.	*	2 JAN 1915	126	.00	.00	.00	0.
2 JAN 0315	62	.06	.01	.05	125.	*	2 JAN 1930	127	.00	.00	.00	0.
2 JAN 0330	63	.05	.01	.05	109.	*	2 JAN 1945	128	.00	.00	.00	0.
2 JAN 0345	64	.06	.01	.05	96.	*	2 JAN 2000	129	.00	.00	.00	0.
2 JAN 0400	65	.05	.01	.05	85.	*						

\*\*\*\*\*  
 TOTAL RAINFALL = 7.80, TOTAL LOSS = 3.16, TOTAL EXCESS = 4.64

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	32.00-HR	
+	273.	136.	45.	34.	34.	
		(INCHES)	3.529	4.622	4.644	4.644
		(AC-FT)	68.	88.	89.	89.

CUMULATIVE AREA = .36 SQ MI

\*\*\*\*\*

\*\*\*\*\*  
 \* \* \*  
 123 KK \* BSN8 \*  
 \* \* \*  
 \*\*\*\*\*

124 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 5 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\*\*\*

\*\*\*\*\*  
 \* \* \*  
 139 KK \* 608P5 \*  
 \* \* \*  
 \*\*\*\*\*

140 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 5 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\*\*\*

```
*****
*          *
*  POND4  *
*          *
*****
```

```
143 KO      OUTPUT CONTROL VARIABLES
            IPRNT      5  PRINT CONTROL
            IPLOT      5  PLOT CONTROL
            QSCAL      0.  HYDROGRAPH PLOT SCALE
```

\*\*\* \*\* \*\* \*\* \*\*

```
*****
*          *
*  BSN10  *
*          *
*****
```

```
150 KO      OUTPUT CONTROL VARIABLES
            IPRNT      5  PRINT CONTROL
            IPLOT      5  PLOT CONTROL
            QSCAL      0.  HYDROGRAPH PLOT SCALE
```

\*\*\* \*\* \*\* \*\*~

```
*****
*          *
*  10PD4  *
*          *
*****
```

```
166 KO      OUTPUT CONTROL VARIABLES
            IPRNT      5  PRINT CONTROL
            IPLOT      5  PLOT CONTROL
            QSCAL      0.  HYDROGRAPH PLOT SCALE
```

\*\*\* \*\* \*\* \*\*~

```
*****
*          *
*  POND3  *
*          *
*****
```

```
169 KO      OUTPUT CONTROL VARIABLES
            IPRNT      5  PRINT CONTROL
            IPLOT      5  PLOT CONTROL
            QSCAL      0.  HYDROGRAPH PLOT SCALE
```

\*\*\* \*\* \*\* \*\*~

```
*****
*          *
*  BSN3   *
*          *
*****
```

```
176 KO      OUTPUT CONTROL VARIABLES
            IPRNT      5  PRINT CONTROL
            IPLOT      5  PLOT CONTROL
            QSCAL      0.  HYDROGRAPH PLOT SCALE
```

\*\*\* \*\* \*\* \*\*~

```
*****  
*           *  
191 KK  *   BSN2 *  
*           *  
*****
```

```
192 KO      OUTPUT CONTROL VARIABLES  
          IPRNT      5 PRINT CONTROL  
          IPLOT      5 PLOT CONTROL  
          QSCAL      0. HYDROGRAPH PLOT SCALE
```

\*\*\*\*\*

```
*****  
*           *  
207 KK  *   POND1 *  
*           *  
*****
```

```
208 KO      OUTPUT CONTROL VARIABLES  
          IPRNT      5 PRINT CONTROL  
          IPLOT      5 PLOT CONTROL  
          QSCAL      0. HYDROGRAPH PLOT SCALE
```

\*\*\*\*\*

```
*****  
*           *  
216 KK  * 3PD1&3 *  
*           *  
*****
```

```
217 KO      OUTPUT CONTROL VARIABLES  
          IPRNT      5 PRINT CONTROL  
          IPLOT      5 PLOT CONTROL  
          QSCAL      0. HYDROGRAPH PLOT SCALE
```

\*\*\*\*\*

```
*****  
*           *  
219 KK  *   POND2 *  
*           *  
*****
```

```
220 KO      OUTPUT CONTROL VARIABLES  
          IPRNT      5 PRINT CONTROL  
          IPLOT      5 PLOT CONTROL  
          QSCAL      0. HYDROGRAPH PLOT SCALE
```

\*\*\*\*\*

```
*****  
*           *  
228 KK  *   RTE6 *  
*           *  
*****
```

```
229 KO      OUTPUT CONTROL VARIABLES  
          IPRNT      5 PRINT CONTROL  
          IPLOT      5 PLOT CONTROL  
          QSCAL      0. HYDROGRAPH PLOT SCALE
```

\*\*\*\*\*

```
*****  
*      *  
231 KK *  NM-UND *  
*      *  
*****
```

```
232 KO      OUTPUT CONTROL VARIABLES  
          IPRNT      5  PRINT CONTROL  
          IPLOT      5  PLOT CONTROL  
          QSCAL      0.  HYDROGRAPH PLOT SCALE
```

\*\*\* \*\* \*\* \*\* \*\*

```
*****  
*      *  
247 KK *  29TH *  
*      *  
*****
```

```
248 KO      OUTPUT CONTROL VARIABLES  
          IPRNT      5  PRINT CONTROL  
          IPLOT      5  PLOT CONTROL  
          QSCAL      0.  HYDROGRAPH PLOT SCALE
```

New Market Sq. - 40-Acre Tract - Prop. Office Park Developm. D/S of Fontana Exist. Cond.

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	
					7.80
HYDROGRAPH AT					
+	BSN5	.02	1	FLOW	32.
				TIME	12.50
ROUTED TO					
+	POND7	.02	1	FLOW	12.
				TIME	13.50
				** PEAK STAGES IN FEET **	
			1	STAGE	171.83
				TIME	13.50
HYDROGRAPH AT					
+	BSN4	.02	1	FLOW	22.
				TIME	12.75
2 COMBINED AT					
+	PD7&4	.04	1	FLOW	31.
				TIME	13.00
ROUTED TO					
+	POND6	.04	1	FLOW	10.
				TIME	15.50
				** PEAK STAGES IN FEET **	
			1	STAGE	172.05
				TIME	15.50
HYDROGRAPH AT					
+	BSN7	.05	1	FLOW	61.
				TIME	12.75
2 COMBINED AT					
+	7PD6	.10	1	FLOW	64.
				TIME	12.75
ROUTED TO					
+	POND5	.10	1	FLOW	35.
				TIME	13.75
				** PEAK STAGES IN FEET **	
			1	STAGE	168.73
				TIME	13.75
HYDROGRAPH AT					
+	BSN6	.01	1	FLOW	12.
				TIME	12.50
ROUTED TO					
+	RTE6	.01	1	FLOW	12.
				TIME	13.25
HYDROGRAPH AT					
+	OFFST	.36	1	FLOW	273.
				TIME	13.50
HYDROGRAPH AT					
+	BSN8	.03	1	FLOW	40.
				TIME	12.25
4 COMBINED AT					
+	608P5	.49	1	FLOW	326.
				TIME	13.50
ROUTED TO					
+	POND4	.49	1	FLOW	232.
				TIME	14.50
				** PEAK STAGES IN FEET **	

New Market Sq. - 40-Acre Tract - Prop. Office Park Developm. D/S of Fontana Exist. Cond.

			1	STAGE	168.71
				TIME	14.50
HYDROGRAPH AT					
+	BSN10	.02	1	FLOW	27.
				TIME	12.50
2 COMBINED AT					
+	10PD4	.51	1	FLOW	236.
				TIME	14.50
ROUTED TO					
+	POND3	.51	1	FLOW	224.
				TIME	15.50
				** PEAK STAGES IN FEET **	
			1	STAGE	168.52
				TIME	15.50
HYDROGRAPH AT					
+	BSN3	.02	1	FLOW	33.
				TIME	12.50
HYDROGRAPH AT					
+	BSN2	.03	1	FLOW	32.
				TIME	12.50
ROUTED TO					
+	POND1	.03	1	FLOW	31.
				TIME	12.75
				** PEAK STAGES IN FEET **	
			1	STAGE	170.78
				TIME	12.75
3 COMBINED AT					
+	3PD1&3	.56	1	FLOW	270.
				TIME	12.50
ROUTED TO					
+	POND2	.56	1	FLOW	267.
				TIME	12.75
				** PEAK STAGES IN FEET **	
			1	STAGE	168.29
				TIME	12.75
ROUTED TO					
+	RTE6	.56	1	FLOW	267.
				TIME	13.25
HYDROGRAPH AT					
+	NM-UND	.06	1	FLOW	108.
				TIME	12.25
2 COMBINED AT					
+	29TH	.62	1	FLOW	316.
				TIME	12.25

\*\*\* NORMAL END OF HEC-1 \*\*\*

**350.0** Maximum Q (cfs)  
**10.000** Weir Width (feet)  
**162.50** Weir Elevation  
**2.900** Weir Flow Coefficient (Never > 3.089)

<u>Q</u> <u>(cfs)</u>	<u>Weir</u> <u>Width</u> <u>(feet)</u>	<u>Weir</u> <u>Elevation</u>	<u>q</u>	<u>Weir</u> <u>Flow</u> <u>Coeff.</u>	<u>Energy</u> <u>Head</u> <u>(feet)</u>	<u>Water</u> <u>Surface</u> <u>Elevation</u>
0.0	10.000	162.50	0.0	2.900	0.00	162.50
35.0	10.000	162.50	3.5	2.900	1.13	163.63
70.0	10.000	162.50	7.0	2.900	1.80	164.30
105.0	10.000	162.50	10.5	2.900	2.36	164.86
140.0	10.000	162.50	14.0	2.900	2.86	165.36
175.0	10.000	162.50	17.5	2.900	3.31	165.81
210.0	10.000	162.50	21.0	2.900	3.74	166.24
245.0	10.000	162.50	24.5	2.900	4.15	166.65
280.0	10.000	162.50	28.0	2.900	4.53	167.03
315.0	10.000	162.50	31.5	2.900	4.90	167.40
350.0	10.000	162.50	35.0	2.900	5.26	167.76

**350.0** Maximum Q (cfs)  
**10.000** Weir Width (feet)  
**159.00** Weir Elevation  
**2.900** Weir Flow Coeffecient (Never > 3.089)

<u>Q</u> (cfs)	<u>Weir</u> <u>Width</u> (feet)	<u>Weir</u> <u>Elevation</u>	<u>q</u>	<u>Weir</u> <u>Flow</u> <u>Coeff.</u>	<u>Energy</u> <u>Head</u> (feet)	<u>Water</u> <u>Surface</u> <u>Elevation</u>
0.0	10.000	159.00	0.0	2.900	0.00	159.00
35.0	10.000	159.00	3.5	2.900	1.13	160.13
70.0	10.000	159.00	7.0	2.900	1.80	160.80
105.0	10.000	159.00	10.5	2.900	2.36	161.36
140.0	10.000	159.00	14.0	2.900	2.86	161.86
175.0	10.000	159.00	17.5	2.900	3.31	162.31
210.0	10.000	159.00	21.0	2.900	3.74	162.74
245.0	10.000	159.00	24.5	2.900	4.15	163.15
280.0	10.000	159.00	28.0	2.900	4.53	163.53
315.0	10.000	159.00	31.5	2.900	4.90	163.90
350.0	10.000	159.00	35.0	2.900	5.26	164.26

DEVELOPED CONDITIONS

Project: **NEWMARKET OFFICE**  
 Date: 4/10/2006  
 Prep. By: SRB

Manual Input

**POST-DEVELOPMENT**

Total Area 50.00 Acres

Soil Group	A (% of Total Area)	B (% of Total Area)	C (% of Total Area)	D (% of Total Area)	Total
	0%	75%	0%	25%	100%
Acres	0.00	30.00		10.00	50.00

Land Use	Commercial (% of Total Area)	Industrial (% of Total Area)	Multi-Family (% of Total Area)	Public (% of Total Area)	Single Family (% of Total Area)	Vacant/Agriculture (% of Total Area)
Existing	40%	0%	0%	0%	20%	40%
Acres	20.00	0.00	0.00	0.00	10.00	20.00

**Developed**

Length of Flow 1300 ft  
 Slope 1.00 %  
 Waterflow Desc IMP. AREA  
 Avg Velocity 1.08 ft/sec  
 Tc 0.33 hours

15 min <= Tc <= 24 hrs

Runoff Coefficients \* Used Soil Group B/D

Return Period (Years)	Commercial	Industrial	Multi-Family	Public	Single Family	Vacant/Agriculture
2	0.68	0.68	0.70	0.49	0.50	0.54
5	0.69	0.69	0.73	0.51	0.54	0.56
10	0.73	0.73	0.79	0.56	0.62	0.61
25	0.75	0.75	0.81	0.59	0.66	0.64
50	0.77	0.77	0.83	0.62	0.70	0.67
100	0.80	0.80	0.86	0.66	0.76	0.70

Existing Conditions

Return Period (Years)	Runoff Coefficient *	Rainfall Intensity (in/hr)	Area (Acres)	Runoff (cfs)
2	0.68	3.33	50.00	113.22
5	0.69	4.00	50.00	138.00
10	0.73	4.60	50.00	167.90
25	0.75	5.35	50.00	200.63
50	0.77	6.00	50.00	231.00
100	0.80	6.53	50.00	261.20

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

```
*****  
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *  
* FEBRUARY 1981 *  
* REVISED 02 AUG 88 *  
* RUN DATE 04/10/2006 TIME 15:29:00 *  
*****
```

```
*****  
* U.S. ARMY CORPS OF ENGINEERS *  
* THE HYDROLOGIC ENGINEERING CENTER *  
* 609 SECOND STREET *  
* DAVIS, CALIFORNIA 95616 *  
* (916) 551-1748 *  
*****
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X X XXXXXX XXXX X  
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 1

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1         ID      MODIFIED FONTANA DRAINAGE PLAN (40-AC NEW MARKET OFFICE SPACE TRACT ADDED)
2         ID      DEVELOPED CONDITIONS
3         ID      BY BLB   DATE 03-13-04, MODIFIED BY PDF 4/10/06

*** LIST ***
*** FREE ***

*DIAGRAM
4         IT      15 01JAN04   1200       0 02JAN04   2000
5         IN      15 01JAN04   1200
6         IO      0           5
7         JR      PREC      7.8
*
*
8         KK      BSN5
9         KO      5
10        BA      0.023
11        PB      1.00
12        PC      0.000  0.003  0.006  0.008  0.011  0.014  0.017  0.019  0.022  0.025
13        PC      0.029  0.032  0.035  0.038  0.042  0.045  0.048  0.052  0.056  0.060
14        PC      0.064  0.068  0.072  0.076  0.080  0.085  0.090  0.095  0.100  0.105
15        PC      0.110  0.115  0.120  0.127  0.134  0.140  0.147  0.155  0.163  0.172
16        PC      0.181  0.193  0.204  0.220  0.235  0.259  0.283  0.387  0.663  0.699
17        PC      0.735  0.754  0.772  0.786  0.799  0.810  0.820  0.828  0.835  0.843
18        PC      0.850  0.858  0.865  0.873  0.880  0.885  0.889  0.894  0.898  0.903
19        PC      0.907  0.912  0.916  0.921  0.925  0.929  0.934  0.938  0.943  0.947
20        PC      0.952  0.955  0.958  0.961  0.964  0.967  0.970  0.973  0.976  0.979
21        PC      0.982  0.985  0.988  0.991  0.994  0.997  1.000
22        LS      0           68      10
23        UD      0.600
*
*
24        KK      POND7
25        KO      5
26        RS      1      ELEV  162.0
27        SA      2.55  2.71  2.88  3.06
28        SE      171.0  172.0  173.0  174.0
29        SQ      0           3.2    6.4    9.6    12.8   16.0   19.2   22.4   25.6   28.8
30        SQ      32.0
31        SE      171.0  171.35  171.56  171.73  171.88  172.02  172.16  172.28  172.40  172.52
32        SE      172.6
*
*
33        KK      BSN4
34        KO      5
35        BA      0.020
36        PB      1.00
37        PC      0.000  0.003  0.006  0.008  0.011  0.014  0.017  0.019  0.022  0.025
38        PC      0.029  0.032  0.035  0.038  0.042  0.045  0.048  0.052  0.056  0.060
39        PC      0.064  0.068  0.072  0.076  0.080  0.085  0.090  0.095  0.100  0.105
40        PC      0.110  0.115  0.120  0.127  0.134  0.140  0.147  0.155  0.163  0.172
41        PC      0.181  0.193  0.204  0.220  0.235  0.259  0.283  0.387  0.663  0.699
42        PC      0.735  0.754  0.772  0.786  0.799  0.810  0.820  0.828  0.835  0.843
    
```

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
43	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
44	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
45	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
46	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
47	LS	0	68	10							
48	UD	0.850									
	*										
49	KK	PD7&4									
50	KD	5									
51	HC	2	0								
	*										
52	KK	POND6									
53	KD	5									
54	RS	1	ELEV	162.0							
55	SA	1.85	1.99	2.14	2.29						
56	SE	170.0	171.0	172.0	173.0						
57	SQ	0	2.2	4.4	6.6	8.8	11.0	13.2	15.4	17.6	19.8
58	SQ	22.0									
59	SE	170.0	170.72	171.11	171.42	171.77	172.21	172.75	173.40	174.14	174.98
60	SE	175.9									
	*										
61	KK	BSN7									
62	KD	5									
63	BA	0.055									
64	PB	1.00									
65	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
66	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
67	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
68	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
69	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
70	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
71	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
72	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
73	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
74	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
75	LS	0	68	10							
76	UD	0.840									
	*										
77	KK	7PD6									
78	KD	5									
79	HC	2	0								
	*										

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 3

LINE	ID	1	2	3	4	5	6	7	8	9	10	
80	KK	POND5										
81	KO	5										
82	RS	1	ELEV	159.0								
83	SA	2.67	2.84	3.01	3.19							
84	SE	167.0	168.0	169.0	170.0							
85	SQ	0	6.3	12.6	18.9	25.2	31.5	37.8	44.1	50.4	56.7	
86	SQ	63.0										
87	SE	167.0	167.55	167.87	168.14	168.39	168.61	168.82	169.01	169.20	169.38	
88	SE	169.6										
	*											
	*											
89	KK	BSN6										
90	KO	5										
91	BA	0.008										
92	PB	1.00										
93	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025	
94	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060	
95	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105	
96	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172	
97	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699	
98	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843	
99	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903	
100	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947	
101	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979	
102	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000				
103	LS	0	68	10								
104	UD	0.530										
	*											
	*											
105	KK	RTE6										
106	KO	5										
107	RT	0	0	3								
	*											
	*											
108	KK	OFFST										
109	KO	5										
110	BA	0.359										
111	PB	1.00										
112	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025	
113	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060	
114	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105	
115	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172	
116	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699	
117	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843	
118	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903	
119	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947	
120	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979	
121	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000				
122	LS	0	70	10								
123	UD	1.575										
	*											
	*											

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 4

LINE	ID	1	2	3	4	5	6	7	8	9	10
124	KK	BSN8									
125	KO	5									
126	BA	0.027									
127	PB	1.00									
128	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
129	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
130	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
131	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
132	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
133	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
134	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
135	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
136	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
137	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
138	LS	0	68	10							
139	UD	0.490									
	*										
	*										
140	KK	608P5									
141	KO	5									
142	HC	4	0								
	*										
	*										
143	KK	POND4									
144	KO	5									
145	RS	1	ELEV	158.0							
146	SA	3.06	3.24	3.42	3.61						
147	SE	166.0	167.0	168.0	169.0						
148	SL	158.0	14.73	0.6	0.5						
149	SS	167.0	0.00	3.0	1.5						
	*										
	*										
150	KK	BSN10									
151	KO	5									
152	BA	0.021									
153	PB	1.00									
154	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
155	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
156	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
157	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
158	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
159	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
160	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
161	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
162	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
163	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
164	LS	0	68	10							
165	UD	0.670									
	*										
	*										

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 5

LINE	ID	1	2	3	4	5	6	7	8	9	10
166	KK	10PDM									
167	KO	5									
168	HC	2	0								
	*										
	*										
169	KK	POND3									
170	KO	5									
171	RS	1	ELEV	162.0							
172	SA	1.70	1.83	1.98	2.12						
173	SE	166.0	167.0	168.0	169.0						
174	SL	158.5	14.73	0.6	0.5						
175	SS	168.0	0.00	3.0	1.5						
	*										
	*										
176	KK	BSN3									
177	KO	5									
178	BA	0.024									
179	PB	1.00									
180	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
181	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
182	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
183	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
184	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
185	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
186	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
187	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
188	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
189	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
190	LS	0	68	10							
191	UD	0.580									
	*										
	*										
192	KK	BSN2									
193	KO	5									
194	BA	0.025									
195	PB	1.00									
196	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
197	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
198	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105
199	PC	0.110	0.115	0.120	0.127	0.134	0.140	0.147	0.155	0.163	0.172
200	PC	0.181	0.193	0.204	0.220	0.235	0.259	0.283	0.387	0.663	0.699
201	PC	0.735	0.754	0.772	0.786	0.799	0.810	0.820	0.828	0.835	0.843
202	PC	0.850	0.858	0.865	0.873	0.880	0.885	0.889	0.894	0.898	0.903
203	PC	0.907	0.912	0.916	0.921	0.925	0.929	0.934	0.938	0.943	0.947
204	PC	0.952	0.955	0.958	0.961	0.964	0.967	0.970	0.973	0.976	0.979
205	PC	0.982	0.985	0.988	0.991	0.994	0.997	1.000			
206	LS	0	68	10							
207	UD	0.670									
	*										
	*										

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 6

LINE	ID	1	2	3	4	5	6	7	8	9	10
208	KK	POND1									
209	KO	5									
210	RS	1	ELEV	162.0							
211	SA	0.36	0.43	0.49	0.57						
212	SE	170.0	171.0	172.0	173.0						
213	SQ	0	3.2	6.4	9.6	12.8	16.0	19.2	22.4	25.6	28.8
214	SQ	32.0									
215	SE	170.0	170.17	170.27	170.35	170.42	170.49	170.56	170.62	170.67	170.73
216	SE	170.8									
	*										
	*										
217	KK	3PD1&3									
218	KO	5									
219	HC	3	0								
	*										
	*										
220	KK	POND2									
221	KO	5									
222	RS	1	ELEV	158.0							
223	SA	2.08	2.23	2.38	2.54						
224	SE	166.0	167.0	168.0	169.0						
225	SQ	0	26.9	53.8	80.7	107.6	134.5	161.4	188.3	215.2	242.1
226	SQ	269.0									
227	SE	166.0	166.50	166.79	167.03	167.25	167.45	167.63	167.81	167.98	168.14
228	SE	168.3									
	*										
	*										
	*										
229	KK	PONDA									
230	KO	5									
	*										
	*	ASSUMED OUTLET	10	WEIR AT ELEV.	162.5						
	*										
231	RS	1	ELEV	162.5							
232	SA	1.30	1.30								
233	SE	162.5	170.0								
234	SQ	0	35	70	105	140	175	210	245	280	315
235	SQ	350.0									
236	SE	162.5	163.63	164.30	164.86	165.36	165.81	166.24	166.65	167.03	167.40
237	SE	167.8									
	*										
	*	10 ACRES NORTH OF PROPOSED DEVELOPMENT									
	*										
238	KK	NORTH									
239	KO	5									
240	BA	0.0156									
241	PB	1.00									
242	PC	0.000	0.003	0.006	0.008	0.011	0.014	0.017	0.019	0.022	0.025
243	PC	0.029	0.032	0.035	0.038	0.042	0.045	0.048	0.052	0.056	0.060
244	PC	0.064	0.068	0.072	0.076	0.080	0.085	0.090	0.095	0.100	0.105



New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

HEC-1 INPUT

PAGE 8

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
276	KK PONDS
277	KO 5
	* * ASSUMED OUTLET 10 WEIR AT ELEV. 159.0 *
278	RS 1 ELEV 159.0
279	SA 5.10 5.10
280	SE 159.0 170.0
281	SQ 0 35 70 105 140 175 210 245 280 315
282	SQ 350.0
283	SE 159.0 160.13 160.80 161.36 161.86 162.31 162.74 163.15 163.53 163.90
284	SE 164.3
	* * *
285	ZZ

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE NO.	(V) ROUTING (.) CONNECTOR	(--->) DIVERSION OR PUMP FLOW (<---) RETURN OF DIVERTED OR PUMPED FLOW
8	BSN5	
	V	
	V	
24	POND7	
	.	
33	.	BSN4
	.	.
49	PD7&4.....	
	V	
	V	
52	POND6	
	.	
61	.	BSN7
	.	.
77	7PD6.....	
	V	
	V	
80	POND5	
	.	
89	.	BSN6
	.	V
	.	V
105	.	RTE6
	.	.
108	.	OFFST
	.	.
124	.	.
	.	BSN8
	.	.
140	608P5.....	
	V	
	V	
143	POND4	
	.	
150	.	BSN10
	.	.
166	10PD4.....	
	V	
	V	
169	POND3	
	.	
176	.	BSN3
	.	.
192	.	BSN2
	.	V
	.	V
208	.	POND1
	.	.
217	3PD1&3.....	
	V	
	V	
220	POND2	
	V	
	V	
229	PONDA	
	.	
238	.	NORTH
	.	.
254	OFFSTE.....	

257 . . . . . DEV-1  
273 29TH.....  
V  
V  
276 PONDB

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

FLOOD HYDROGRAPH PACKAGE (HEC-1)
FEBRUARY 1981
REVISED 02 AUG 88
RUN DATE 04/10/2006 TIME 15:29:00

U.S. ARMY CORPS OF ENGINEERS
THE HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 551-1748

MODIFIED FONTANA DRAINAGE PLAN (40-AC NEW MARKET OFFICE SPACE TRACT ADDED)
DEVELOPED CONDITIONS
BY BLB DATE 03-13-04, MODIFIED BY PDF 4/10/06

6 IO OUTPUT CONTROL VARIABLES
IPRNT 0 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IT HYDROGRAPH TIME DATA
NMNIN 15 MINUTES IN COMPUTATION INTERVAL
IDATE 1JAN 4 STARTING DATE
ITIME 1200 STARTING TIME
NQ 129 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 2JAN 4 ENDING DATE
NDTIME 2000 ENDING TIME
ICENT 19 CENTURY MARK
COMPUTATION INTERVAL .25 HOURS
TOTAL TIME BASE 32.00 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
NPLAN 1 NUMBER OF PLANS
JR MULTI-RATIO OPTION
RATIOS OF PRECIPITATION
7.80

\*\*\*\*\*

8 KK BSN5

9 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 5 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\*\*\*

24 KK POND7

25 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\* \*\*

\*\*\*\*\*  
\* \*  
33 KK \* BSN4 \*  
\* \*  
\*\*\*\*\*

34 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\* \*\*

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\* \*  
49 KK \* PD7&4 \*  
\* \*  
\*\*\*\*\*

50 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
52 KK \* POND6 \*  
\* \*  
\*\*\*\*\*

53 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
61 KK \* BSN7 \*  
\* \*  
\*\*\*\*\*

62 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
77 KK \* 7PD6 \*  
\* \*  
\*\*\*\*\*

78 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPLLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
80 KK \* POND5 \*  
\* \*  
\*\*\*\*\*

81 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\*\*\*\*\*  
\* \*  
89 KK \* BSN5 \*  
\* \*  
\*\*\*\*\*

90 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
105 KK \* RTE6 \*  
\* \*  
\*\*\*\*\*

106 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\*

\*\*\*\*\*  
\* \*  
108 KK \* OFFST \*  
\* \*  
\*\*\*\*\*

109 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
124 KK \* BSN8 \*  
\* \*  
\*\*\*\*\*

125 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\* \*\*

\*\*\*\*\*  
\* \*  
80 KK \* POND5 \*  
\* \*  
\*\*\*\*\*

81 KD OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\* \*\*

\*\*\*\*\*  
\* \*  
89 KK \* BSN6 \*  
\* \*  
\*\*\*\*\*

90 KD OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\*~

\*\*\*\*\*  
\* \*  
105 KK \* RTE6 \*  
\* \*  
\*\*\*\*\*

106 KD OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\*~

\*\*\*\*\*  
\* \*  
108 KK \* OFFST \*  
\* \*  
\*\*\*\*\*

109 KD OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\*~

\*\*\*\*\*  
\* \*  
124 KK \* BSN8 \*  
\* \*  
\*\*\*\*\*

125 KD OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
140 KK \* 608P5 \*  
\* \*  
\*\*\*\*\*

141 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
143 KK \* POND4 \*  
\* \*  
\*\*\*\*\*

144 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
150 KK \* BSN10 \*  
\* \*  
\*\*\*\*\*

151 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
166 KK \* 10PDA \*  
\* \*  
\*\*\*\*\*

167 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
169 KK \* POND3 \*  
\* \*  
\*\*\*\*\*

170 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
176 KK \* BSN3 \*  
\* \*  
\*\*\*\*\*

177 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
192 KK \* BSN2 \*  
\* \*  
\*\*\*\*\*

193 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
208 KK \* POND1 \*  
\* \*  
\*\*\*\*\*

209 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
217 KK \* 3PD1&3 \*  
\* \*  
\*\*\*\*\*

218 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPL0T 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
220 KK \* POND2 \*  
\* \*  
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221 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
229 KK \* PONDA \*  
\* \*  
\*\*\*\*\*

230 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
238 KK \* NORTH \*  
\* \*  
\*\*\*\*\*

239 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
254 KK \* OFFSTE \*  
\* \*  
\*\*\*\*\*

255 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
257 KK \* DEV-1 \*  
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258 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 5 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

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\* \*  
273 KK \* 29TH \*  
\* \*  
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274 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL

IPL0T            5 PLOT CONTROL  
QSCAL           0. HYDROGRAPH PLOT SCALE

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\*            \*  
276 KK    \*    POND8   \*  
\*            \*  
\*\*\*\*\*

277 RD            OUTPUT CONTROL VARIABLES  
                  IPRNT            5 PRINT CONTROL  
                  IPL0T            5 PLOT CONTROL  
                  QSCAL            0. HYDROGRAPH PLOT SCALE

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO	1
					7.80
HYDROGRAPH AT					
+	BSN5	.02	1	FLOW	32.
				TIME	12.50
ROUTED TO					
+	POND7	.02	1	FLOW	12.
				TIME	13.50
				** PEAK STAGES IN FEET **	
			1	STAGE	171.83
				TIME	13.50
HYDROGRAPH AT					
+	BSN4	.02	1	FLOW	22.
				TIME	12.75
2 COMBINED AT					
+	PD7&4	.04	1	FLOW	31.
				TIME	13.00
ROUTED TO					
+	POND6	.04	1	FLOW	10.
				TIME	15.50
				** PEAK STAGES IN FEET **	
			1	STAGE	172.05
				TIME	15.50
HYDROGRAPH AT					
+	BSN7	.05	1	FLOW	61.
				TIME	12.75
2 COMBINED AT					
+	7PD6	.10	1	FLOW	64.
				TIME	12.75
ROUTED TO					
+	POND5	.10	1	FLOW	35.
				TIME	13.75
				** PEAK STAGES IN FEET **	
			1	STAGE	168.73
				TIME	13.75
HYDROGRAPH AT					
+	BSN6	.01	1	FLOW	12.
				TIME	12.50
ROUTED TO					
+	RTE5	.01	1	FLOW	12.
				TIME	13.25
HYDROGRAPH AT					
+	OFFST	.36	1	FLOW	273.
				TIME	13.50
HYDROGRAPH AT					
+	BSN8	.03	1	FLOW	40.
				TIME	12.25
4 COMBINED AT					
+	608P5	.49	1	FLOW	326.
				TIME	13.50
ROUTED TO					
+	POND4	.49	1	FLOW	232.
				TIME	14.50
				** PEAK STAGES IN FEET **	

New Market Sq. - 40-Ac. Tract - Proposed Office Park Develop. - Proposed Conditions

			1	STAGE	168.71
				TIME	14.50
HYDROGRAPH AT					
+	BSN10	.02	1	FLOW	27.
				TIME	12.50
2 COMBINED AT					
+	10PDA	.51	1	FLOW	236.
				TIME	14.50
ROUTED TO					
+	POND3	.51	1	FLOW	224.
				TIME	15.50
				** PEAK STAGES IN FEET **	
			1	STAGE	168.52
				TIME	15.50
HYDROGRAPH AT					
+	BSN3	.02	1	FLOW	33.
				TIME	12.50
HYDROGRAPH AT					
+	BSN2	.03	1	FLOW	32.
				TIME	12.50
ROUTED TO					
+	POND1	.03	1	FLOW	31.
				TIME	12.75
				** PEAK STAGES IN FEET **	
			1	STAGE	170.78
				TIME	12.75
3 COMBINED AT					
+	3PDI&3	.56	1	FLOW	270.
				TIME	12.50
ROUTED TO					
+	POND2	.56	1	FLOW	267.
				TIME	12.75
				** PEAK STAGES IN FEET **	
			1	STAGE	168.29
				TIME	12.75
ROUTED TO					
+	PONDA	.56	1	FLOW	264.
				TIME	13.00
				** PEAK STAGES IN FEET **	
			1	STAGE	166.86
				TIME	13.00
HYDROGRAPH AT					
+	NORTH	.02	1	FLOW	27.
				TIME	12.25
2 COMBINED AT					
+	OFFSTE	.58	1	FLOW	274.
				TIME	13.00
HYDROGRAPH AT					
+	DEV-1	.06	1	FLOW	184.
				TIME	12.00
2 COMBINED AT					
+	29TH	.64	1	FLOW	411.
				TIME	12.00
ROUTED TO					
+	PONDB	.64	1	FLOW	321.
				TIME	12.50
				** PEAK STAGES IN FEET **	
			1	STAGE	163.97
				TIME	12.50

\*\*\* NORMAL END OF HEC-1 \*\*\*

## DESIGN AIDS

KS-2-5

County	Expected 24-hour Storm Rainfall in Inches						Normal Annual Precipitation Inches
	Storm Frequency in Years						
	100	50	25	10	5	2	
Pawnee	6.6	6.0	5.2	4.5	3.7	2.8	23.3
Phillips	6.0	5.5	4.8	4.1	3.4	2.5	23.6
Pottawatomie	7.5	6.6	5.9	5.1	4.3	3.4	33.6
Pratt	7.2	6.4	5.6	4.8	4.1	3.0	24.6
Rawlins	5.5	5.0	4.3	3.6	3.1	2.3	21.0
Reno	7.4	6.6	5.8	5.0	4.2	3.2	27.7
Republic	6.8	6.0	5.4	4.6	3.9	2.9	28.6
Rice	7.3	6.4	5.6	4.8	4.1	3.0	26.6
Riley	7.4	6.5	5.8	5.1	4.3	3.3	33.5
Rooks	6.1	5.7	4.9	4.1	3.4	2.5	23.9
Rush	6.5	5.9	5.0	4.3	3.6	2.7	23.3
Russell	6.7	5.9	5.2	4.4	3.7	2.8	26.8
Saline	7.3	6.4	5.7	4.9	4.1	3.1	28.4
Scott	5.7	5.3	4.5	3.8	3.2	2.4	20.2
Sedgwick	7.8	7.0	6.1	5.3	4.5	3.5	30.6
Seward	6.0	5.7	4.8	4.2	3.5	2.6	19.8
Shawnee	7.8	6.8	6.1	5.3	4.5	3.5	34.7
Sheridan	5.7	5.3	4.5	3.8	3.2	2.4	21.3
Sherman	5.3	4.8	4.2	3.5	3.0	2.2	16.7
Smith	6.3	5.7	5.0	4.2	3.5	2.6	24.4
Stafford	7.1	6.2	5.5	4.7	4.0	2.9	25.1
Stanton	5.6	5.2	4.5	3.8	3.2	2.4	15.8
Stevens	5.9	5.5	4.7	4.1	3.4	2.5	19.7
Sumner	8.0	7.1	6.2	5.4	4.6	3.6	34.0

$$x\text{-slope} = \frac{3}{8} \frac{1}{4} = 0.03125\%$$

$$z = \frac{1}{x\text{-slope}} = \frac{1}{0.03125} = 32$$

$$n = 0.016$$

$$\frac{z}{n} = \frac{32}{0.016} = 2000$$

always

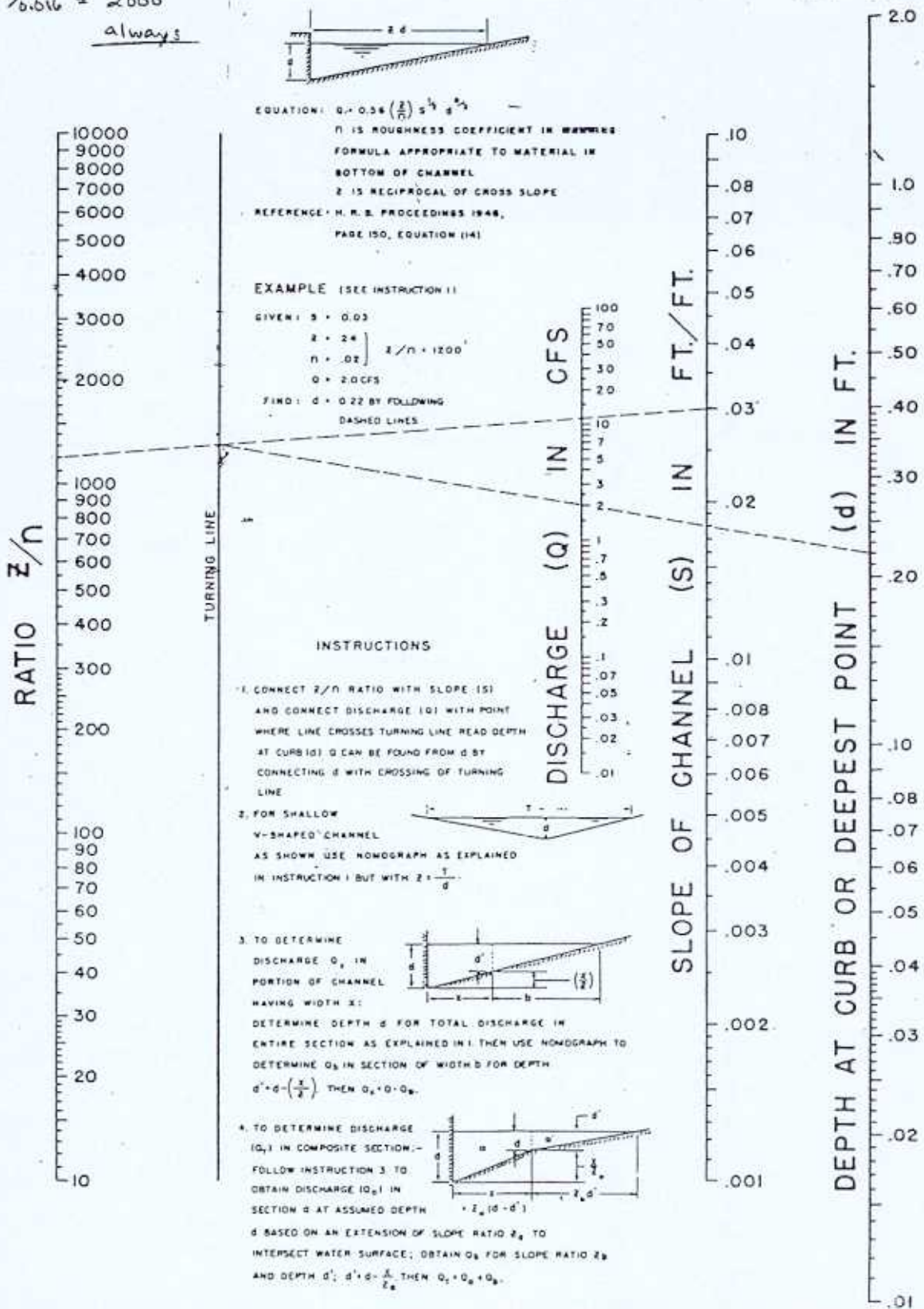


EQUATION:  $Q = 0.56 \left(\frac{z}{n}\right)^{5/3} d^{8/3}$   
 $n$  IS ROUGHNESS COEFFICIENT IN MANNING'S  
 FORMULA APPROPRIATE TO MATERIAL IN  
 BOTTOM OF CHANNEL  
 $z$  IS RECIPROCAL OF CROSS SLOPE  
 REFERENCE: H. R. S. PROCEEDINGS 1948,  
 PAGE 150, EQUATION (14)

EXAMPLE (SEE INSTRUCTION 1)

GIVEN:  $z = 0.03$   
 $z = 24$   
 $n = .02$  }  $z/n = 1200$   
 $Q = 2.0 \text{ CFS}$

FIND:  $d = 0.22$  BY FOLLOWING  
 DASHED LINES



#### INSTRUCTIONS

1. CONNECT  $z/n$  RATIO WITH SLOPE (S) AND CONNECT DISCHARGE (Q) WITH POINT WHERE LINE CROSSES TURNING LINE. READ DEPTH AT CURB (d).  $d$  CAN BE FOUND FROM  $d$  BY CONNECTING  $d$  WITH CROSSING OF TURNING LINE.

2. FOR SHALLOW V-SHAPED CHANNEL AS SHOWN USE NOMOGRAPH AS EXPLAINED IN INSTRUCTION 1 BUT WITH  $z = \frac{1}{d}$ .

3. TO DETERMINE DISCHARGE  $Q_1$  IN PORTION OF CHANNEL HAVING WIDTH  $x$ : DETERMINE DEPTH  $d$  FOR TOTAL DISCHARGE IN ENTIRE SECTION AS EXPLAINED IN 1. THEN USE NOMOGRAPH TO DETERMINE  $Q_2$  IN SECTION OF WIDTH  $d$  FOR DEPTH  $d' = d \left(\frac{x}{d}\right)$ . THEN  $Q_1 = d \cdot Q_2$ .

4. TO DETERMINE DISCHARGE ( $Q_1$ ) IN COMPOSITE SECTION.— FOLLOW INSTRUCTION 3 TO OBTAIN DISCHARGE ( $Q_2$ ) IN SECTION  $d$  AT ASSUMED DEPTH  $d$  BASED ON AN EXTENSION OF SLOPE RATIO  $z_1$  TO INTERSECT WATER SURFACE; OBTAIN  $Q_3$  FOR SLOPE RATIO  $z_2$  AND DEPTH  $d'$ :  $d' = d \cdot \frac{z_1}{z_2}$ . THEN  $Q_1 = Q_2 + Q_3$ .

- ATTACHMENT A  
DRAINAGE CRITERIA MANUAL

RAINFALL INTENSITY TABLE FOR SEDGWICK COUNTY, KANSAS

The following tabulation contains rainfall intensity in inches per hour as derived from ESSA Weather Bureau Technical Paper 40 Modified to NWS Hydro-35, 1977 During First Hour

$(\frac{1}{2})$ DURATION IN MINUTES	RETURN PERIODS OF						
	1-YR	2-YR	5-YR	10-YR	25-YR	50-YR	100-YR
5	$i = 4.18$	5.57	6.53	7.41	8.52	9.48	10.32
6	3.99	5.32	6.25	7.09	8.16	9.09	9.89
7	3.81	5.09	5.99	6.81	7.84	8.74	9.50
8	3.66	4.89	5.75	6.55	7.55	8.42	9.15
9	3.52	4.70	5.54	6.31	7.28	8.13	8.83
10	3.39	4.52	5.34	6.09	7.04	7.86	8.54
11	3.27	4.36	5.16	5.89	6.81	7.61	8.27
12	3.18	4.21	4.99	5.71	6.60	7.38	8.02
13	3.05	4.08	4.84	5.53	6.41	7.17	7.79
14	2.96	3.95	4.69	5.37	6.23	6.97	7.57
15	2.87	3.83	4.56	5.22	6.06	6.78	7.37
16	2.78	3.72	4.43	5.08	5.90	6.60	7.18
17	2.71	3.61	4.31	4.95	5.75	6.44	7.00
18	2.63	3.51	4.20	4.83	5.61	6.29	6.84
19	2.56	3.42	4.10	4.71	5.47	6.14	6.68
20	2.50	3.33	4.00	4.60	5.35	6.00	6.53
21	2.44	3.25	3.90	4.50	5.23	5.87	6.39
22	2.38	3.17	3.81	4.40	5.12	5.75	6.26
23	2.32	3.10	3.73	4.31	5.01	5.63	6.13
24	2.27	3.03	3.65	4.22	4.91	5.52	6.01
25	2.22	2.96	3.57	4.13	4.81	5.41	5.90
26	2.20	2.90	3.50	4.05	4.72	5.31	5.79
27	2.16	2.84	3.43	3.98	4.63	5.21	5.69
28	2.14	2.78	3.37	3.90	4.55	5.12	5.59
29	2.11	2.72	3.30	3.83	4.47	5.03	5.49
30	2.08	2.67	3.24	3.76	4.39	4.94	5.40
31	2.05	2.62	3.19	3.70	4.32	4.86	5.32
32	2.02	2.57	3.10	3.63	4.25	4.79	5.22
33	1.99	2.52	3.05	3.57	4.18	4.71	5.14
34	1.96	2.48	3.01	3.51	4.11	4.63	5.07
35	1.93	2.44	2.98	3.46	4.05	4.56	5.00
36	1.91	2.39	2.93	3.41	3.99	4.50	4.93
37	1.89	2.35	2.88	3.36	3.93	4.43	4.86
38	1.87	2.32	2.84	3.31	3.87	4.37	4.79
39	1.85	2.28	2.80	3.26	3.82	4.31	4.73
40	1.83	2.24	2.76	3.22	3.76	4.25	4.66
41	1.81	2.21	2.72	3.17	3.71	4.19	4.60
42	1.79	2.18	2.68	3.13	3.66	4.13	4.54
43	1.77	2.14	2.64	3.09	3.61	4.08	4.49
44	1.75	2.11	2.61	3.05	3.57	4.03	4.43
45	1.73	2.08	2.57	3.01	3.52	3.98	4.38

## ATTACHMENT A CONTINUED

Page 2

DURATION IN MINUTES	RETURN PERIODS OF						
	<u>1-YR</u>	<u>2-YR</u>	<u>.5-YR</u>	<u>10-YR</u>	<u>25-YR</u>	<u>50-YR</u>	<u>100-YR</u>
46	1.70	2.05	2.54	2.97	3.48	3.93	4.33
47	1.67	2.02	2.50	2.93	3.44	3.88	4.28
48	1.66	2.00	2.47	2.90	3.39	3.84	4.23
49	1.64	1.97	2.44	2.86	3.35	3.79	4.18
50	1.61	1.95	2.41	2.83	3.32	3.75	4.13
51	1.59	1.92	2.38	2.79	3.28	3.71	4.09
52	1.56	1.89	2.35	2.76	3.24	3.67	4.05
53	1.54	1.86	2.33	2.73	3.20	3.63	4.00
54	1.52	1.84	2.30	2.70	3.17	3.59	3.96
55	1.50	1.81	2.27	2.67	3.14	3.55	3.92
56	1.47	1.79	2.25	2.64	3.10	3.51	3.88
57	1.45	1.76	2.22	2.61	3.07	3.48	3.84
58	1.43	1.74	2.20	2.59	3.04	3.44	3.81
59	1.42	1.72	2.18	2.56	3.01	3.41	3.77
60	1.40	1.69	2.15	2.53	2.98	3.37	3.73
61	1.38	1.67	2.13	2.51	2.95	3.34	3.70
62	1.36	1.65	2.11	2.48	2.92	3.31	3.67
63	1.34	1.63	2.09	2.46	2.89	3.28	3.63
64	1.33	1.61	2.07	2.44	2.86	3.25	3.60
65	1.31	1.59	2.05	2.41	2.84	3.22	3.57
66	1.30	1.57	2.03	2.39	2.81	3.19	3.54
67	1.28	1.56	2.01	2.37	2.79	3.16	3.51
68	1.26	1.54	1.99	2.35	2.76	3.13	3.48
69	1.25	1.52	1.97	2.33	2.74	3.10	3.45
70	1.24	1.50	1.95	2.31	2.71	3.08	3.42
71	1.22	1.49	1.93	2.28	2.69	3.05	3.39
72	1.21	1.47	1.92	2.26	2.67	3.02	3.36
73	1.20	1.46	1.90	2.25	2.64	3.00	3.34
74	1.18	1.44	1.88	2.23	2.63	2.98	3.31
75	1.17	1.43	1.86	2.21	2.61	2.95	3.29
76	1.16	1.41	1.85	2.19	2.58	2.93	3.26
77	1.15	1.40	1.83	2.17	2.55	2.90	3.24
78	1.13	1.38	1.82	2.15	2.53	2.88	3.22
79	1.12	1.37	1.80	2.14	2.50	2.86	3.19
80	1.11	1.36	1.79	2.12	2.48	2.84	3.16
81	1.10	1.34	1.77	2.10	2.46	2.82	3.13
82	1.09	1.33	1.76	2.08	2.43	2.79	3.10
83	1.08	1.32	1.74	2.06	2.41	2.76	3.07
84	1.07	1.31	1.73	2.04	2.39	2.74	3.04
85	1.06	1.30	1.72	2.02	2.37	2.71	3.01
86	1.05	1.28	1.70	2.00	2.34	2.69	2.99
87	1.04	1.27	1.69	1.99	2.32	2.66	2.96
88	1.03	1.26	1.68	1.97	2.30	2.64	2.93
89	1.02	1.25	1.68	1.95	2.28	2.62	2.91
90	1.01	1.24	1.66	1.93	2.26	2.59	2.88

ATTACHMENT A CONTINUED  
Page 3

<u>DURATION IN MINUTES</u>	<u>RETURN PERIODS OF</u>						
	<u>1-YR</u>	<u>2-YR</u>	<u>5-YR</u>	<u>10-YR</u>	<u>25-YR</u>	<u>50-YR</u>	<u>100-YR</u>
91	1.00	1.23	1.65	1.92	2.24	2.57	2.86
92	1.00	1.22	1.63	1.90	2.22	2.55	2.83
93	0.99	1.21	1.62	1.89	2.20	2.53	2.81
94	0.98	1.20	1.61	1.87	2.19	2.51	2.79
95	0.97	1.19	1.59	1.85	2.17	2.49	2.76
96	0.96	1.18	1.58	1.84	2.15	2.46	2.74
97	0.96	1.17	1.57	1.82	2.13	2.44	2.72
98	0.95	1.16	1.56	1.81	2.12	2.42	2.70
99	0.94	1.15	1.54	1.80	2.10	2.41	2.67
100	0.93	1.14	1.53	1.78	2.08	2.39	2.65
101	0.93	1.13	1.52	1.77	2.07	2.39	2.65
102	0.92	1.13	1.51	1.75	2.05	2.35	2.61
103	0.91	1.12	1.50	1.74	2.04	2.33	2.59
104	0.90	1.11	1.49	1.73	2.02	2.31	2.57
105	0.90	1.10	1.47	1.72	2.01	2.30	2.55
106	0.89	1.09	1.46	1.70	1.99	2.28	2.54
107	0.88	1.09	1.45	1.69	1.98	2.26	2.52
108	0.88	1.08	1.44	1.68	1.96	2.25	2.50
109	0.87	1.07	1.43	1.67	1.95	2.23	2.48
110	0.87	1.06	1.42	1.65	1.93	2.21	2.46
111	0.86	1.06	1.41	1.64	1.92	2.20	2.45
112	0.85	1.05	1.40	1.63	1.91	2.18	2.43
113	0.85	1.04	1.39	1.62	1.89	2.17	2.41
114	0.84	1.03	1.38	1.61	1.88	2.15	2.40
115	0.84	1.03	1.37	1.60	1.87	2.14	2.38
116	0.83	1.02	1.36	1.59	1.86	2.12	2.36
117	0.82	1.01	1.36	1.58	1.84	2.11	2.35
118	0.82	1.01	1.35	1.57	1.83	2.09	2.33
119	0.81	1.00	1.34	1.56	1.82	2.08	2.32
120	0.81	0.99	1.33	1.55	1.81	2.07	2.30

<u>DURATION IN HOURS</u>	<u>RETURN PERIODS OF</u>						
	<u>1-YR</u>	<u>2-YR</u>	<u>5-YR</u>	<u>10-YR</u>	<u>25-YR</u>	<u>50-YR</u>	<u>100-YR</u>
2	0.81	0.99	1.33	1.55	1.81	2.07	2.30
3	0.59	0.72	0.97	1.13	1.32	1.51	1.68
4	0.47	0.58	0.78	0.91	1.06	1.21	1.35
5	0.40	0.49	0.66	0.77	0.89	1.02	1.14
6	0.35	0.42	0.57	0.67	0.78	0.89	0.99
8	0.28	0.34	0.46	0.53	0.62	0.71	0.79
10	0.23	0.29	0.39	0.45	0.52	0.60	0.67
12	0.20	0.25	0.33	0.39	0.45	0.52	0.58
18	0.15	0.18	0.24	0.28	0.33	0.38	0.42
24	0.12	0.15	0.20	0.23	0.27	0.31	0.34

ATTACHMENT B  
DRAINAGE CRITERIA MANUAL

INCREMENTAL INFILTRATION VALUES IN INCHES

Time Minutes**	SCS Hydrologic Soil Group			
	<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>
5	.33	.26	.19	.12
10	.25	.17	.09	.04
15	.18	.11	.05	.02
20	.13	.07	.03	.02
25	.10	.05	.03	.02
30	.08	.05	.03	.02
35	.08	.05	.03	.02
40	.08	.05	.03	.02
45	.08	.05	.03	.02
50	.08	.05	.03	.02
55	.08	.05	.03	.02
60	.08	.05	.03	.02
65	.08	.05	.03	.02
70	.08	.05	.03	.02
75	.08	.05	.03	.02
80	.08	.05	.03	.02
85	.08	.05	.03	.02
90	.08	.05	.03	.02
95	.08	.05	.03	.02
100	.08	.05	.03	.02
105	.08	.05	.03	.02
110	.08	.05	.03	.02
115	.08	.05	.03	.02
120	.08	.05	.03	.02

\*\*Time at end of the time increment

NOTE: Values for 125 minutes and additional 5 minute increments shall be the same as those shown for 120 minutes.

# ATTACHMENT C

## DRAINAGE CRITERIA MANUAL

### DEPRESSION STORAGE LOSSES

<u>Surface Type</u>	<u>Total Loss (Inches)</u>
<b>Impervious:</b>	
Paved Areas	0.1
Flat Roofs	0.1
Sloped Roofs	0.05
<b>Pervious:</b>	
Lawns and Grass	0.3
Wooded Areas and Open Fields	0.4

ATTACHMENT

DETERMINATION OF DIMENSIONLESS  
WATERSHED CONVEYANCE FACTOR ( $\emptyset$ )

$$\emptyset = \emptyset_1 + \emptyset_2$$

$\emptyset_1$	Classification
0.6	Extensive channel improvement and storm sewer system, closed conduit channel system
0.7	Moderate channel improvement and storm sewer system.
0.8	Some channel improvement and storm sewers, mainly cleaning and enlargement of existing channel.
0.9	Little channel improvement and storm sewers.
1.0	Natural channel conditions.
$\emptyset_2$	Classification
0.0	No channel vegetation.
0.1	Light channel vegetation.
0.2	Moderate channel vegetation.
0.3	Heavy channel vegetation.

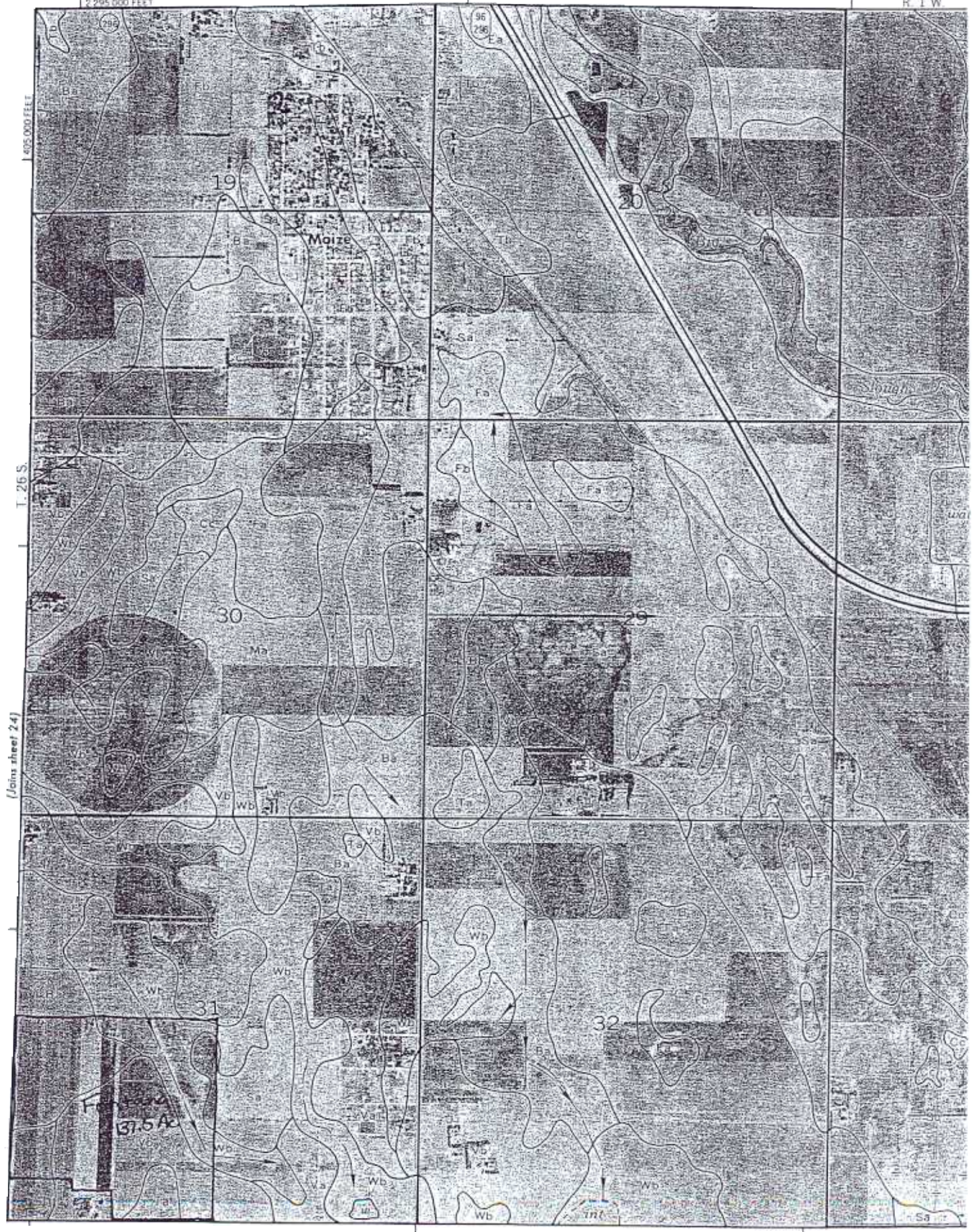
## EXHIBIT NO. 1

## SOIL LEGEND

<u>SYMBOL</u>	<u>HYDROLOGIC GROUP</u>	<u>NAME</u>
Aa	B	Albion-Shellabarger sandy loams, 1 to 4 percent slopes
Ab	B	Albion and Shellabarger sandy loams, 7 to 15 percent slopes
Ba	C	Blanket silt loam, 0 to 1 percent slopes
Bb	C	Blanket silt loam, 1 to 3 percent slopes
Ca	B	Canadian fine sandy loam
Cb	B	Canadian-Waldeck fine sandy loams
Cc	D	Carwile fine sandy loam
Cd	B	Clark-Ost clay loams, 1 to 4 percent slopes
Ce	C	Clime silty clay, 3 to 6 percent slopes
Ea	B	Elandco silt loam
Eb	B	Elandco silt loam, occasionally flooded
Ec	B	Elandco silt loam, frequently flooded
Fa	B	Farnum loam, 0 to 1 percent slopes
Fb	B	Farnum loam, 1 to 3 percent slopes
Fc	B	Farnum loam, sandy substratum, 0 to 1 percent slopes
Ga	D	Goessel silty clay, 0 to 1 percent slopes
Gb	D	Goessel silty clay, 1 to 2 percent slopes
Ia	D	Irwin silty clay loam, 1 to 3 percent slopes
Ib	D	Irwin silty clay loam, 3 to 6 percent slopes
Ic	D	Irwin silty clay loam, 2 to 6 percent slopes, eroded
La	C	Lesho loam
Lb	A	Lincoln soils
Ma	B	Milan loam, 1 to 3 percent slopes
Mb	B	Milan form, 3 to 6 percent slopes
Mc	B	Milan clay loam, 2 to 6 percent slopes, eroded
Na	B	Naron fine sandy loam
Oc	D	Owens clay loam, 1 to 3 percent slopes
Od	D	Owens-Rock outcrop complex, 3 to 10 percent slopes
Pa		Pits
Pb	D	Plevna fine sandy loam
Pc	A	Pratt loamy fine sand, undulating
Pd	A	Pratt-Tivoli complex, rolling
Ra	D	Renfrow silty clay loam, 1 to 3 percent slopes
Rb	D	Renfrow silty clay loam, 3 to 6 percent slopes
Rc	D	Renfrow-Owens clay loams, 1 to 4 percent slopes
Rd	D	Rosehill silty clay, 1 to 3 percent slopes
Sa	B	Shellabarger sandy loam, 1 to 3 percent slopes
Sb	B	Shellabarger sandy loam, 3 to 6 percent slopes
Sc	B	Shellabarger sandy loam, 3 to 6 percent slopes, eroded
Ta	D	Tabler silty clay loam
Tb	D	Tabler-Drummond complex
Ua	B	Urban land-Canadian complex
Ub	B	Urban land-Elandco complex
Uc	B	Urban land-Farnum complex, 0 to 3 percent slopes
Ud	D	Urban land-Irwin complex, 1 to 3 percent slopes
Ue	D	Urban land-Tabler complex
Va	B	Vanoss silt loam, 0 to 1 percent slopes
Vb	B	Vanoss silt loam, 1 to 3 percent slopes
Vc	B	Vanoss silt loam, 3 to 6 percent slopes
Vd	B	Vanoss silt loam, 3 to 6 percent slopes, eroded
Ve	D	Vernon sandy loam, 1 to 3 percent slopes
Vf	D	Vernon sandy loam, 3 to 6 percent slopes
Wa	C	Waldeck sandy loam
Wb	D	Waurika silt loam

1:2,295,000 FEET

R. 1 W



(Joins sheet 24)

405,000 FEET

T. 26 S.

F 4000  
37.5 AC

Moize

Slough

19

20

30

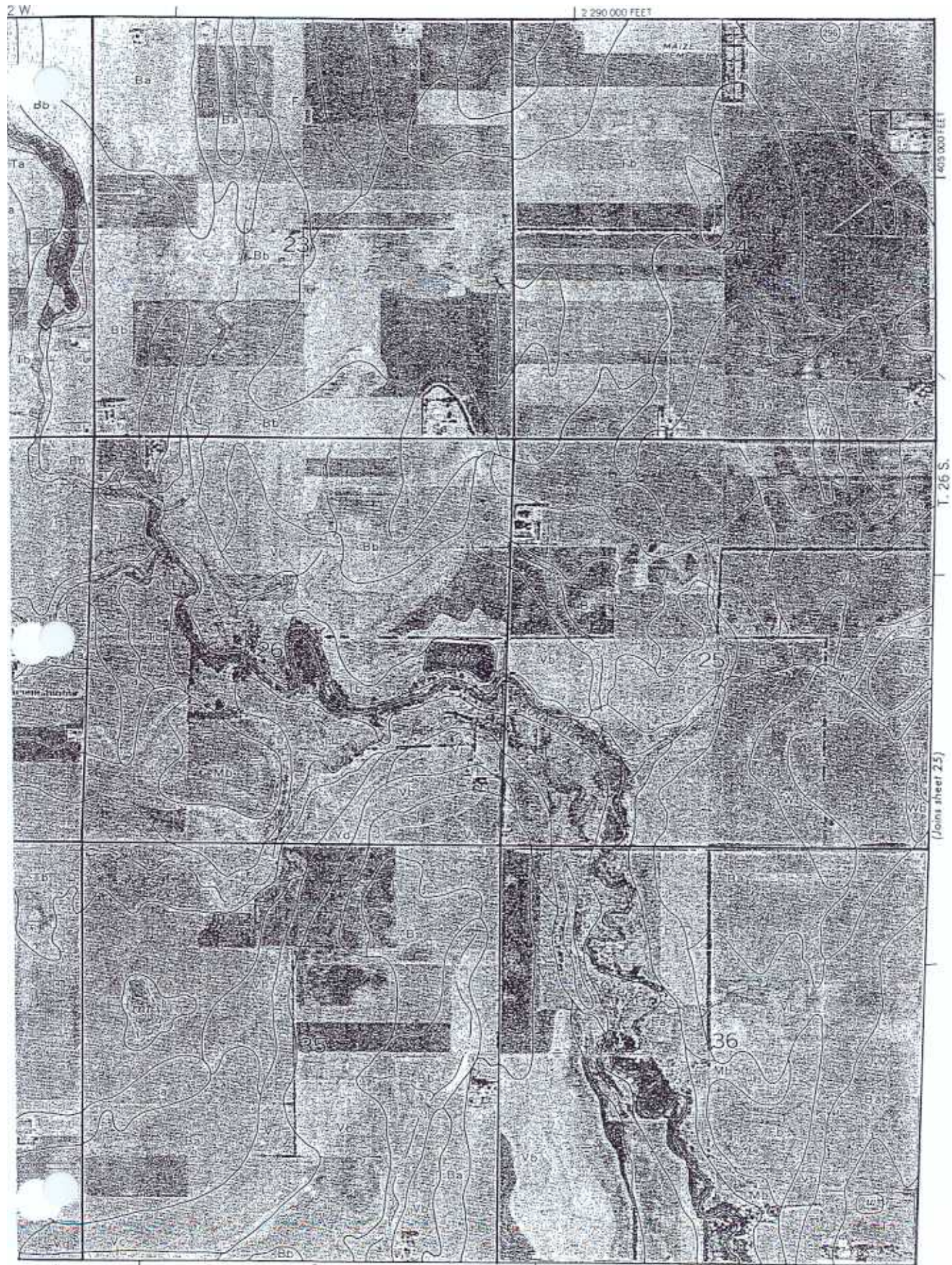
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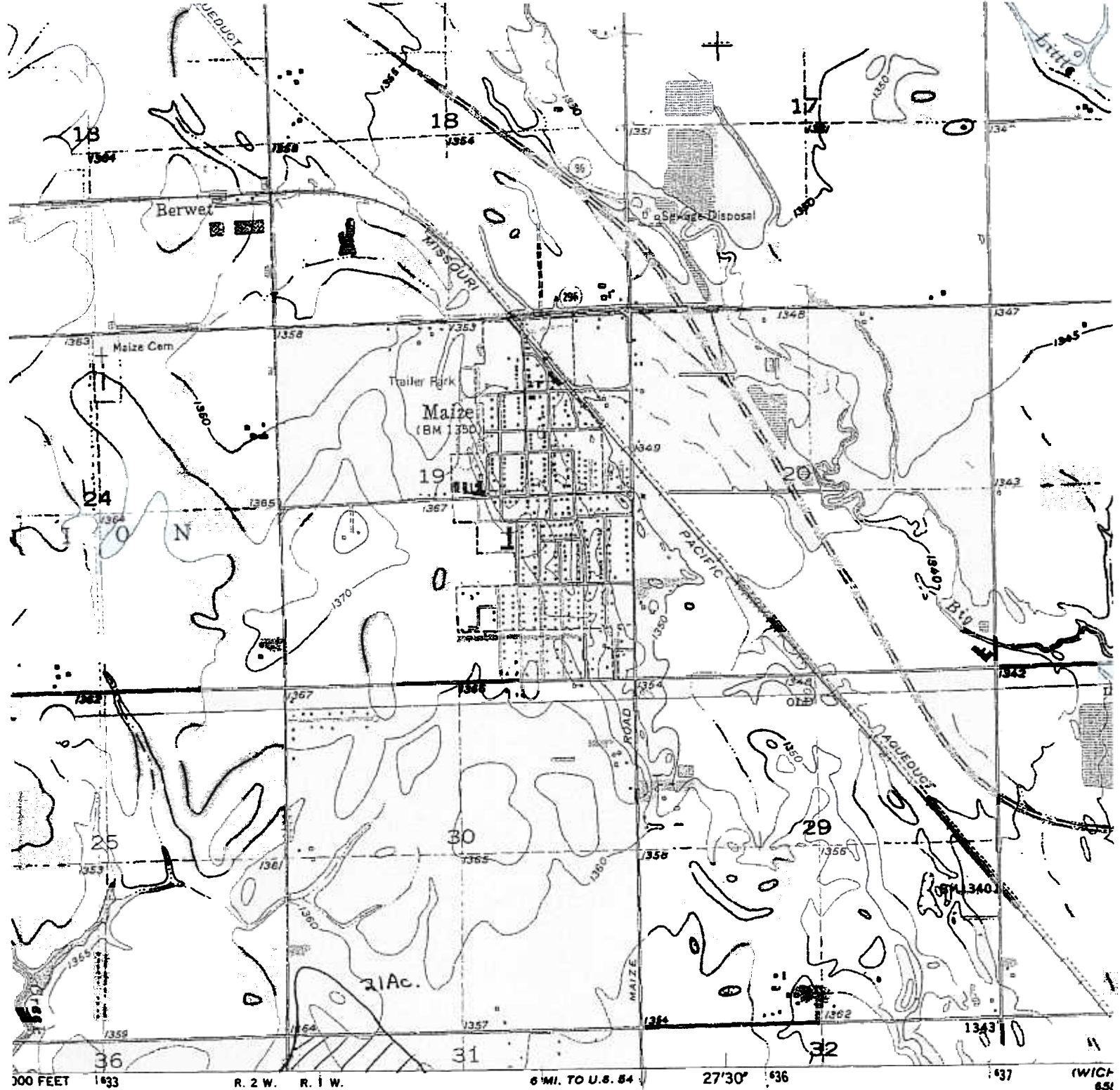
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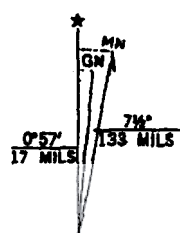


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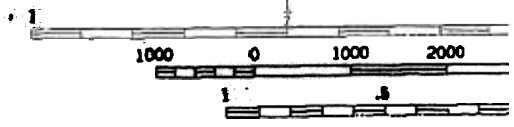
Image in part compiled from aerial photographs  
 55. Topography by planetable surveys 1939

ation. 1927 North American datum  
 d based on Kansas coordinate system, south zone  
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as area in which only landmark buildings are shown  
 l lines indicate selected fence and field lines where  
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UTM GRID AND 1982 MAGNETIC NORTH  
 DECLINATION AT CENTER OF SHEET

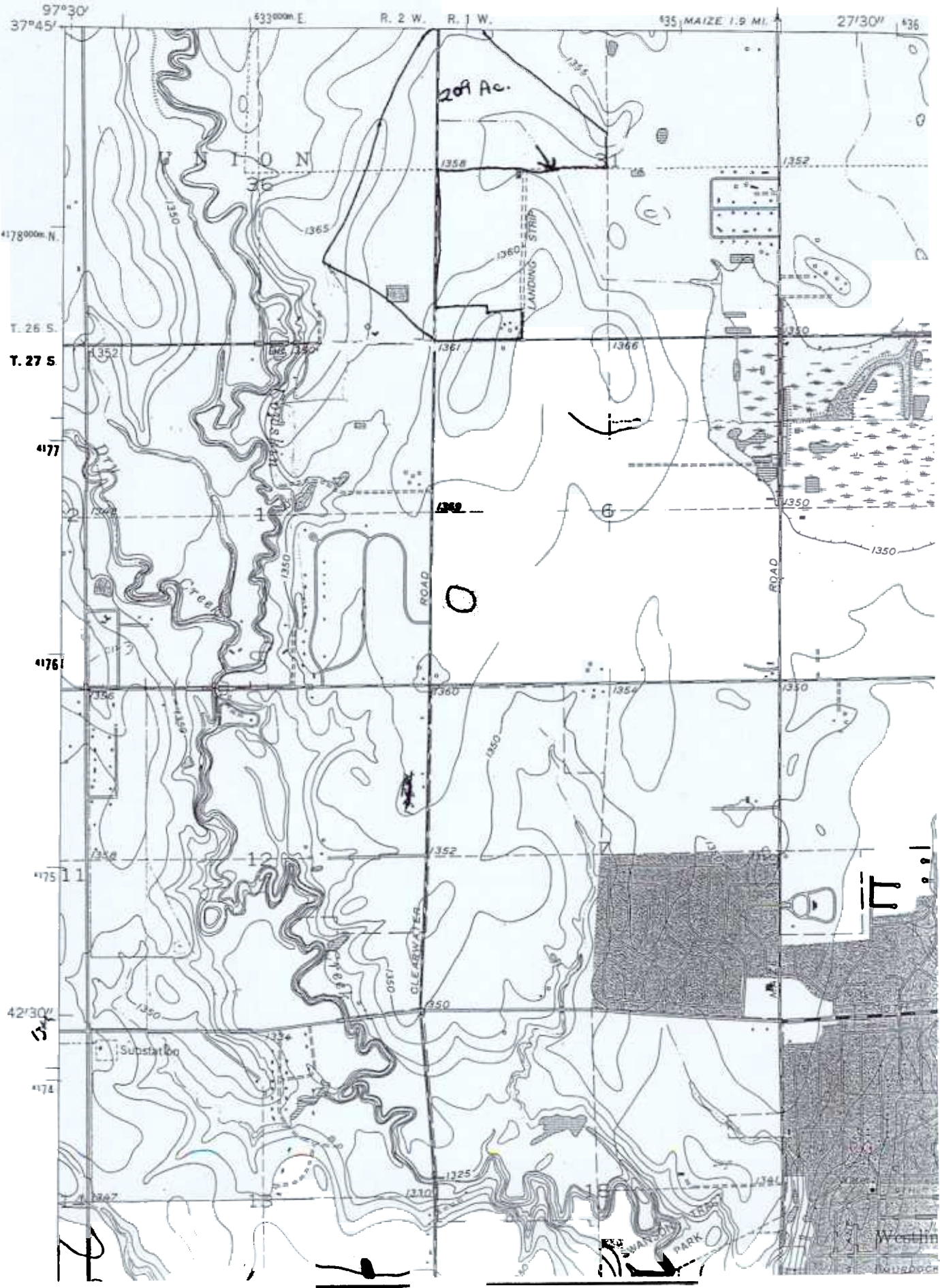


CONTOUR 1  
 NATIONAL GEODETTIC

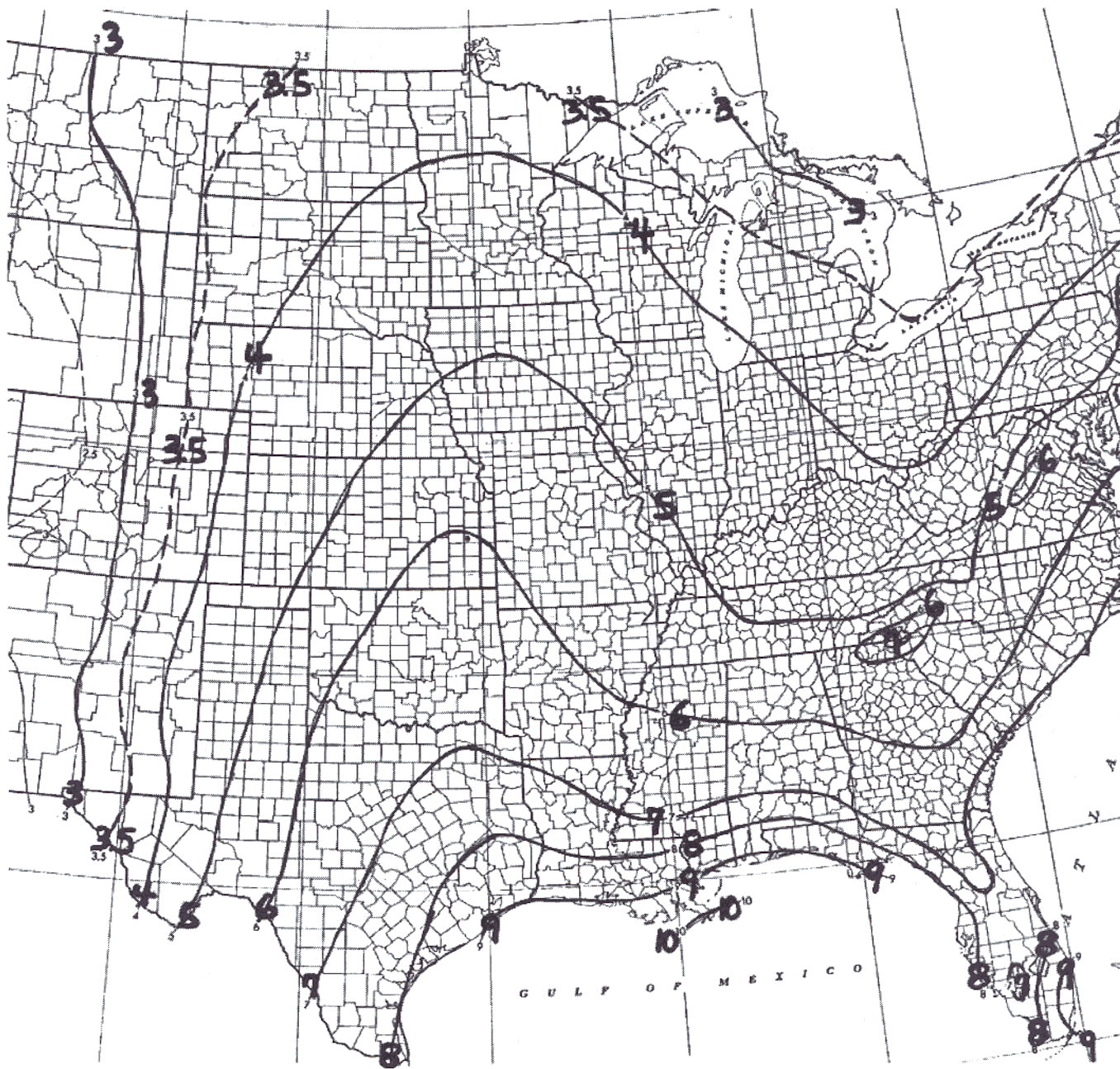
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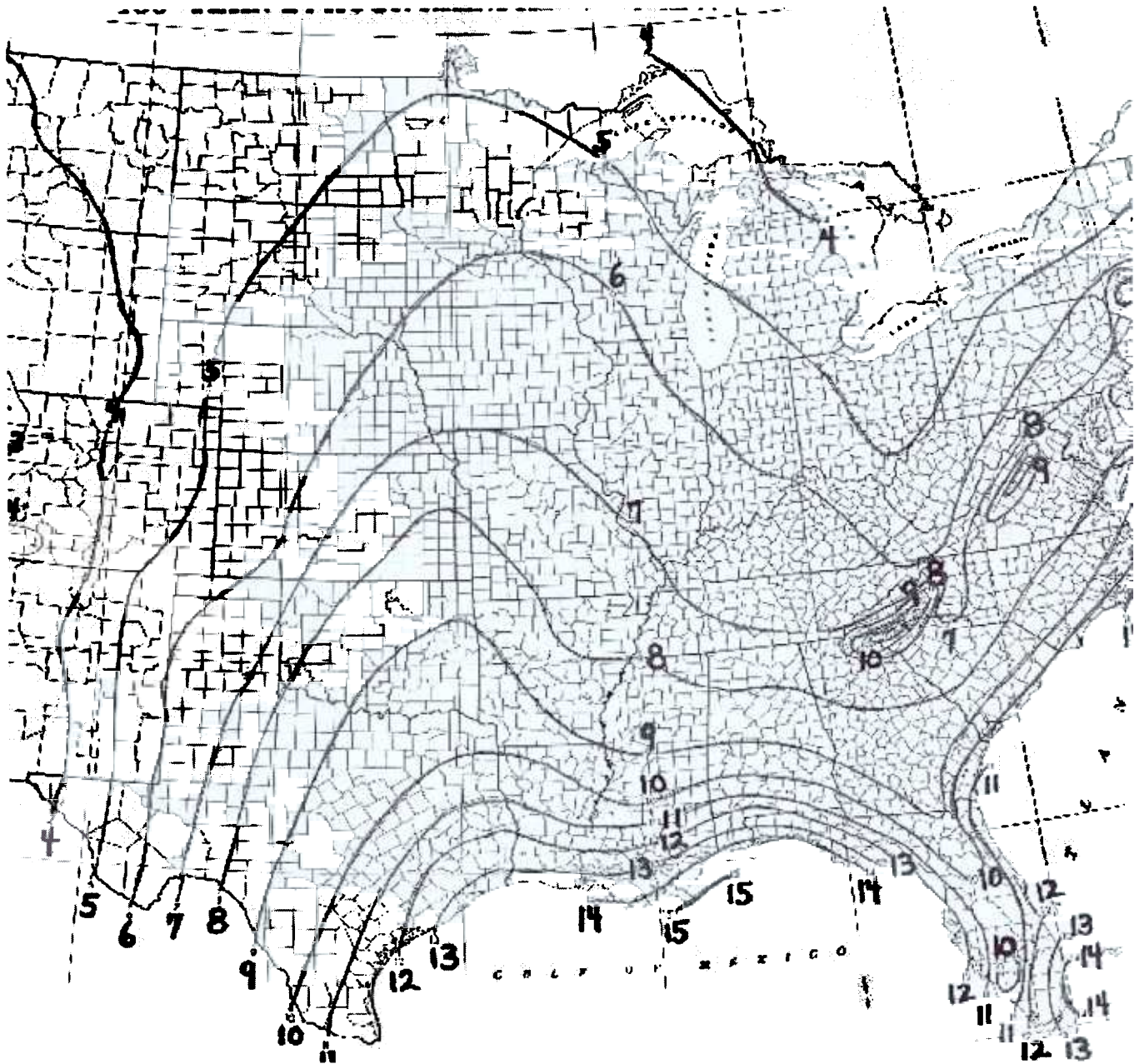
UNITED STATES  
DEPARTMENT OF THE INTERIOR  
GEOLOGICAL SURVEY



# 100 YEAR 6 HOUR RAINFALL (INCHES)



# 100 YEAR 24 HOUR RAINFALL (INCHES)



## ATTACHMENT D

## DRAINAGE CRITERIA

RECOMMENDED RUNOFF COEFFICIENTS FOR RATIONAL METHOD  
AND PERCENT IMPERVIOUS FOR UNIT HYDROGRAPH METHOD

Land Use or Surface Characteristics	Percent Impervious	Frequency			
		2	5	10	100
<b>1 Business:</b>					
Downtown Areas	95	0.84	0.85	0.87	0.91
Neighborhood Areas	70	0.68	0.69	0.73	0.80
<b>2. Residential:</b>					
<u>Single Family (Soil Group D)</u>					
1/8 Acre	50	0.57	0.61	0.66	0.79
1/4 Acre	38	0.50	0.54	0.62	0.76
1/3 Acre	30	0.46	0.50	0.59	0.73
1/2 Acre	25	0.42	0.48	0.56	0.72
3/4 Acre	22	0.42	0.46	0.55	0.71
1 Acre	20	0.41	0.45	0.54	0.71
<u>Multi-Family (Soil Group D)</u>					
Multi-Unit (detached)	60	0.62	0.66	0.72	0.82
Multi-Unit (attached)	65	0.64	0.68	0.73	0.83
Apartments	75	0.70	0.73	0.79	0.86
<u>Single Family (Soil Group C)</u>					
1/8 Acre	50	0.55	0.58	0.64	0.73
1/4 Acre	38	0.48	0.51	0.57	0.68
1/3 Acre	30	0.43	0.46	0.53	0.65
1/2 Acre	25	0.40	0.43	0.50	0.63
3/4 Acre	22	0.39	0.42	0.49	0.62
1 Acre	20	0.37	0.40	0.48	0.61
<u>Multi-Family (Soil Group C)</u>					
Multi-Unit (detached)	60	0.60	0.63	0.69	0.77
Multi-Unit (attached)	65	0.63	0.66	0.71	0.79
Apartments	75	0.68	0.72	0.77	0.83
<u>Single-Family (Soil Group B)</u>					
1/8 Acre	50	0.52	0.54	0.59	0.67
1/4 Acre	38	0.44	0.46	0.52	0.61
1/3 Acre	30	0.39	0.41	0.47	0.57
1/2 Acre	25	0.36	0.38	0.44	0.54
3/4 Acre	22	0.34	0.36	0.42	0.52
1 Acre	20	0.33	0.35	0.40	0.51
<u>Multi-Family (Soil Group B)</u>					
Multi-Unit (detached)	60	0.58	0.60	0.65	0.72
Multi-Unit (attached)	65	0.61	0.64	0.68	0.75
Apartments	75	0.67	0.70	0.74	0.80

Land Use or Area Characteristics	Percent Impervious	Frequency			
		2	5	10	100
<u>Single Family (Soil Group A)</u>					
1/8 Acre	50	0.47	0.50	0.54	0.60
1/4 Acre	38	0.39	0.41	0.45	0.52
1/3 Acre	30	0.33	0.35	0.39	0.47
1/2 Acre	25	0.30	0.31	0.35	0.44
3/4 Acre	22	0.28	0.29	0.33	0.42
1 Acre	20	0.26	0.28	0.32	0.40
<u>Multi-Family (Soil Group A)</u>					
Multi-Unit (detached)	60	0.55	0.57	0.61	0.67
Multi-Unit (attached)	65	0.58	0.60	0.64	0.70
Apartments	75	0.65	0.68	0.72	0.77
3. Industrial:					
Light Areas	70	0.68	0.69	0.73	0.80
Heavy Areas	80	0.74	0.76	0.79	0.84
4. Playgrounds:	15	0.33	0.35	0.42	0.55
5. Schools:	40	0.49	0.51	0.56	0.66
6. Railroad Yard Areas:	30	0.43	0.45	0.50	0.62
Undeveloped Urban Areas: Offsite Flow Analysis (when land use not defined)	45	0.52	0.54	0.59	0.68
8. Streets:					
Paved	99	0.87	0.88	0.90	0.93
Gravel	00	0.24	0.26	0.33	0.48
9. Drive, Parking Lots and Walks:	96	0.87	0.87	0.88	0.89
10. Roofs:	90	0.80	0.85	0.90	0.93
11. Urban Lawn Areas (See Note No. 1 below):					
<u>Soil Group A</u>					
Slope less than 1%	00	0.08	0.09	0.13	0.23
Slope 1% to 4%	00	0.12	0.13	0.17	0.27
Slope more than 4%	00	0.16	0.17	0.21	0.31
<u>Soil Group B</u>					
Slope less than 1%	00	0.16	0.18	0.24	0.37
Slope 1% to 4%	00	0.20	0.22	0.28	0.41
Slope more than 4%	00	0.24	0.26	0.32	0.45
<u>Soil Group C</u>					
Slope less than 1%	00	0.24	0.27	0.35	0.51
Slope 1% to 4%	00	0.26	0.29	0.37	0.53
Slope more than 4%	00	0.28	0.31	0.39	0.55

<u>Land Use or Space Characteristics</u>	<u>Percent Impervious</u>	<u>Frequency</u>			
		<u>2</u>	<u>5</u>	<u>10</u>	<u>100</u>
<u>Soil Group D</u>					
Slope less than 1%	00	0.28	0.33	0.43	0.63
Slope 1% to 4%	00	0.30	0.35	0.45	0.65
Slope more than 4%	00	0.32	0.37	0.47	0.67

Note No. 1: Coefficients shown in the above table are for pervious open space areas with thick turf which includes pervious areas in parks and cemeteries. Coefficients shown above must be increased 0.02 for use with agricultural pasture areas. Coefficients shown above must be reduced by 0.04 for use with agricultural cultivated areas. Group A soils are well-drained, coarse textured sands with high infiltration rates. Group B soils are moderately well-drained, moderately coarse textured soils with moderate infiltration rates. Group C soils are moderately poor-drained, moderately fine textured soils with slow infiltration rates. Group D soils are poor-drained, fine textured soils with very slow infiltration rates.

GENERAL NOTE: These Rational Formula Coefficients may not be valid for basins 320 acres or larger.

ATTACHMENT E

DRAINAGE CRITERIA

AVERAGE OVERLAND FLOW VELOCITY FOR USE WITH URBANIZED AREAS

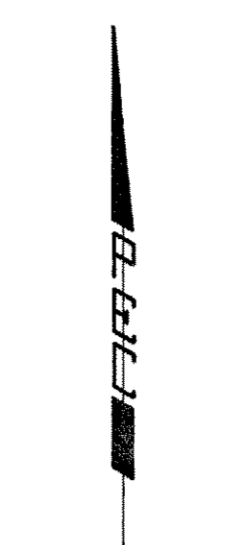
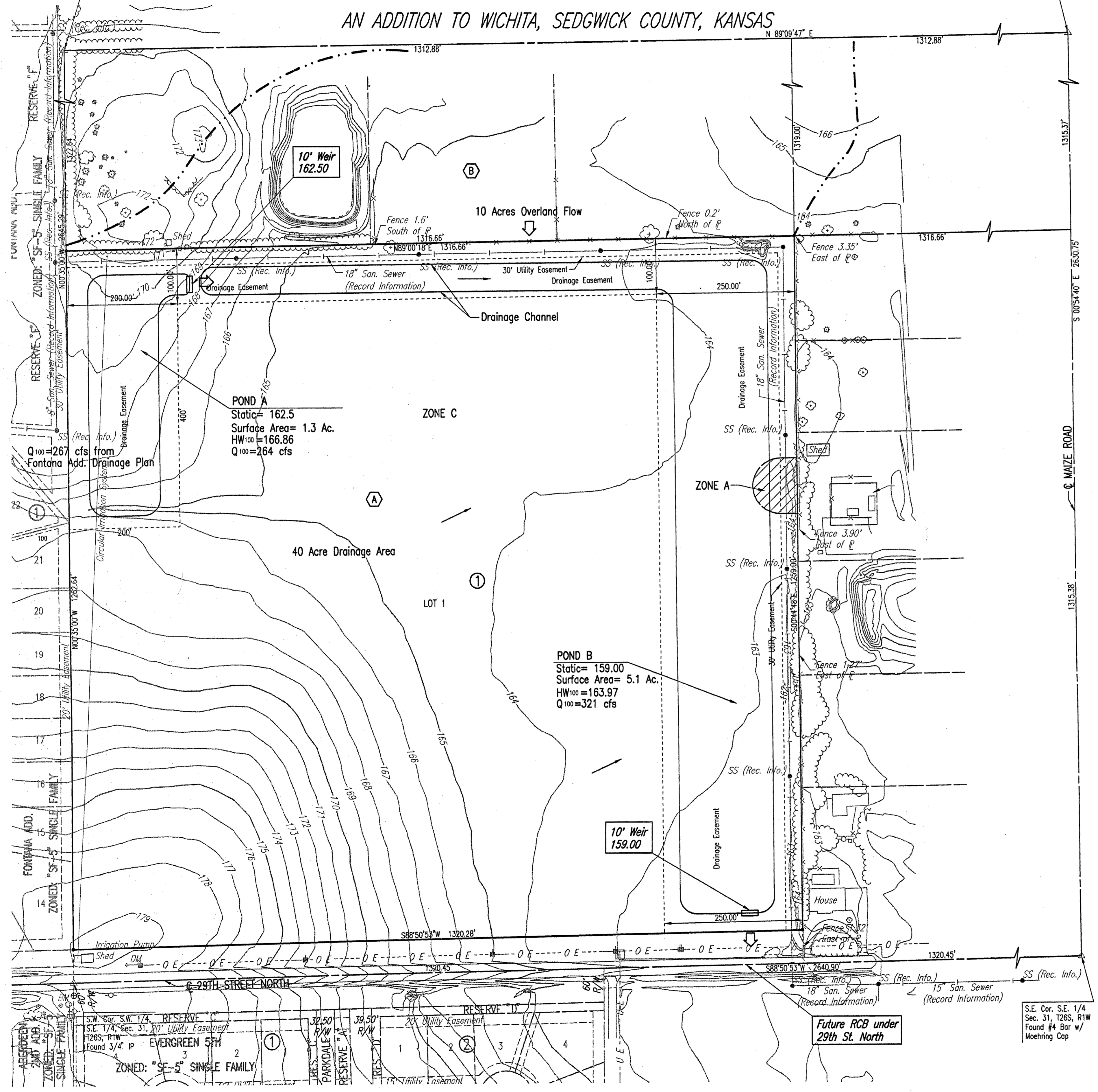
Surface Type	VELOCITY IN FEET/SECOND FOR SLOPES IN PERCENT SHOWN																			
	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0	20.0
Forest with Heavy Ground Litter or Meadow	0.03	0.04	0.06	0.07	0.08	0.09	0.10	0.11	0.12	0.13	0.16	0.21	0.28	0.33	0.39	0.46	0.53	0.60	0.72	1.10
Fallow or Minimum Tillage Cultivation	0.06	0.08	0.10	0.12	0.13	0.14	0.16	0.17	0.18	0.19	0.29	0.40	0.51	0.66	0.78	0.91	1.05	1.20	1.44	2.10
Short Grass Pasture or Lawns	0.09	0.13	0.15	0.18	0.20	0.21	0.23	0.25	0.26	0.28	0.45	0.60	0.77	0.96	1.17	1.33	1.50	1.68	1.98	3.20
Almost Bare Ground	0.16	0.22	0.28	0.31	0.35	0.38	0.41	0.44	0.46	0.49	0.70	0.85	1.05	1.26	1.50	1.75	2.03	2.32	2.79	4.40
Grassed Waterway	0.35	0.48	0.58	0.67	0.77	0.84	0.91	0.98	1.05	1.12	1.54	1.82	2.10	2.38	2.78	3.20	3.66	4.14	4.56	7.00
Paved Areas (Sheet Flow) or Shallow Gutter Flow	0.44	0.62	0.77	0.91	1.05	1.12	1.19	1.26	1.33	1.40	2.00	2.55	3.20	3.83	4.41	5.04	5.70	6.00	6.20	9.00

# PLAN MAP

DRAINAGE PLAN  
**NEWMARKET OFFICE**  
 AN ADDITION TO WICHITA, SEDGWICK COUNTY, KANSAS

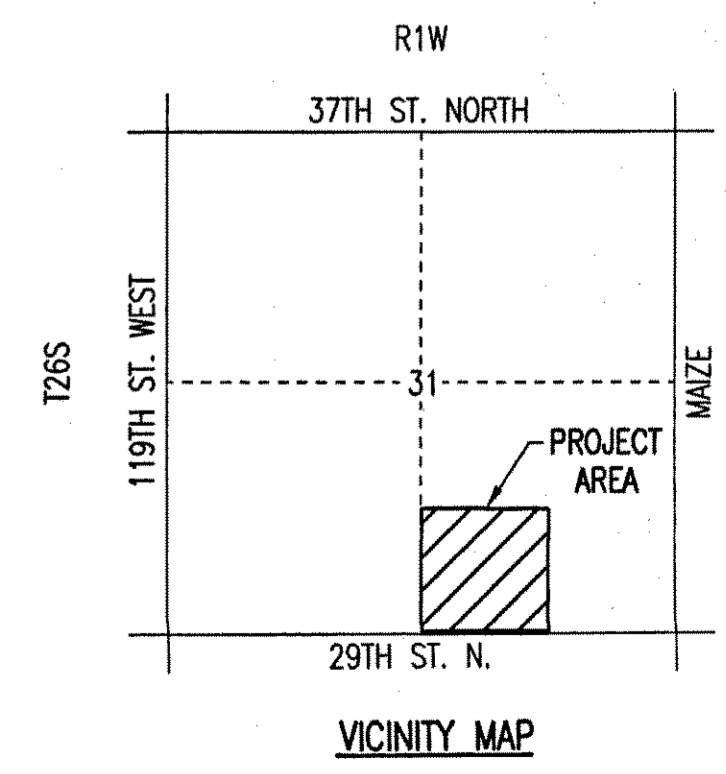
E. 1/4 Cor. Sec. 31,  
 T26S, R1W  
 Found 3/4" IP  
 Moehring Cap

Center of Sec. 31  
 T26S, R1W  
 Found 3/4" IP



SCALE: 1" = 100'

- LEGEND**
- BASIN IDENTIFIER
  - MAJOR BASIN BOUNDARY
  - EMERGENCY STORM WATER FLOW
  - STORM WATER FLOW
- SEE SUPPORTING CALCULATIONS FOR HYDROLOGY



SOURCE: UNPUBLISHED RECORDS FILE #7, 2004  
 DATE: 10/10/04 10:00 AM 4:00:02 PM BY: SMW  
 DRAWN: 10/13/04 10:00 AM 10:00:00 PM BY: SMW