

Sheet

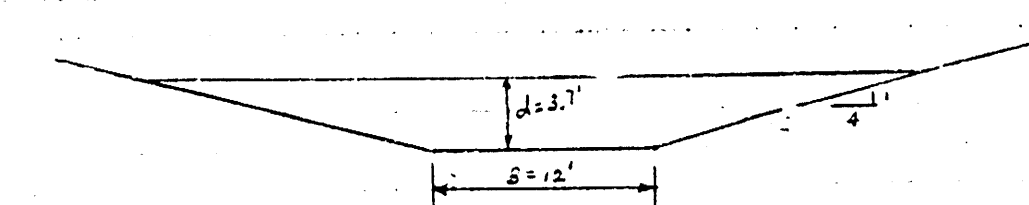
With a lot of checks. - 100% = 100%

used on the $H = H - h_1 - h_2 = 5.25 - 0.5 - 0.25 = 4.5$ ft. $Q = 3.0 \times 10^3$ cfs
 in $H = 5.4$ ft for inlet water. It is assumed that the loss due to
 that to keep current under inlet water level. This gives
 $Q = 4.5 - H + 0.5 = 5.25 - 0.25 = 5.0$ ft
 in order for flow to continue west of the old
 ditch will be required. For approx. the nearest 5'
 in this is approximately 350' or 420'. The slope of
 the ditch, $S = \frac{4.5 - 1.5}{350} = .0086$ for 350' or
 420'. Else in this area $Q = 190$ is depth $h = 1.25$ ft
 Try $B = 20'$, $h = 1.5$ ft, $S = .0086$, $Q = 1.25 \times 10^3$ cfs
 Try $B = 25'$, $h = 1.5$ ft, $S = .0086$, $Q = 2.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 2.0$ ft, $S = .0086$, $Q = 3.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 2.5$ ft, $S = .0086$, $Q = 4.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 3.0$ ft, $S = .0086$, $Q = 6.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 3.5$ ft, $S = .0086$, $Q = 7.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 4.0$ ft, $S = .0086$, $Q = 9.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 4.5$ ft, $S = .0086$, $Q = 10.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 5.0$ ft, $S = .0086$, $Q = 12.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 5.5$ ft, $S = .0086$, $Q = 13.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 6.0$ ft, $S = .0086$, $Q = 15.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 6.5$ ft, $S = .0086$, $Q = 16.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 7.0$ ft, $S = .0086$, $Q = 18.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 7.5$ ft, $S = .0086$, $Q = 19.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 8.0$ ft, $S = .0086$, $Q = 21.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 8.5$ ft, $S = .0086$, $Q = 22.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 9.0$ ft, $S = .0086$, $Q = 24.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 9.5$ ft, $S = .0086$, $Q = 25.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 10.0$ ft, $S = .0086$, $Q = 27.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 10.5$ ft, $S = .0086$, $Q = 28.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 11.0$ ft, $S = .0086$, $Q = 30.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 11.5$ ft, $S = .0086$, $Q = 31.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 12.0$ ft, $S = .0086$, $Q = 33.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 12.5$ ft, $S = .0086$, $Q = 34.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 13.0$ ft, $S = .0086$, $Q = 36.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 13.5$ ft, $S = .0086$, $Q = 37.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 14.0$ ft, $S = .0086$, $Q = 39.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 14.5$ ft, $S = .0086$, $Q = 40.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 15.0$ ft, $S = .0086$, $Q = 42.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 15.5$ ft, $S = .0086$, $Q = 43.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 16.0$ ft, $S = .0086$, $Q = 45.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 16.5$ ft, $S = .0086$, $Q = 46.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 17.0$ ft, $S = .0086$, $Q = 48.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 17.5$ ft, $S = .0086$, $Q = 49.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 18.0$ ft, $S = .0086$, $Q = 51.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 18.5$ ft, $S = .0086$, $Q = 52.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 19.0$ ft, $S = .0086$, $Q = 54.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 19.5$ ft, $S = .0086$, $Q = 55.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 20.0$ ft, $S = .0086$, $Q = 57.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 20.5$ ft, $S = .0086$, $Q = 58.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 21.0$ ft, $S = .0086$, $Q = 60.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 21.5$ ft, $S = .0086$, $Q = 61.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 22.0$ ft, $S = .0086$, $Q = 63.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 22.5$ ft, $S = .0086$, $Q = 64.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 23.0$ ft, $S = .0086$, $Q = 66.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 23.5$ ft, $S = .0086$, $Q = 67.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 24.0$ ft, $S = .0086$, $Q = 69.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 24.5$ ft, $S = .0086$, $Q = 70.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 25.0$ ft, $S = .0086$, $Q = 72.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 25.5$ ft, $S = .0086$, $Q = 73.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 26.0$ ft, $S = .0086$, $Q = 75.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 26.5$ ft, $S = .0086$, $Q = 76.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 27.0$ ft, $S = .0086$, $Q = 78.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 27.5$ ft, $S = .0086$, $Q = 79.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 28.0$ ft, $S = .0086$, $Q = 81.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 28.5$ ft, $S = .0086$, $Q = 82.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 29.0$ ft, $S = .0086$, $Q = 84.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 29.5$ ft, $S = .0086$, $Q = 85.5 \times 10^3$ cfs
 Try $B = 25'$, $h = 30.0$ ft, $S = .0086$, $Q = 87.0 \times 10^3$ cfs
 Try $B = 25'$, $h = 30.5$ ft, $S = .0086$, $Q = 88.5 \times 10$

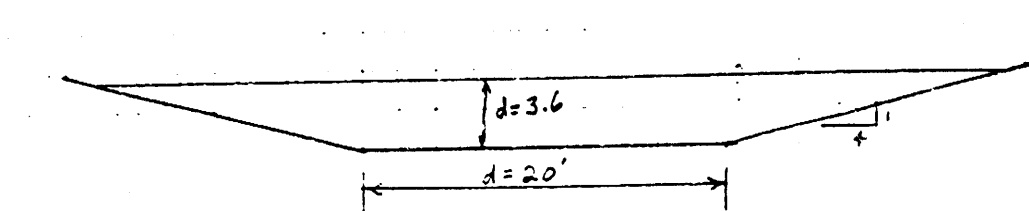
Ditch Cross-Sections - 1

Ditch in Reserve A, N.E. 3-12 RCPs

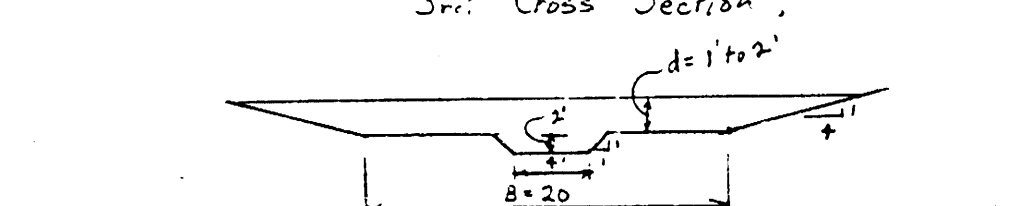
Initial Cross Section



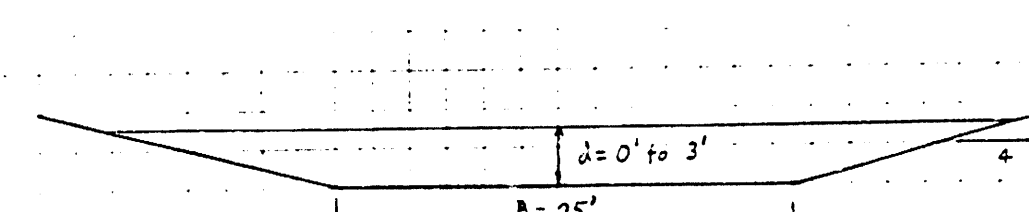
2nd Cross Section



3rd Cross Section

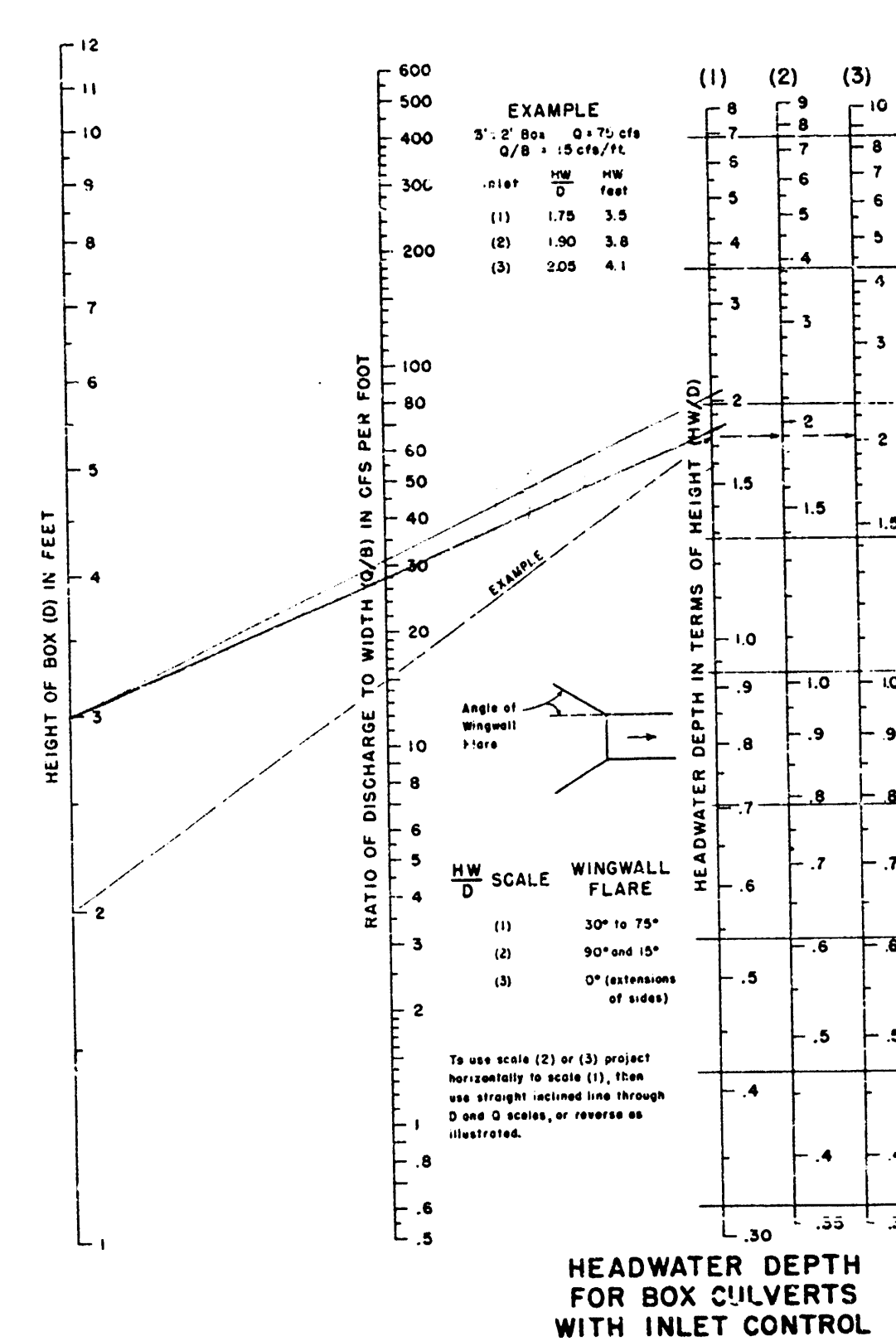


Ditch in Reserve A, South of Double 4'x3' Box Culverts



Continued H.E. Tech. Center
RBN 1/28/84

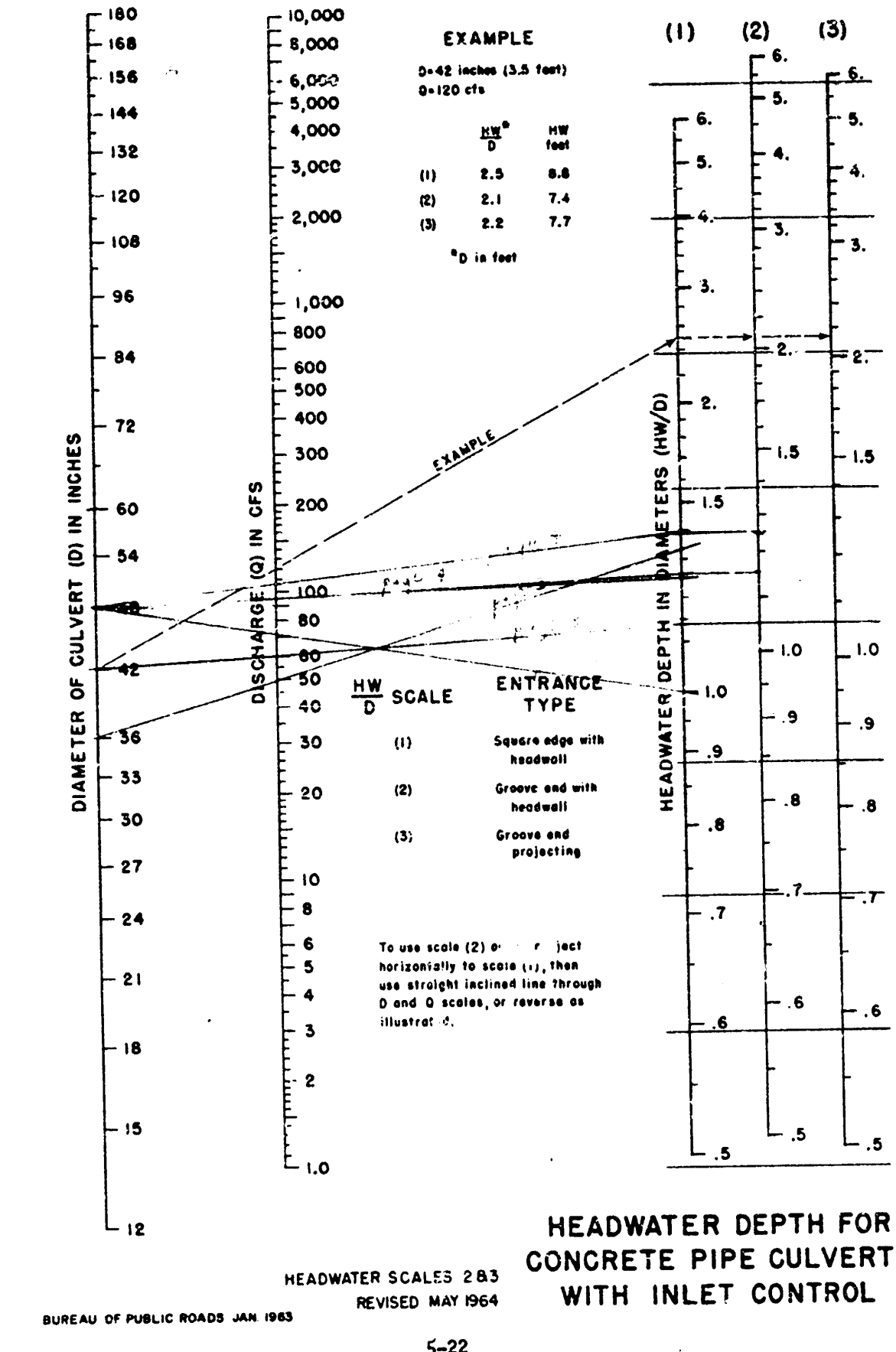
CHART 1



BUREAU OF PUBLIC ROADS JAN 1963

HEADWATER DEPTH FOR BOX CULVERTS WITH INLET CONTROL

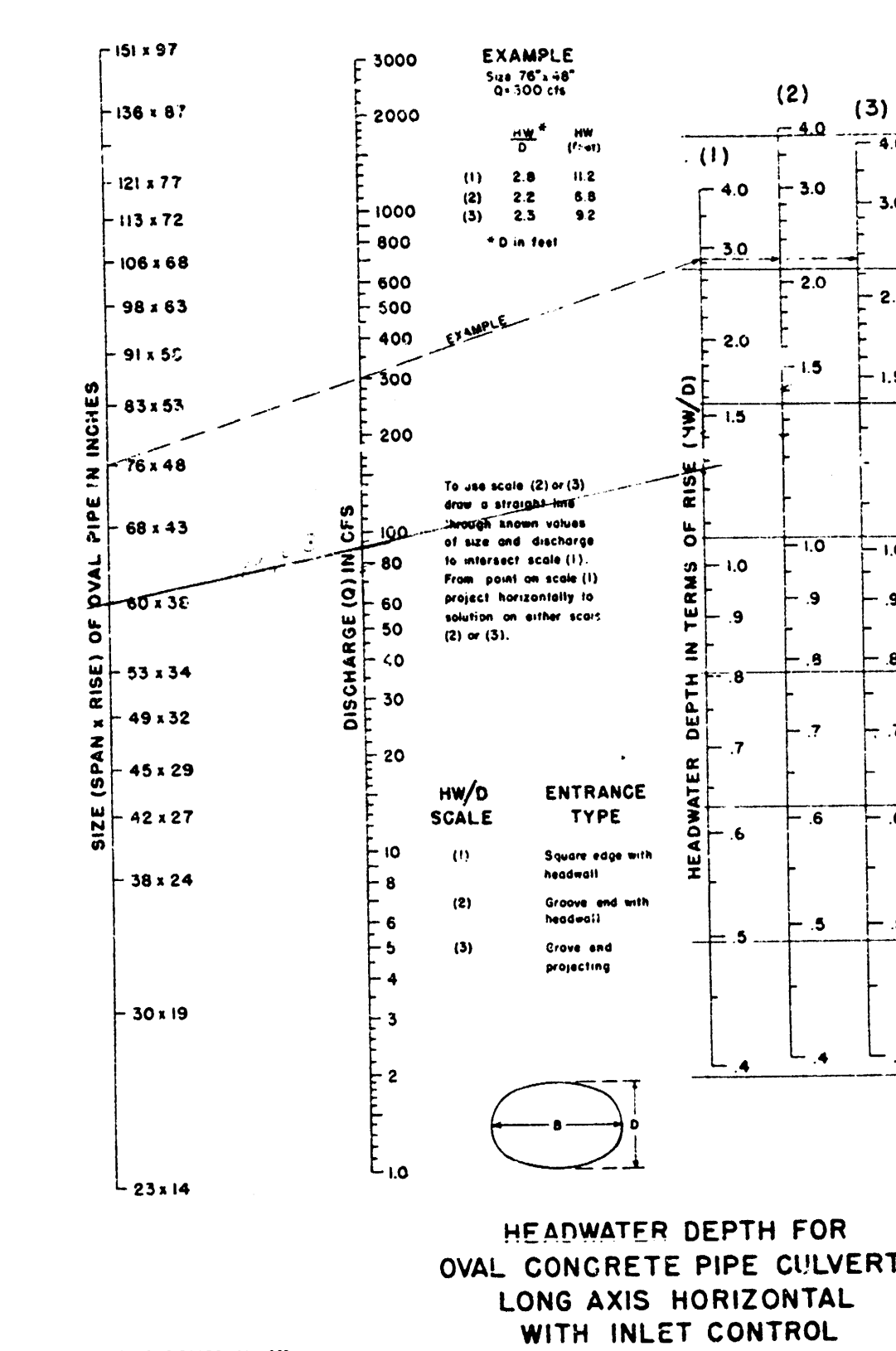
CHART 2



BUREAU OF PUBLIC ROADS JAN 1963

HEADWATER DEPTH FOR CONCRETE PIPE CULVERTS WITH INLET CONTROL

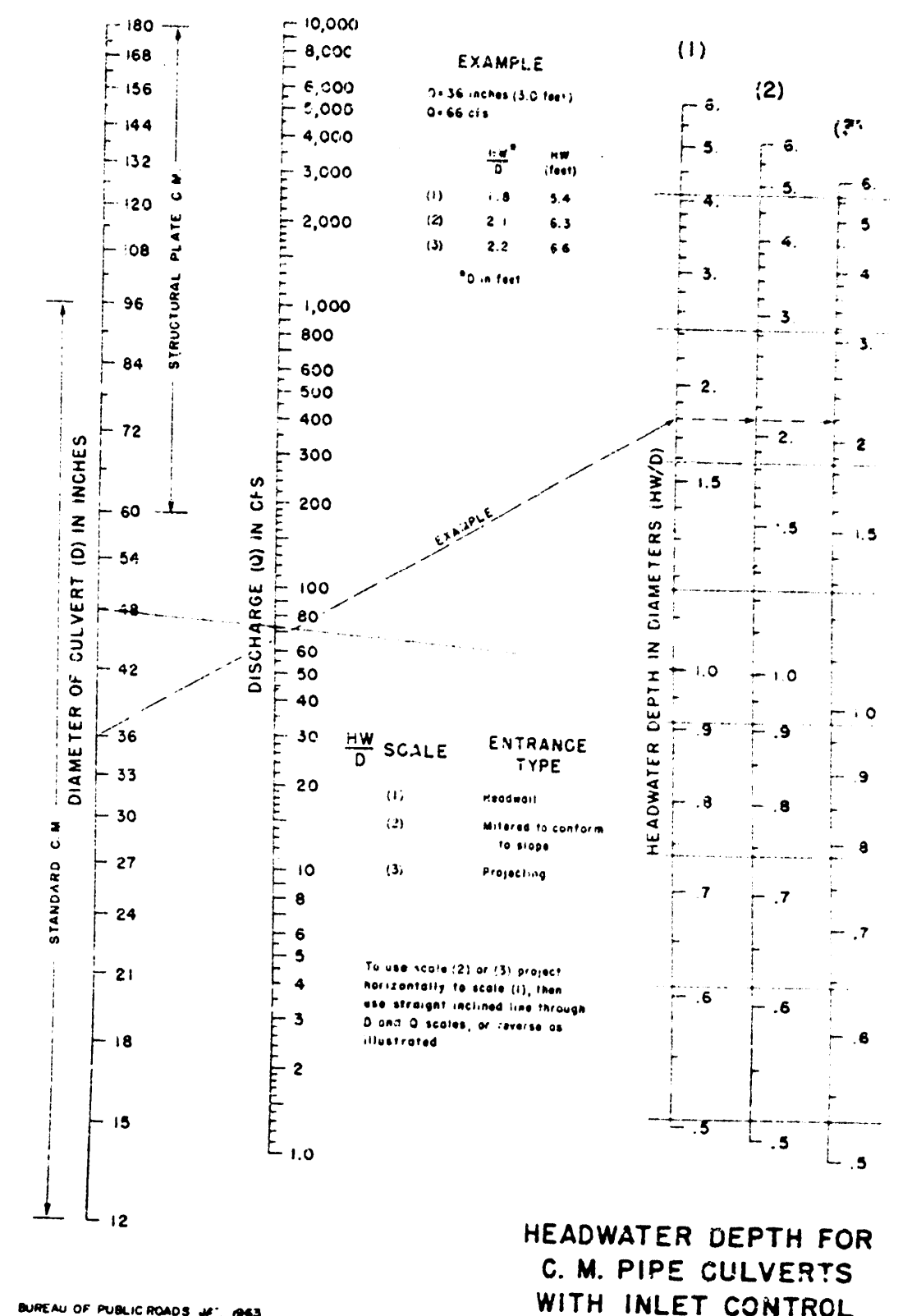
CHART 3



BUREAU OF PUBLIC ROADS JAN 1963

HEADWATER DEPTH FOR OVAL CONCRETE PIPE CULVERTS LONG AXIS HORIZONTAL WITH INLET CONTROL

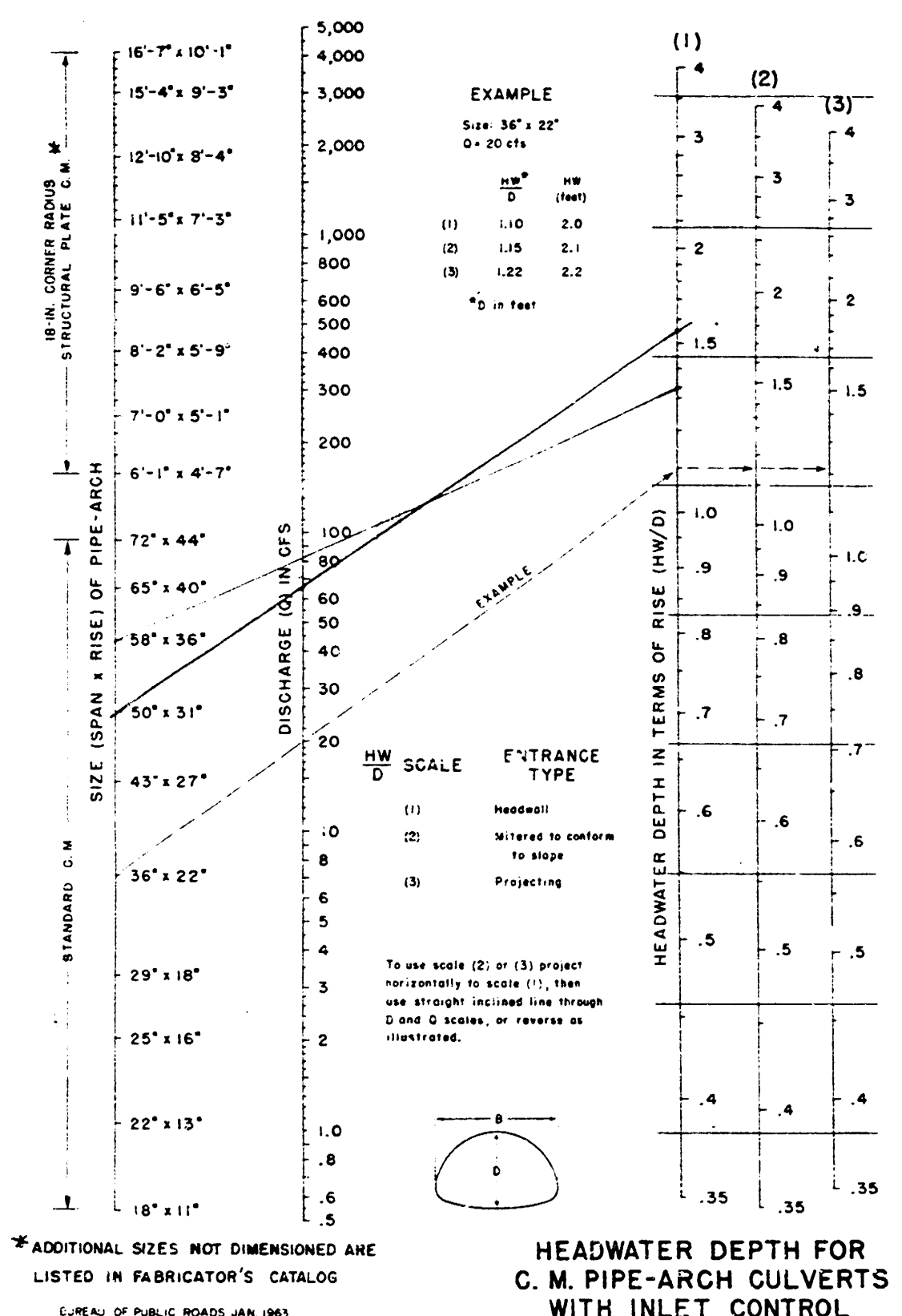
CHART 5



BUREAU OF PUBLIC ROADS JAN 1963

HEADWATER DEPTH FOR C.M. PIPE CULVERTS WITH INLET CONTROL

CHART 6

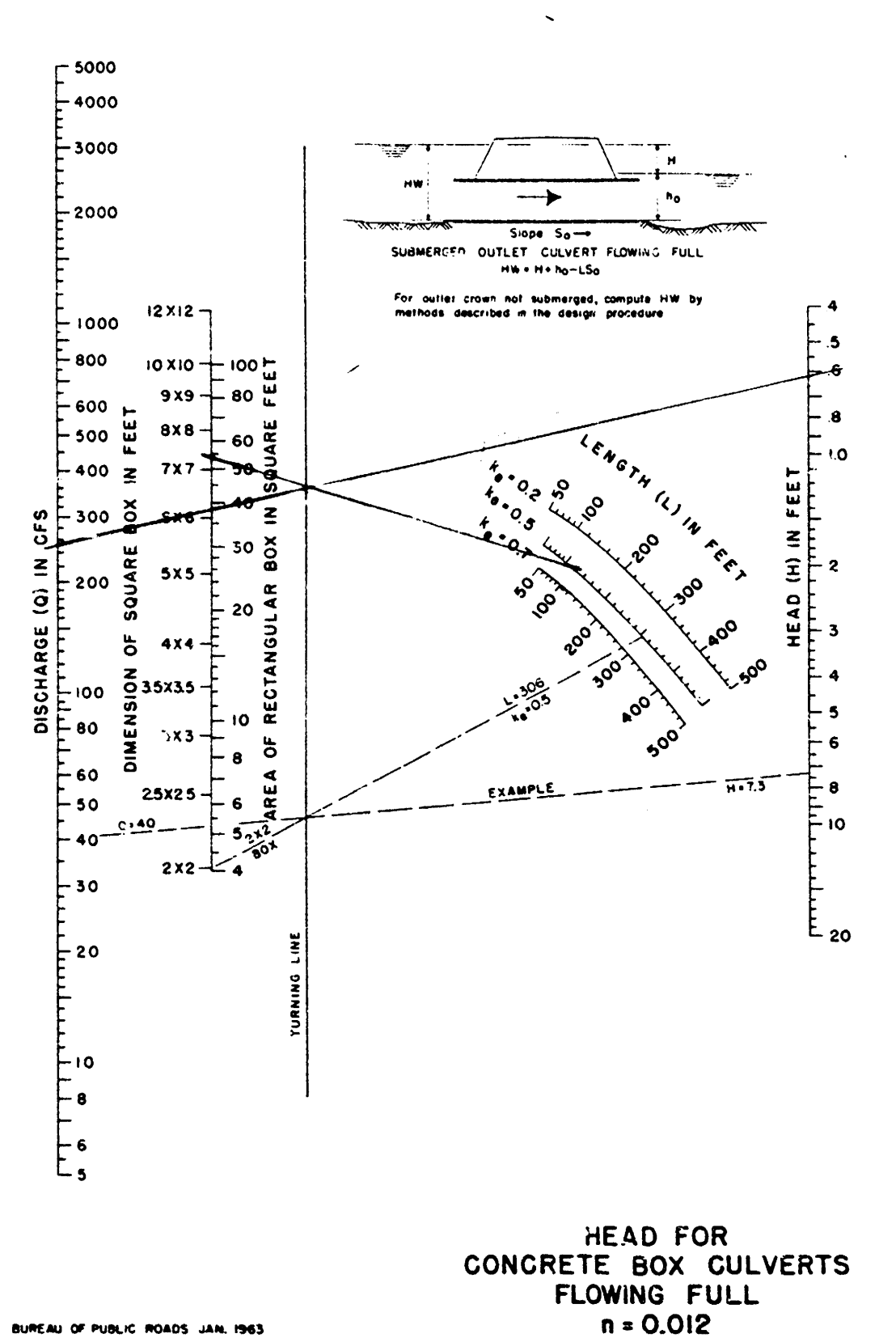


ADDITIONAL SIZES NOT DIMENSIONED ARE LISTED IN FABRICATOR'S CATALOGS

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HEADWATER DEPTH FOR C.M. PIPE-ARCH CULVERTS WITH INLET CONTROL

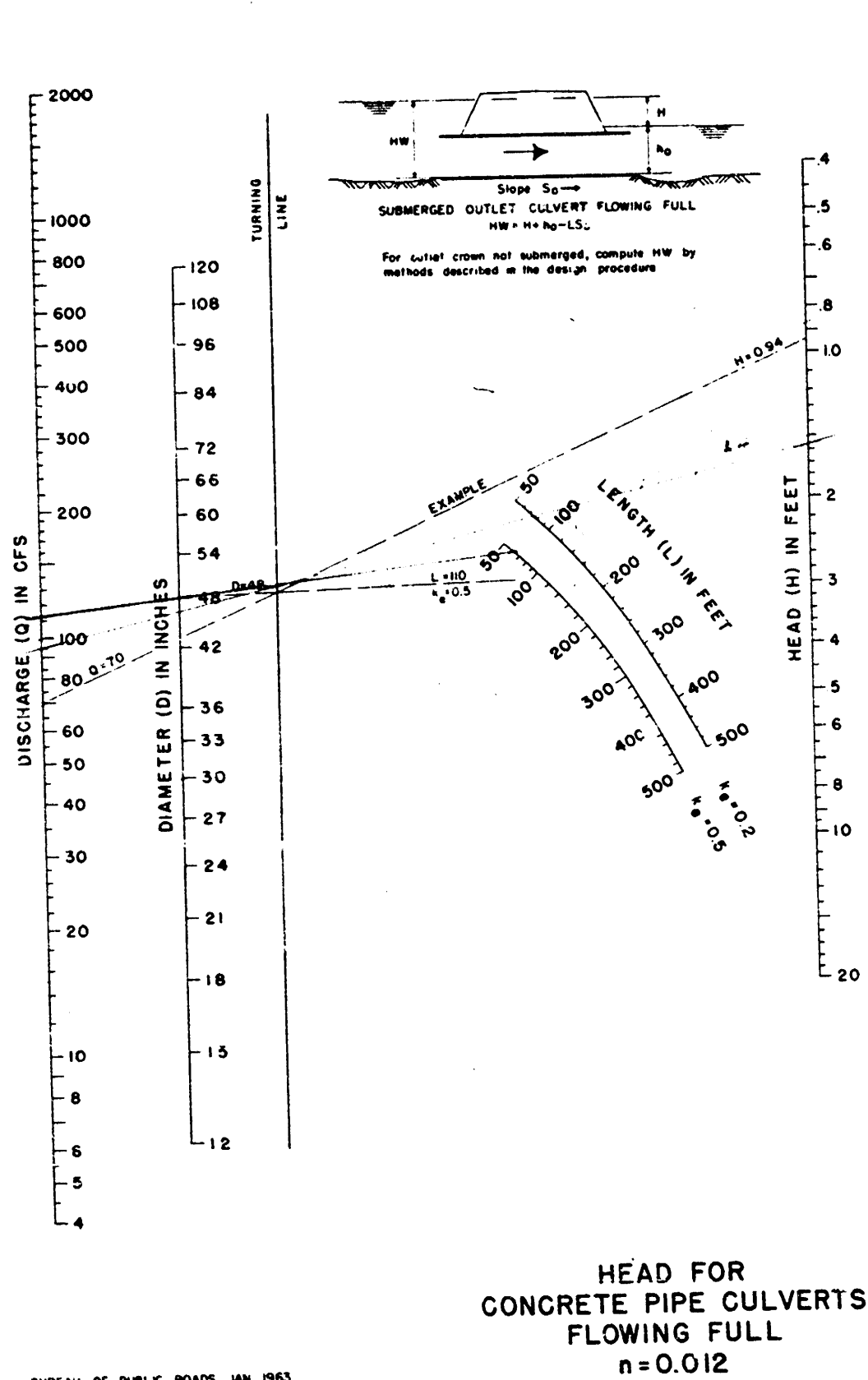
CHART 8



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HEAD FOR CONCRETE BOX CULVERTS FLOWING FULL n=0.012

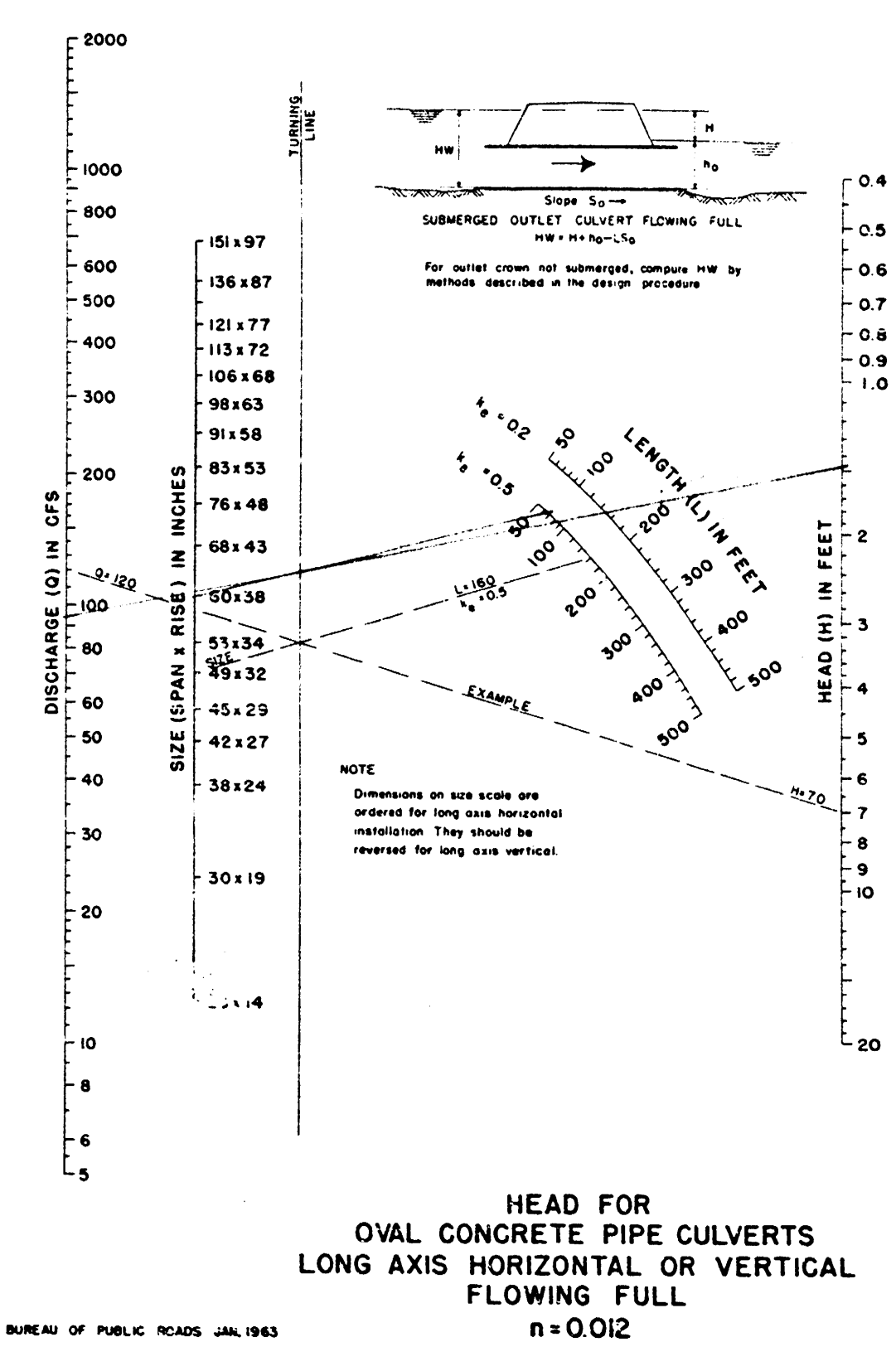
CHART 9



BUREAU OF PUBLIC ROADS JAN 1963

HEAD FOR CONCRETE PIPE CULVERTS FLOWING FULL n=0.012

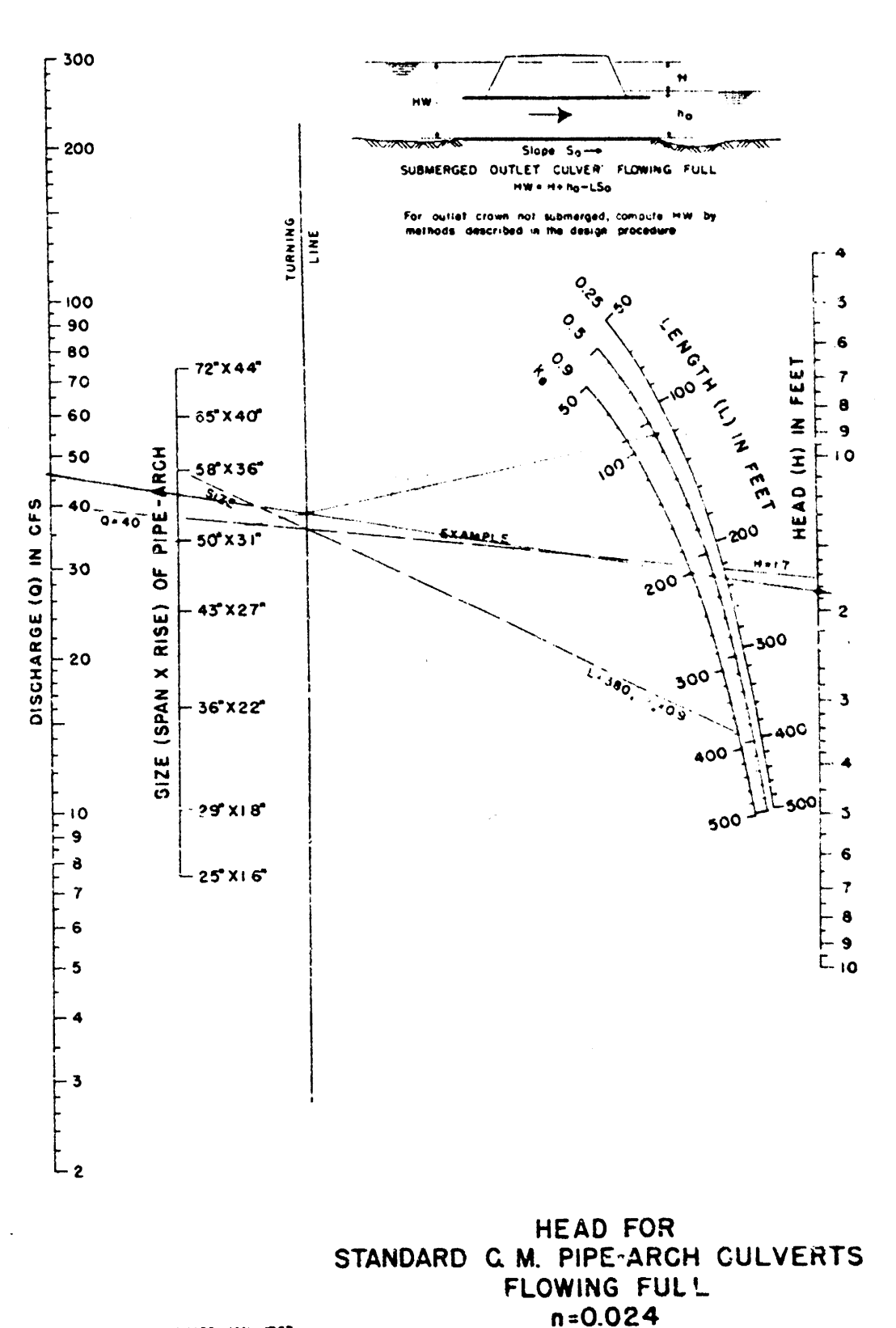
CHART 10



BUREAU OF PUBLIC ROADS JAN 1963

HEAD FOR OVAL CONCRETE PIPE CULVERTS LONG AXIS HORIZONTAL OR VERTICAL FLOWING FULL n=0.012

CHART 12



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HEAD FOR STANDARD C.M. PIPE-ARCH CULVERTS FLOWING FULL n=0.024

Chart 15

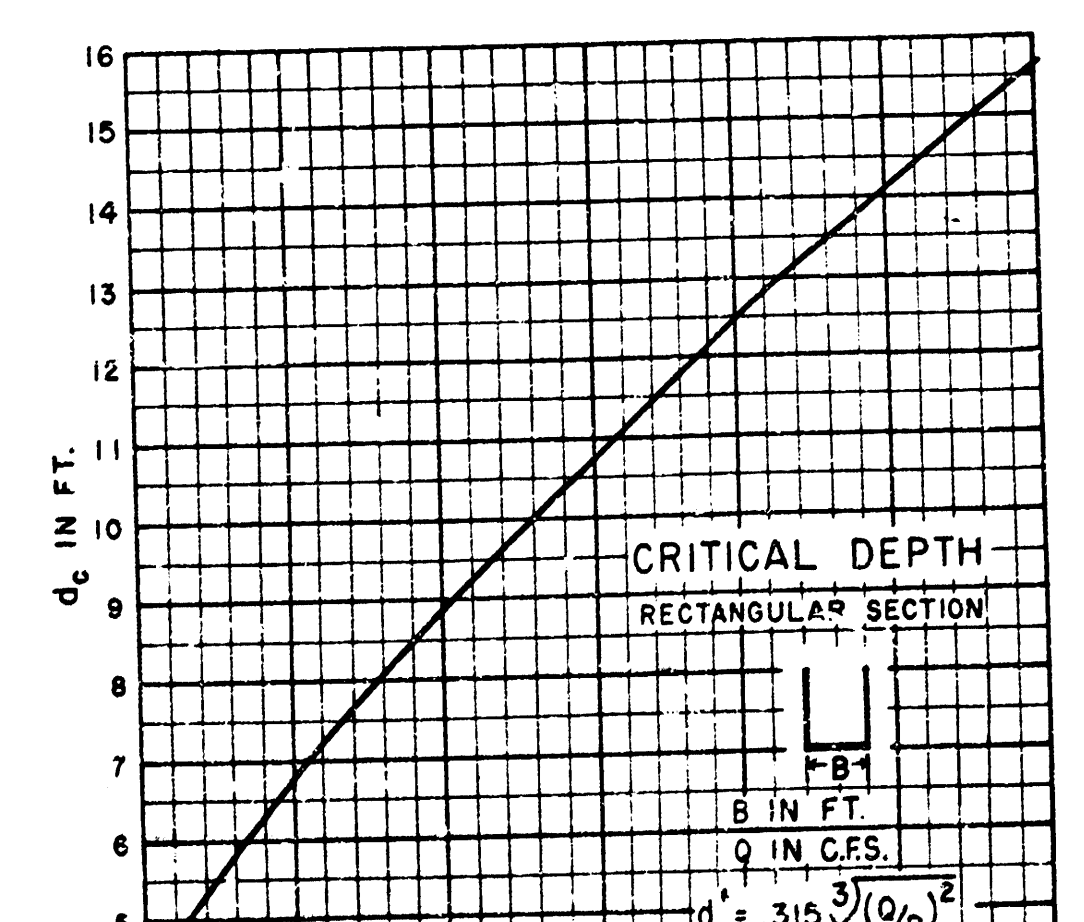
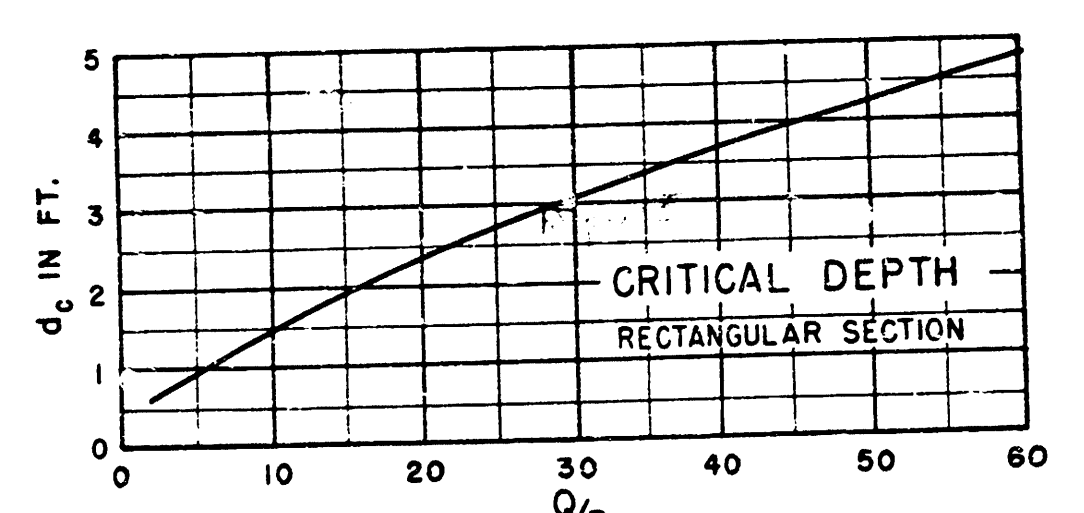


CHART 16

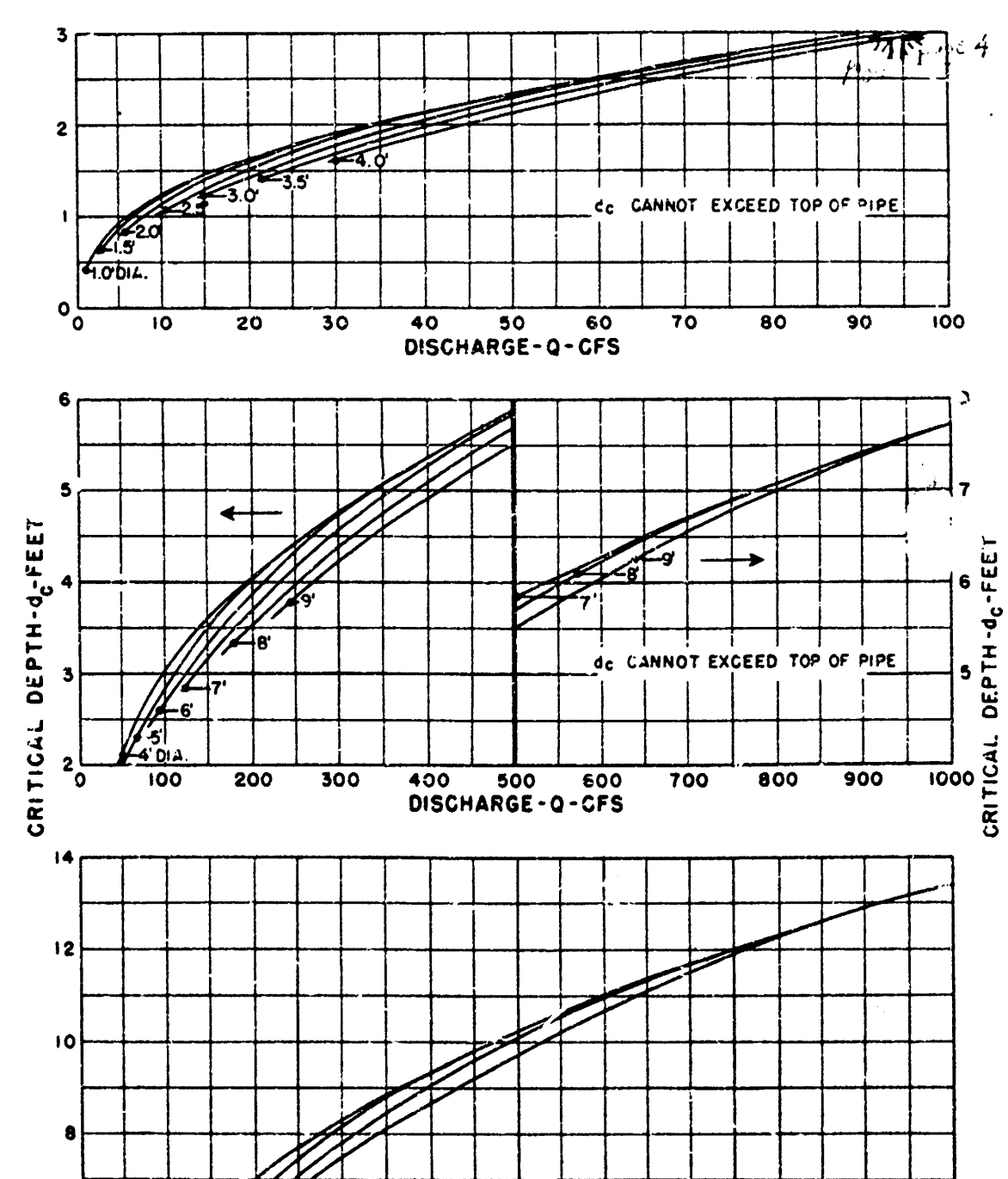


CHART 17

